

Pressure Drop Calculations & Optimum Line Size Selection



302 ft

Image shows approximate pipe length required, add extra 20% margin for piping turns & elevations

These are python libraries needed for unit conversion & mathematical functions

```
In [1]: 1 import handcalcs.render
        2 from handcalcs.decorator import handcalc
        3 from math import log, log10, sqrt, pi, exp
```

```
In [2]: 1 import forallpeople as si
        2 si.environment('ukhan', top_level=True)
```

Table -1 Pipe Fittings Equivalent Lengths

| Fitting | Types | (L/D)eq |
|----------------------------------|----------------------------------|---------|
| 90° Elbow Curved, Threaded | Standard Radius (R/D = 1) | 30 |
| | Long Radius (R/D = 1.5) | 16 |
| 90° Elbow Curved, Flanged/Welded | Standard Radius (R/D = 1) | 20 |
| | Long Radius (R/D = 2) | 17 |
| | Long Radius (R/D = 4) | 14 |
| | Long Radius (R/D = 6) | 12 |
| | 1 weld (90°) | 60 |
| 90° Elbow Mitered | 2 welds (45°) | 15 |
| | 3 welds (30°) | 8 |
| 45° Elbow Curved, Threaded | Standard Radius (R/D = 1) | 16 |
| | Long Radius (R/D = 1.5) | |
| 45° Elbow Mitered | 1 weld 45° | 15 |
| | 2 welds 22.5° | 6 |
| 180° Bend | threaded, close-return (R/D = 1) | 50 |
| | flanged (R/D = 1) | |
| | all types (R/D = 1.5) | |
| Tee Through-branch as an Elbow | threaded (r/D = 1) | 60 |
| | threaded (r/D = 1.5) | |
| | flanged (r/D = 1) | 20 |
| | stub-in branch | |
| Tee Run-through | threaded (r/D = 1) | 20 |
| | flanged (r/D = 1) | |
| Angle valve | stub-in branch | |
| | 45°, full line size, β = 1 | 55 |
| Globe valve | 90° full line size, β = 1 | 150 |
| | standard, β = 1 | 340 |
| Plug valve | branch flow | 90 |
| | straight through | 18 |
| Gate valve | three-way (flow through) | 30 |
| | standard, β = 1 | 8 |
| Ball valve | standard, β = 1 | 3 |
| Diaphragm | dam type | |

| | | |
|-------------------|---|-----|
| Swing check valve | $V_{\min} = 35 [\rho \text{ (lbm/ft}^3\text{)}]^{-1/2}$ | 100 |
| Lift check valve | $V_{\min} = 40 [\rho \text{ (lbm/ft}^3\text{)}]^{-1/2}$ | 600 |
| Hose Coupling | Simple Full Bore | 5 |

Table-2 Absolute Roughness ξ

| Material | Roughness (mm) |
|--|----------------|
| Drawn Tubing, Glass, Plastic | 0.0015-0.01 |
| Drawn Brass, Copper, Stainless Steel (New) | >0.0015-0.01 |
| Flexible Rubber Tubing - Smooth | 0.006-0.07 |
| Flexible Rubber Tubing - Wire Reinforced | 0.3-4 |
| Stainless Steel | 0.03 |
| Wrought Iron (New) | 0.045 |
| Carbon Steel (New) | 0.02-0.05 |
| Carb on Steel (Slightly Corroded) | 0.05-0.15 |
| Carbon Steel (Moderately Corroded) | 0.15-1 |
| Carbon Steel (Badly Corroded) | 1-3 |
| Carbon Steel (Cement-lined) | 1.5 |
| Asphalted Cast Iron | 0.1-1 |
| Cast Iron (new) | 0.25 |
| Cast Iron (old, sandblasted) | 1 |
| Sheet Metal Ducts (with smooth joints) | 0.02-0.1 |
| Galvanized Iron | 0.025-0.15 |
| Wood Stave | 0.18-0.91 |
| Wood Stave, used | 0.25-1 |
| Smooth Cement | 0.5 |
| Concrete – Very Smooth | 0.025-0.2 |
| Concrete – Fine (Floated, Brushed) | 0.2-0.8 |
| Concrete – Rough, Form Marks | 0.8-3 |
| Riveted Steel | 0.91-9.1 |
| Water Mains with Tuberculations | 1.2 |
| Brickwork, Mature Foul Sewers | 3 |

Source: <https://neutrium.net> (<https://neutrium.net/fluid-flow/pressure-loss-from-fittings-in-pipe-summary/>)

```
In [3]: 1 %%render params 1
2 PipeL = (302*1.2) *ft.to(m) #20% additional Length
3 PipeID = 50 *mm #Internal Dia
4 PP_xi = 0.01 *mm #PolyPropylene Roughness
```

PipeL = 110.5 m (20% additional length) PipeID = 50.0 mm (Internal Dia) $PP_{\xi} = 10.0 \mu\text{m}$ (PolyPropylene Roughness)

```
In [4]: 1 %%render params 1
2 flow_H2O = 5 *m3_h
3 rho_H2O = 988 *kg_m3.prefix('unity') # at 50°C
4 nu_H2O = 0.5465 *cP #Viscosity in centiPoise is equal to mPa.s
```

$\text{flow}_{H_2O} = 5.0 \text{ m}^3 \cdot \text{h}^{-1}$ $\rho_{H_2O} = 988.0 \text{ kg} \cdot \text{m}^{-3}$ (at 50°C) $\nu_{H_2O} = 546.5 \mu\text{Pa} \cdot \text{s}$ (Viscosity in centiPoise is equal to mPa.s)

Water physical properties: <https://wiki.anton-paar.com/en/water/> (<https://wiki.anton-paar.com/en/water/>)

```
In [5]: 1 %%render params 1
2 Elbows = 10 #90° Elbow Threaded Standard
3 Elbow_EqFactor = 30
4 Valves = 2 #Ball valve
5 Valve_EqFactor = 3 #Refer Table-1
```

Elbows = 10 (90° Elbow Threaded Standard) Elbow_{EqFactor} = 30 Valves = 2 (Ball valve)

Valve_{EqFactor} = 3 (Refer Table-1)

```
In [6]: 1 %%render long
2 Sigma_PipeL = PipeL + (Elbows*Elbow_EqFactor*PipeID) + (Valves*Valve_EqFactor*PipeID)
```

$\Sigma_{PipeL} = \text{PipeL} + (\text{Elbows} \cdot \text{Elbow}_{EqFactor} \cdot \text{PipeID}) + (\text{Valves} \cdot \text{Valve}_{EqFactor} \cdot \text{PipeID})$
= 110.460 m + (10 · 30 · 50.000 mm) + (2 · 3 · 50.000 mm)
= 125.760 m

```
In [7]: 1 @handcalc(jupyter_display=True)
2 def reynolds(D, F, rho, nu):
3     A = 0.25 * pi * D**2
4     velocity = F / A #Calculate velocity
5     NRe = (D * velocity * rho) / nu #Calculate Reynold's number
6     return velocity, NRe
```

```
In [8]: 1 velocity, NRe = reynolds(PipeID, flow_H2O, rho_H2O, nu_H2O)
```

$$A = 0.25 \cdot \pi \cdot (D)^2 = 0.25 \cdot 3.142 \cdot (50.000 \text{ mm})^2 = 1963.495 \text{ mm}^2$$

$$\text{velocity} = \frac{F}{A} = \frac{5.000 \text{ m}^3 \cdot \text{h}^{-1}}{1963.495 \text{ mm}^2} = 707.355 \text{ mm} \cdot \text{s}^{-1} \quad (\text{Calculate velocity})$$

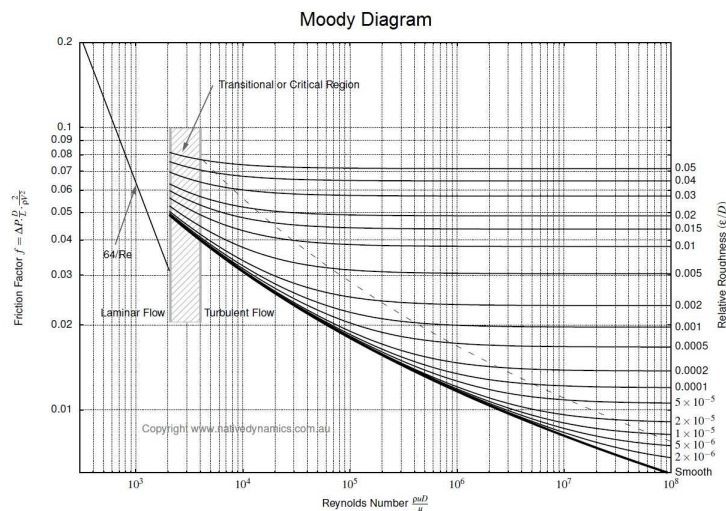
$$\text{NRe} = \frac{D \cdot \text{velocity} \cdot \rho}{\nu} = \frac{50.000 \text{ mm} \cdot 707.355 \text{ mm} \cdot \text{s}^{-1} \cdot 988.000 \text{ kg} \cdot \text{m}^{-3}}{546.500 \mu\text{Pa} \cdot \text{s}} = 63940.260 \quad (\text{Calculate Reynold's number})$$

```
In [9]: 1 %%render 4
2 if NRe <= 2100: Flow = 'Laminar'
3 elif NRe <= 4000: Flow = 'Transient'
4 elif NRe > 4000: Flow = 'Turbulent'
5
6 PipeRR = PP_xi/PipeID #Pipe Relative Roughness
```

Since, NRe > 4000 \rightarrow (63940.2597 > 4000) :

Flow = Turbulent

$$\text{PipeRR} = \frac{PP_{\xi}}{\text{PipeID}} = \frac{10.0000 \mu\text{m}}{50.0000 \text{ mm}} = 0.0002 \quad (\text{Pipe Relative Roughness})$$



Moody Friction Factor Figure

Method-1 Using Graph

Relative Roughness is 0.0002

Reynolds number is approximately $6.4 \cdot 10^4$

Friction factor f is approximately 0.022

```
In [10]: 1 @handcalc(jupyter_display=True)
2 def pressuredrop(f, Sigma_L, D, rho, velocity):
3     Delta_p = f * (Sigma_L/D) * (rho*velocity**2)/2
4     return Delta_p
```

```
In [11]: 1 Delta_p = pressuredrop(0.022,Sigma_PipeL, PipeID, rho_H2O, velocity)
```

$$\Delta_p = f \cdot \left(\frac{\Sigma_L}{D} \right) \cdot \frac{\rho \cdot (\text{velocity})^2}{2}$$

$$= 0.022 \cdot \left(\frac{125.760 \text{ m}}{50.000 \text{ mm}} \right) \cdot \frac{988.000 \text{ kg} \cdot \text{m}^{-3} \cdot (707.355 \text{ mm} \cdot \text{s}^{-1})^2}{2}$$

$$= 13.677 \text{ kPa}$$

Method-2 Using Churchill Emperical Equation

```
In [12]: 1 @handcalc(jupyter_display=True, precision=4)
2 def churchill(NRe, D, xi):
3     A = ( 2.457*log( 1 / ( (7/NRe)**0.9 + 0.27*xi/D ) ) )**16
4     B = (37530/NRe)**16
5     f = 8 * ( (8/NRe)**12 + 1/(A+B)**1.5 )**(1/12)
6     return f
```

In [13]: 1 f_churchill = churchill(NRe, PipeID, PP_xi)

$$A = \left(2.457 \cdot \ln \left(\frac{1}{\left(\frac{7}{\text{NRe}} \right)^{0.9} + 0.27 \cdot \frac{\xi}{D}} \right) \right)^{16}$$

$$= \left(2.457 \cdot \ln \left(\frac{1}{\left(\frac{7}{63940.2597} \right)^{0.9} + 0.27 \cdot \frac{10.0000 \mu\text{m}}{50.0000 \text{ mm}}} \right) \right)^{16}$$

$$= 524038602297619775488.0000$$

$$B = \left(\frac{37530}{\text{NRe}} \right)^{16} = \left(\frac{37530}{63940.2597} \right)^{16} = 0.0002$$

$$f = 8 \cdot \left(\left(\frac{8}{\text{NRe}} \right)^{12} + \frac{1}{(A+B)^{1.5}} \right)^{\left(\frac{1}{12} \right)}$$

$$= 8 \cdot \left(\left(\frac{8}{63940.2597} \right)^{12} + \frac{1}{(524038602297619775488.0000 + 0.0002)^{1.5}} \right)^{\left(\frac{1}{12} \right)}$$

$$= 0.0206$$

In [14]: 1 Delta_pChurchill = pressuredrop(f_churchill, Sigma_PipeL, PipeID, rho_H2O, velocity)

$$\Delta_p = f \cdot \left(\frac{\Sigma_L}{D} \right) \cdot \frac{\rho \cdot (\text{velocity})^2}{2}$$

$$= 0.021 \cdot \left(\frac{125.760 \text{ m}}{50.000 \text{ mm}} \right) \cdot \frac{988.000 \text{ kg} \cdot \text{m}^{-3} \cdot (707.355 \text{ mm} \cdot \text{s}^{-1})^2}{2}$$

$$= 12.786 \text{ kPa}$$

Method-3 Using Serghides Emperical Equation

In [15]: 1 @handcalc(jupyter_display=True, precision=4)
2 def serghide(NRe, D, xi):
3 A = -2*log10((xi/D)/3.7 + 12/NRe)
4 B = -2*log10((xi/D)/3.7 + 2.51*A/NRe)
5 C = -2*log10((xi/D)/3.7 + 2.51*B/NRe)
6 f = (A - ((B-A)**2) / (C - 2*B + A))**(-2)
7 return f

In [16]: 1 f_serghide = serghide(NRe, PipeID, PP_xi)

$$A = (-2) \cdot \log_{10} \left(\frac{\frac{\xi}{D}}{3.7} + \frac{12}{\text{NRe}} \right) = (-2) \cdot \log_{10} \left(\frac{\frac{10.0000 \mu\text{m}}{50.0000 \text{ mm}}}{3.7} + \frac{12}{63940.2597} \right) = 7.2333$$

$$B = (-2) \cdot \log_{10} \left(\frac{\frac{\xi}{D}}{3.7} + 2.51 \cdot \frac{A}{\text{NRe}} \right)$$

$$= (-2) \cdot \log_{10} \left(\frac{\frac{10.0000 \mu\text{m}}{50.0000 \text{ mm}}}{3.7} + 2.51 \cdot \frac{7.2333}{63940.2597} \right)$$

$$= 6.9422$$

$$C = (-2) \cdot \log_{10} \left(\frac{\frac{\xi}{D}}{3.7} + 2.51 \cdot \frac{B}{\text{NRe}} \right)$$

$$= (-2) \cdot \log_{10} \left(\frac{\frac{10.0000 \mu\text{m}}{50.0000 \text{ mm}}}{3.7} + 2.51 \cdot \frac{6.9422}{63940.2597} \right)$$

$$= 6.9720$$

$$f = \left(A - \frac{(B-A)^2}{C - 2 \cdot B + A} \right)^{(-2)} = \left(7.2333 - \frac{(6.9422 - 7.2333)^2}{6.9720 - 2 \cdot 6.9422 + 7.2333} \right)^{(-2)} = 0.0206$$

In [17]: 1 Delta_pSerghide = pressuredrop(f_serghide, Sigma_PipeL, PipeID, rho_H2O, velocity)

$$\Delta_p = f \cdot \left(\frac{\Sigma_L}{D} \right) \cdot \frac{\rho \cdot (\text{velocity})^2}{2}$$

$$= 0.021 \cdot \left(\frac{125.760 \text{ m}}{50.000 \text{ mm}} \right) \cdot \frac{988.000 \text{ kg} \cdot \text{m}^{-3} \cdot (707.355 \text{ mm} \cdot \text{s}^{-1})^2}{2}$$

$$= 12.800 \text{ kPa}$$

Method-4 Goudar- Sonnad

```
In [18]: 1 @handcalc(jupyter_display=True, precision=4)
2 def gsonnad(NRe, D, xi):
3     a = 2/log(10)
4     b = (xi/D)/3.7
5     d = log(10)/5.02 *NRe
6     s = b*d + log(d)
7     q = s*( s/(s+1) )
8     g = b*d + log(d/q)
9     zeta = q/g
10    delta_LA = (g/(g+1))*zeta
11    delta_CFA = delta_LA * ( 1 + (zeta/2)/( (g+1)**2 + (zeta/3)*(2*g-1) ) )
12    f = 1/( a* ( log(d/q)+ delta_CFA ) )**2
13    return f
```

```
In [19]: 1 f_gsonnad = gsonnad(NRe, PipeID, PP_xi)
```

$$a = \frac{2}{\ln(10)} = 0.8686$$

$$b = \frac{\frac{\xi}{D}}{3.7} = \frac{\frac{10.0000 \mu\text{m}}{50.0000 \text{ mm}}}{3.7} = 0.0001$$

$$d = \frac{\ln(10)}{5.02} \cdot \text{NRe} = \frac{\ln(10)}{5.02} \cdot 63940.2597 = 29328.2647$$

$$s = b \cdot d + \ln(d) = 0.0001 \cdot 29328.2647 + \ln(29328.2647) = 11.8716$$

$$q = (s)^{\left(\frac{s}{s+1}\right)} = (11.8716)^{\left(\frac{11.8716}{11.8716+1}\right)} = 9.7956$$

$$g = b \cdot d + \ln\left(\frac{d}{q}\right) = 0.0001 \cdot 29328.2647 + \ln\left(\frac{29328.2647}{9.7956}\right) = 9.5897$$

$$\zeta = \frac{q}{g} = \frac{9.7956}{9.5897} = 1.0215$$

$$\delta_{LA} = \left(\frac{g}{g+1}\right) \cdot \zeta = \left(\frac{9.5897}{9.5897+1}\right) \cdot 1.0215 = 0.9250$$

$$\delta_{CFA} = \delta_{LA} \cdot \left(1 + \frac{\frac{\zeta}{2}}{(g+1)^2 + \left(\frac{\zeta}{3}\right) \cdot (2 \cdot g - 1)}\right)$$

$$= 0.9250 \cdot \left(1 + \frac{\frac{1.0215}{2}}{(9.5897+1)^2 + \left(\frac{1.0215}{3}\right) \cdot (2 \cdot 9.5897 - 1)}\right)$$

$$= 0.9290$$

$$f = \frac{1}{\left(a \cdot \left(\ln\left(\frac{d}{q}\right) + \delta_{CFA}\right)\right)^2}$$

$$= \frac{1}{\left(0.8686 \cdot \left(\ln\left(\frac{29328.2647}{9.7956}\right) + 0.9290\right)\right)^2}$$

$$= 0.0166$$

```
In [20]: 1 Delta_pGsonnad = pressuredrop(f_gsonnad, Sigma_PipeL, PipeID, rho_H2O, velocity)
```

$$\Delta_p = f \cdot \left(\frac{\Sigma_L}{D}\right) \cdot \frac{\rho \cdot (\text{velocity})^2}{2}$$

$$= 0.017 \cdot \left(\frac{125.760 \text{ m}}{50.000 \text{ mm}}\right) \cdot \frac{988.000 \text{ kg} \cdot \text{m}^{-3} \cdot (707.355 \text{ mm} \cdot \text{s}^{-1})^2}{2}$$

$$= 10.326 \text{ kPa}$$

Method-5 Using Tkachenko, Mileikovskiy

Source Moscow University (https://link.springer.com/chapter/10.1007/978-3-030-57340-9_37)

```
In [21]: 1 @handcalc(jupyter_display=True, precision=4)
2 def tkmile(NRe, D, xi):
3     A_0 = -0.79638*log( (xi/D)/8.208 + 7.3357/NRe )
4     A_1 = NRe*(xi/D) + 9.3120665*A_0
5     f = ( 8.128943 + A_1)/( 8.128943*A_0 - 0.86859209*A_1*log(A_1/(3.7099535*NRe)) ) )**2
6     return f
```

```
In [22]: 1 f_tkmile = tkmile(NRe, PipeID, PP_xi)
```

$$\begin{aligned} A_0 &= (-0.79638) \cdot \ln\left(\frac{\frac{\xi}{D}}{8.208} + \frac{7.3357}{NRe}\right) \\ &= (-0.79638) \cdot \ln\left(\frac{\frac{10.0000 \mu\text{m}}{50.0000 \text{ mm}}}{8.208} + \frac{7.3357}{63940.2597}\right) \\ &= 7.0721 \\ A_1 &= NRe \cdot \left(\frac{\xi}{D}\right) + 9.3120665 \cdot A_0 = 63940.2597 \cdot \left(\frac{10.0000 \mu\text{m}}{50.0000 \text{ mm}}\right) + 9.3120665 \cdot 7.0721 = 78.6443 \\ f &= \left(\frac{8.128943 + A_1}{8.128943 \cdot A_0 - 0.86859209 \cdot A_1 \cdot \ln\left(\frac{A_1}{3.7099535 \cdot NRe}\right)}\right)^2 \\ &= \left(\frac{8.128943 + 78.6443}{8.128943 \cdot 7.0721 - 0.86859209 \cdot 78.6443 \cdot \ln\left(\frac{78.6443}{3.7099535 \cdot 63940.2597}\right)}\right)^2 \\ &= 0.0206 \end{aligned}$$

```
In [23]: 1 Delta_pTkmile = pressuredrop(f_tkmile, Sigma_PipeL, PipeID, rho_H2O, velocity)
```

$$\begin{aligned} \Delta_p &= f \cdot \left(\frac{\Sigma_L}{D}\right) \cdot \frac{\rho \cdot (\text{velocity})^2}{2} \\ &= 0.021 \cdot \left(\frac{125.760 \text{ m}}{50.000 \text{ mm}}\right) \cdot \frac{988.000 \text{ kg} \cdot \text{m}^{-3} \cdot (707.355 \text{ mm} \cdot \text{s}^{-1})^2}{2} \\ &= 12.799 \text{ kPa} \end{aligned}$$

```
In [24]: 1 from IPython.display import HTML, display
2
3 def display_table(data):
4     html = "<table>"
5     for row in data:
6         html += "<tr>"
7         for field in row:
8             html += "<td><h4>%s</h4></td>"%(field)
9         html += "</tr>"
10    html += "</table>"
11    display(HTML(html))
12
13 data = [['Emperical Relationship', 'Friction Factor', 'Pressure Drop'],
14         ['Churchill', round(f_churchill,4), Delta_pChurchill],
15         ['Serghide', round(f_serghide,4), Delta_pSerghide],
16         ['Goudar-Sonnad', round(f_gsonnad,4), Delta_pGsonnad],
17         ['Tkachenko, Mileikovskiy', round(f_tkmile,4), Delta_pTkmile]]
18 display_table(data)
```

| Emperical Relationship | Friction Factor | Pressure Drop |
|-------------------------|-----------------|---------------|
| Churchill | 0.0206 | 12.786 kPa |
| Serghide | 0.0206 | 12.800 kPa |
| Goudar-Sonnad | 0.0166 | 10.326 kPa |
| Tkachenko, Mileikovskiy | 0.0206 | 12.799 kPa |

```
In [25]: 1 %reload_ext version_information
2 %version_information handcalcs, forallpeople
```

Out[25]:

| Software | Version |
|--------------|---|
| Python | 3.9.18 32bit [Clang 14.0.7 (https://android.googlesource.com/toolchain/llvm-project 4c603efb)] |
| IPython | 8.7.0 |
| OS | Linux 4.19.191 25884040 abA137FXXS3CWL2 armv8l with libc |
| handcalcs | 1.6.5 |
| forallpeople | 2.6.7 |

Mon Jan 22 22:10:49 2024 +03