

## Step 2a, revision 4 - Filter the tones, Detect the phase in a narrow tracking band

Input data file name

DataFileName := "Data3.NoSpin.NoPhNoise.byte"

A priori Doppler Polynomial model file name

DpcFileName0 := "Data3.Det.Pass0.tone0.fitcoeffs.txt"

All zeroes so far

Pass1 Doppler Polynomial model file name

DpcFileName1 := "Data3.Det.Pass1.tone0.fitcoeffs.txt"

### Data set and processing essential parameters

Band Width

$BW := 250 \cdot \text{kHz}$

Filter ratio

$FR := 100$

Output bandwidth

$BW_o := BW \cdot FR^{-1}$   $BW_o = 2500 \text{ s}^{-1}$

Scan length (in samples)

$N_t := 8 \cdot 1000 \cdot 1000$

Number of samples in the output signal

$N_{to} := \text{floor}(N_t \cdot FR^{-1})$   $N_{to} = 80000$

N of points to input FFT segment

$N_{psi} := 10 \cdot 1000$

Number of points in output segment

$N_{pso} := N_{psi} \cdot FR^{-1}$   $N_{pso} = 100$

Overlapping of FFT segments

$Ovlp := 2$

Note the decimal number for FFT length !

And input length is abbreviated to make  
a nice decimal number of output samples

Number of spectral points to extract to output FFT

$N_{pfo} := N_{pso} \cdot 0.5 + 1$

$N_{pfo} = 51$

Zero padding of output FFT

$N_{pfz} := N_{pso} \cdot 0.5 - 1$

$jp_{fz} := 0 .. N_{pfz} - 1$

$N_{pfz} = 49$

padding array for neg. frequencies

$dpadd_{jp_{fz}} := 0 + i \cdot 0$

Derived parameters (some of them are just for illustration)

Sampling rate

$Sr := 2 \cdot BW$

And sampling interval

$dt := Sr^{-1}$

Dimensionless

$dtn := dt \cdot s^{-1}$

Total time span

$Tspan := N_t \cdot dt$

$Tspan = 16 \text{ s}$

Input Time grid

$jt := 0 .. N_t - 1$

$tt_{jt} := jt \cdot dt$

Output sampling interval

$dto := dt \cdot FR$

$dto = 0.0002 \text{ s}$

Output Time grid

$jto := 0 .. N_{to} - 1$

$tto_{jto} := jto \cdot dto$

Binning within FFT input and output segments

$jpsi := 0 .. N_{psi} - 1$

$jpso := 0 .. N_{pso} - 1$

Input Window function in time domain

$Wini_{jpsi} := \cos\left[\frac{\pi}{N_{psi}} \cdot (jpsi - 0.5 \cdot N_{psi} + 0.5)\right]$

Output Window function in time domain

$Wino_{jpso} := \cos\left[\frac{\pi}{N_{pso}} \cdot (jpso - 0.5 \cdot N_{pso} + 0.5)\right]$

## Derived parameters , Continue

Number of FFT segments to process ( accounting for overlap)

$$N_{\text{segm}} := \text{floor}\left(\frac{N_t}{N_{\text{psi}}}\right) \cdot \text{Ovlp} - (\text{Ovlp} - 1) \quad N_{\text{segm}} = 1599$$

shift (in samples) between overlapping segments

$$\text{Oshifti} := \frac{N_{\text{psi}}}{\text{Ovlp}} \quad \text{Oshifto} := \frac{N_{\text{pso}}}{\text{Ovlp}}$$

Frequency resolution of the input FFT

$$\text{dfi} := (N_{\text{psi}} \cdot \text{dt})^{-1} \quad \text{dfi} = 50 \text{ s}^{-1}$$

Filter set-up time

$$T_{\text{setup}} := 0.5 \cdot N_{\text{psi}} \cdot \text{dt} \quad T_{\text{setup}} = 0.01 \text{ s}$$

Number of points at the start and the end of the output array to disregard due to filter set-up time:

$$N_{\text{pout\_setup}} := T_{\text{setup}} \cdot \text{dto}^{-1} \quad N_{\text{pout\_setup}} = 50$$

Read Doppler Frequency polynomials

```
Fcd0 := READPRN(DpcFileName0)
Fcd1 := READPRN(DpcFileName1)
```

```
Npf := Fcd0_0      Npf = 3      jpf := 0 .. Npf
Cf0_jpf := Fcd0_jpf+2
Cf1_jpf := Fcd1_jpf+2      Tspanp := Fcd1_1      Tspanp = 16.777216      Tspanps := Tspanp · s
```

Step 0 frequency polys (a-priory) are all zeroes here

Combine all data sets

```
Cf := Cf0 + Cf1      Cf_0 := Cf1_0
```

Select the Doppler constant offset from the last pass data, well, it will not be used anyway, just keep a track on it

Make Phase polynomials

```
Cpp_0 := 0      Cpp_jpf+1 := 2π · Cf_jpf / (jpf + 1)      Npp := Npf + 1
```

Frequency polynomial

$$Cf = \begin{pmatrix} 70048.91028919304 \\ 7052.868226490915 \\ -7888.813451185823 \\ 1.104737497866154 \end{pmatrix}$$

Phase polynomial

$$Cpp = \begin{pmatrix} 0 \\ 440130.2839129986 \\ 22157.23900708073 \\ -16522.292255857148 \\ 1.735317603720739 \end{pmatrix}$$

Defining the start/end bin of the filter, which will put tone lines in the center of the output band

We want to put the tone in the center of the output band:  $BW_{oh} := BW_o \cdot 0.5$  with an accuracy of the input FFT resolution  $dfi = 50 \text{ s}^{-1}$

We know, that several tones have certain offsets from the carrier line

			Start and End bins to extract		Frequency of the start bin	
carrier	$F_{cc} := Cf_0 \cdot \text{Hz}$	$B_{sc} := \text{floor}\left[\left(F_{cc} - BW_{oh}\right) \cdot dfi^{-1}\right]$	$B_{sc} = 1375$	$B_{ec} := B_{sc} + N_{pfo} - 1$	$F_{startc} := B_{sc} \cdot dfi$	$F_{startc} = 68750 \text{ s}^{-1}$
tones	$F_{c1} := F_{cc} - 10000 \cdot \text{Hz}$	$B_{s1} := \text{floor}\left[\left(F_{c1} - BW_{oh}\right) \cdot dfi^{-1}\right]$	$B_{s1} = 1175$	$B_{e1} := B_{s1} + N_{pfo} - 1$	$F_{start1} := B_{s1} \cdot dfi$	$F_{start1} = 58750 \text{ s}^{-1}$
	$F_{c2} := F_{cc} - 50000 \cdot \text{Hz}$	$B_{s2} := \text{floor}\left[\left(F_{c2} - BW_{oh}\right) \cdot dfi^{-1}\right]$	$B_{s2} = 375$	$B_{e2} := B_{s2} + N_{pfo} - 1$	$F_{start2} := B_{s2} \cdot dfi$	$F_{start2} = 18750 \text{ s}^{-1}$
	$F_{c3} := F_{cc} + 20000 \cdot \text{Hz}$	$B_{s3} := \text{floor}\left[\left(F_{c3} - BW_{oh}\right) \cdot dfi^{-1}\right]$	$B_{s3} = 1775$	$B_{e3} := B_{s3} + N_{pfo} - 1$	$F_{start3} := B_{s3} \cdot dfi$	$F_{start3} = 88750 \text{ s}^{-1}$

Integrate the phase

$$\text{Phdopp}_{jt} := T_{\text{spanp}} \cdot \left[ \sum_{jjp=2}^{N_{pf}} \left[ C_{pp,jjp} \cdot \left( \frac{tt_{jt}}{T_{\text{spanps}}} \right)^{jjp} \right] \right]$$

Make a segment time shift phase correction coefficient, actually a start bin of the filter can be selected in such way, that this coeff will be +1, although it can be even complex

$F_{\text{startc}} \cdot O_{\text{shifti}} \cdot dt = 687.5$	$P_{\text{ssc}} := F_{\text{startc}} \cdot O_{\text{shifti}} \cdot dt - \text{floor}(F_{\text{startc}} \cdot O_{\text{shifti}} \cdot dt)$	$E_{\text{sc}} := \exp(i \cdot 2 \cdot \pi \cdot P_{\text{ssc}})$	$E_{\text{sc}} = -1$
$F_{\text{start1}} \cdot O_{\text{shifti}} \cdot dt = 587.5$	$P_{\text{ss1}} := F_{\text{start1}} \cdot O_{\text{shifti}} \cdot dt - \text{floor}(F_{\text{start1}} \cdot O_{\text{shifti}} \cdot dt)$	$E_{\text{s1}} := \exp(i \cdot 2 \cdot \pi \cdot P_{\text{ss1}})$	$E_{\text{s1}} = -1$
$F_{\text{start2}} \cdot O_{\text{shifti}} \cdot dt = 187.5$	$P_{\text{ss2}} := F_{\text{start2}} \cdot O_{\text{shifti}} \cdot dt - \text{floor}(F_{\text{start2}} \cdot O_{\text{shifti}} \cdot dt)$	$E_{\text{s2}} := \exp(i \cdot 2 \cdot \pi \cdot P_{\text{ss2}})$	$E_{\text{s2}} = -1$
$F_{\text{start3}} \cdot O_{\text{shifti}} \cdot dt = 887.5$	$P_{\text{ss3}} := F_{\text{start3}} \cdot O_{\text{shifti}} \cdot dt - \text{floor}(F_{\text{start3}} \cdot O_{\text{shifti}} \cdot dt)$	$E_{\text{s3}} := \exp(i \cdot 2 \cdot \pi \cdot P_{\text{ss3}})$	$E_{\text{s3}} = -1$

```

MakeFiltX(Phcorr, Fbinstart, Fbinend, Es) :=
  for jjo ∈ 0 .. Nto - 1
    foutjjo ← 0
    for jsegm ∈ 0 .. Nsegm - 1
      skip ← jsegm · Oshifti
      din ← READBIN(DataFileName, "byte", 0, 1, skip, Npsi)
      din ← din - 127
      din ← (din · Wini)
      phc ← submatrix(Phcorr, skip, skip + Npsi - 1, 0, 0)
      ephc ← exp(i · phc)
      din ← (din · ephc)
      sp ← cfft(din)
      spo ← submatrix(sp, Fbinstart, Fbinend, 0, 0)
      spo0 ← 1 · Re(spo0)
      spoNpfo-1 ← 1 · Re(spoNpfo-1)
      spop ← stack(spo, dpadd)
      dout ← icfft(spop)
      dout ← (dout · Wino)
      for jjso ∈ 0 .. Npso - 1
        foutjjso+jsegm·Oshifto ← foutjjso+jsegm·Oshifto + doutjjso · Esjsegm
    return fout

```

Major function to do Phase Tracking,  
Down-conversion, Filtering and Hilbert transform

Phase integration should be done differently in C

Multiple tones can be extracted in parallel,  
using only 1 "big" input Fourier transform  
and several "small" output FFTs.

Mathematically this filter is equivalent to PUB,  
but better, because it allows arbitrary positioning  
of output channels, (within the input FFT granularity),  
and even imply different bandwidth for output channels.

And it's faster !

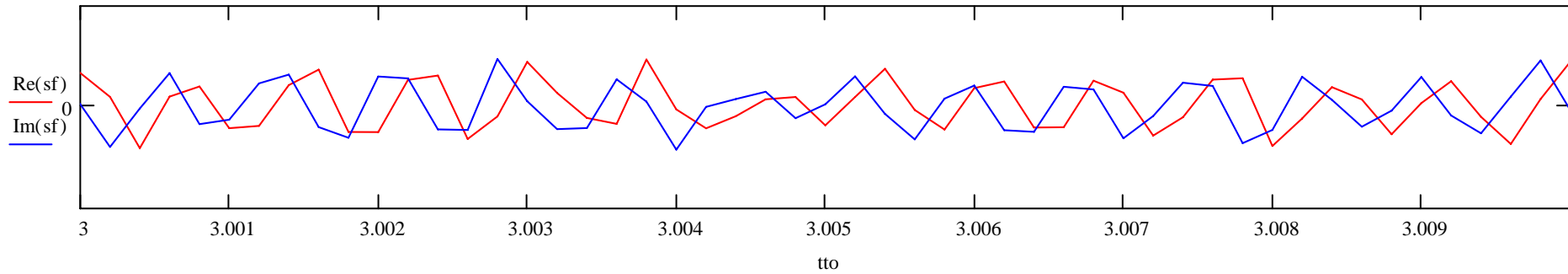
Although more demanding for higher precision..

This is a tricky part to make in C

Make a filtered signal for major tone

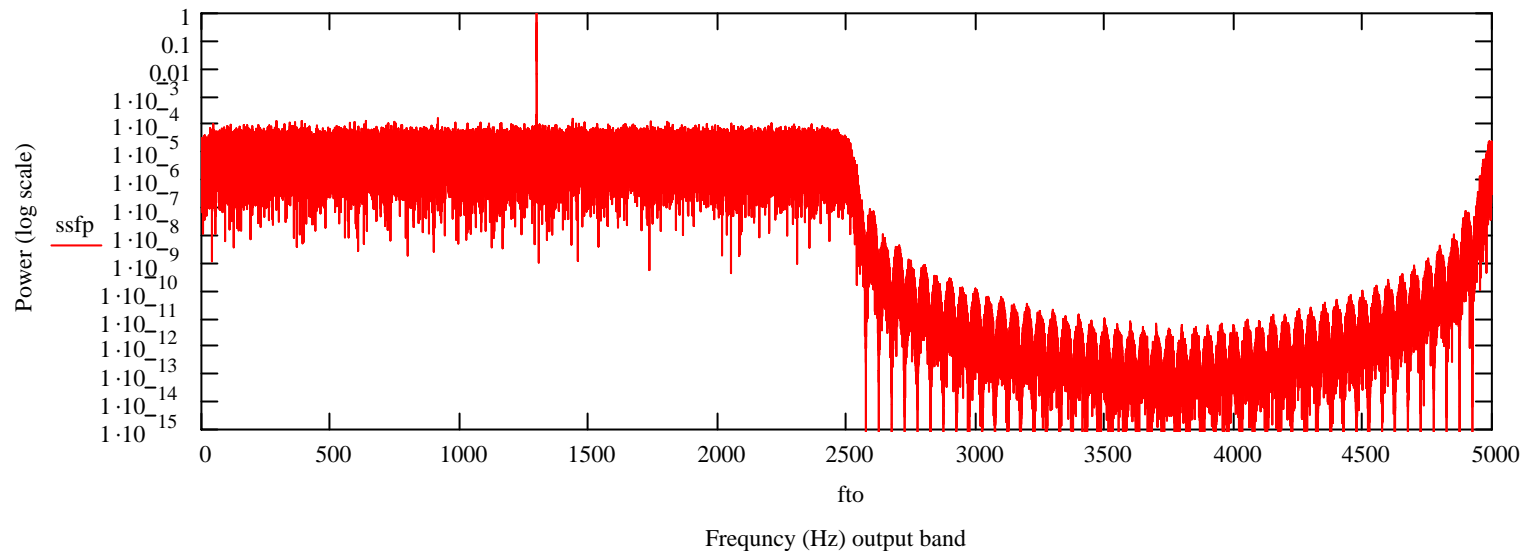
$\text{sf} := \text{MakeFiltX}(\text{Phdopp}, \text{Bsc}, \text{Bec}, \text{Esc}) \quad \text{length}(\text{sf}) = 80000$

fragment of the filtered complex signal in a time domain



Full length spectrum (two-sided FFT), shows good suppression of negative frequencies

$\text{ssf} := \text{cfft}(\text{sf}) \quad \text{ssf}p := (|\text{ssf}|)^2 \quad \text{xssf}p := \max(\text{ssf}p) \quad \text{ssf}p := \text{ssf}p \cdot \text{xssf}p^{-1} \quad \text{dfto} := \text{Tspan}^{-1} \quad \text{fto}_{\text{jto}} := \text{dfto} \cdot \text{jto}$



Determine the frequency of the max power  $\text{xf} := \text{FindMax}(\text{ssf}p, \text{fto}, 0 \cdot \text{Hz}, 2500 \cdot \text{Hz}) \quad \text{fmax} := \text{xf}_1 \cdot \text{dfto} \quad \text{fmax} = 1299.061579255918 \text{ s}^{-1}$

To make SNR estimation, extract the noise data in range 200 - 1000 Hz

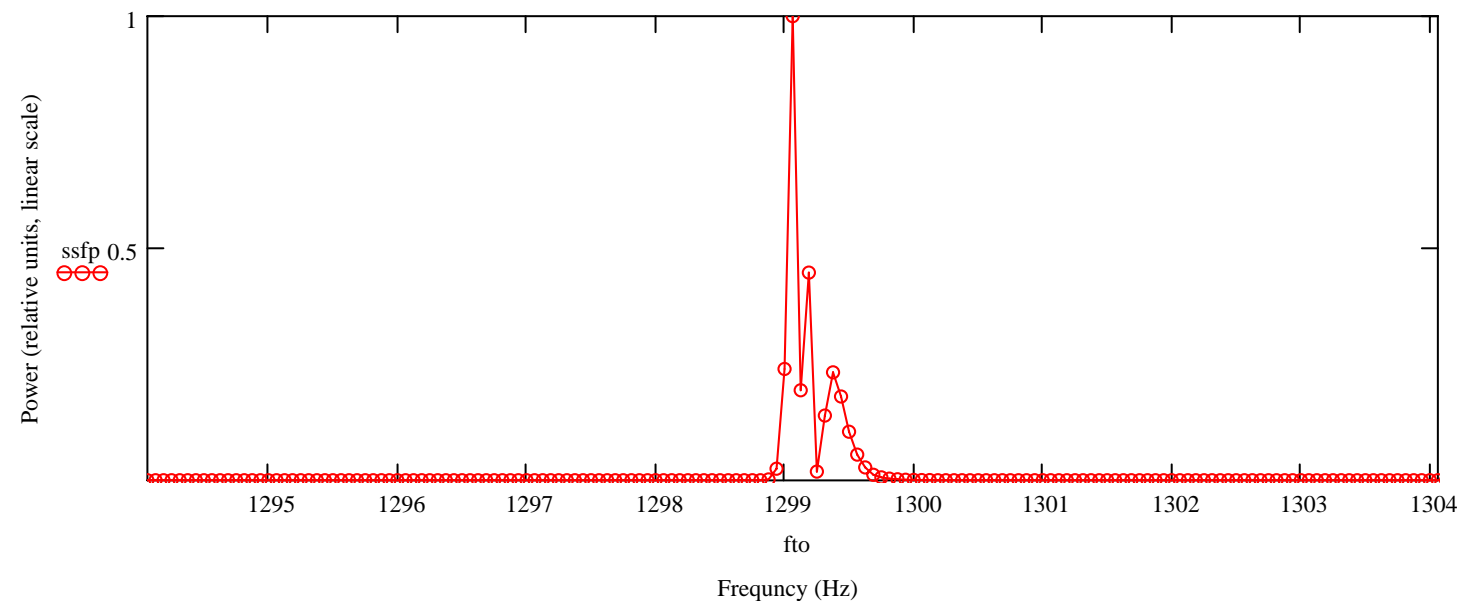
$\text{spnoise} := \text{submatrix}(\text{ssf}p, 200 \cdot \text{Hz} \cdot \text{dfto}^{-1}, 1100 \cdot \text{Hz} \cdot \text{dfto}^{-1}, 0, 0) \quad \text{length}(\text{spnoise}) = 14401 \quad \text{stdev}(\text{spnoise}) = 0.000013463398363 \quad \text{SNR} := \text{stdev}(\text{spnoise})^{-1}$

Predicted SNR (based on how this test signal was generated) is 53 dB for 1/16 of a Hz resolution

And here we have:

$\text{dbSNR} := 10 \cdot \log(\text{SNR}, 10) \quad \text{dbSNR} = 48.708453038649395$

Zoom into central line, all the power is concentrated in a sub-Hz wide line, SNR at 50 dB level.



Line power is still split between many spectral bins (each of 1/16 Hz wide), that's because the phase correction applied was not error free. Although, now in the narrow band we can make further perfection, like PLL it.

Detecting the phase of the tone in narrow band (call it PLL)

Set a narrower bandwidth, say 100 Hz. Decide to move the line to the center of this narrower band  $BW_n := 20 \cdot \text{Hz}$   $F_{\text{targ}} := 0.5 \cdot BW_n$

Check if the target frequency of is exactly representable in the frequency grid  $\text{floor}\left(\frac{F_{\text{targ}}}{dfto}\right) \cdot dfto = 10 \text{ s}^{-1}$  Yes it is

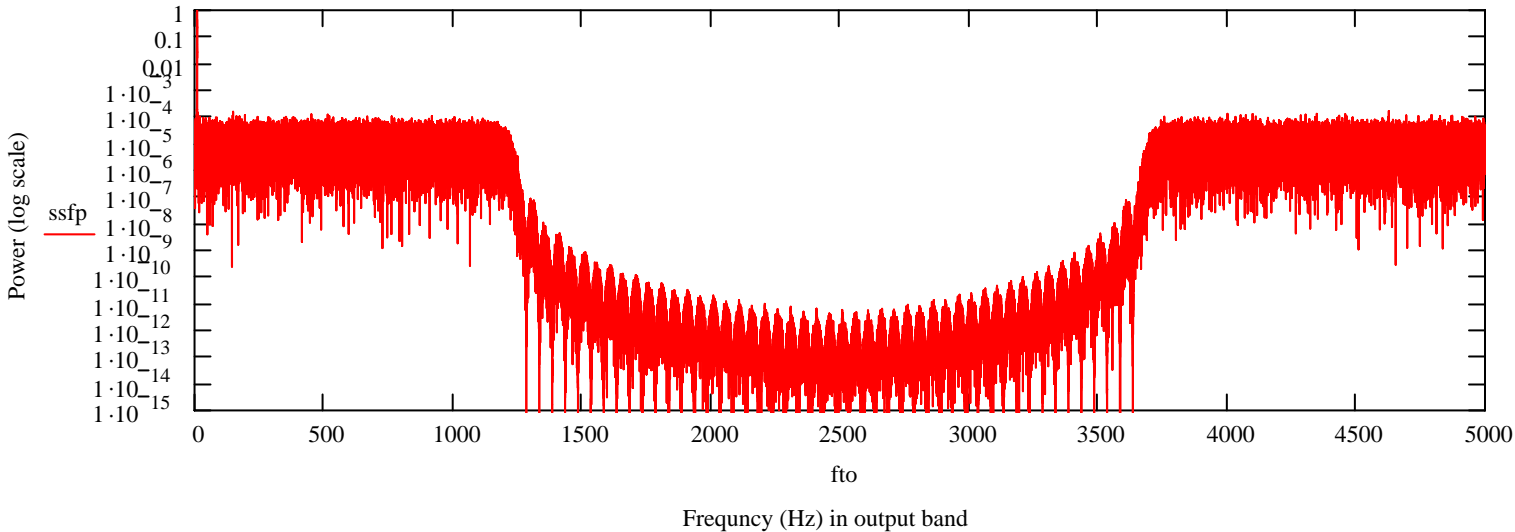
Move the line to the target frequency by rotation if with a frequency:  $F_{\text{rot}} := f_{\text{max}} - F_{\text{targ}}$   $F_{\text{rot}} = 1289.061579255918 \text{ s}^{-1}$

$sfc_{jto} := sf_{jto} \cdot \exp(2\pi \cdot i \cdot F_{\text{rot}} \cdot tto_{jto})$

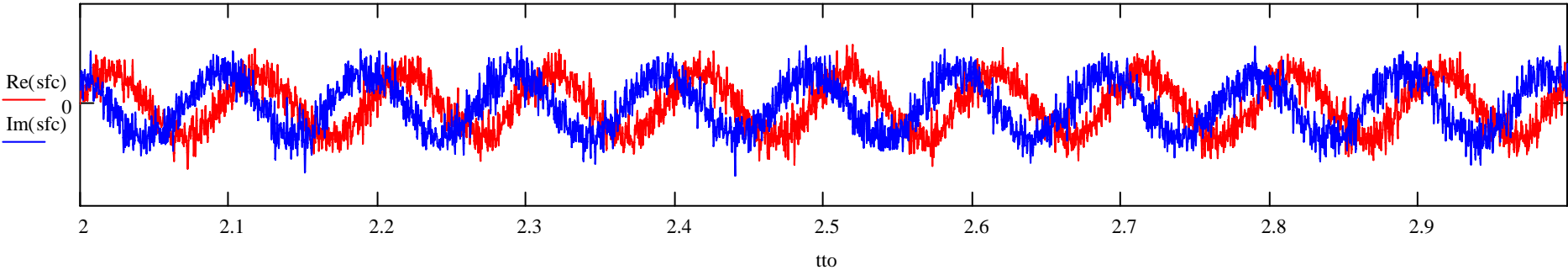
Check the spectrum

$ssf := \text{cfft}(sfc)$   $ssfp := (|ssf|)^2$   $xssfp := \text{max}(ssfp)$   $ssfp := ssfp \cdot xssfp^{-1}$   $dfto := Tspan^{-1}$   $f_{to_{jto}} := dfto \cdot jto$

Line is close to the DC edge of the band now



Check the time domain pattern, resembles a sine wave, with noise still representing the full noise in 2500 Hz band





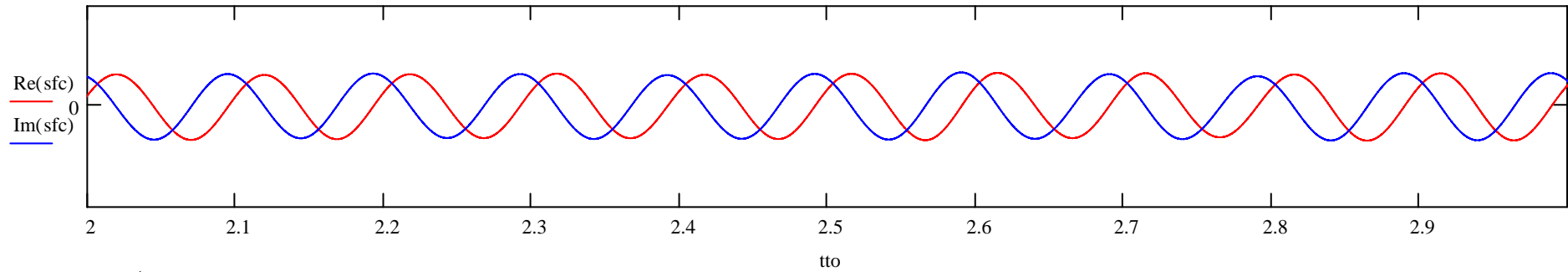
Make the BWn - wide filter around the line (note it's a one side filter)

$$\text{ssff}_{\text{jto}} := \text{if} \left( \text{fto}_{\text{jto}} < \text{BWn}, \text{ssf}_{\text{jto}}, 0 \right)$$

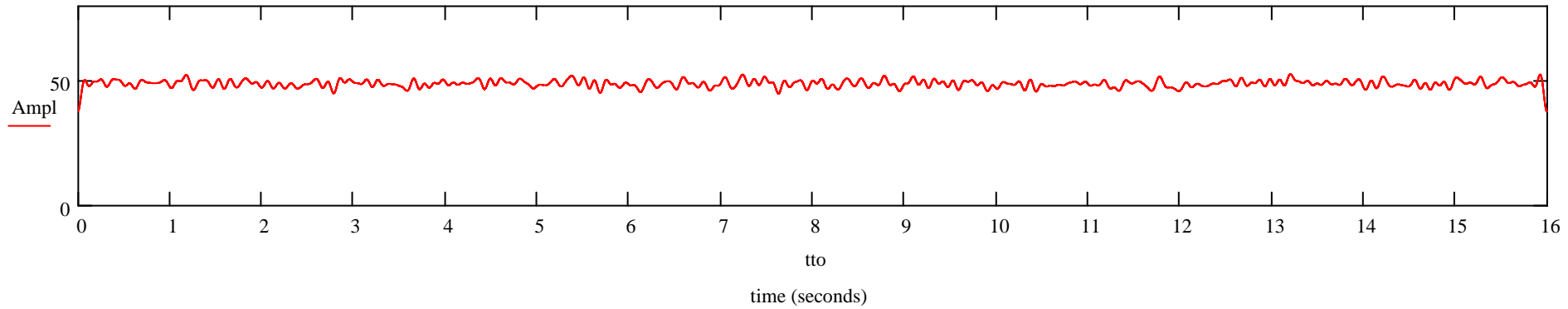
And get the signal back to time domain

$$\text{sfc} := \text{icfft}(\text{ssff})$$

Check the time domain pattern, even more likely the sine wave, not much of noise left after the last filter



$$\text{Ampl} := \overrightarrow{|\text{sfc}|}$$

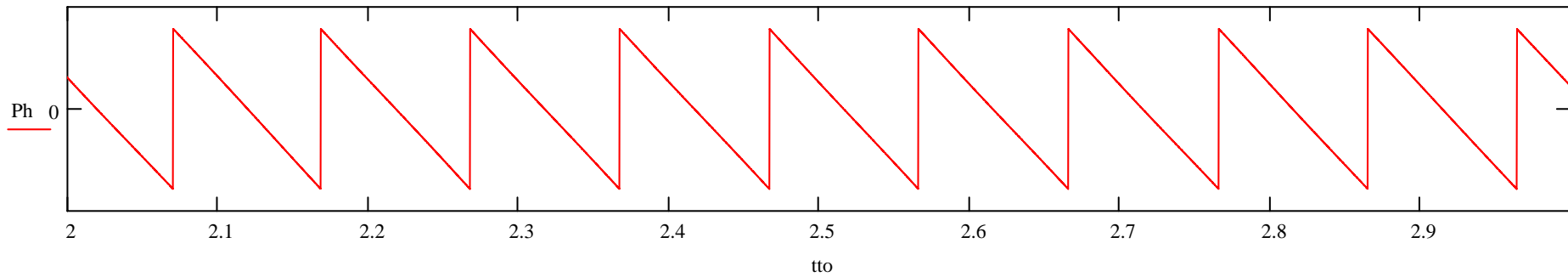


Note the amplitude drop at the start and at the end of the scan, which is due to filter set-up time

## Get the phase

$$\text{Ph}_{\text{jto}} := \arg(\text{sfc}_{\text{jto}})$$

Phase is wrapping over  $2\pi$  each cycle of  $\text{Ftarg}$



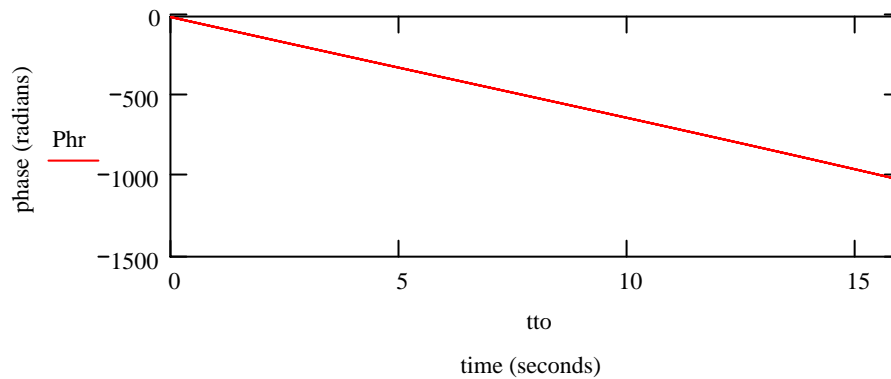
De-wrapping function

```
DeWrap(ph) :=
  np ← length(ph)
  dph0 ← 0
  for jj ∈ 1 .. np - 1
    dphjj ← if (|phjj - phjj-1| < π, 0, sign(phjj - phjj-1))
  qph0 ← 0
  for jj ∈ 1 .. np - 1
    qphjj ← qphjj-1 + dphjj
  for jj ∈ 0 .. np - 1
    phcjj ← phjj - 2π · qphjj
  return phc
```

$\text{Phr} := \text{DeWrap}(\text{Ph})$

is a de-wrapped phase

This one looks like a dull straight line

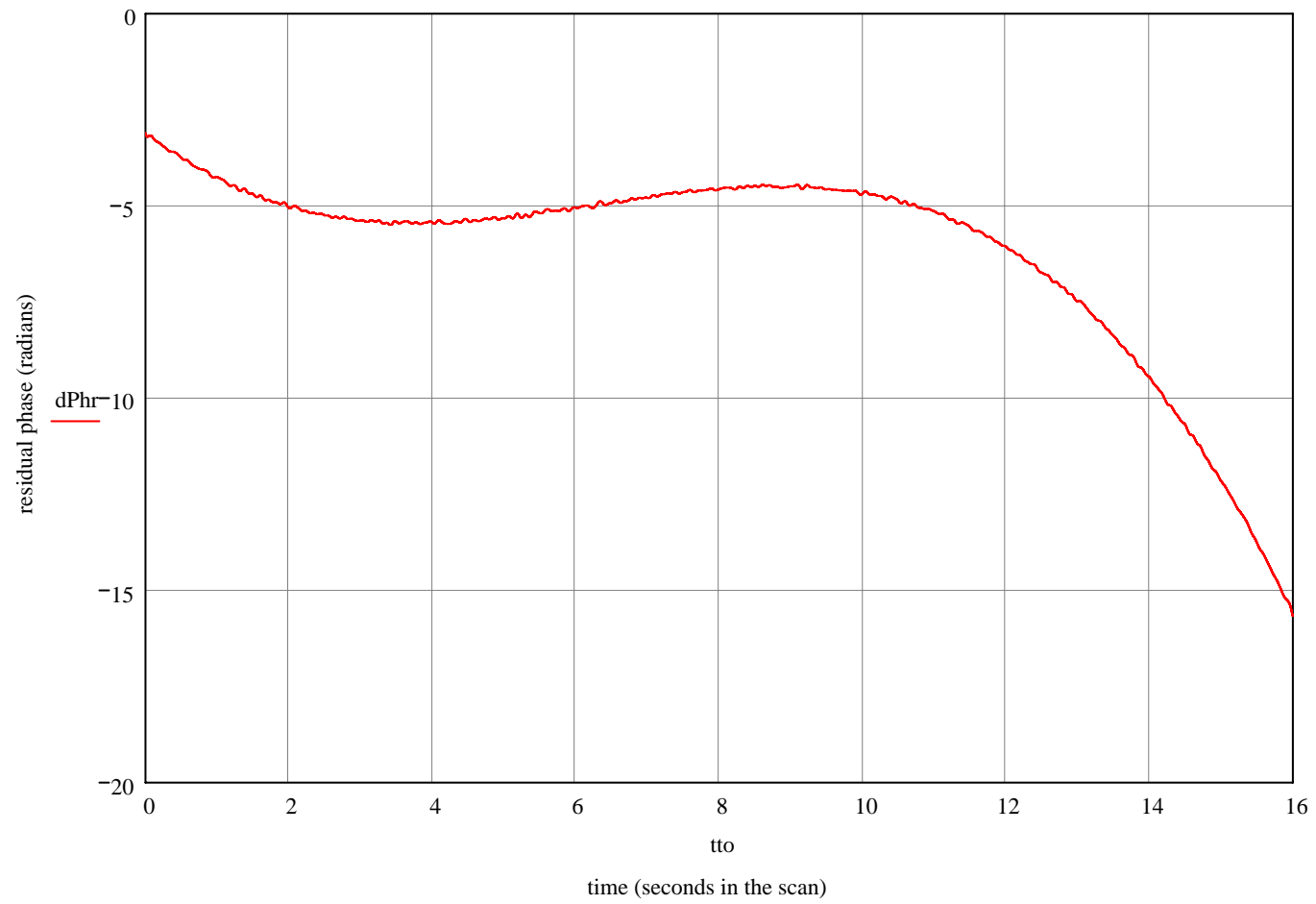


Note that de-wrapping works better for a significantly oversampled signal, like it this case it is 25 times oversampled

It looks dull because it has a huge offset of central frequency of the line

remove the trend line

$$d\text{Phr} := \text{Phr} + 2\pi \cdot \text{Ftarg} \cdot \text{tto}$$



To check the quality, remove the dPhr from the signal

$$\text{sfcc}_{\text{jto}} := \text{sfc}_{\text{jto}} \cdot \exp(-i \cdot \text{dPhr}_{\text{jto}})$$

Check the spectrum

$$\begin{array}{llll} \text{ssf} := \text{cfft}(\text{sfcc}) & \xrightarrow{\quad} & \text{ssfp} := (|\text{ssf}|)^2 & \text{xssf} := \max(\text{ssfp}) \quad \text{ssfp} := \text{ssfp} \cdot \text{xssf}^{-1} \end{array}$$

$$\text{rmsf} := \text{GetRMS}(\text{ssfp}, \text{fto}, \text{Ftarg}, 0.4 \cdot \text{BWn}, 0.1 \cdot \text{BWn})$$

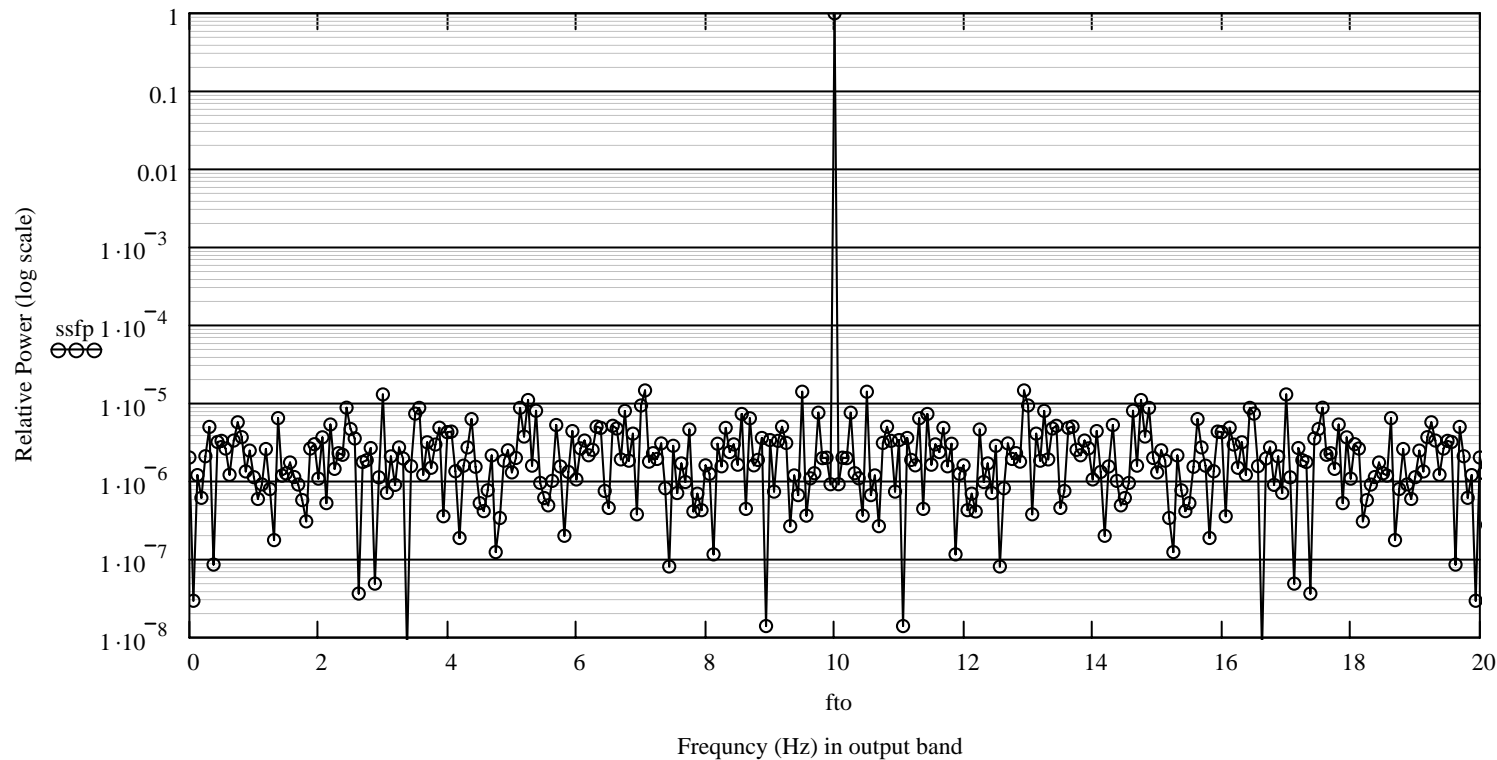
$$\text{SNR} := \frac{1 - \text{rmsf}_0}{\text{rmsf}_1}$$

$$\text{SNR} = 346071.6452928409$$

$$\text{dbSNR} := 10 \cdot \log(\text{SNR}, 10)$$

dbSNR = 55.39166017678077 achieved, in a good agreement with a predicted value of 53 dB, **even better!** but there is a rational explanation for that

**Residual spectrum is squeezed into a single bit at an ultimate frequency resolution (full scan long single FFT)**



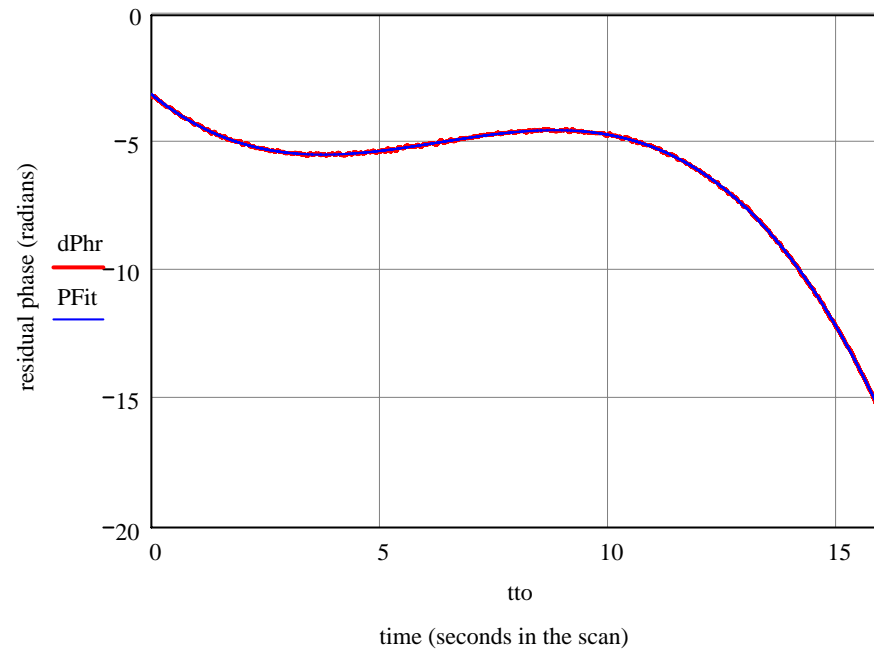
$$\text{Resolution} \quad \text{dfto} = 0.0625 \text{ s}^{-1}$$

Also note, that noise in this spectrum is symmetrical with respect to the line, because the detected phase absorbed the "phase noise" of noise.

This spectrum is not a result, it's just illustration that phase was tracked and part of the noise was absorbed by the created phase model

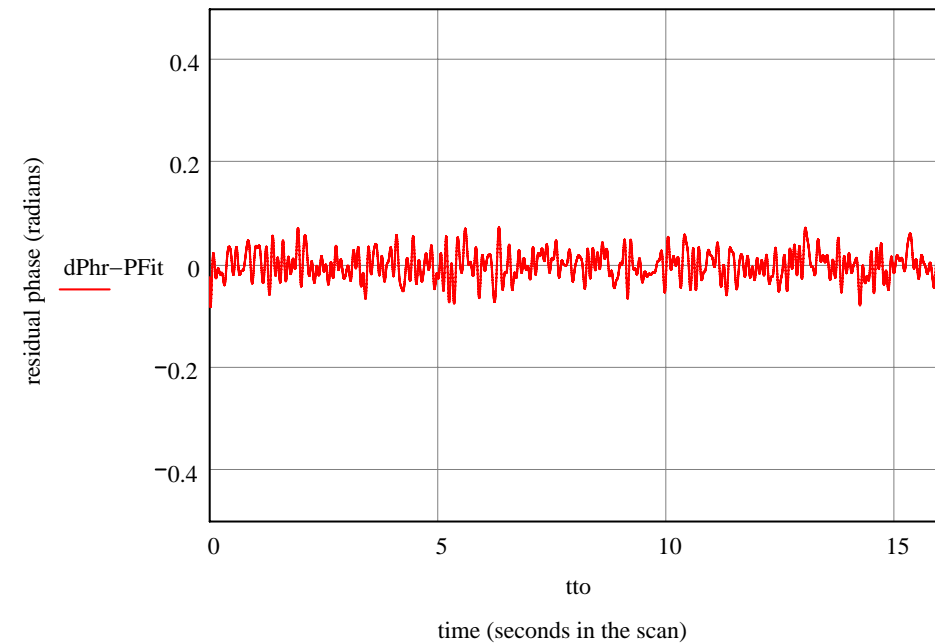
Make a "noise-free" residual phase:

```
wto_jto := 1    Nppf := 4    PFit := PolyfitW(tto,dPhr,wto,Nppf)
```



difference between residual phase and fit

$\text{stdev}(\text{dPhr} - \text{PFit}) = 0.026789318367263$



4th order polynomial fit over 16s interval effectively is a coherent integration over 4 s, so it's almost noise free

remove the PFit from the signal

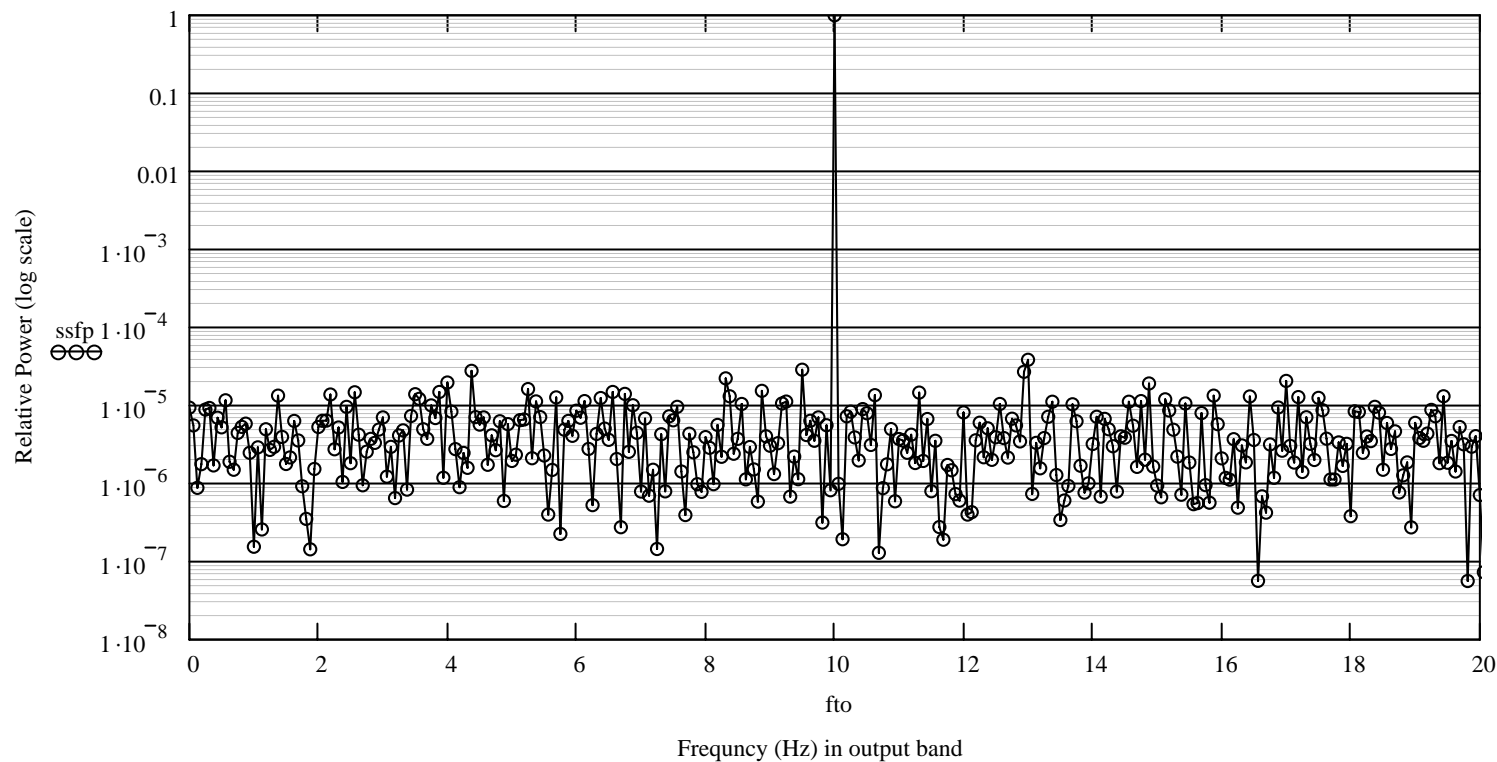
$$\text{sfcc}_{\text{jto}} := \text{sfc}_{\text{jto}} \cdot \exp(-i \cdot \text{PFit}_{\text{jto}})$$

Check the spectrum

$$\begin{aligned} \text{ssf} &:= \text{cfft}(\text{sfcc}) & \text{ssfp} &:= (|\text{ssf}|)^2 & \text{xssfp} &:= \max(\text{ssfp}) & \text{ssfp} &:= \text{ssfp} \cdot \text{xssfp}^{-1} \\ \text{rmsf} &:= \text{GetRMS}(\text{ssfp}, \text{fto}, \text{Ftarg}, 0.4 \cdot \text{BWn}, 0.1 \cdot \text{BWn}) & \text{SNR} &:= \frac{1 - \text{rmsf}_0}{\text{rmsf}_1} & \text{SNR} &= 183610.3433839685 & \text{dbSNR} &:= 10 \cdot \log(\text{SNR}, 10) \end{aligned}$$

dbSNR = 52.63897142813222 achieved, in a good agreement with a predicted value of 53 dB, now it's right !

**Residual spectrum is squeezed into a single bit at an ultimate frequency resolution (full scan long single FFT)**



Resolution  $\text{dfto} = 0.0625 \text{ s}^{-1}$

Also note, that noise in this spectrum is not simmetrical any more.

dPhr is **the result, the final product**, residual phase after other detected phases were subtracted.

Full "SKY" phase can be reconstructed by adding all subtracted phases, just keep a record on what was subtracted.

So, read the input phase model

```
Phid := READPRN("Data3.NoSpin.NoPhNoise.PhaseModel.txt")
tti := Phid<0>      Phm := Phid<2>
```

Spline the input model into the output time grid

```
Phmi := Spline(tti, Phm, tto · s-1)
```

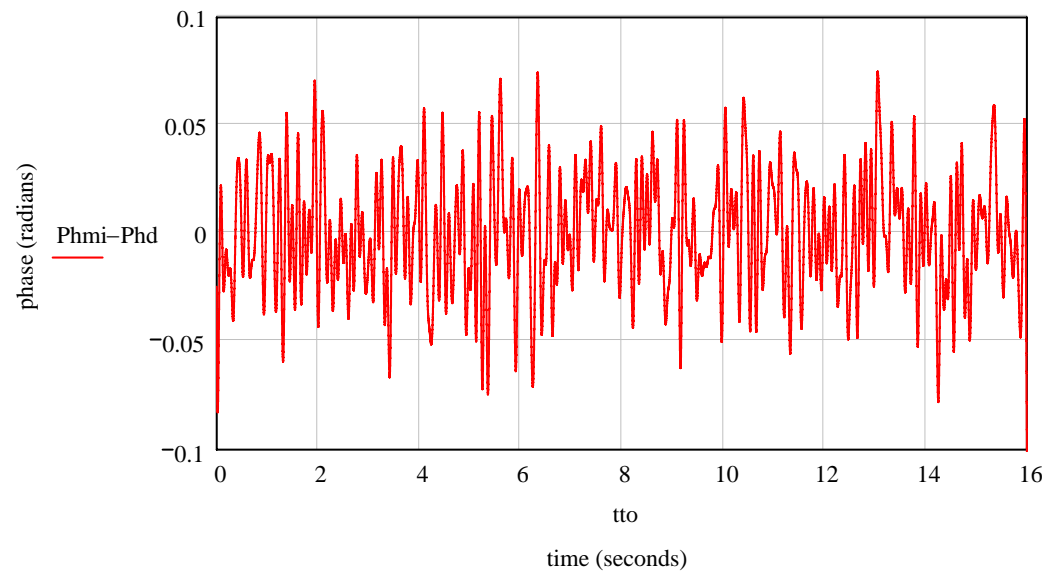
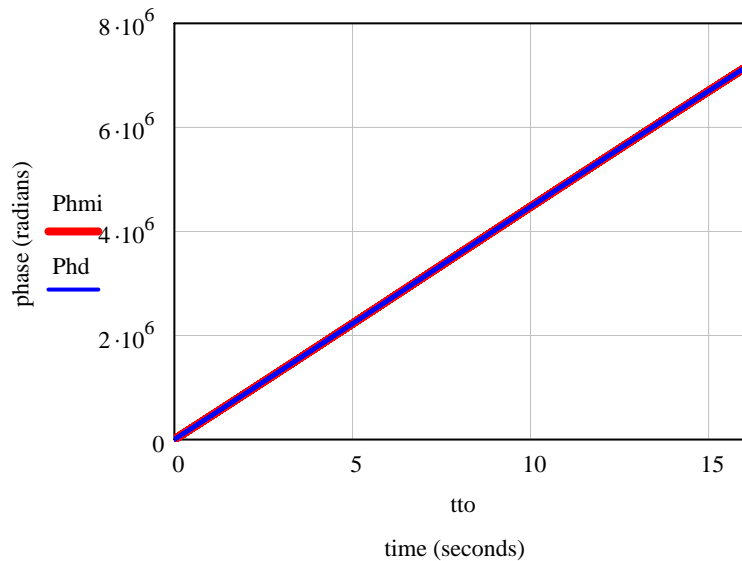
Reconstruct the full detected phase in video band  
by adding the terms which were removed

$$\text{Phd}_{\text{jto}} := -\text{dPhr}_{\text{jto}} + 2 \cdot \pi \cdot \text{Ftarg} \cdot \text{tto}_{\text{jto}} + 2\pi \cdot \text{Frot} \cdot \text{tto}_{\text{jto}} + 2\pi \cdot \text{Fstartc} \cdot \text{tto}_{\text{jto}} + \text{Tspanp} \cdot \left[ \sum_{\text{jjp}=2}^{\text{Npf}} \left[ \text{Cpp}_{\text{jjp}} \cdot \left( \frac{\text{tto}_{\text{jto}}}{\text{Tspanps}} \right)^{\text{jjp}} \right] \right]$$

residual ----- constant frequency terms ----- polynomial from frequency lock

Both input and detected phases

Difference between the input phase model and detected one



Phase noise     $\text{stdev}(\text{Phmi} - \text{Phd}) = 0.026854373491077$     in     $\text{BW}_n = 20 \text{ s}^{-1}$     wide band

bias     $\text{mean}(\text{Phmi} - \text{Phd}) = 0.000254676110411$