

We've studied inductance generally, but now we want see how it might be used more practically. We noticed a few things about self inductance,

$$\phi = LI$$

the emf that is generated when the current changes with time $I = I(t)$, is a back emf, which reflects Lenz's Law. The EMF will be produced to fight the change,

$$\mathcal{E} = -\frac{d\phi}{dt} = -L \frac{dI}{dt}$$

In this equation we can see that the inductance, L , acts like a damping constant on the current, I . We will study the inductors in circuits so let's remind ourselves of the different circuit elements

<u>Symbol</u>	<u>Circuit Relation</u>	<u>Geometry</u>	<u>Field</u>
	$Q = CV$ or $I = C dV/dt$	$C = \frac{\epsilon_0 A}{d}$ (parallel plates)	$E = \sigma_0 / \epsilon_0$
	$V = IR$	$R = \rho L / A$ (uniform rod)	$J = \sigma E$
	$V = -L \frac{dI}{dt}$	$L = \mu_0 N A * N_{turns}$	$B = \mu_0 n I$ or $\phi_B = L I$

Kirchoff's Laws say, $\sum_{\text{around any closed loop}} \Delta V = 0$ and $\sum_{\text{all currents entering any node}} I_{in} = 0$

"Solving a circuit problem" means finding $I(t)$ &/or $V(t)$ for all circuit elements.

A few more notes before we get into solving problems,

Sources in circuits can be AC or DC, voltage or current sources,

Constant Voltage

$$\frac{1}{T} \text{ Battery} \quad V=V_0$$

Function Generators

AC Voltage Source
 $V = V_0 \sin(\omega t + \delta)$

AC Current Source
 $I = I_0 \sin(\omega t + \delta)$

More Notes:

$$\epsilon_0 = 8.85 \cdot 10^{-12} \frac{\text{farad}}{\text{m}}$$

- real capacitors range from $\underbrace{< 1 \mu\text{F}}_{10^{-12} \text{ F}}$ to $\underbrace{> 1 \text{ F}}$ serious dielectrics

- Typical resistors range from $< 1 \Omega$ to several $M\Omega$ $\approx 10^6 \Omega$

$$\mu_0 = 4\pi \cdot 10^{-7} \frac{\text{H}}{\text{m}} \quad (\text{and } L = \frac{\mu_0 N^2 A}{l}) \text{ means}$$

- real life inductors range from $< 10^{-6} \text{ H}$ to $\sim 1 \text{ Henry}$

You might be worried about putting an inductor into a circuit and how we define a potential drop across it. This is where ΔV & EMF start to get a little confusing. Both are related to energy &/or work. So what we are saying when we say $E = -L \frac{dI}{dt}$ is that the work per unit charge for this element is $-L \frac{dI}{dt}$ so we can use this form in Kirchoff's law

$$\sum \Delta V = 0$$

Example: An RL circuit.

The resistance might be distributed (in wires, battery, etc.). And so might the inductance. This is a model.

This model will allow us to see the general solution method.

Intuitively, the inductor doesn't "like" instant changes in current. We expect that at $t=0$, the current slowly changes from zero. After a long time, there are no more changes.

We've reached steady state! $\Delta V_{\text{inductor}} = 0$, so it acts like an ideal wire now.

Using Kirchoff's Loop Rule we find,

$$V - IR - L \frac{dI}{dt} = 0$$

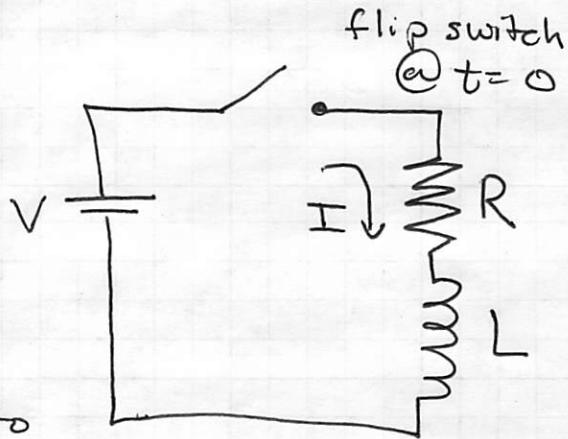
Hence, we assume that $V, R, \& L$ are all known and we are seeking $I(t)$.

This equation is a 1st order, inhomogeneous ODE,

$$L \frac{dI}{dt} + IR = V$$

There are several methods to solve this ODE. We will discuss two

- ① Direct method using homogeneous & particular solutions
- ② Using the "phasors" method, which is very powerful and can be much simpler.



Method #1 : Direct Solution (maybe remember from ODEs)

① Find the general homogeneous solution to :

$$L \frac{dI_H}{dt} + I_H R = 0$$

② Find some particular solution to the full (inhomog) eqn.

③ Add these solutions ($I = I_H + I_p$) to get the full solution.

④ Determine the one arbitrary constant in I_H using initial conditions.

This method works for $V = V_0$ (battery)

also if $V = V_0 \cos(\omega t)$ (AC power supply)

and thus, by superposition, we can solve for any periodic $V(t)$ because Fourier says,

$$V(t) = \sum_n V_n \cos(\omega_n t + \delta_n)$$

* This method is fairly general.

Back to the example, the homogeneous equation is,

$$\frac{dI_H}{dt} = -\frac{R}{L} I_H \Rightarrow \text{separates} \Rightarrow \frac{dI_H}{I_H} = -\frac{R}{L} dt$$

$$I_H(t) = I_H(t=0) e^{-Rt/L}$$

this is an undetermined constant.

The resistor, R , kills off the current while the inductor, L , stretches that time out.

To find particular solutions, you don't need generality. Any solution that works is the solution. Guess & check is just fine.

Let's say that $V = V_0 = \text{constant}$,

$$L \frac{dI_p}{dt} + I_p R = V_0$$

Given our homogeneous solution maybe something like this works,

$$I_p(t) = a e^{-Rt/L} + b \quad \text{let's check if this works.}$$

$$\frac{dI_p}{dt} = -\frac{R}{L} a e^{-Rt/L} \quad \text{so that,}$$

$$L \left(-\frac{R}{L} a e^{-Rt/L} \right) + (a e^{-Rt/L} + b) R = V_0$$

the exponential terms cancel! this leaves
 $bR = V_0$ so our proposed solution works if

$$b = V_0/R$$

Add the solutions together,

$$I(t) = I_p + I_H = \underbrace{(I_H(t=0) + a)}_{\text{call this a constant, } C} e^{-Rt/L} + \frac{V_0}{R}$$

call this a constant, C

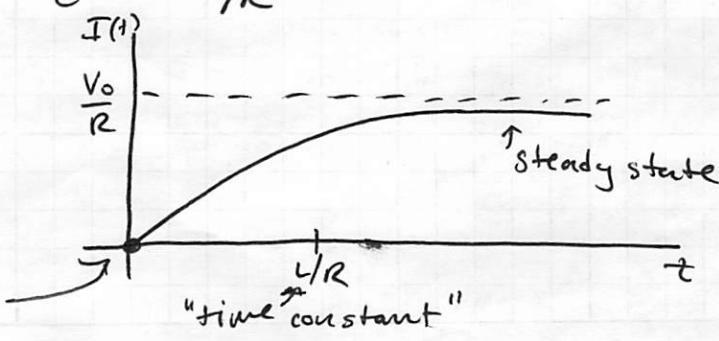
$$I(t) = Ce^{-Rt/L} + \frac{V_0}{R} \quad \text{if at } t=0, I=0 \text{ then,}$$

$$I(0) = C + \frac{V_0}{R} = 0$$

so our solution is,

$$I(t) = \frac{V_0}{R} (1 - e^{-Rt/L})$$

starts @
 $I=0$.



We will observe more interesting results when we have an AC supply. Let's work on this for,

$$V(t) = V_0 \cos(\omega t)$$

We have already found the homogeneous solution, I_H , so we just need a good guess for $I_p(t)$.

We'd expect that a sinusoidal source would result in a sinusoidal solution, so let's try,

$$I_p(t) = a \cos(\omega t + \varphi)$$

\leftarrow these are both undetermined coefficients.
Our differential equation is now,

$$L \frac{dI_p}{dt} + I_p R = V_0 \cos(\omega t)$$

$$-La\omega \sin(\omega t + \varphi) + aR \cos(\omega t + \varphi) = V_0 \cos(\omega t)$$

this looks a little complex but we can simplify things ~~with~~ with standard trig identities,

$$\sin(a+b) = \sin a \cos b + \cos a \sin b$$

$$\cos(a+b) = \cos a \cos b - \sin a \sin b$$

If we use these identities we find,

$$-La\omega \sin \omega t \cos \varphi - aR \sin \omega t \sin \varphi = 0$$

$$-La\omega \cos \omega t \sin \varphi + aR \cos \omega t \cos \varphi = V_0 \cos \omega t$$

if the coeffs in front of the $\sin \omega t$ terms vanish and those in front of the $\cos \omega t$ terms give V_0 , it works!

$$\begin{aligned} -La\omega \cos \varphi - aR \sin \varphi &= 0 \\ -La\omega \sin \varphi + aR \cos \varphi &= V_0 \end{aligned} \quad \left. \begin{array}{l} \text{Two eqn's and} \\ \text{two unknowns } (\alpha \text{ and } \varphi) \end{array} \right\}$$

\Rightarrow the first equation we have gives

$$-La \cos \varphi = aR \sin \varphi$$

- if $a=0$, this works, but that means $I_p(+)=0$

- if instead,

$$\tan \varphi = -\frac{L\omega}{R} \quad \text{or} \quad \boxed{\varphi = \tan^{-1}\left(-\frac{L\omega}{R}\right)}$$

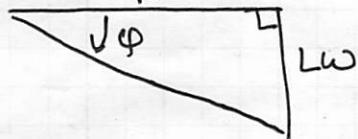
then we get a nonzero I_p .

So φ is not an arbitrary constant and is not dependent on initial conditions. It is determined by the circuit elements and the driver.

\Rightarrow the second equation we have gives,

$$a(-L\omega \sin \varphi + R \cos \varphi) = V_0$$

We can use a triangle that shows $\tan \varphi = -\frac{L\omega}{R}$,



We can read off $\sin \varphi$ & $\cos \varphi$,

$$\sin \varphi = \frac{-L\omega}{\sqrt{R^2 + L^2\omega^2}} \quad \cos \varphi = \frac{+R}{\sqrt{R^2 + L^2\omega^2}}$$

Let's put these back into the 2nd equation,

$$a \left(\frac{L^2\omega^2}{\sqrt{R^2 + L^2\omega^2}} + \frac{R^2}{\sqrt{R^2 + L^2\omega^2}} \right) = a \left(\sqrt{R^2 + L^2\omega^2} \right) = V_0$$

$$\boxed{a = \frac{V_0}{\sqrt{R^2 + L^2\omega^2}}}$$

So with $\varphi = \tan^{-1}\left(-\frac{L\omega}{R}\right)$ and $a = \frac{V_0}{\sqrt{R^2 + L^2\omega^2}}$,

$$I_p(+) = a \cos(\omega t + \varphi) \text{ works.}$$

So our full solution is,

$$I(t) = I_p + I_H = a \cos(\omega t + \varphi) + I_{H0} e^{-Rt/L}$$

= persistent oscillatory + dying away piece
response

\Rightarrow a and φ are determined already (on previous page)

I_{H0} is not determined; it is determined by initial conditions.

So if, for example, at $t=0$, $I=0$ then,

$$I(t>0) = a \cos(\omega t + \varphi) - \underbrace{a \cos \varphi}_{\text{makes } I(t=0)=0} e^{-Rt/L}$$

with amplitude $a = \frac{V_0}{\sqrt{R^2 + L^2 \omega^2}}$ and phase, $\varphi = \tan^{-1}\left(-\frac{L\omega}{R}\right)$

- When R is large, a is small. Big R kills off long term currents.
- When $\omega=0$ (battery), $a \rightarrow V_0/R$ and $\tan^{-1}(0) = 0 = \varphi$.
the inductor acts like an ideal wire in
the long term limit w/ DC voltage.
- When $\omega \rightarrow \infty$, $a \rightarrow 0$; Inductors don't like rapid
changes (big Back EMFs!)

This method works just fine, but it's a real pain when you have a more complex circuit.
especially w/ multiple R 's, L 's, & C 's.
in series and/or parallel.

Method 2. Phasors

- The phasor method is a bit more sophisticated, but it's incredibly powerful and widely used.
 - It gets rid of the sines & cosines and changes our problem to a simple algebra problem using exponentials.
 - We will make use of Euler's famous formula,
- $$e^{i\theta} = \cos\theta + i\sin\theta \quad \text{or for our purposes,}$$
- $$e^{i\omega t} = \cos\omega t + i\sin\omega t.$$

What's nice about the exponential form is how they work under derivatives (and integrals),

$\frac{d}{dt}(\cos\omega t) = -\omega\sin\omega t$ is a new, linearly ind. function
(leads to complications.)

But,

$\frac{d}{dt}(e^{i\omega t}) = i\omega e^{i\omega t}$, just proportional to the original function, $\frac{df}{dt} \propto f$.
(much easier!)

So here's what we are going to do. Instead of $V_0 \cos\omega t$ as the driver, we will use $V_0 e^{i\omega t}$. Now, this might bother you b/c the voltage is complex. That's fine, at the end of the day we will take the real part.

$$V_{\text{true}} = \text{Re}[V_{\text{fiction}}] \quad \text{and} \quad I_{\text{true}} = \text{Re}[I_{\text{fiction}}]$$

We can do this b/c the ODE is linear, so $\text{Re}(I)$ arises from $\text{Re}(V)$. The ODE will be simpler, but we will remember to take the real part.

Let's rework the problem again using the phasor method,

$$L \frac{dI}{dt} + IR = V(t) = \tilde{V} e^{i\omega t}$$

so we have this (fictitious) driving voltage, $\tilde{V} e^{i\omega t}$. It's complex

- the real voltage is $\text{Re}(\tilde{V} e^{i\omega t})$

- if \tilde{V} is itself a complex constant (i.e., $\tilde{V} = V_0 e^{i\delta}$),
then we can have more complex drivers $V_0 \cos(\omega t + \delta)$

We know the solution for I_H , so we just need to find I_p .

We will guess & check. This time we guess a simple form: $I_p = \tilde{I} e^{i\omega t}$

$$L \frac{dI_p}{dt} + I_p R = \tilde{V} e^{i\omega t} \text{ is the ODE,}$$

$$L \tilde{I}(i\omega) e^{i\omega t} + \tilde{I} R e^{i\omega t} = \tilde{V} e^{i\omega t} \text{ the } e^{i\omega t} \text{'s cancel out!}$$

$$L \tilde{I}(i\omega) + \tilde{I} R = \tilde{V} \quad \text{or} \quad \tilde{I} = \frac{\tilde{V}}{R + i\omega L}$$

that's it! \tilde{I} is a constant \rightarrow and our solution is simply,

$$I_{\text{true}} = \text{Re}(I_{\text{fictitious}}) = \text{Re}(\tilde{I} e^{i\omega t}) + I_H$$

see how much simpler that is! from before

The solution looks like $\tilde{V} = \tilde{I} \tilde{R}$ with \tilde{R} now complex

\tilde{R} is the impedance (or complex impedance), we label it \tilde{Z}

for



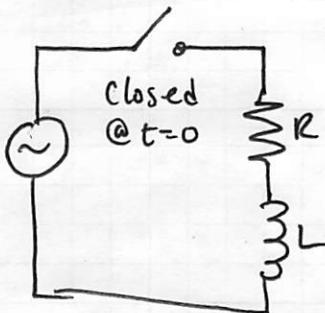
We got $\left. \begin{array}{l} \text{a series circuit} \\ \text{just add the} \\ \text{impedances} \end{array} \right\}$ More general actually!

$$\tilde{Z}_R = R \text{ resistor}$$

$$\tilde{Z}_L = i\omega L \text{ inductor}$$

(turns out a capacitor has $\tilde{Z}_C = -\frac{i}{\omega C}$)

Let's return to the RL example and wrap it up,



$$Z_{\text{tot}} = R + i\omega L$$

$$\text{so we have, } \tilde{V} = \tilde{I}(R + i\omega L)$$

$$\text{and } V_{\text{true}} = \text{Re } \tilde{V} e^{i\omega t}$$

$$I_{\text{true}} = \text{Re } \tilde{I} e^{i\omega t} = \text{Re} \left(\frac{\tilde{V} e^{i\omega t}}{R + i\omega L} \right)$$

In our original setup, $V_{\text{real}} = V_0 \cos \omega t$ so $\tilde{V} = V_0$

So we have:

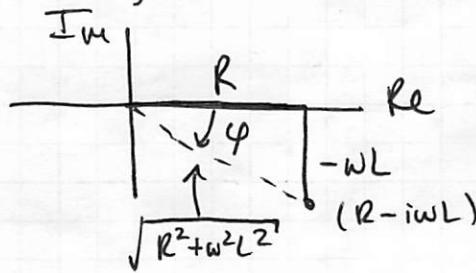
$$I_{\text{true}} = \text{Re} \left(\frac{V_0 e^{i\omega t}}{R + i\omega L} \right) = \text{Re} \left(\frac{V_0 e^{i\omega t}}{R + i\omega L} \frac{R - i\omega L}{R - i\omega L} \right)$$

↑ standard method

$$\text{so, } I = \frac{V_0}{R^2 + \omega^2 L^2} \text{Re} (e^{i\omega t} (R - i\omega L))$$

How do we deal with the rest of the expression?

Another standard method, draw $R - i\omega L$ in the complex plane,



In the complex plane,

this point is simply,

$$\sqrt{R^2 + \omega^2 L^2} e^{i\phi} \quad \text{with } \phi = \tan^{-1} \left(\frac{-\omega L}{R} \right) \text{ as before}$$

$$\text{so, } I = \frac{V_0}{\sqrt{R^2 + \omega^2 L^2}} \text{Re} (e^{i\omega t} e^{i\phi}) = \frac{V_0}{\sqrt{R^2 + \omega^2 L^2}} \cos(\omega t + \phi)$$

This is the exact solution we had before but now $V = IZ$

This works for $V = V_0 \cos(\omega t + \delta) \Rightarrow$ use $\tilde{V} = V_0 e^{i\delta}$

or for $V = V_0 \sin(\omega t) \Rightarrow$ use $\tilde{V} = V_0 e^{i\pi/2}$

What if there's a capacitor? Can we use the same tools?

$$\text{---+---} \quad V = \frac{Q}{C} \Rightarrow \frac{dV}{dt} = \frac{I}{C} \quad \text{or that } I = C \frac{dV}{dt}$$

So if the driver is $V(t) = \tilde{V} e^{i\omega t}$ then,

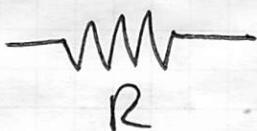
$$I = C i \omega \tilde{V} e^{i\omega t} = i \omega C V$$

This looks like $V = I "R"$ but this time the

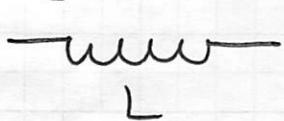
impedance is $Z_C = \frac{1}{i\omega C} = \frac{-i}{\omega C}$ (we use Z to indicate complex impedance)

Summary

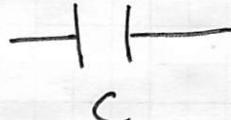
$$Z = R$$



$$Z = i\omega L$$



$$Z = -i/\omega C$$



General Result! you can treat each passive element like a simple resistor with the impedances given above. You can construct Z_{eff} using the standard "rules" for resistors.

In series,

$$Z_{eff} = Z_1 + Z_2 + Z_3 + \dots$$

In parallel,

$$\frac{1}{Z_{eff}} = \frac{1}{Z_1} + \frac{1}{Z_2} + \frac{1}{Z_3} + \dots$$

Can apply usual Kirchhoff's Laws to them as well.

Example! An RC CircuitTurn it on at $t = 0$ with $V(+)=V_0 \cos \omega t$ think of this as two Z 's,

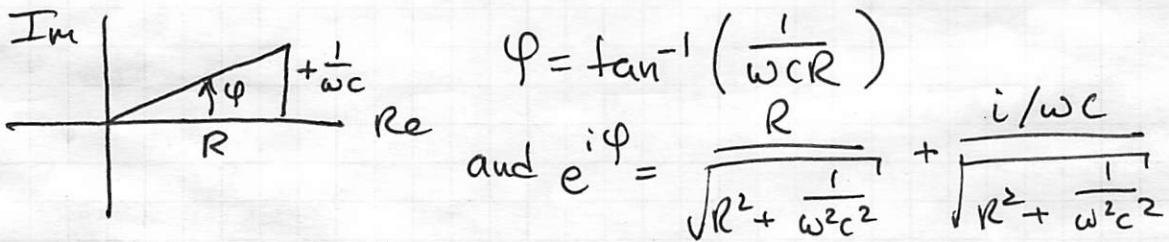
$$Z_{\text{tot}} = Z_R + Z_C = R - \frac{i}{\omega C}$$

$$\text{with, } \tilde{V} = \tilde{I} Z \Rightarrow \tilde{I} = \frac{\tilde{V}}{R - i/\omega C} \text{ and } I_{\text{real}} = V_0 \text{Re} \left(\frac{e^{i\omega t}}{R - i/\omega C} \right)$$

The first part uses this method again,

$$I = V_0 \text{Re} \left(\frac{e^{i\omega t}}{R - i/\omega C} \frac{R + i/\omega C}{R + i/\omega C} \right) = \frac{V_0}{R^2 + \frac{1}{\omega^2 C^2}} \text{Re} \left(e^{i\omega t} \left(R + \frac{i}{\omega C} \right) \right)$$

Use the second method, draw a picture,



So the particular solution is,

$$I_p = \frac{V_0}{\sqrt{R^2 + \frac{1}{\omega^2 C^2}}} \cos(\omega t + \varphi)$$

We still need to solve the homogeneous equation,

$$0 = IR + Q/C \quad \cancel{\text{dq/dt}} \Rightarrow \frac{dI}{dt} R = -\frac{I}{C}$$

take time derivative
($dQ/dt = I$)

$$\text{so, } \frac{dI}{I} = -\frac{1}{RC} dt \Rightarrow I_H = I_0 e^{-t/RC}$$

$$I_{\text{tot}} = \underbrace{\frac{V_0}{\sqrt{R^2 + \frac{1}{\omega^2 C^2}}} \cos(\omega t + \varphi)}_{\text{Steady solution}} + I_0 e^{-t/RC}$$

↑
TBD
by initial conditions.

transient dies off

Initial Conditions: ΔV_{cap} cannot suddenly change.

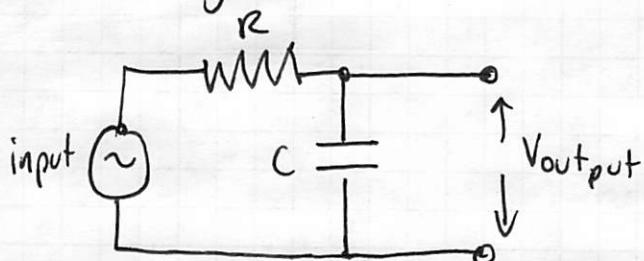
If it was zero before then just after $V_0 = IR$ b/c $\Delta V_{cap} = 0$ for just a quick moment. So $I(t=0) = V_0/R$.

So, this gives,

$$I(t) = \frac{V_0}{\sqrt{R^2 + 1/\omega^2 C^2}} \cos(\omega t + \varphi) + \underbrace{\left(\frac{V_0}{R} - \frac{V_0 \cos \varphi}{\sqrt{R^2 + 1/\omega^2 C^2}} \right)}_{\text{picked so } @t=0 I = V_0/R} e^{-t/RC}$$

- time constant is "RC"
- After waiting several RC times the circuit oscillates with driver frequency, ω
- If $\omega \rightarrow 0$, $I_{\text{long term}} \rightarrow 0$, the capacitor blocks steady current.
- if $\omega \rightarrow \infty$, $I_{\text{long term}} \rightarrow \frac{V_0}{R} \cos(\omega t)$ like the capacitor isn't there.

It's often useful to put this setup in a circuit where you can read out a voltage (as a signal)



We know I in this circuit and V_{out} is,

$$V_{out} = I Z_C = I (-i/\omega C)$$

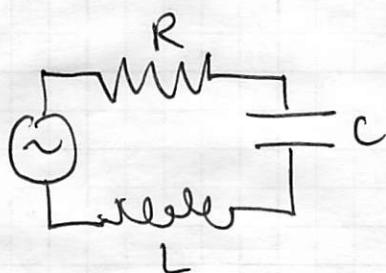
$$V_{out} = \frac{V_{in}}{Z_{\text{tot}}} Z_C = \frac{V_{in}}{R - \frac{i}{\omega C}} \left(-i/\omega C \right) = V_{in} \left(\frac{1}{1 + i\omega RC} \right)$$

With $\omega \rightarrow 0$, $V_{out} = V_{in}$, cap does nothing.

With $\omega \rightarrow \infty$, $V_{out} \rightarrow 0$, "low pass filter"

Allows low frequencies to pass; suppresses high frequency.

with the phasor method & impedance, any circuit is basically a 184 circuit.



$$\text{just use } Z = R + i\omega L - \frac{i}{\omega C}$$

$$\text{and then } \tilde{V} = \tilde{I} \tilde{Z}$$