

Spectral-element method - part 2

Recall: 1D heat equation

$$\rho c_v \partial_t T = \partial_x (K \partial_x T)$$

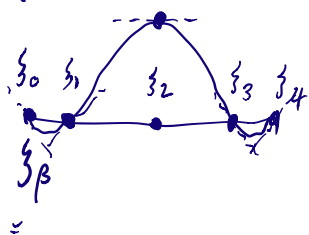
with density ρ , heat capacity c_v , conductivity K
and temperature $T = T(x, t)$

The weak-form becomes

$$\int_0^L w \underbrace{\rho c_v \partial_t T}_{\text{mass/capacity term}} dx = - \int_0^L \underbrace{K \partial_x w \partial_x T}_{\text{stiffness}} dx + \underbrace{w K \partial_x T \Big|_0^L}_{\text{boundary}}$$

Matrix form: we expand our functions

$w=1$: $l_2^4(\xi_2) \approx 1$



$$w(x(\xi)) = \sum_{\beta=0}^N w^{\beta} \underbrace{l_{\beta}^N(\xi)}_{\substack{\text{high-order degree } N \\ \text{Lagrange polynomial}}}$$

$$T(x(\xi), t) = \sum_{\alpha=0}^N T^{\alpha}(t) \underbrace{l_{\alpha}^N(\xi)}$$

$$\begin{aligned} w(x(\xi)) &= 0 \\ \text{except} \\ w(x(\xi_2)) &= 1 \end{aligned}$$

Note that we can choose the test function coefficients w^{β} to be all equal to zero except one (which is set to 1) such that we can treat of the Lagrange polynomials

one at a time (which means one GLL point at a time)

Mass matrix: Let's look at the left-hand side term

$$\int_{\Omega} w \rho c \partial_t T dx = \sum_c \int_{\Omega_c} w \rho c \partial_t T dx$$

The contribution from element Ω_c

$$\int_{\Omega_c} w \rho c \partial_t T dx = \int_{-1}^{+1} \rho(x(\xi)) c(x(\xi)) \underbrace{w(x(\xi))}_{\substack{\text{shape function} \\ l_\beta^N(\xi_j)}} \underbrace{\partial_t T(x(\xi), t)}_{\substack{\text{temperature} \\ T^\alpha}} d\xi$$

$$\approx \sum_{j=0}^N \hat{\omega}_j \rho^j c^j J^j \underbrace{\sum_{\beta=0}^N w^\beta l_\beta^N(\xi_j)}_{l_\beta(\xi_j) = \delta_{\beta j}} \underbrace{\sum_{\alpha=0}^N \partial_t T^\alpha l_\alpha^N(\xi_j)}_{\delta_{\alpha j}}$$

$$= \sum_{j=0}^N \hat{\omega}_j \rho^j c^j J^j w^j \partial_t T^j$$

local contribution to element Ω_c

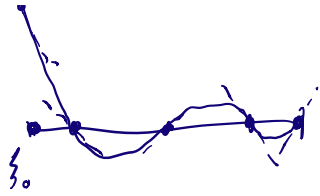
Stiffness matrix: For the contribution of element Ω_c

$$\int_{\Omega_c} k \partial_x w \partial_x T dx = \int_{-1}^{+1} k(x(\xi)) \underbrace{[\partial_x w(x(\xi))]}_{\substack{\text{shape function} \\ l_\beta^N(\xi_j) \partial_x \xi(\xi_j)}} \underbrace{[\partial_x T(x(\xi), t)]}_{\substack{\text{temperature} \\ T^\alpha}} d\xi$$

$$\approx \sum_{j=0}^N \hat{\omega}_j k^j J^j \left[\sum_{\beta=0}^N w^\beta \underbrace{l_\beta^N(\xi_j) \partial_x \xi(\xi_j)}_{\substack{\text{shape function} \\ l_\beta^N(\xi_j) \partial_x \xi(\xi_j)}} \right] \left[\sum_{\alpha=0}^N T^\alpha \underbrace{l_\alpha^N(\xi_j) \partial_x \xi(\xi_j)}_{\substack{\text{shape function} \\ l_\alpha^N(\xi_j) \partial_x \xi(\xi_j)}} \right]$$

$$l_0^4(\xi)$$

$$\text{note: } \frac{\partial l_\alpha}{\partial x} = \frac{\partial l_\alpha}{\partial \xi} \frac{\partial \xi}{\partial x}$$



and $l_{\beta}^{'N}(\xi_j) \neq \delta_{\beta j}$

Let's choose as test function

$$\begin{cases} w^{\beta_1} = 1 \\ w^{\beta} = 0 \text{ for all } \beta \neq \beta_1 \end{cases}$$

then we find

$$\underbrace{\hat{\omega}_{\beta_1} g^{\beta_1} c^{\beta_1} j^{\beta_1} \overbrace{w^{\beta_1}}^{=1}}_{M_{\beta_1}} \partial_t T^{\beta_1} = - \sum_{\gamma=0}^N \hat{\omega}_{\gamma} k^{\gamma} j^{\gamma} [l_{\beta_1}^{'N}(\xi_j) \partial_x \xi(\xi_j)] \cdot \left[\sum_{\alpha=0}^N T^{\alpha} l_{\alpha}^{'N}(\xi_j) \partial_x \xi(\xi_j) \right]$$

or

$$M_{\beta_1} \partial_t T^{\beta_1}(t) = \sum_{\alpha=0}^N K_{\beta_1, \alpha} T^{\alpha}(t)$$

$$\underline{M} \partial_t \underline{T} = \underline{K} \underline{T} + \text{boundary}$$

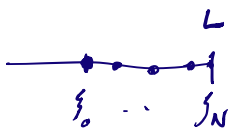
where $M_{\beta_1} = \hat{\omega}_{\beta_1} \underline{g^{\beta_1} c^{\beta_1} j^{\beta_1}}$

$$K_{\beta_1, \alpha} = - \sum_{\gamma=0}^N \hat{\omega}_{\gamma} \underline{k^{\gamma} j^{\gamma}} l_{\beta_1}^{'N}(\xi_j) l_{\alpha}^{'N}(\xi_j) [\partial_x \xi(\xi_j)]^2$$

material
properties

Notice that mass & stiffness matrices are constructed at (reference) element level, which allows for material heterogeneities within an element.

Boundary conditions: In 1D, the conditions write as



$$\text{at } x=L: \quad w K \partial_x T = w^N K^N \sum_{\alpha=0}^N T^\alpha(t) \underbrace{\ell'_\alpha(\xi_N)}_{\partial_x \xi_N} \xi_N^\alpha$$

$$x=0: \quad w K \partial_x T = w^0 K^0 \sum_{\alpha=0}^N T^\alpha(t) \ell'_\alpha(\xi_0) \partial_x \xi_0$$