Instrumentation Design of a Spatial FFT and FX Correlator for the BEST-2 Array

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ABSTRACT

A spatial FFT imager and FX correlator has been developed using CASPER FPGA hardware for the BEST-2 array at the Radiotelescopi di Medicina in Italy. The digital design is implemented on three Xilinx Virtex 5 based ROACH boards interconnected via streaming XAUI interfaces. The spatial FFT imager takes advantage of BEST-2 as a regularly gridded array to produce a complete set of correlations for all unique baseline spacings by perform a 2D spatial FFT using $O(n\log n)$ operations. This is the first time a spatial FFT instrument has been used as a correlator on a radio telescope array. The FX correlator has been used to solve complex gain calibrations which are applied in the spatial FFT during observation. During the initial deployment of the instruments several bright radio sources were observed over multiple epochs.

1 INTRODUCTION

The Basic Element for SKA Training II (BEST-2) array is a subset of the Northern Cross cylindrical array, at the Radiotelescopi di Medicina in Italy. In this paper we present a new digital backend designed for this array, implemented on Field Programable Gate Array (FPGA) based hardware from the Collaboration for Astronomy Signal Processing and Electronics Research (CASPER¹; Parsons et al. (2006)). The system developed provides fast-dump correlation, direct imaging, and beamforming capabilities.

The digital backend developed for BEST-2 comprises a 32 element digitizer and channeliser, a correlator, spatial Fast Fourier Transform (FFT) imager, and beamformer, implemented on ROACH² FPGA boards. Of particular interest is the spatial FFT imager which can produce a complete set of unique baselines using $O(n \log n)$ operations by taking advantage of the regularly gridded array geometry. This is the first time a spatial FFT instrument has been used as a correlator on a radio telescope array. The FX correlator computes all possible baseline pairs which scales as $O(n^2)$. Along with producing correlation data the spatial FFT functions as a gridded beamformer.

In the first section of this paper we give an overview of the BEST-2 Array, Sections 2.1, 2.2 and 2.3 cover a description of the channelization, correlation and image-domain processing system. Results from preliminary observations of bright radio sources from these systems are presented in section 3.1 and section 3.2.

1.1 BEST-2 Array

The BEST-2 testbed at the Radiotelescopi di Medicina consists of 8 East-West oriented cylindrical concentrators, each with 64 dipole receivers critically sampling a focal line at 408MHz. Signals from these 64 dipoles are summed in groups of 16, resulting in 4 channels per cylinder, and a total of 32 effective receiving elements laid out on a 4-by-8 grid, shown in Figure 1.

BEST-2 was developed as a reliable, low cost frontend to be used in SKA development, with a core design requirement of simplicity in interfacing with different digital backends (Montebugnoli et al. 2009b). Extensive documentation of the development of the analogue chain developed for BEST-2 can be found in a number of papers (Perini (2009); Perini et al. (2009)). The top level specifications of the array are shown in Table 1.

In 2008 the initial digital correlator backend of the array was based on iBOB and BEE2 FPGA boards from the CASPER group (Montebugnoli et al. 2009a). An upgraded digital backend has been developed using the ROACH board, also developed by CASPER, which consists on an FX correlator, spatial FFT imager and beamformer.

2 DIGITAL INSTRUMENT DESIGN

An FX correlator and spatial FFT imager have been implemented in digital hardware for use with the BEST-2 array. Both instruments use the same digitization and channelization frontend. The hybrid design of the digital instruments make it possible to use both the correlator and imager concurrently. This allows a streamlined process for calibrating the spatial FFT imager, reduces the amount of hardware and allows for simultaneous observation with both instruments. The instruments have been implemented on ROACH boards

¹ https://casper.berkeley.edu/

² Reconfigurable Open Architecture Computing Hardware – https://casper.berkeley.edu/wiki/ROACH

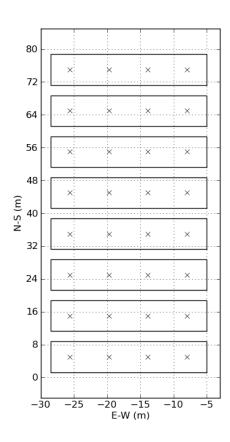


Figure 1. The 32 effective receiving elements of BEST-2, indicated by crosses, lie on a regular 4x8 grid. Each receiver is the analogue sum of 16 dipoles, critically spaced at 408 MHz in the East-West direction.

which are a generic field programmable gate array (FPGA) board designed by CASPER for radio astronomy applications. The ROACH platform is based on a XILINX Virtex 5SX95T³ FPGA with interfaces to DRAM and QDR memory, high speed CX-4 connectors and a generic Z-DOK interface for connecting ADCs and various daughter boards, Figure 2. Additionally, the board has a PowerPC running BORPH (So & Brodersen 2008), a variant of Debian Linux, which allows access to software registers and shared memory on the FPGA. Firmware is designed using MATLAB Simulink which is extended with XILINX DSP blocks and CASPER's open source DSP blocks⁴. Design specific DSP blocks and hardware interfaces have also created. Design models and control software are available from our project repository⁵. Instrument design specifications are presented in Table 2, further design detail are described in Sections 2.1, 2.2 and 2.3.

BEST-2 Array Specifications		
Array Properties		
Number of Cylinders	8	
Total Number of receivers	32	9
Total Collecting Area	1411.2	$m^2 \ m^2/K$
A_{eff}/T_{sys}	11.65	m-/K
Longest Baseline		
E-W	17.04	m
N-S	70.00	m
Bandpass		
Central Frequency	408	MHz
Analogue Bandwidth	16	MHz
Primary Beam		
Primary Beam Size	37.62	deg^2
Declination	5.7	\deg
Right Ascension	6.6	deg
PSF		
PSF FWHM	0.9	deg^2
Declination	0.52	\deg
Right ascension	1.73	\deg

Table 1. The top level specifications of the BEST-2 Array, a subset of the collecting area of the Northern Cross, located in Medicina, Italy.



Figure 2. The 'F-engine' ROACH board, a Virtex 5 SX95T FPGA board, with the 64 input ADC connected via two Z-DOK connectors.

2.1 Digitization and Channelization

Signal digitization is performed using the Texas Instruments ADS5272 8 channel, 12 bit ADC. The ADC board, developed by Rick Raffanti⁶, uses eight ADCs to channelize 64 streams at up to 65 Msps. In our design 32 signal streams

 $^{^{3}\ \}mathrm{http://www.xilinx.com/support/documentation/virtex-}5.\mathrm{htm}$

 $^{^4}$ https://casper.berkeley.edu/

⁵ https://github.com/griffinfoster/medicina

 $^{^6}$ https://casper.berkeley.edu/wiki/64ADCx64-12

Digital Backend Specifications			
Digitizer/Channelizer (F-Engine)			
ADC Sampling Rate	40	Msps	
ADC Sampling Precision	12	bit	
Antenna-polarizations	32	single pol	
PFB	$4 ext{ tap FIR} + 2048 ext{ point FFT}$	Radix-2 Biplex Real FFT	
Quantization	4	bit	
FX Correlator (X-Engine)			
Auto Correlations	32		
Cross Correlations	496		
Minimum Integration Length	6.55	ms	
Output	10 GbE	SPEAD protocol	
Spatial FFT Imager (S-Engine)			
2D FFT	8 x 16		
Beams	128		
Minimum Integration Length	1	s	
Output	1 GbE	SPEAD protocol	
Beamformer Output	10 GbE	Up to 8 Beams	

Table 2. A three ROACH design where the correlator and spatial FFT imager use the same digitizer/channelizer frontend.

are digitized at 40 Msps which covers the 16 MHz analogue band of the BEST-2 system. The ADC is clocked with a 160 MHz clock which is locked to a local maser source. During the analogue stage the radio frequency (RF) signal, centred at 408 MHz, is mixed down to baseband. Prior to digitization the last amplifier stage of the analogue chain has per signal adjustable gain useful for setting levels for optimum ADC quantization. This ADC is connected via a dual Z-DOK interface to an 'F-Engine' ROACH which performs the frequency channelization. A block diagram of the design layout is shown in Figure 3.

The ROACH board is clocked at four times the sample rate such that four signals are time division multiplexed onto a single stream. Frequency channelization is performed with a four tap Hann filter, 2048 point polyphase filterbank (PFB) to produce 1024 samples per real antenna stream. The CASPER PFB has been modified to account for the signal multiplexing. Each channel has a width of 19.5 kHz and the output of the FFT stage is 36 bit complex. The narrow channel widths and PFB windowing are required for good frequency separation in the high RFI environment at the observatory.

After channelization the samples are quantized down to 8 bit complex. An adjustable, per channel complex gain equalizer is used for amplitude and phase corrections before quantization. Complex gain calibration is essential to proper spatial FFT imaging and must be applied before the spatial FFT operation. The FX correlator is used to generate calibration coefficients which are applied back into the equalizers. A selectable mux is available to skip the phase coefficients on the FX correlator data stream.

Post equalization, the data stream is duplicated and split for specific reordering for the correlator and imager. The correlator data stream is blocked into 128 samples of

single antenna, single frequicy channel. This requires the use of a large memory block for performing the corner turn operation, this has been implemented using the on board QDR RAM. The spatial FFT imager is blocked into 32 antennas for a single time and single frequicy channel. After data reordering each stream is sent over high speed XAUI at a rate of 5.12 Gbps to the correlator and imaging boards. There are sufficient resources to include additional features in the 'F-Engine', including, for example, finer channelization, an increase in antennas or an increase in bandwidth should a future expansion of the design be warranted.

2.2 FX Correlator

An FX correlator design is a standard design for large bandwidth, many antenna arrays. The F component represents the frequency channelization, and the X is a complex multiply and accumulate (CMAC). An overview of the architecture is presented in Romney (1999). Architecture efficiency goes as $O(M\log M) + O(N^2)$ where M is the number of frequency channels and N is the number of antennapolarizations. The core component to the X stage of the FX correlator is the complex multiplication of all pairs of independent signals for each frequency channel. A pipelined X-engine, based on the general CASPER block originally designed by Lynn Urry(Urry et al. 2007), is used for optimal multiplier efficiency. The pipeline design is constructed out of M/2 'taps' where the i^{th} tap computes the correlation between antennas A_j and A_{j+i} for every antenna A_j of Mtotal antennas. To maximize the multiplier usage a loopback is added to use every i^{th} tap to compute the correlation of antennas A_j and $A_{M/2+j+i}$, Figure 4. Each tap accumulates for t time samples to reduce the output data rate.

An asynchronous architecture is used between the F-

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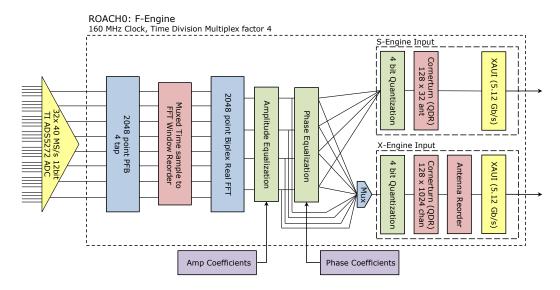


Figure 3. Block diagram of the ROACH F-Engine. During observations amplitude and phase coefficients are applied to scale the power for the 4 bit correlation and apply phase corrections for the spatial FFT.

Pipelined X-Engine M time sample per antenna, N antennas

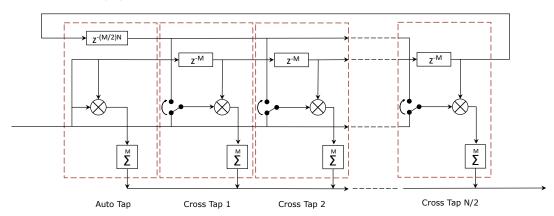


Figure 4. Pipelined X-enigne design schematic. The input is ordered as M time samples per antenna per frequency channel. An accumulation stage after the complex multiply reduces the data rate of each tap. Outputs are multiplexed onto the same output using a valid signal.

enigne and X-engine boards. The X-engine board has been clocked to 200 MHz, well above the 160 MHz F-engine board, this assures the x-engine board will never have input buffer overflows during the windowing stage. The XAUI interboard connection is a streaming interface which guarantees the same output order as input order but with variable latency. In rare cases the XAUI interface can drop 64 bit words during the streaming, this requires an initial error correction stage to track the number of words received within a XAUI frame. In case of missing words the entire payload is dropped and counters reset for the next header.

A correlation is only performed on a per channel basis. The channelized band can be split up into portions and processed in parallel across multiple X-engines. This allows a larger bandwidth to be processed at the cost of increased logic and multiplier resource utilization. We currently under utilize the available resources on the FPGA. For this design

two pipelined X-engines are used which each processes half of the band, Figure 5.

The X-engine design requires a continuous stream of data for 128 samples of all antennas for a single frequency channel. Prior to the X-engine, samples are buffered up into windows to guarantee valid data during a cycle of the X-engine. During the X-engine stage an initial accumulation of 128 sample is performed after the complex multiply to reduce the output rate to roughly the input rate. This limits the minimum integration time to 6.55 ms.

A vector accumulator using the on board QDR memory is used for longer integration lengths. This second accumulator is software controlled with integration lengths ranging from milliseconds to minutes. A completed integration is sent to a receive computer over a 10 GbE connection. In-

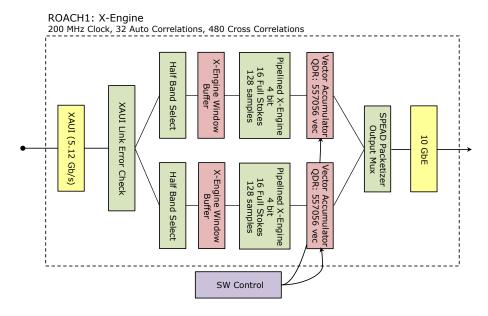


Figure 5. ROACH X-engine block diagram, two parallel pipelined x-engines are used, each processes half of the band.

tegrations are packetized using the SPEAD protocol 7 and transmitted over UDP.

2.3 Spatial FFT

When N receiving elements in an antenna array are placed on a regularly spaced grid, a well known method for producing a complete set of orthogonal beams on the sky is the spatial fast Fourier transform (Williams 1968). Such a beamforming implementation will generate N beams on the sky, with a computational cost of $O(N \log N)$. For large arrays, where many beams are desired, this can be a significant computational saving, with the alternative, so-called DFT beamforming, requiring O(N) operations per synthesized beam. To date, the largest such astronomical implementation of such a spatial fast Fourier transform beamformer is the 64 element dish array constructed in 1994 at Waseda University, Japan (Otobe et al. 1994).

More recently, spatial FFT based processing has been revisited in the literature with an emphasis on the correlation matrix, rather than the collection of beams, as the mathematical object of interest (Tegmark & Zaldarriaga 2009) (Tegmark & Zaldarriaga 2010). In the method outlined by Tegmark & Zaldarriaga, zero padding is applied to the matrix of antenna signals before the spatial FFT is performed, and as such, the complete set of visibilities for all unique baselines in the array can be obtained, post integration, by inverse Fourier transform. Conversely, in the image plane, the zero-padding required by the prescribed algorithm results in the generation of $2^m N$ beams on the sky and is dependent on the number of dimensions, m, in the antenna array. Regardless of potential downstream visibility domain processing, this oversampling of the sky by a factor 2^m has the benefit of increasing the instantaneous uniformity of sky coverage by synthesized beams, which somewhat alleviates

the limitations associated with the inability to steer multiple beams independently.

In the BEST-2 backend described here, the requirements on the spatial FFT processor were multifold. Firstly, the system should be capable of generating images on an O(second) timescale, by the method described by (Tegmark & Zaldarriaga 2009). Further, the system should be capable of passing formed beams at full bandwidth, i.e. without any accumulation, to downstream time domain processing systems such as the real-time pulsar dedispersion engine (Magro et al. 2011).

This redundancy for the BEST-2 array is show in Figure 6. Instead of making individual correlations of the same baseline as in an FX correlator the correlation of the average of each baseline can be computed. This optimization relies on the assumption that each redundant baseline measurement is indeed identical. Thus any calibration to the complex gains must be applied before the spatial FFT.

Though the X-Engine and S-Engine use the same F-Engine, each requires a unique data windowing order. For the S-Engine a window is made up of N antennas by M time samples for a given frequency channel. A similar XAUI interface and windowing scheme is used as in the X-Engine which buffers up windows of valid data to stream into the spatial transform.

The 2D spatial transform is performed using an 8 point FFT followed by a cornerturn and 16 point FFT. A block diagram of the design layout is shown in figure 7. The BEST-2 array is a grid of 4 by 8 antennas, the data is zero padded before input into the 8 by 16 point spatial transform. A 4 by 8 point spatial transform will only produce gain information for each spatial position, which can be interpreted as an array of beamformers covering the field of view. This zero padding is necessary to produce both the gain and phase information of each spatial position which is an effective baseline. Each effective baseline is an average of all possible baselines with the same spatial dimensions.

⁷ https://github.com/ska-sa/PySPEAD

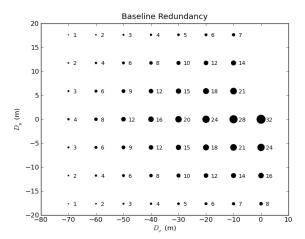


Figure 6. A 4 by 8 regularly gridded array has 53 unique baselines, 480 cross correlations are performed. The number of redundant baseline measurements is labelled and represented by the size of each circle.

The four fold increase is the number of outputs from the spatial transform by double padding introduces a number of redundant calculations. The spatial transform produces 128 outputs. There are only 53 unique baselines in a 4 by 8 grid.

The datarate out of the S-Engine is reduced by a two stage vector accumulator. A fixed 128 sample vector accumulator reduces the output of the second stage FFT so that the 1024 channels of the 128 computed spatial components can be multiplexed onto one line and accumulated in a software controllable QDR vector accumulator. Accumulations are sent out over the 1 GbE PowerPC interface using the a SPEAD UDP packet format.

Individual beams can be selected out before accumulation and sent over 10 GbE in a LOFAR beam packet format which is used for pulsar processing.

3 DEPLOYMENT AND INITIAL OBSERVATIONS

Instrumentation was installed and tested during March 2012, during which time various bright radio sources were observed. Since the Northern Cross is a transiting array there is a limited period of time each day in which a source is in the primary beam. Bright sources such as Cygnus A, Cassiopeia A and Taurus A along with a number of 3C sources were observed along with multiple constant declination 24 hour cycles.

Raw data from the correlator and imager is recorded to HDF5 files using a SPEAD protocol receive script. A suite of python scripts have been written to interface and manipulate the data in this pre-calibration stage. A python FITS-IDI package has been written to convert HDF5 files into the standard FITS format which can be read by AIPS and CASA⁸. This allows for conversion to the Measurement Set format which standard interferometry and imaging packages can interface with.

3.1 FX Correlator Imaging

We have verified the digital system by observing a set of bright radio point sources with the FX correlator. The contour plots in Figure 8 show the various stages of imaging derived from a two minute snapshot observation of the bright source Taurus A. After applying a source tracking phase we generate Figure 8a which shows the resulting image before any phase and amplitude correction is added. Once calibrations have been derived and applied we can see the unresolved source Taurus A in the dirty image, Figure 8c. The sidelobes of the array point spread function (PSF), Figure 8b, can can be seen in the dirty image. After deriving a clean model of the field the clean image, Figure 8d, is dominated by a single point source.

3.2 Spatial FFT Imaging

The spatial FFT imager has the effect of averaging together all identical spacing baselines, and produces a set of correlations for each unique baseline. As such, phase and amplitude calibration needs to be applied to the spatial FFT imager data during observations. If these calibrations are not applied during the observation the resulting imager, Figure 9a, has flux scattered through out the image. Calibration coefficients are derived from FX correlator data of bright point sources. Once proper calibration is applied the resulting dirty image, Figure 9b, is similar to the FX correlator dirty image, Figure 8c, taken during the same observation.

4 CONCLUSION

An FX correlator and spatial FFT imager have been successfully installed on the BEST-2 array at Medicina Observatory. The digital firmware was developed using the open source CASPER libraries and their generic ROACH hardware. This is the first time a spatial FFT imager has been used to produce complex baseline correlations. Both instruments can operate simulatenously which has allowed us to compare the respective data quality. An in depth initial study of the data quality of the spatial FFT imager ciompared to the FX correlator can be found in our results paper (Foster et al. 2012).

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⁸ https://github.com/telegraphic/pyfitsidi

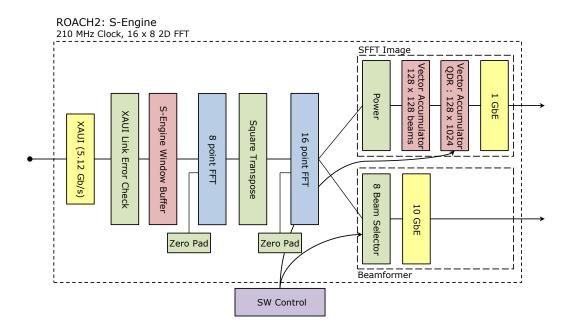


Figure 7. During the two stage spatial FFT the streams are zero padded to provide phase information of each baseline.

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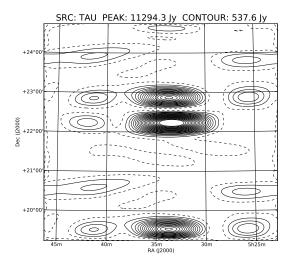
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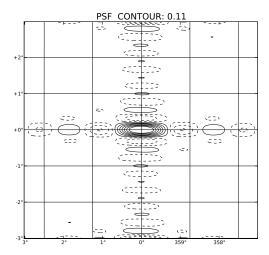
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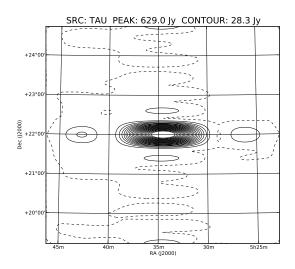
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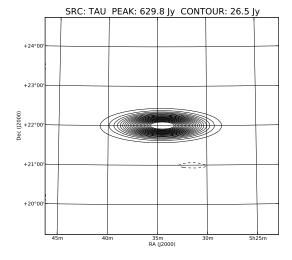
(a) Uncalibrated image of Taurus A.



(b) Point spread function. The high, regular side lobes are an effect of the regularly gridded array. $\,$

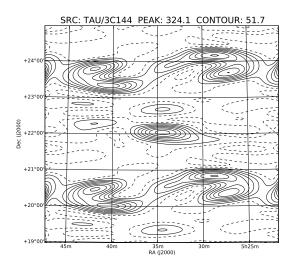


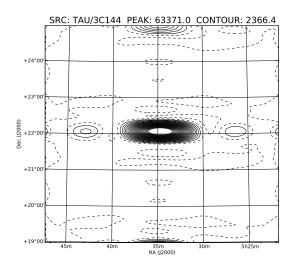
(c) Dirty image formed, using natural weighting, after applying complex gain solutions. The structure from the PSF is clearly visible. The dynamic range of this image is $\sim 150.$



(d) Cleaned image of the field, Taurus A is the dominating point source with a peak of 730 Jy, the image have a dynamic range of $\sim 350.$

Figure 8. Images and PSF formed from an FX correlator two minute snapshot observation of Taurus A.





- (a) Dirty image of Tau/3c144 formed before applying complex gain calibrations in the F-Engine for the spatial FFT. The uncalibrated phases spread the power through out the image.
- (b) Dirty image of ${\rm Tau/3c144}$ with complex gain calibrations applied. This image has a signal to noise ratio around 100, a standard CLEAN method can be used to improve the image dynamic range.

Figure 9. After applying complex gain calibration a bright point source such as Tau/3c144 appears similar to the array PSF, and has a significant improvement in the image fidelity compared to the uncalibrated image.