

## Spectral-element method

1D wave equation: Let's recall the 1D wave equation

$$\rho \partial_t^2 s = \partial_x (\mu \partial_x s)$$

for displacement  $s$  and density  $\rho$ ,  
shear modulus  $\mu$ .

As example, we use one of the following  
initial & boundary conditions

$$\begin{cases} s(x, 0) = f(x) \\ s(L, t) = 0 \\ s(0, t) = 0 \end{cases} \quad \text{or} \quad \begin{cases} s(x, 0) = f(x) \\ \mu \partial_x s(L, t) = B_L(t) \\ \mu \partial_x s(0, t) = B_0(t) \end{cases}$$

"Dirichlet" "Neumann"

Weak form: The weak form of the wave equation is

$$\underbrace{\int_0^L w \rho \partial_t^2 s \, dx}_{\text{mass}} = \underbrace{\int_0^L w \partial_x (\mu \partial_x s) \, dx}_{\text{stiffness}} = \underbrace{-\int_0^L \mu \partial_x w \partial_x s \, dx}_{\text{stiffness}} + \underbrace{w \mu \partial_x s \Big|_0^L}_{\text{boundary}}$$

integration by part

and similar to the heat equation problem, we have

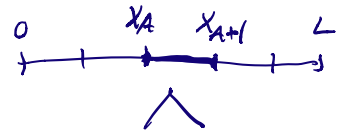
$$M_{\alpha} \partial_t^2 s^{\alpha} = \sum_{\gamma=0}^N K_{\alpha\gamma} s^{\gamma}$$

Note that the mass & stiffness look the same as for the heat equation. Here, we have a second-order time derivative.

Meshing: We subdivide the (physical) domain  $\Omega$  into a number of non-overlapping elements  $\Omega_e$ ,  $e=1, \dots, n$  such that  $\Omega = \bigcup_{e=1}^n \Omega_e$

The mapping to the reference element

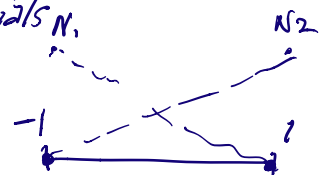
$$x(\xi) = \sum_{a=1}^2 x_a N_a(\xi)$$



use low-degree Lagrange polynomials  $N_i$

$$N_1(\xi) = \frac{1}{2}(1-\xi)$$

$$N_2(\xi) = \frac{1}{2}(1+\xi)$$



The Jacobian of the mapping is

$$J = \frac{\partial x}{\partial \xi} = \frac{1}{2}(x_{A+1} - x_A) \quad \text{where} \quad \begin{aligned} x(-1) &= x_A \\ x(+1) &= x_{A+1} \end{aligned}$$

Interpolation on an element: We represent the displacement field by higher-degree Lagrange polynomials

$$f(x(\xi)) = \sum_{\alpha=0}^N f^{\alpha} \underbrace{l_{\alpha}^N(\xi)}_{\text{Lagrange polynomials of degree } N}$$

Integration over an element: For the spectral-element method, we use a Gauss-Lobatto-Legendre integration rule

$$\int_{\Omega_e} f(x) dx = \int_{-1}^1 f(x(\xi)) J(\xi) d\xi$$

$$\approx \sum_{\alpha=0}^N \underbrace{\hat{\omega}_{\alpha}}_{\text{integration weights}} f^{\alpha} J^{\alpha}$$



where the integration points are the GLL points, i.e., roots of  $(1-\xi^2) P_N'(\xi) = 0$

Discretization of the weak form: To obtain explicit

expressions for the weak form, we expand displacement and test functions as

$$s(x(\xi), t) = \sum_{\alpha=0}^N s^{\alpha}(t) l_{\alpha}^N(\xi)$$

$$w(x(\xi)) = \sum_{\alpha=0}^N w^{\alpha} l_{\alpha}^N(\xi)$$

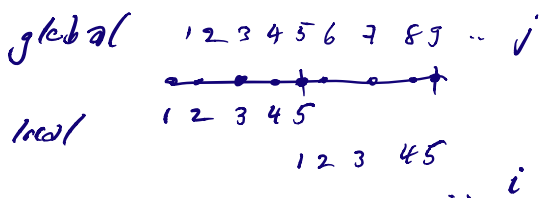
This choice makes the SEM a Galerkin method, where the basis functions are the same for the test (vector) function as for the displacement field.

At element level, we find the following local contributions

- mass matrix:  $M_{\beta, \gamma} = \hat{\omega}_{\beta, \gamma} \int_{\beta_1}^{\beta_2} J^{\beta_1}$

- stiffness matrix:  $K_{\beta, \alpha} = - \sum_{\gamma=0}^N \hat{\omega}_{\gamma} \mu^{\gamma} l_{\beta}^N(\xi_{\gamma}) l_{\alpha}^N(\xi_{\gamma}) J^{\gamma} [d_{\alpha}^{\xi}(\xi_{\gamma})]^2$

Assembly: We use a local to global array indexing



$$iglob(element, i) = j$$