

Example : Glasshouse Climate Control



ESE 505 & MEAM 513

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Lecture Adapted From This Paper



Pergamon

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MODELLING AND PIP CONTROL OF A GLASSHOUSE MICRO-CLIMATE

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- Suggestion for Motivated Students
 - Read the Paper
 - Write Down Stuff You Don't Understand
 - Ask Lots of Questions!
 - Read Again @ End of Semester!

Temperature Dynamics Inside Glasshouse

- “Complex, non-linear model”
- “11 coupled, non-linear, first-order differential equations”
- “Used to design and evaluate a series of controllers for the internal climate of the glasshouse”
- “Necessary to develop a reduced-order, linearized control model which adequately describes the small perturbation dynamics of the system.”

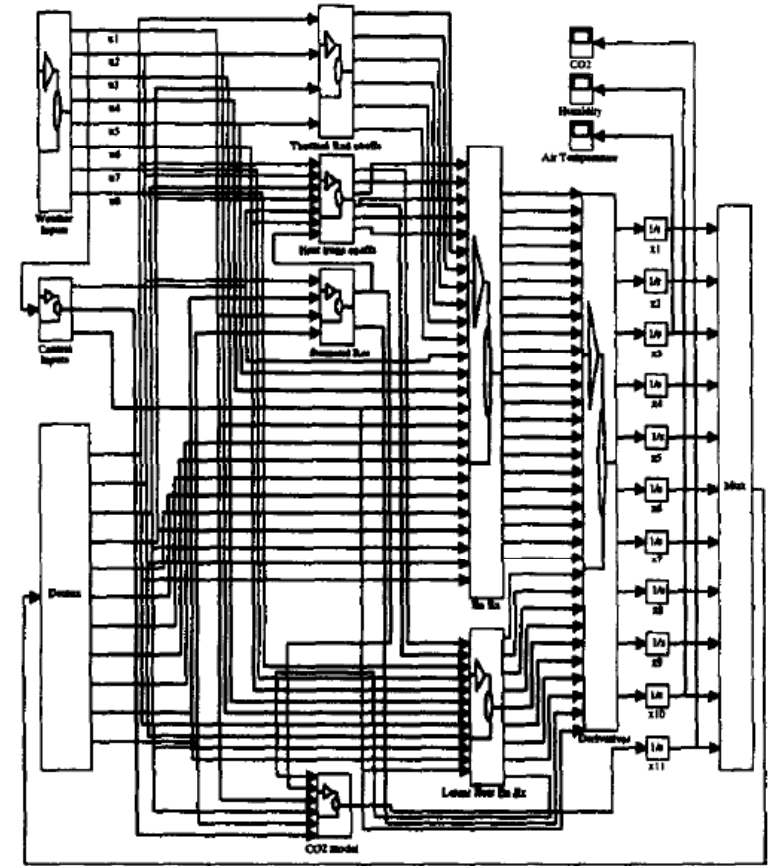


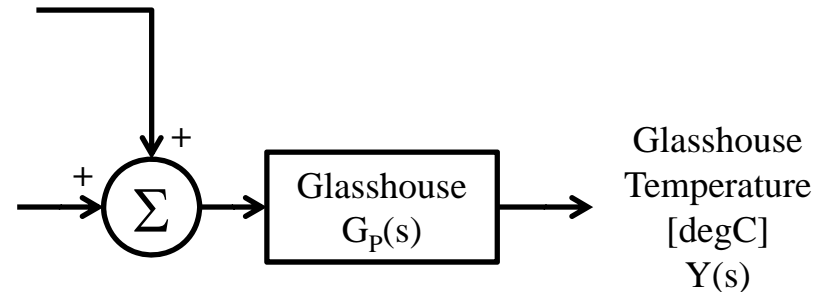
Fig 1 SIMULINK representation of the glasshouse climate model

Linear Approximation to Plant Dynamics

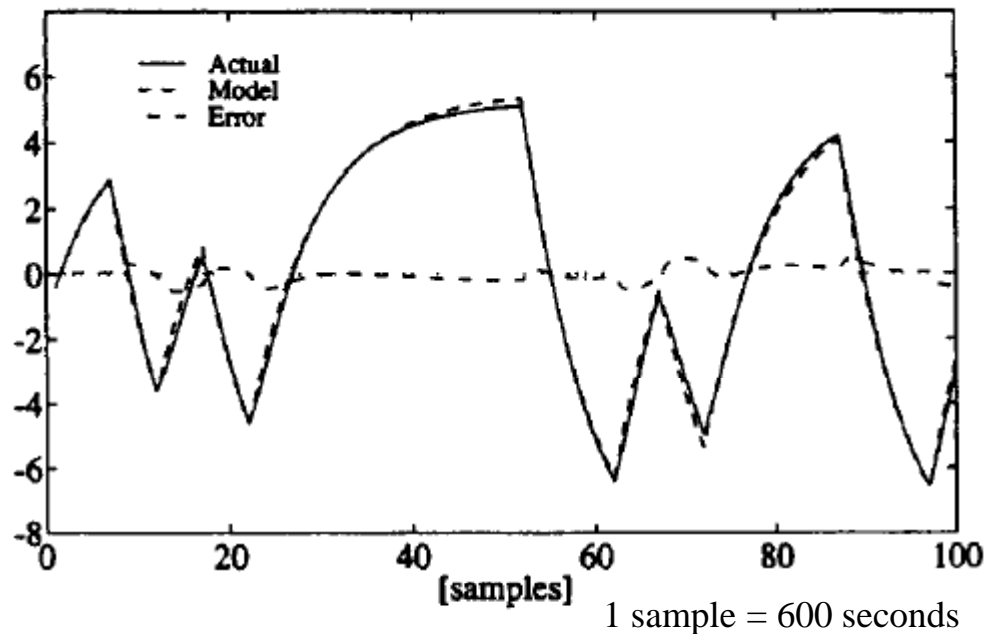
Complex Non-Linear Models Often Well-Approximated by Low-Order Linear Systems!

Solar Heating or Wind Cooling Disturbance $W(s)$

Valve Fractional Opening [percent] $U(s)$



(b) First Order Model Fit and Error



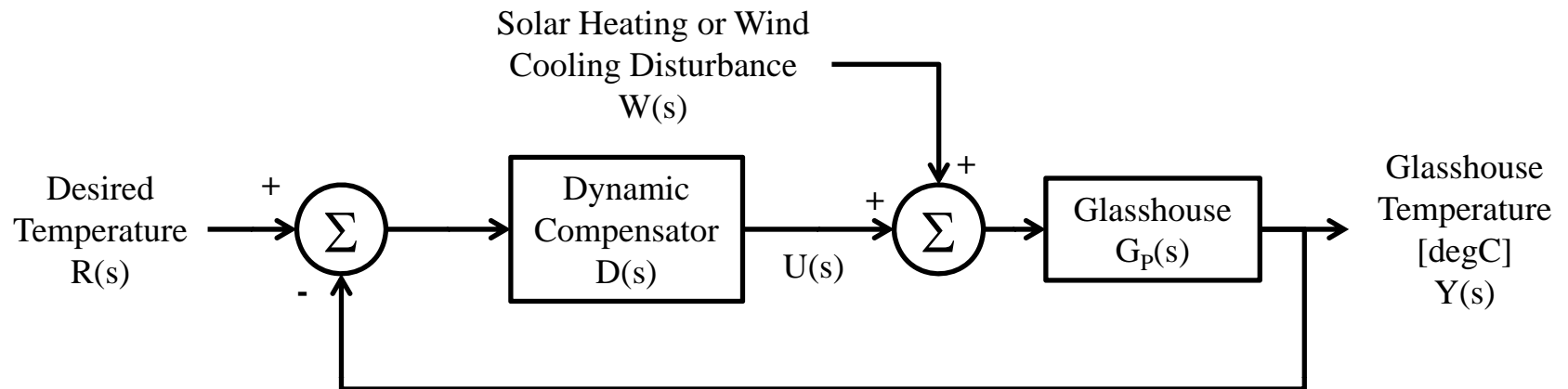
$$G_P(s) = \frac{Ae^{-T_d s}}{\tau s + 1}$$

$$A = 0.32 \text{ degC/percent}$$

$$T_d = 600 \text{ sec (10 min)}$$

$$\tau = 4440 \text{ sec (74 min)}$$

A Simple Candidate Architecture



$$Y(s) = \frac{DG_P}{1 + DG_P} R(s) + \frac{G_P}{1 + DG_P} W(s)$$

“Loop Transfer Function”

$$G(s) \triangleq D(s)G_P(s)$$

Both Terms Have Same
Denominator = $\Delta_{CL}(s)$

$$\Delta_{CL}(s) = 1 + G(s)$$

Some Requirements

- Perfect Temperature Regulation
 - We Interpret To Mean Zero Steady-State Error
 - Need Type 1 System \rightarrow $D(s)$ Must Include Integral Feedback
- Reject Daily Temperature Swings (Solar Heating & Atmospheric Temperature)
 - Want Substantial Disturbance Rejection For 1-Per-Day Disturbances
(Frequency = $2\pi/(24*3600) = 0.000072$ rad/sec)
- “Reduced Actuator Operation (to Minimize Wear)”
 - We Will Interpret As “Don’t Push Crossover Frequency Higher Than Necessary to Achieve Good Disturbance Rejection”
 - Many More Advanced Ideas Here \rightarrow Google “Optimal Control”
 - Minimum Fuel Usage Very Important on Spacecraft
- Rise Time ~ 1 Hour
 - I Made This Up, Based on Data in Paper (“Typical” for Tomatoes?)
- Very Little (No?) Overshoot
 - Closed-Loop Damping Ratio > 0.8

Preliminary Analysis (Ignore Delay at First)

Start with Something
Very Simple: Use Only
Integral Feedback

$$D(s) = \frac{K_I}{s} \quad G_P(s) = \frac{A}{\tau s + 1}$$

Look @ Closed-Loop
Pole Locations

$$\Delta_{CL}(s) = 1 + \frac{AK_I}{s(\tau s + 1)} = 0$$

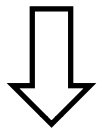
Multiply by $s(\tau s + 1) \rightarrow$

$$s(\tau s + 1) + AK_I = 0$$

“Root Locus” Varying Integral Gain

$$s(\tau s + 1) + AK_I = 0$$

$$\zeta = 0.8$$



$$K_I = 0.000275$$

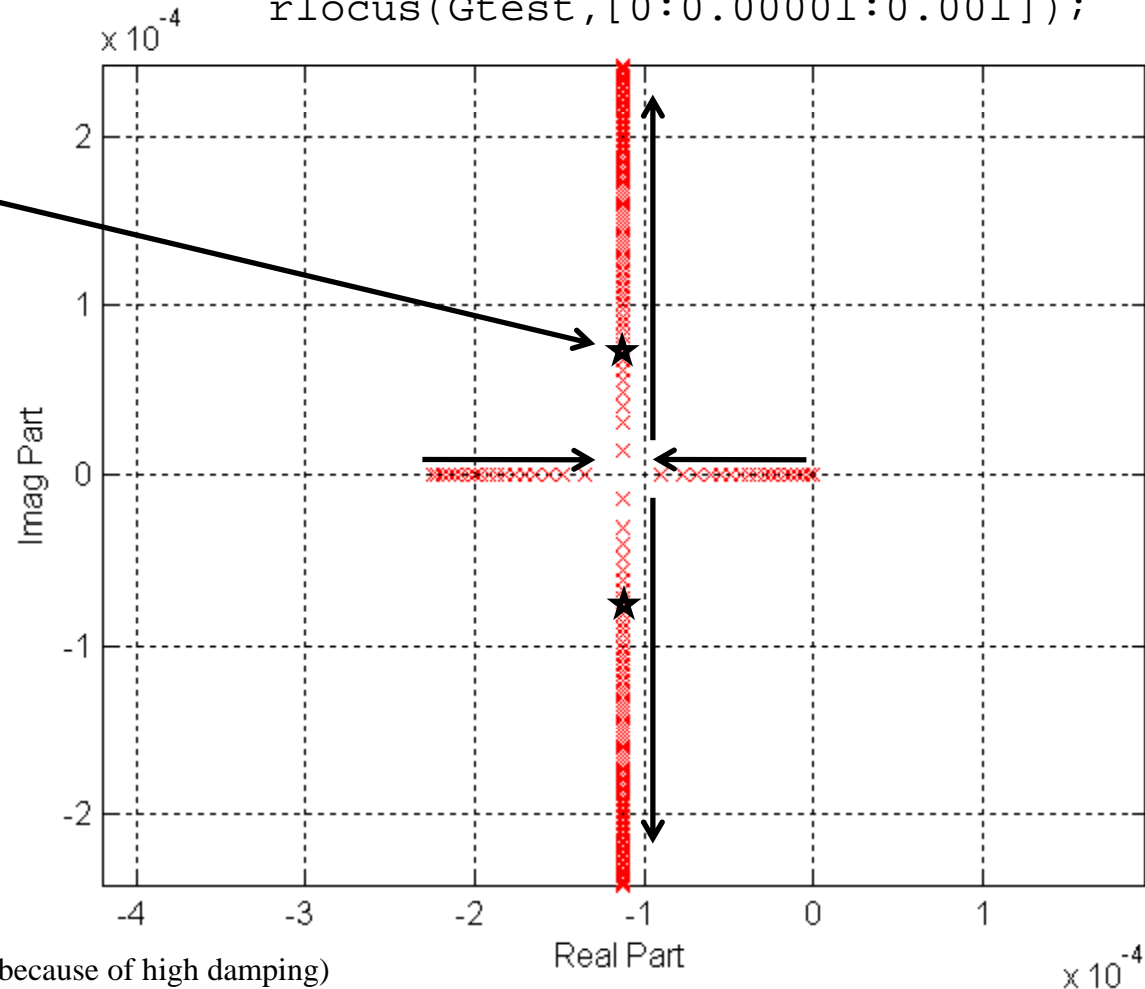
$$\omega_n^2 = \frac{AK_I}{\tau}$$

$$\omega_n = 0.00014 \text{ rps}$$

$$t_r \approx \frac{2}{\omega_n} = 4 \text{ hours}$$

(actual rise time longer because of high damping)

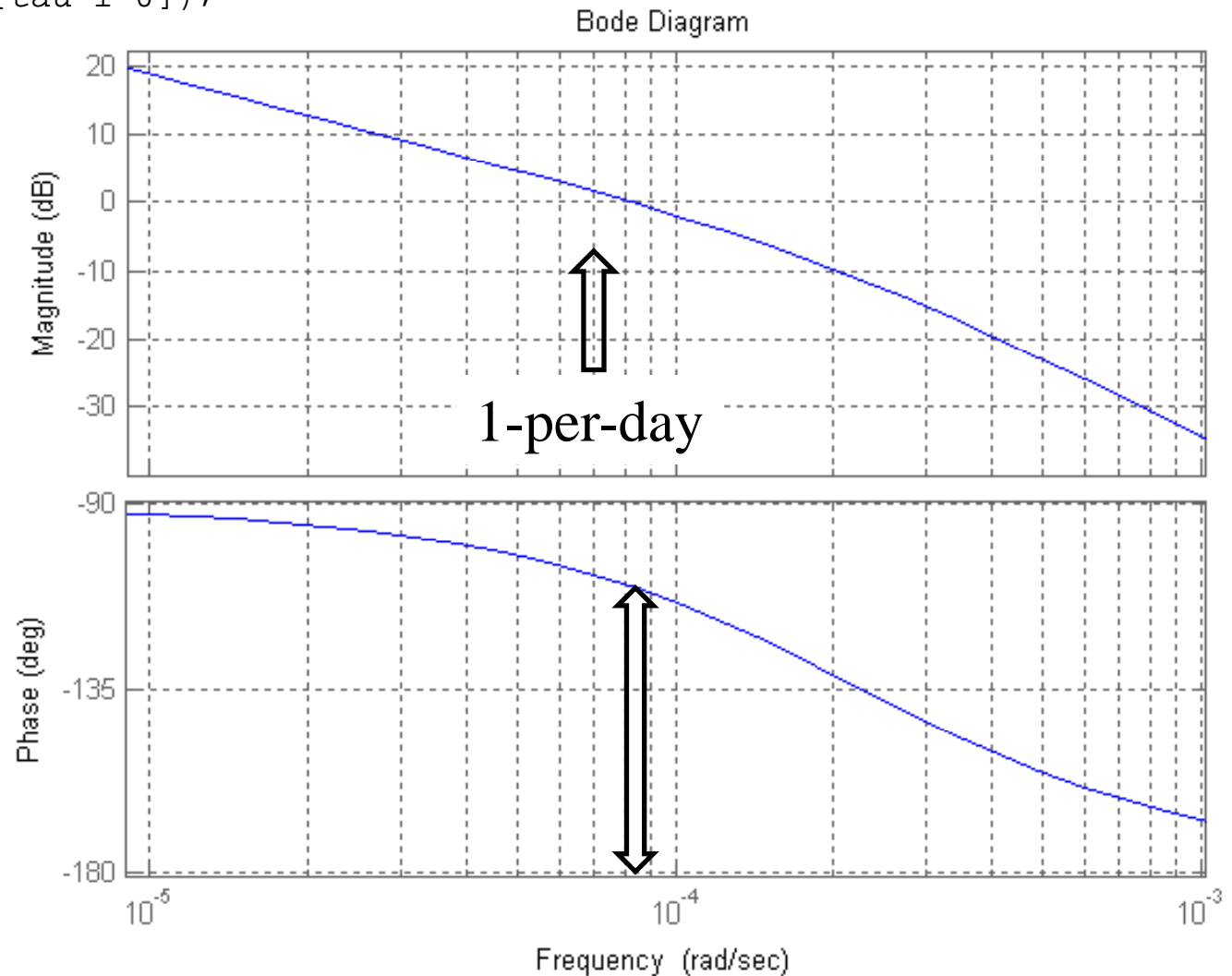
```
Gtest = tf(A,[tau 1 0]);  
rlocus(Gtest,[0:0.00001:0.001]);
```



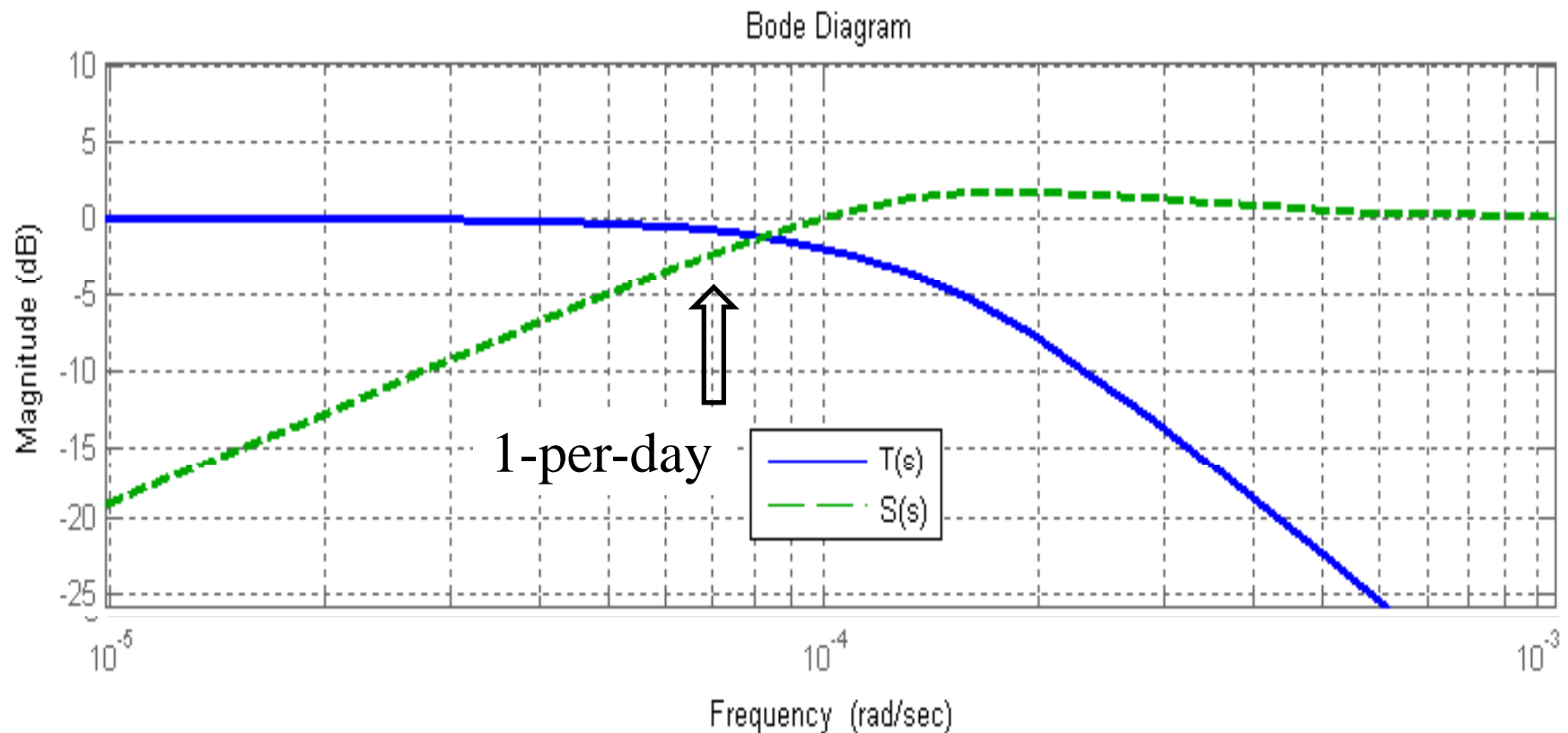
Bode Plot of Loop Gain = $G(s)$

```
Gtest = 0.000275*tf(A,[tau 1 0]);  
bode(Gtest);
```

- Crossover Near 1/day (Too Little Rejection of Daily Temperature Effects!)
- Stability Looks Very Good (Phase @ Crossover Far From -180)



Sensitivity Bodes for Integral Feedback Only



We Need to Add Proportional Feedback

Change to PI
Compensator

$$D(s) = \frac{K_I}{s} + K_P \quad G_P(s) = \frac{A}{\tau s + 1}$$

Look @ Closed-Loop
Pole Locations

$$\Delta_{CL}(s) = 1 + \frac{A(K_I + K_P s)}{s(\tau s + 1)} = 0$$

Multiply by $s(\tau s + 1) \rightarrow$ $s(\tau s + 1) + A(K_I + K_P s) = 0$



$$\tau s^2 + (AK_P + 1)s + AK_I = 0$$

Proportional + Integral Feedback Comments

$$\tau s^2 + (AK_P + 1)s + AK_I = 0$$

- Theoretically, Can Place Closed-Loop Poles Anywhere We Want
 - KI Controls Natural Frequency
 - KP Controls Damping
- Practically, We Have Some Serious Limits
 - Thermal Control System Has Limited Heating Capability (Can't Add Energy Quickly Enough to Increase Temperature Arbitrarily Fast)
 - Remember Our "Reduced Actuator Operation" Requirement!
 - We Ignored Effects of Delay (Remember—Always Destabilizing!)
- Actual Design Chosen for Good Rejection of 1-per-day Disturbances, Quick Response & Low Actuation Use
 - $K_P = 9.9$
 - $K_I = 0.0046$ (~17X Larger Than with KI Alone!)

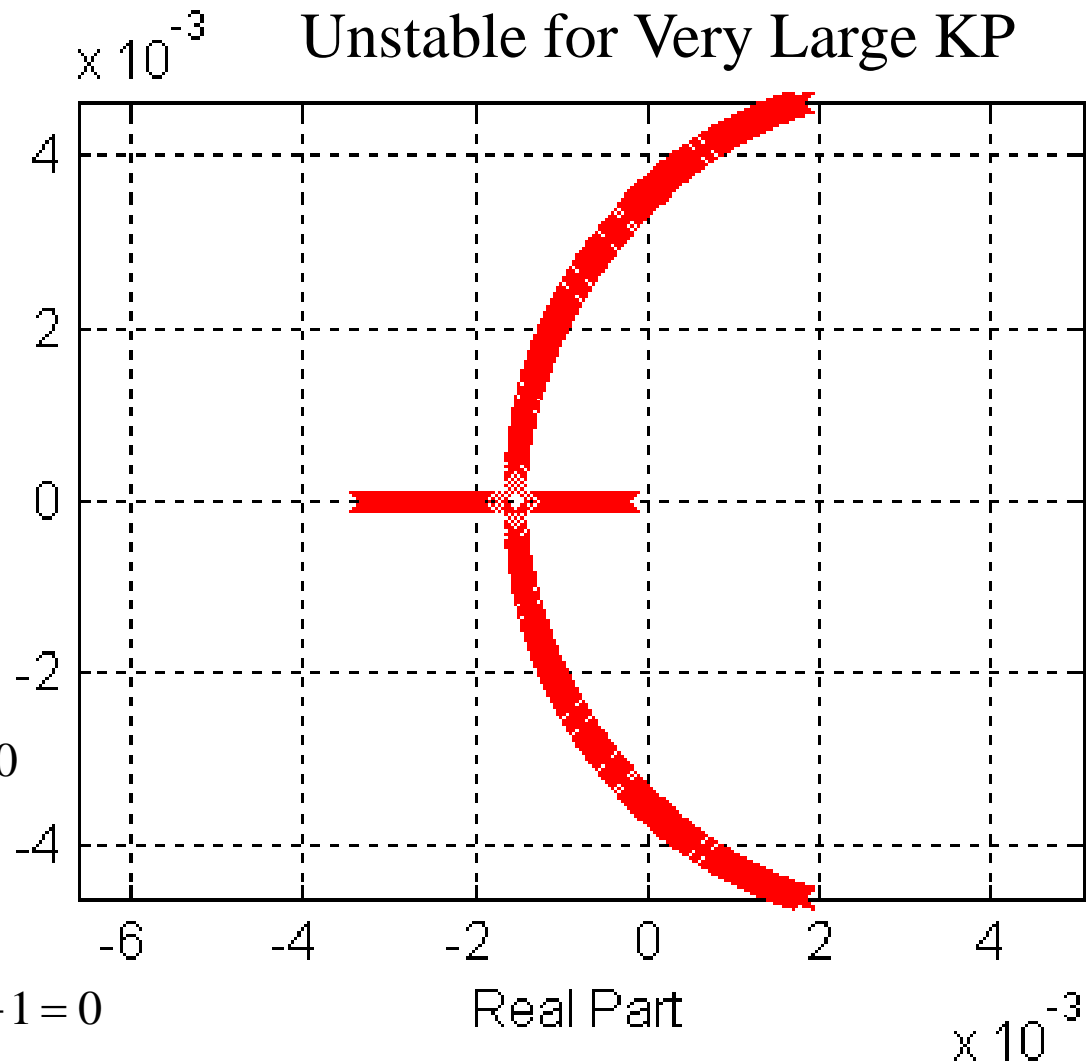
Effect of Proportional-Only Feedback with Delay

$$G_p(s) \approx \frac{A\left(-\frac{T_d}{2}s + 1\right)}{(\tau s + 1)\left(\frac{T_d}{2}s + 1\right)}$$

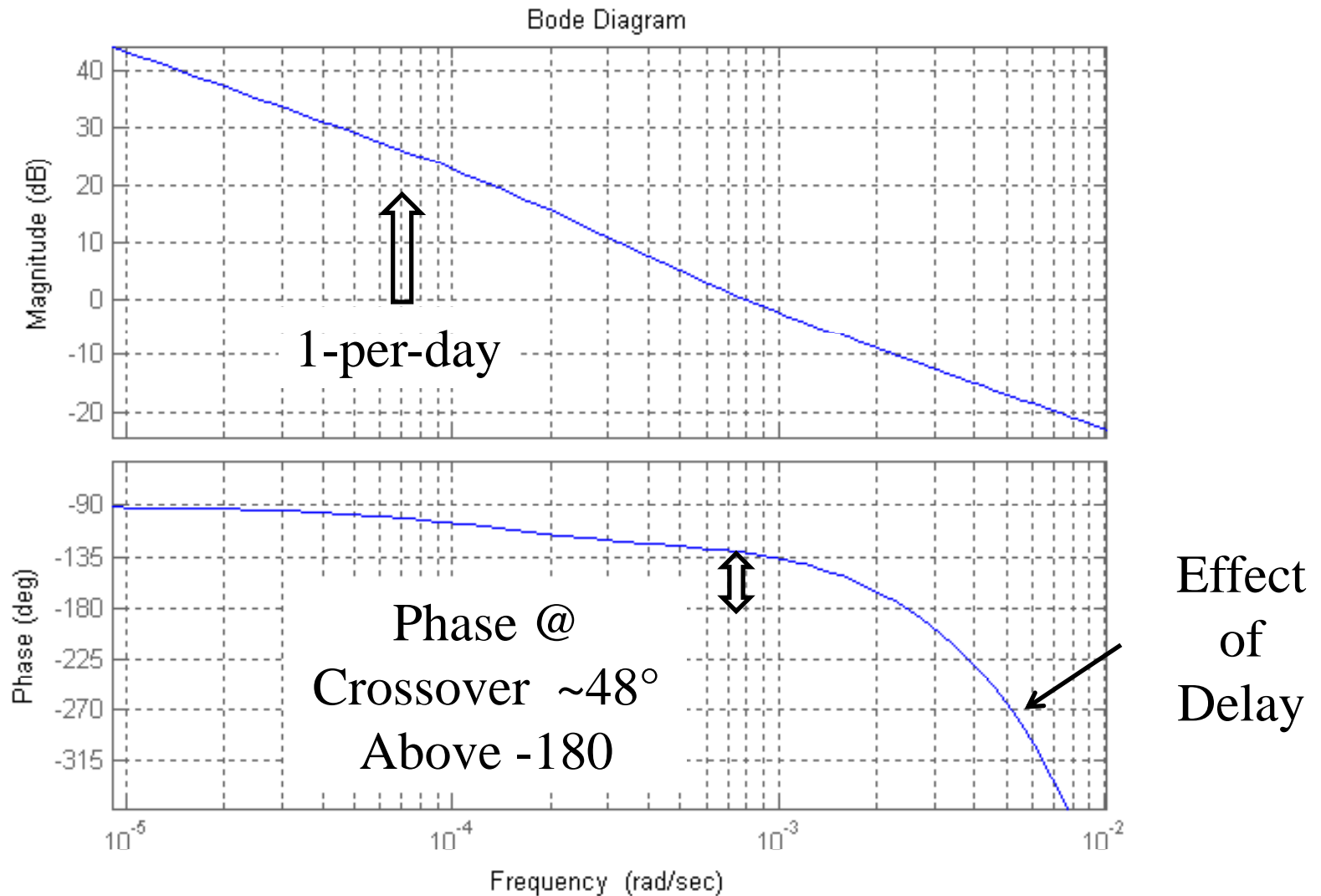
$$\Delta_{CL}(s) = 1 + \frac{AK_p\left(-\frac{T_d}{2}s + 1\right)}{(\tau s + 1)\left(\frac{T_d}{2}s + 1\right)} = 0$$

$$(\tau s + 1)\left(\frac{T_d}{2}s + 1\right) + AK_p\left(-\frac{T_d}{2}s + 1\right) = 0$$

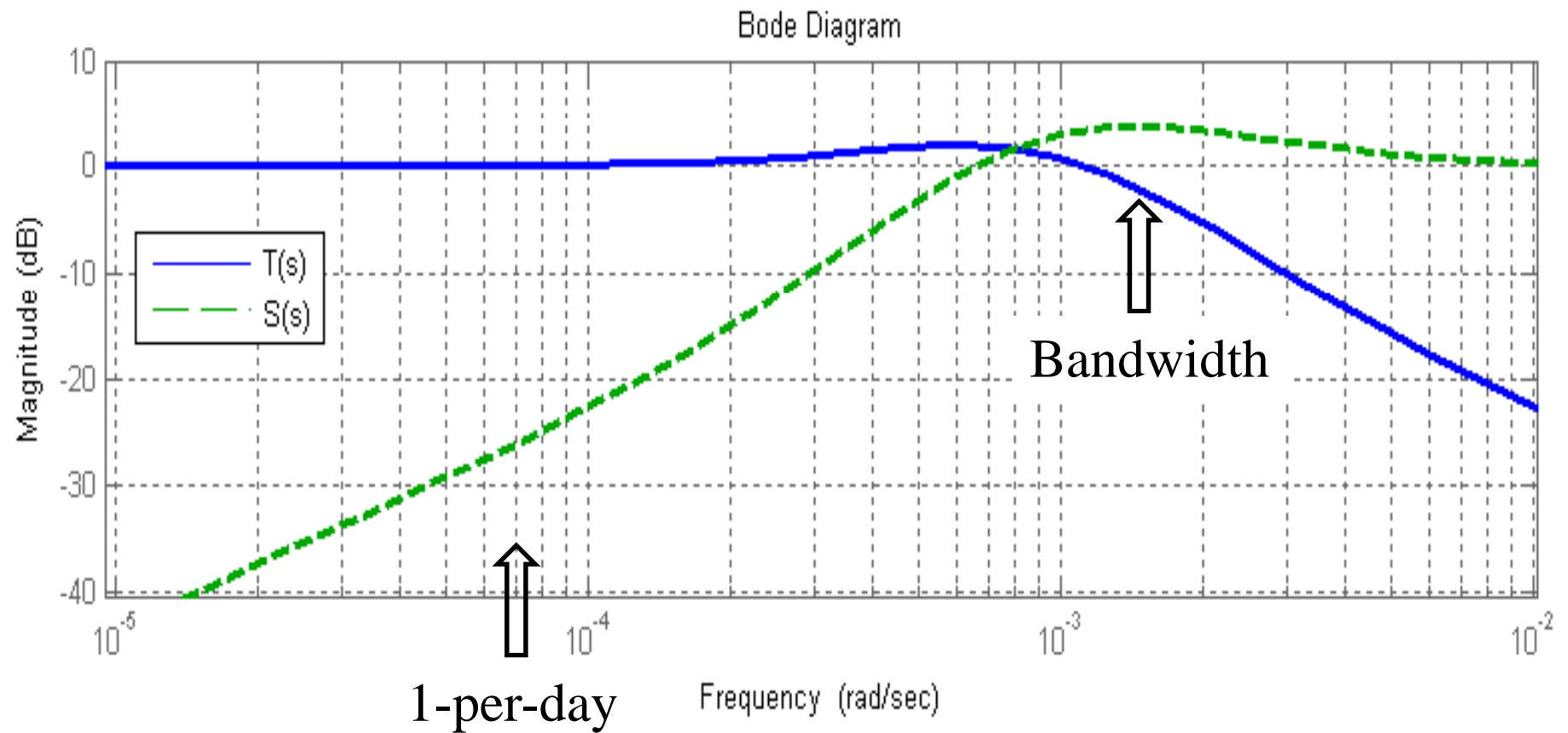
$$\frac{\tau T_d}{2}s^2 + \left(\tau + \frac{T_d}{2} - AK_p \frac{T_d}{2}\right)s + AK_p + 1 = 0$$



Bode Plot of Final Loop Transfer Function $G(s)$

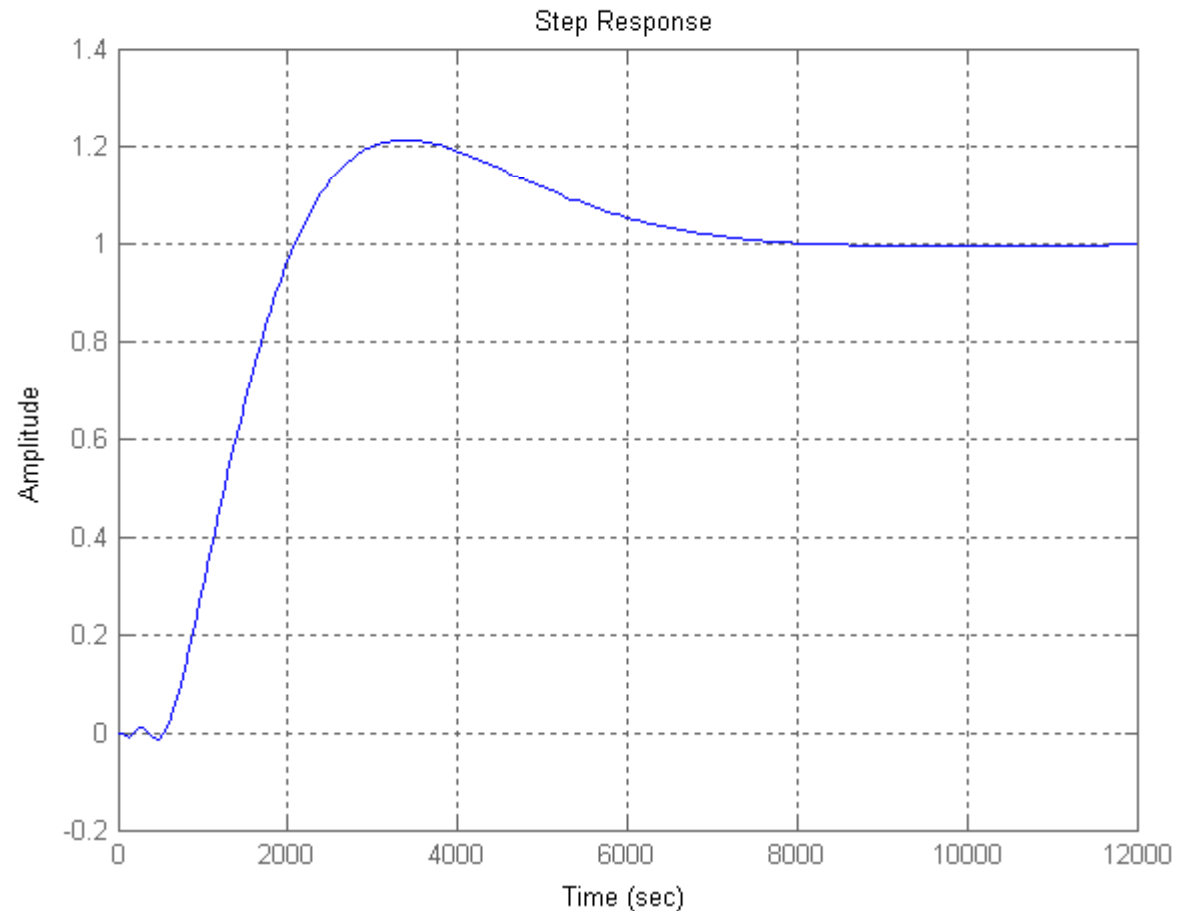


Sensitivity Bodes for Final Controller

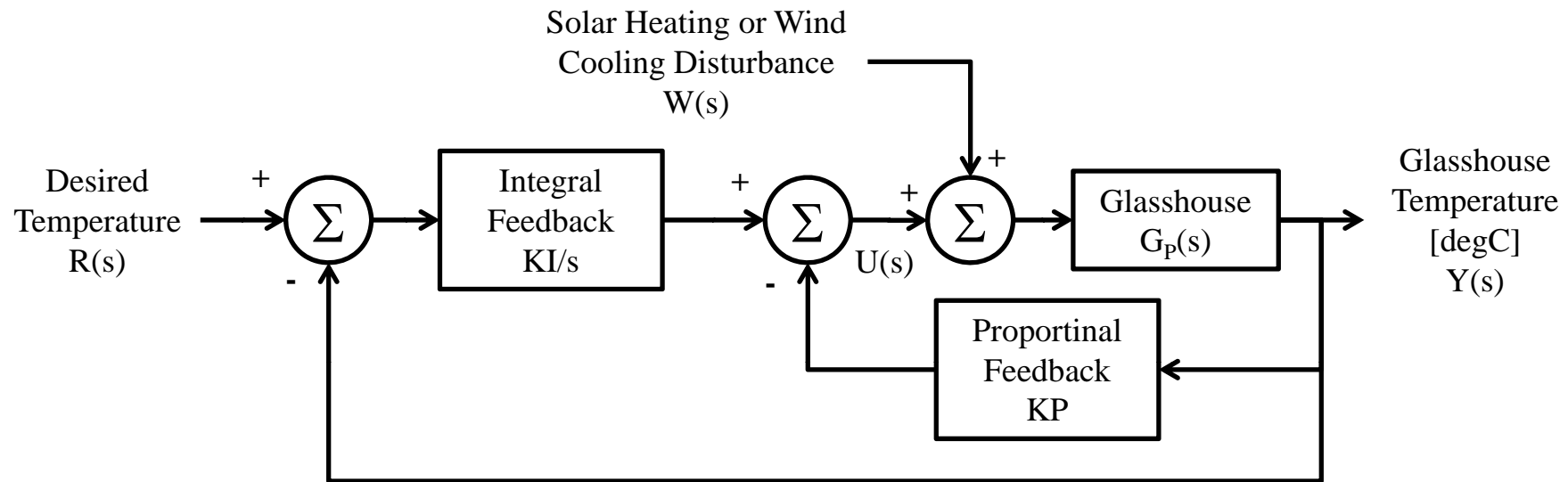


Step Response for Final Controller

- Oops! Zero in Closed-Loop Generates More Overshoot Than Desired, Despite Very High Damping Ratio!
- Fast Response Suggests Possible Over-Use of Actuator!

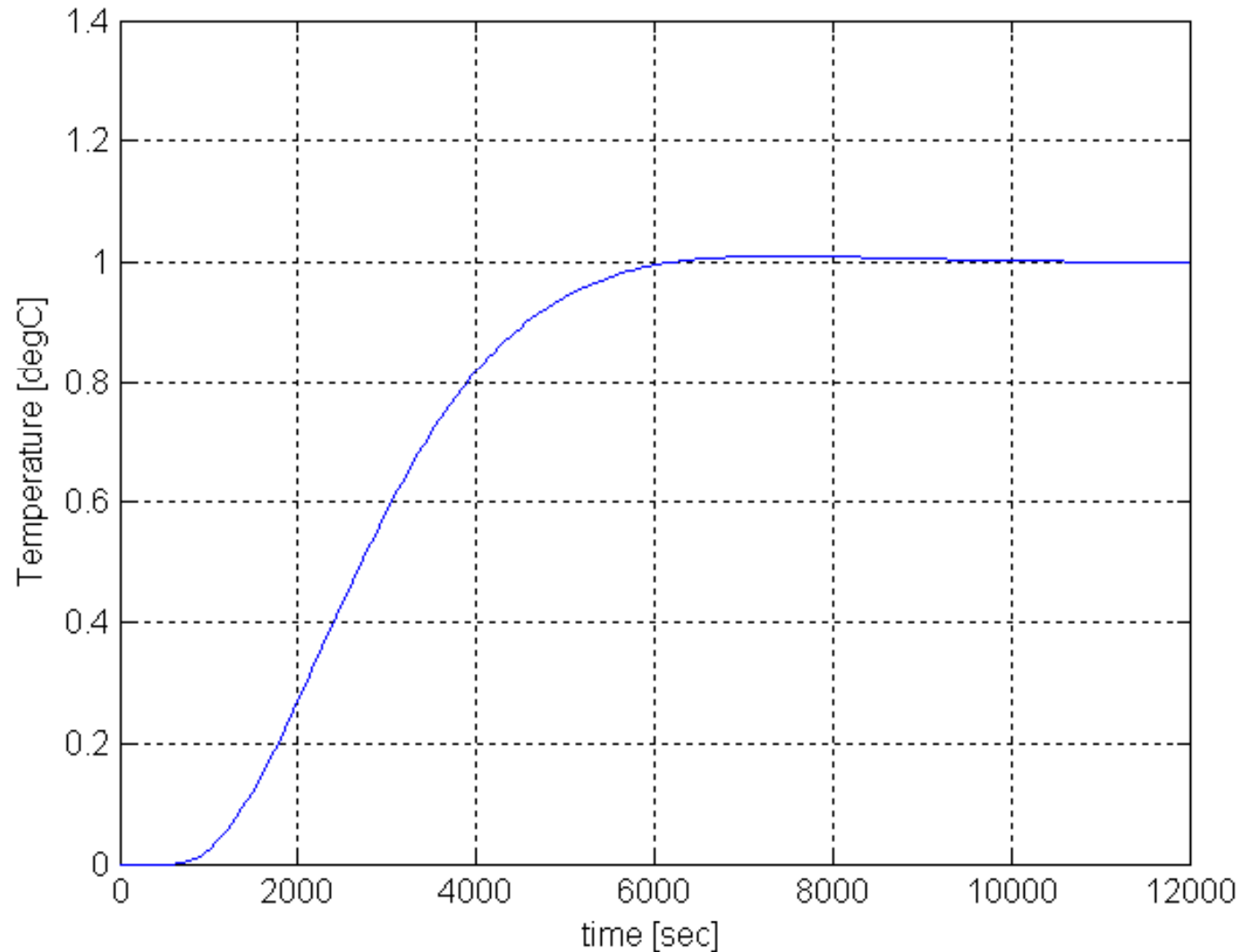


Simple Solution : Put KP on Feedback Only

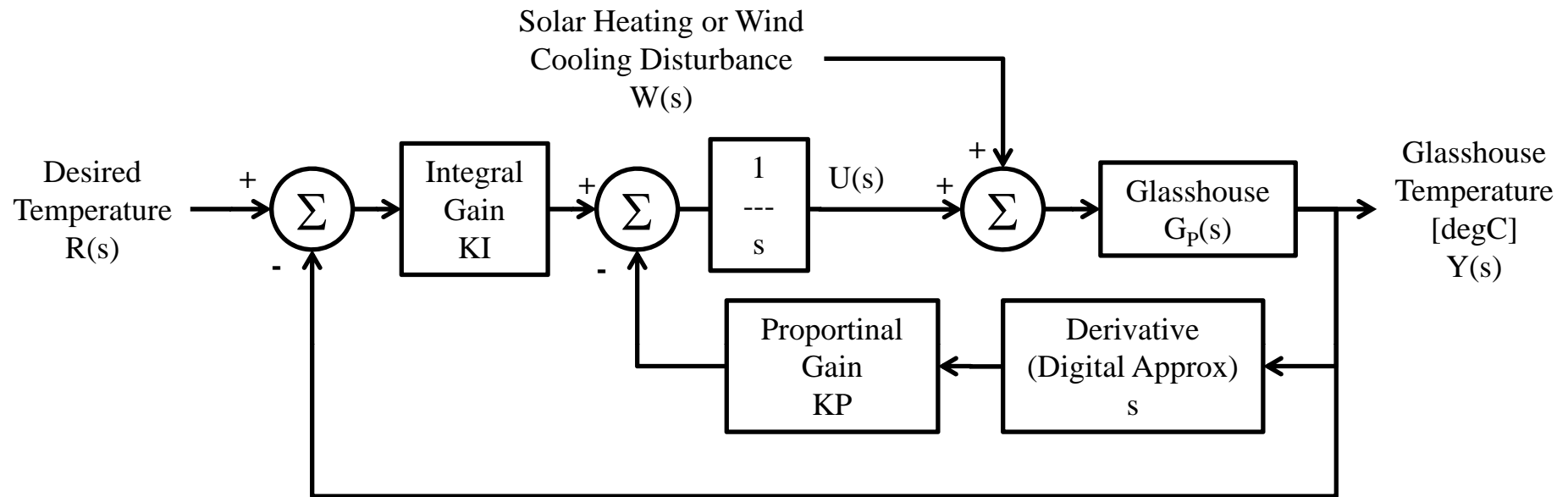


- Closed-Loop Denominator Unchanged
- Disturbance Rejection Unchanged
- Numerator of $Y(s)/R(s)$ Has No Zero with This Architecture
 - Lower Actuator Usage
 - Overshoot Eliminated (Slightly Longer Rise Time)

Step Response with Modified Final Design



More Details of Actual Implementation...



- Proportional Feedback Implemented as Integrated Derivative!
- Integrator Output Limited
 - Prevents “Integrator Windup” With Persistent Steady Errors When Heating System Unable to Keep Up with Extreme Conditions
 - MANY Other Anti-Windup & Other Limiting Schemes Exist

Actual Implementation Using Digital Computer

$$\frac{du}{dt} = K_I (y - r) + K_p \frac{dy}{dt}$$

$$\frac{u(t) - u(t - T_s)}{T_s} \approx K_I (y(t) - r(t)) + K_p \frac{y(t) - y(t - T_s)}{T_s}$$

$$u(t) = u(t - T_s) + T_s K_I (y(t) - r(t)) + K_p (y(t) - y(t - T_s))$$

New Control = Old Control + Linear Combination of New Measurement, Old Measurement, New Command

We Need to Learn How to Do This Carefully!