

Frequency Response



ESE 505 & MEAM 513

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Response to Sinusoidal Input

Step Response $Y(s) = G(s)U(s) = G(s) \frac{\omega}{s^2 + \omega^2}$

Partial Fraction Expansion $Y(s) = \frac{C_0}{s - j\omega} + \frac{\bar{C}_0}{s + j\omega} + \underbrace{\frac{C_1}{(s - p_1)} + \dots + \frac{C_n}{(s - p_n)}}_{\text{Transient Response}}$

$$C_0 = A + jB$$

$$Y(s) = \frac{A + jB}{s - j\omega} + \frac{A - jB}{s + j\omega} + \dots$$

Transient
Response
($\rightarrow 0$ in Steady
State for Stable
System)

$$Y(s) = \frac{2As - 2B\omega}{s^2 + \omega^2} + \dots$$

$$y(t) = \left[2A \cos(\omega t) - 2B \sin(\omega t) \right] + \underbrace{C_1 e^{p_1 t} + \dots + C_n e^{p_n t}}_{\text{Transient Response}}$$

Response to Sinusoidal Input (Continued)

“Cover Up” Rule $C_0 = \lim_{s \rightarrow j\omega} [(s - j\omega) Y(s)] = G(j\omega) \frac{\omega}{2j\omega}$

$$G(j\omega) = Me^{j\phi} \implies C_0 = \frac{Me^{j\phi}}{2j} = \frac{M}{2} [-j \cos \phi + \sin \phi]$$

$$A = \frac{M}{2} \sin \phi \quad B = -\frac{M}{2} \cos \phi$$

$$y(t) = M [\cos(\omega t) \sin \phi + \sin(\omega t) \cos \phi] = M \sin(\omega t + \phi)$$

Response to Unit Sinusoidal Input of Frequency ω is Sinusoidal Output of Frequency ω with Magnitude M and Phase Shift ϕ , where $G(j\omega) = Me^{j\phi}$

Long Journey to Get Here...Still More to Go!

- Develop ODE Model of Dynamic System
- Linearize ODE Model
 - Trim
 - Small Perturbations From Trim
- $G(s)$ = Transfer Function (Zero Initial Perturbation)
- Evaluate $G(j\omega)$ to Find Magnitude & Phase of Response to Sinusoidal Input

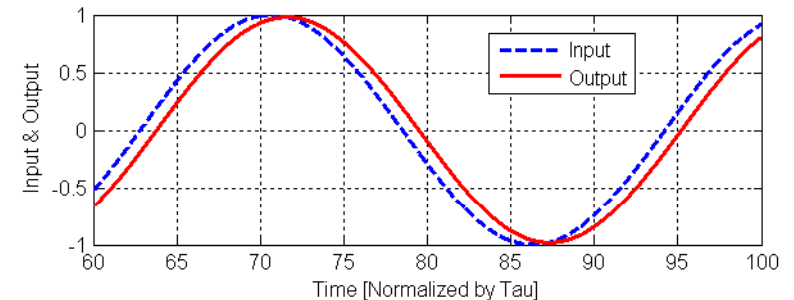
First-Order Example : Low-Pass Filter

$$G(s) = \frac{1}{\tau s + 1} = \frac{\sigma}{s + \sigma}$$

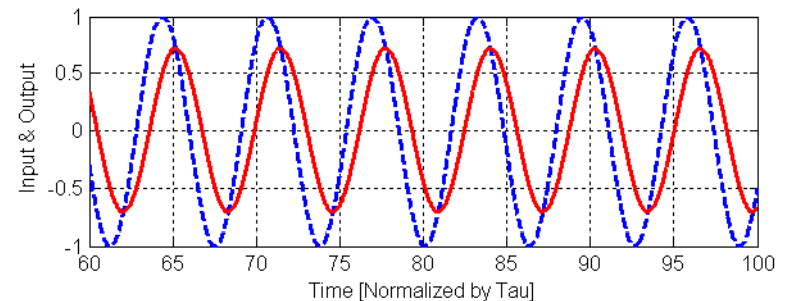
$$G(j\omega) = \frac{\sigma}{j\omega + \sigma}$$

$$M = \frac{\sigma}{\sqrt{\sigma^2 + \omega^2}} = \frac{1}{\sqrt{1 + (\tau\omega)^2}}$$

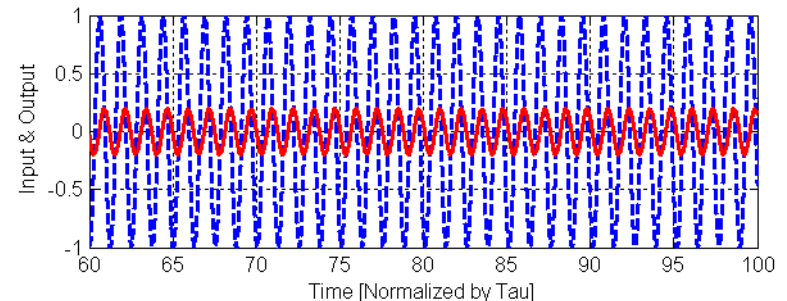
$$\phi = -\tan^{-1}\left(\frac{\omega}{\sigma}\right) = -\tan^{-1}(\tau\omega)$$



$$\tau\omega = 0.2 \quad M = 0.98 \quad \phi = -11.3^\circ$$



$$\tau\omega = 1.0 \quad M = 0.707 \quad \phi = -45^\circ$$



$$\tau\omega = 5.0 \quad M = 0.20 \quad \phi = -79^\circ$$

First-Order Example : High-Pass Filter

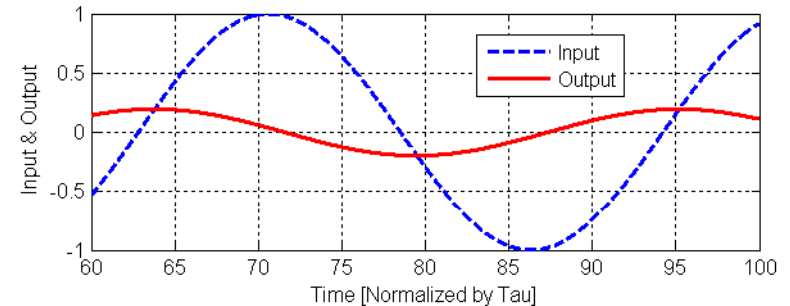
$$G(s) = \frac{\tau s}{\tau s + 1} = \frac{s}{s + \sigma}$$

$$G(j\omega) = \frac{j\omega}{j\omega + \sigma}$$

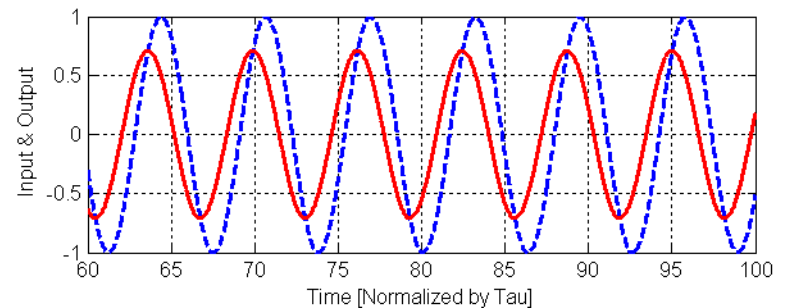
$$M = \frac{\omega}{\sqrt{\sigma^2 + \omega^2}} = \frac{\tau\omega}{\sqrt{1 + (\tau\omega)^2}}$$

$$\phi = 90^\circ - \tan^{-1}(\tau\omega)$$

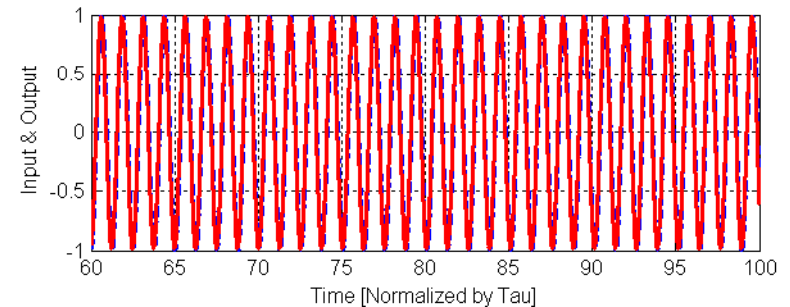
Output Leads Input!



$$\tau\omega = 0.2 \quad M = 0.20 \quad \phi = 79^\circ$$

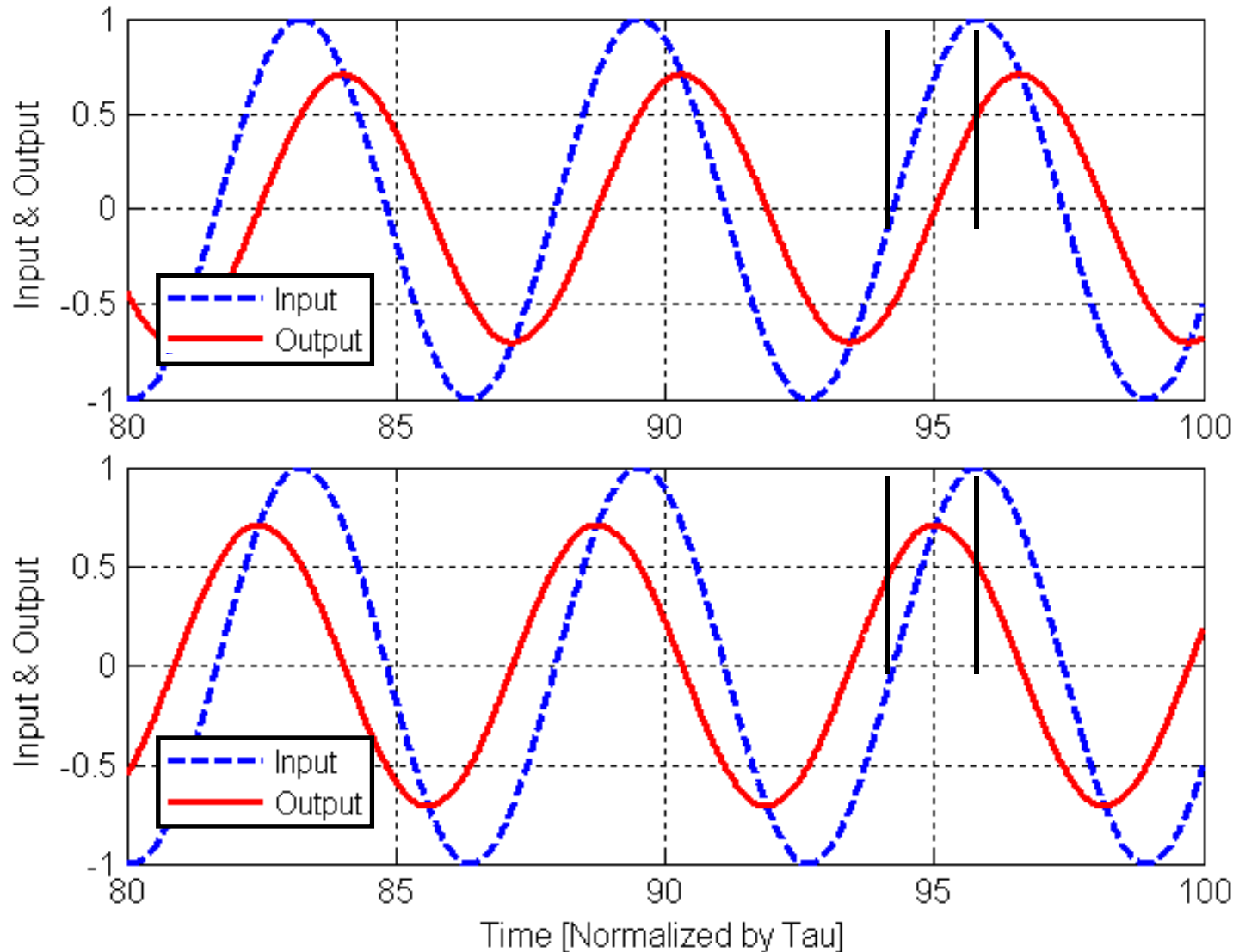


$$\tau\omega = 1.0 \quad M = 0.707 \quad \phi = 45^\circ$$



$$\tau\omega = 5.0 \quad M = 0.98 \quad \phi = 11.3^\circ$$

Low-Pass vs. High-Pass @ $\omega = 1/\tau$



Low-Pass
 $M=0.707$
 $\phi = -45^\circ$

High-Pass
 $M=0.707$
 $\phi = +45^\circ$

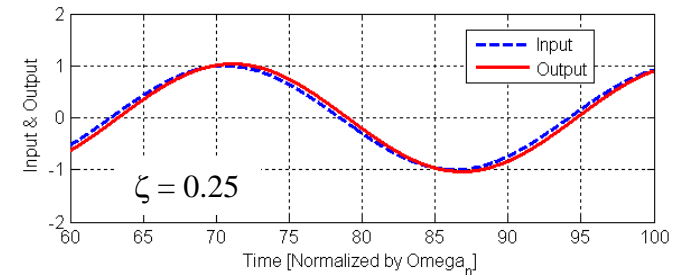
Second-Order Example

$$G(s) = \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2}$$

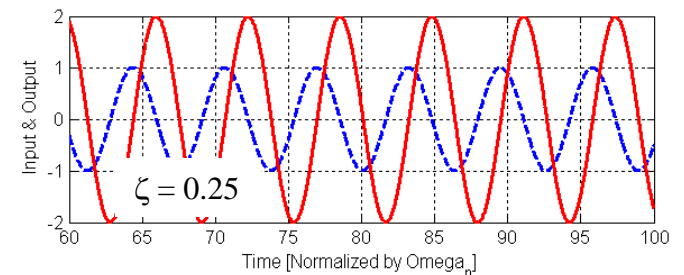
$$G(j\omega) = \frac{\omega_n^2}{\omega_n^2 - \omega^2 + j2\zeta\omega_n\omega}$$

$$M = \left[\left(1 - \left(\frac{\omega}{\omega_n} \right)^2 \right)^2 + \left(\frac{2\zeta\omega}{\omega_n} \right)^2 \right]^{-1/2}$$

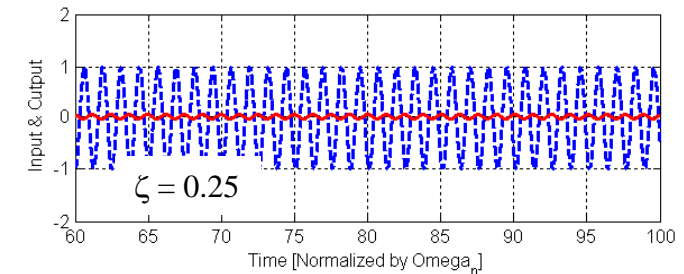
$$\phi = -\tan^{-1} \left(\frac{2\zeta \frac{\omega}{\omega_n}}{1 - \left(\frac{\omega}{\omega_n} \right)^2} \right)$$



$$\omega / \omega_n = 0.2 \quad M = 1.0 \quad \phi = -5.9^\circ$$



$$\omega / \omega_n = 1.0 \quad M = 2.0 \quad \phi = -90^\circ$$



$$\omega / \omega_n = 5.0 \quad M = 0.04 \quad \phi = -174^\circ$$

Second-Order System “At Resonance”

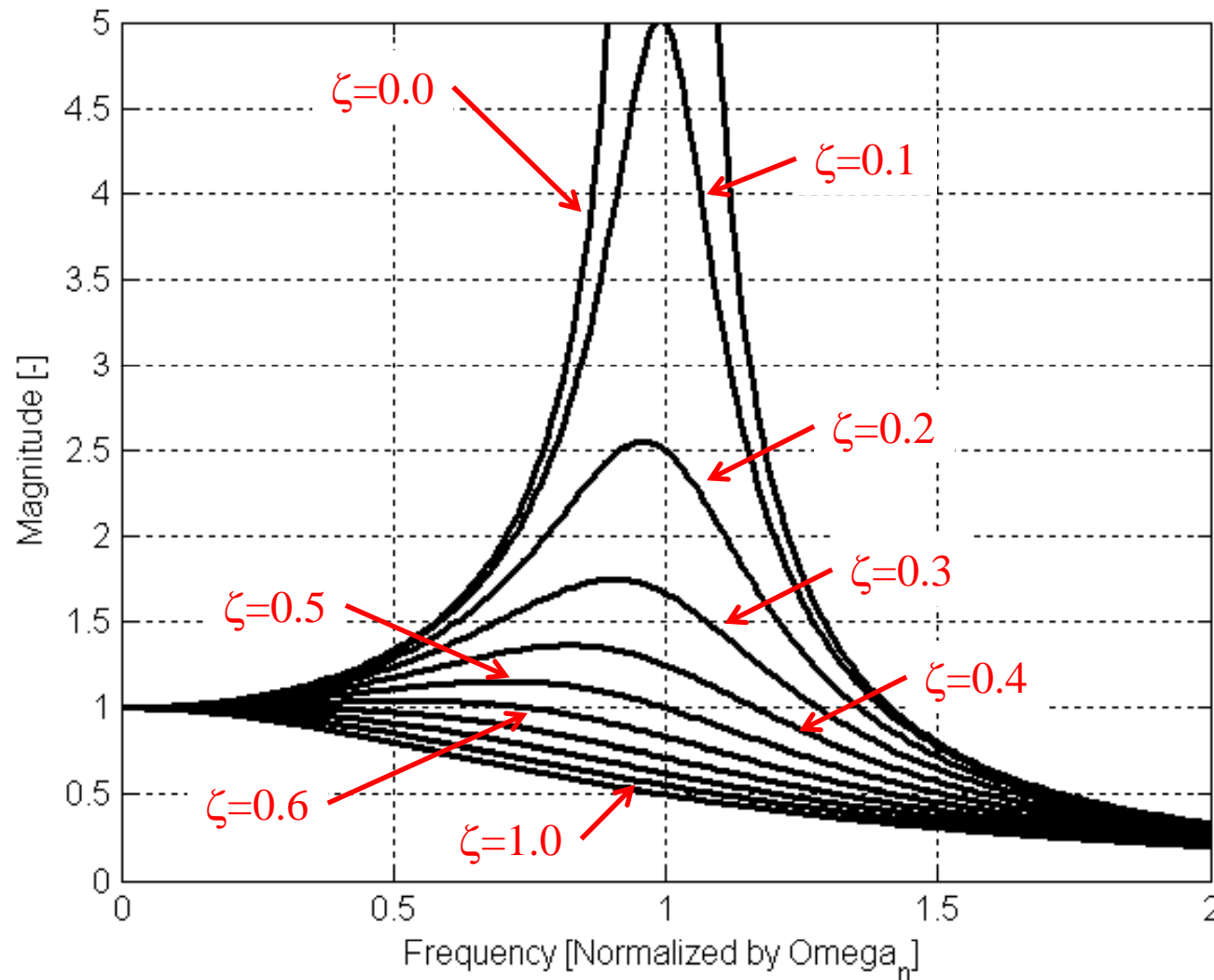
$$G(j\omega_n) = \frac{\omega_n^2}{\omega_n^2 - \omega_n^2 + j2\zeta\omega_n^2} = \frac{1}{j2\zeta}$$

$$M = \frac{1}{2\zeta} \quad \phi = -90^\circ$$

Second-Order System Forced at Natural Frequency → “Mass” & “Spring” Cancel → Only “Damper” Balances Applied Force!

Second-Order System Forced at Natural Frequency → ALWAYS 90 Degrees Phase Lag!

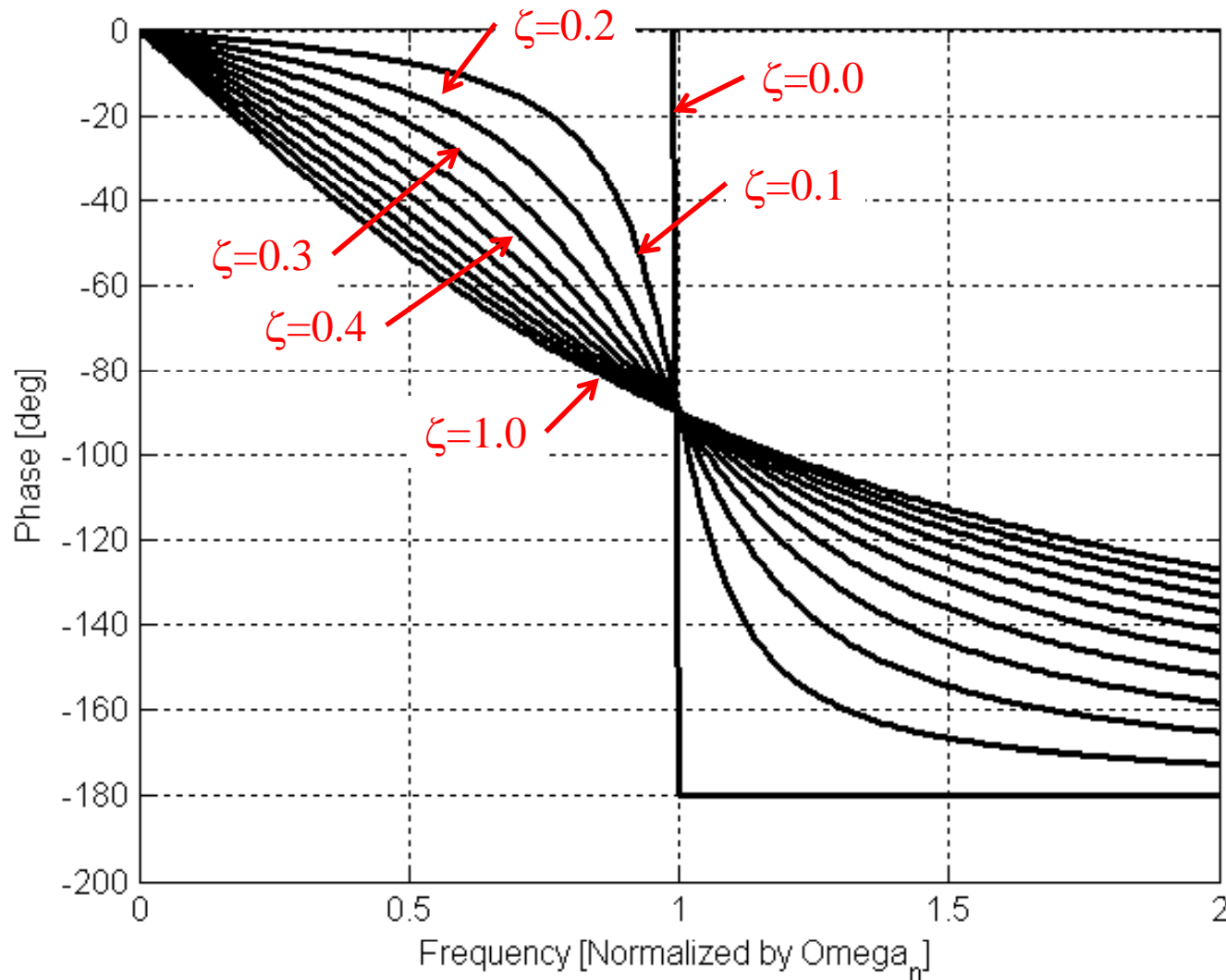
2nd-Order Frequency Response Magnitude



This is How Most
Books on
Vibration Plot
Second-Order
System Response

We'll Do It
Differently
Soon...

2nd-Order Frequency Response Phase



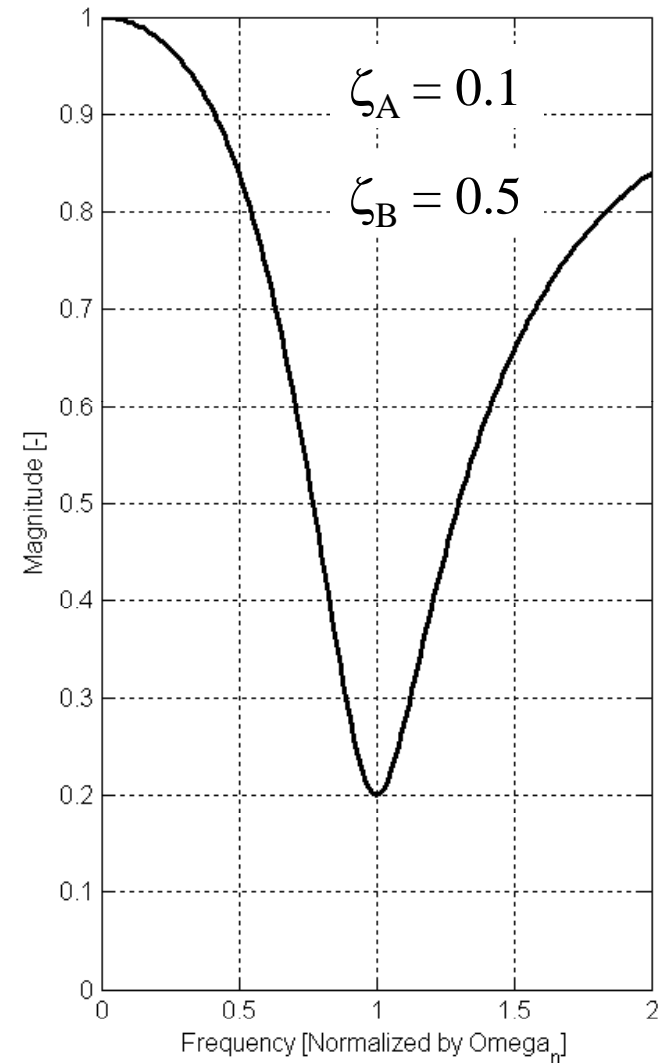
We'll Do This
Differently
Soon, Too...

Second-Order Notch Filter

$$G(s) = \frac{s^2 + 2\zeta_A \omega_n s + \omega_n^2}{s^2 + 2\zeta_B \omega_n s + \omega_n^2}$$

$$G(j\omega) = \frac{\omega_n^2 - \omega^2 + j2\zeta_A \omega_n \omega}{\omega_n^2 - \omega^2 + j2\zeta_B \omega_n \omega}$$

$$M = \sqrt{\frac{\left(1 - \left(\frac{\omega}{\omega_n}\right)^2\right)^2 + \left(\frac{2\zeta_B \omega}{\omega_n}\right)^2}{\left(1 - \left(\frac{\omega}{\omega_n}\right)^2\right)^2 + \left(\frac{2\zeta_A \omega}{\omega_n}\right)^2}}$$



Higher-Order Systems...

$$G(s) = G(0)G_1(s)G_2(s)\cdots$$

$$G_k(s) = \frac{\tau_{A_k}s + 1}{\tau_{B_k}s + 1} \quad \dots \text{OR} \dots \quad G_k(s) = \frac{\left(\frac{s}{\omega_{A_k}}\right)^2 + 2\zeta_{A_k}\left(\frac{s}{\omega_{A_k}}\right)s + 1}{\left(\frac{s}{\omega_{B_k}}\right)^2 + 2\zeta_{B_k}\left(\frac{s}{\omega_{B_k}}\right)s + 1}$$

$$G(j\omega) = G(0)G_1(j\omega)G_2(j\omega)\cdots$$

$$M = G(0)M_1M_2\cdots$$

$$\phi = \phi_1 + \phi_2 + \cdots$$

We'll Make This Easy
Next Lecture...