

Implementation of periodic boundary conditions in the finite element program ABAQUS

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Interdisciplinary Centre For Advanced Materials Simulation

March 15, 2013



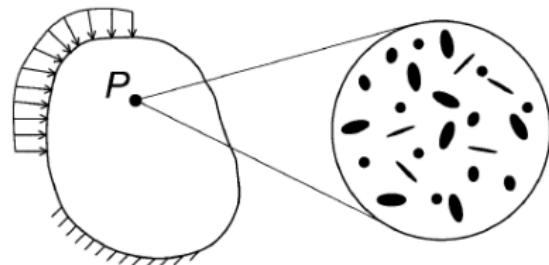
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Representative volume element

- Representative volume element (RVE) is the statistical representation of properties of a material
 - Contains all informations of microstructure
 - Significantly smaller than the macroscopic structural dimensions
 - Deformation gradient is known from Macro Model → should be applied to Micro Model



The same informations can be obtained using the RVE while significantly reducing the computational effort.

Representative volume element

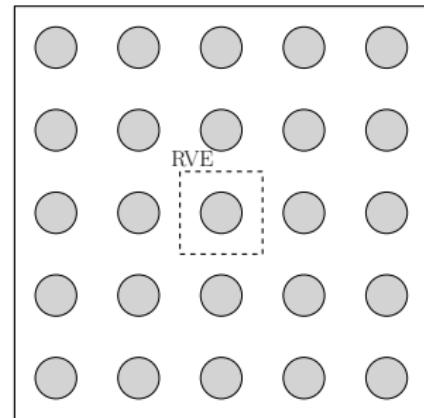
Periodic features

1. Periodic repeating geometry

- ▶ RVE represents whole microstructure

2. Periodic boundary conditions

- ▶ Boundary conditions are whether free nor fixed
- ▶ Opposite sides are deforming in the same manner (periodic) but allowing lateral shrinkage due to Poisson's ratio



Representative volume element

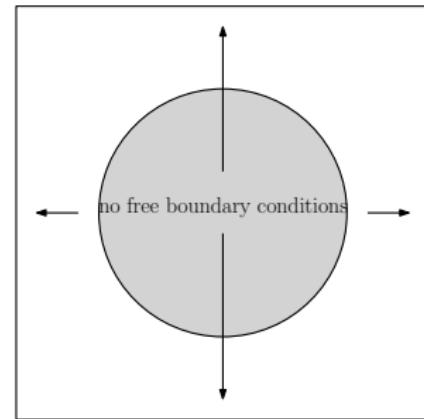
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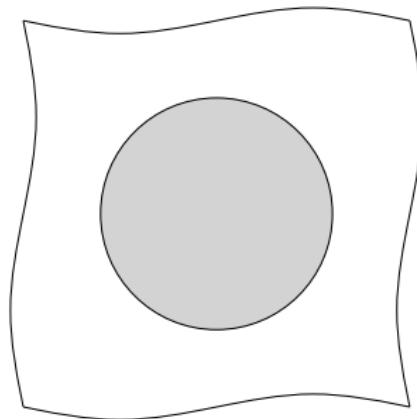
- ▶ Boundary conditions are whether free nor fixed
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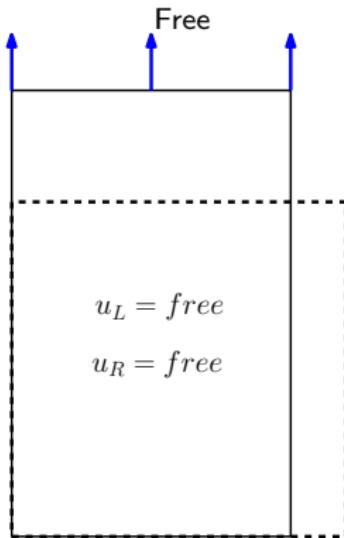
Representative volume element

Periodic features

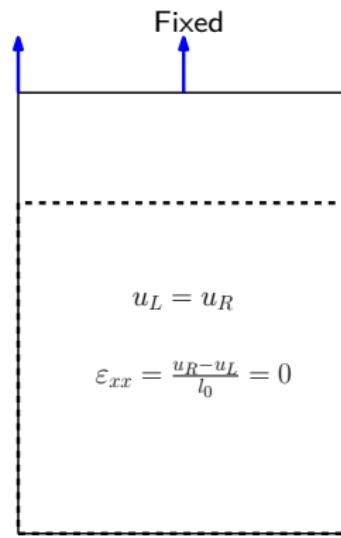
1. Periodic repeating geometry
 - ▶ RVE represents whole microstructure
2. Periodic boundary conditions
 - ▶ Boundary conditions are whether **free** nor **fixed**
 - ▶ Opposite sides are deforming in the same manner (**periodic**) but allowing lateral shrinkage due to Poisson's ratio



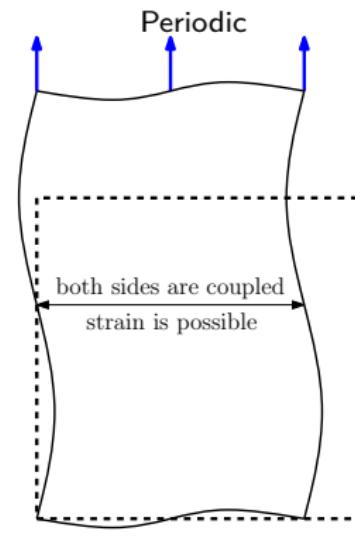
Boundary conditions



► To soft



► To stiff



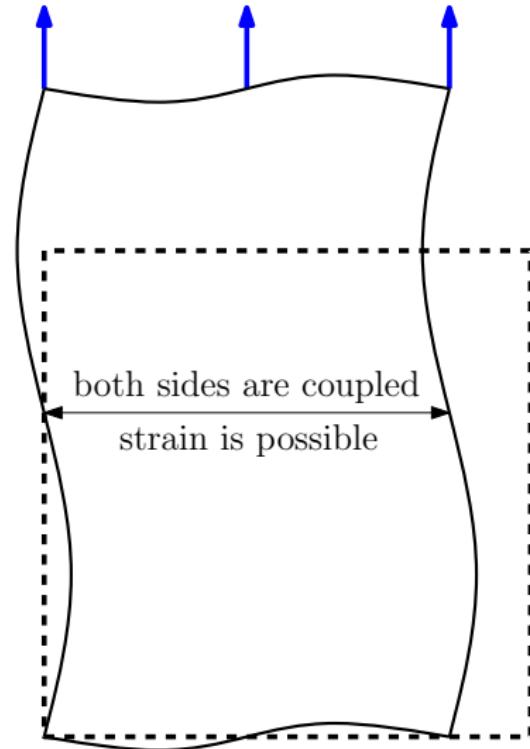
► Presents periodicity

Periodic boundary conditions

- ▶ $u_i^{\text{Side}} - u_j^{\text{Opposite side}} = \Delta\varepsilon_{ij} \cdot l_i$
- ▶ $u_x^{\text{Right}} - u_x^{\text{Left}} = \Delta\varepsilon_{xx} \cdot l_x$
- ▶ $u_y^{\text{Top}} - u_y^{\text{Bottom}} = \Delta\varepsilon_{yy} \cdot l_y$
- ▶ $u_y^{\text{Right}} - u_y^{\text{Left}} = \Delta\varepsilon_{xy} \cdot l_x$
- ▶ $u_x^{\text{Top}} - u_x^{\text{Bottom}} = \Delta\varepsilon_{yx} \cdot l_y$

Key features

- ▶ Ability to apply displacement boundary conditions
- ▶ Correctly represent strains due to Poisson's ratio
- ▶ Avoid overconstrained model

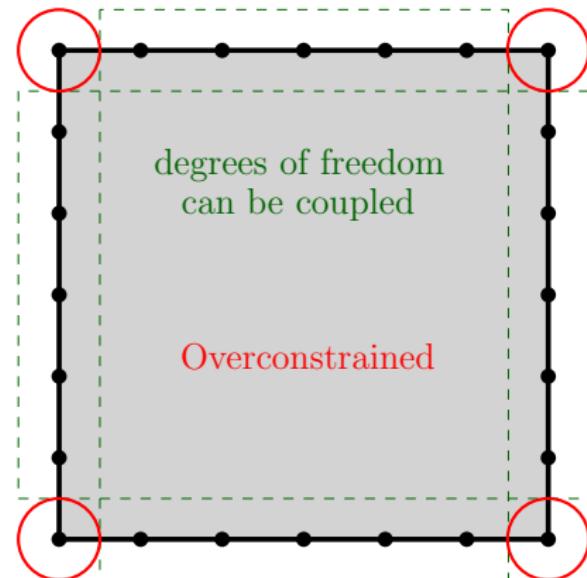


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Periodic boundary conditions - Abaqus implementation 2D

Left to right

$$\blacktriangleright \mathbf{u}_i^R - \mathbf{u}_i^L = \mathbf{u}^{V_2} - \mathbf{u}^{V_1}$$

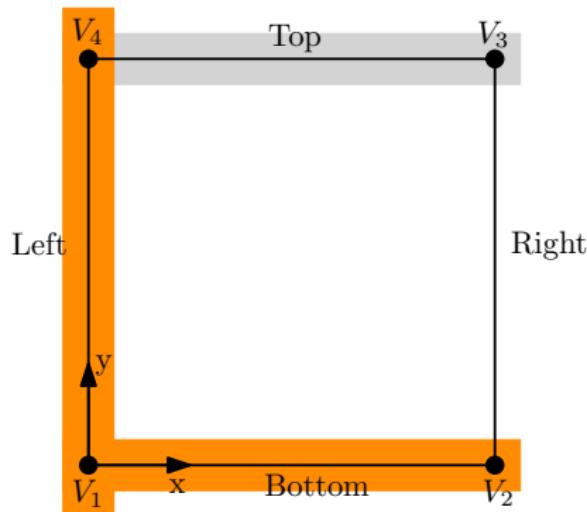
Bottom to top

$$\blacktriangleright \mathbf{u}_i^T - \mathbf{u}_i^B = \mathbf{u}^{V_4} - \mathbf{u}^{V_1}$$

Dependent vertex

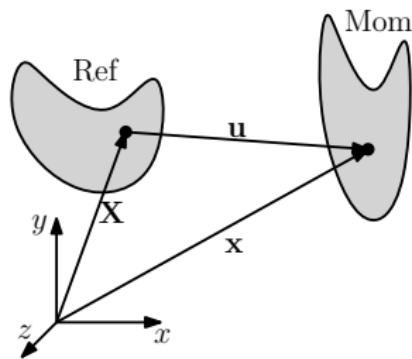
$$\blacktriangleright \mathbf{u}^{V_3} - \mathbf{u}^{V_4} = \mathbf{u}^{V_2} - \mathbf{u}^{V_1}$$

\mathbf{u} := Displacement vector



Application of deformation gradient

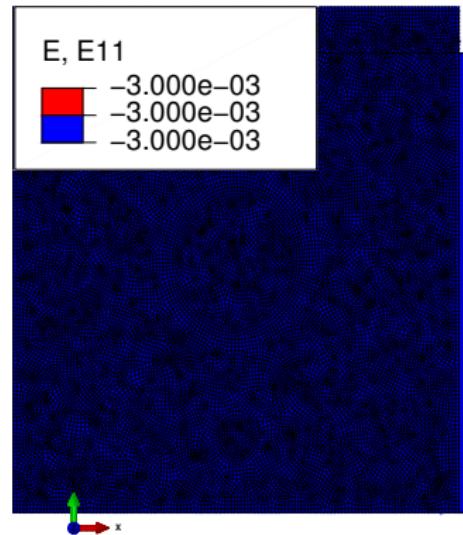
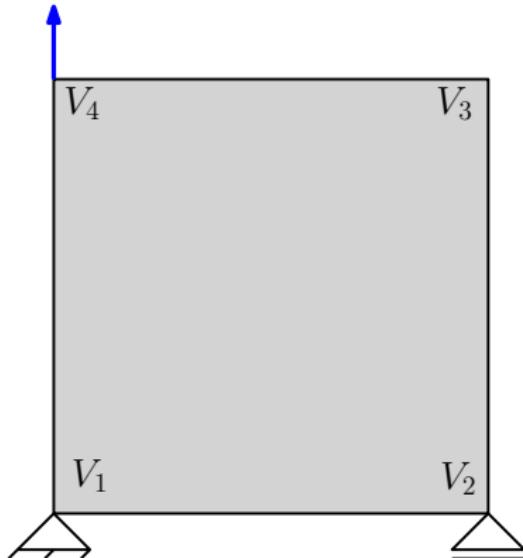
- ▶ $\mathbf{F} = \begin{pmatrix} \frac{\partial x_1}{\partial X_1} & \frac{\partial x_1}{\partial X_2} \\ \frac{\partial x_2}{\partial X_1} & \frac{\partial x_2}{\partial X_2} \end{pmatrix}$
- ▶ $\mathbf{x} = \mathbf{X} + \mathbf{u} \quad \rightarrow \mathbf{F} = \mathbf{I} + \begin{pmatrix} \frac{\partial u_1}{\partial X_1} & \frac{\partial u_1}{\partial X_2} \\ \frac{\partial u_2}{\partial X_1} & \frac{\partial u_2}{\partial X_2} \end{pmatrix}$



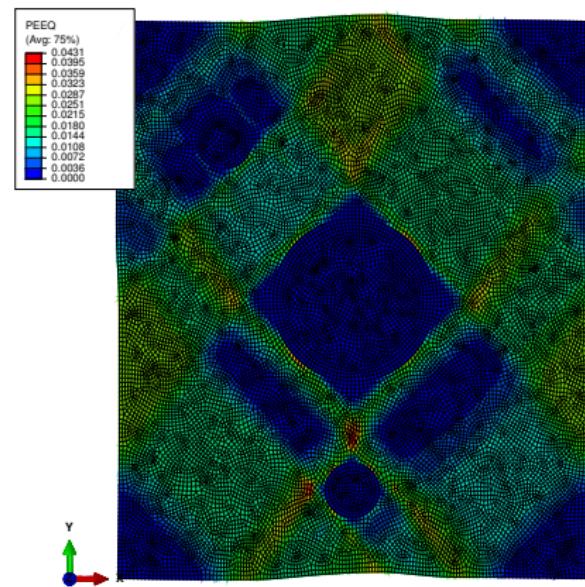
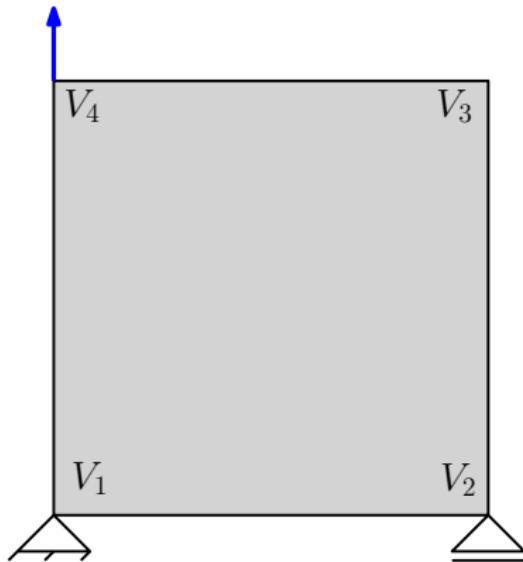
- ▶ Prescribing boundary conditions to vertices
 V_1, V_2, V_4 can present any arbitrary deformation gradient

Simple tension test

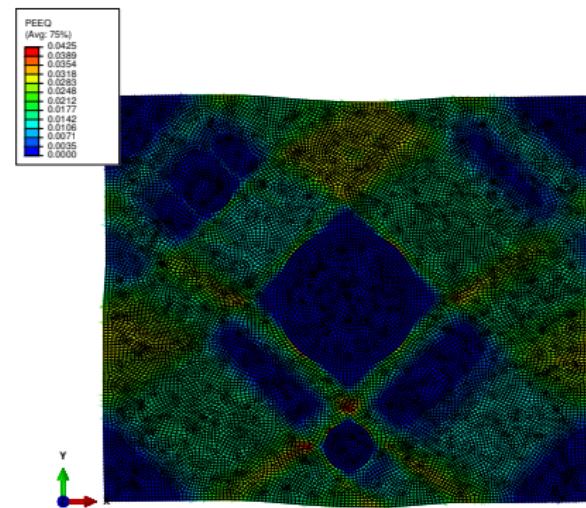
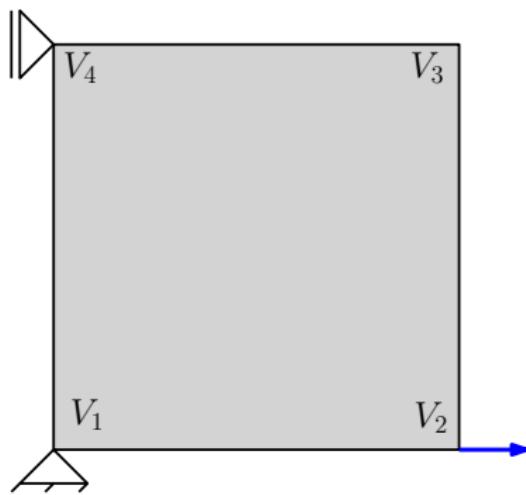
- ▶ Applied strain $\varepsilon_{yy} = 1\%$ due to displ. BC at V_4
- ▶ Due to Poisson's ratio ($\nu = 0.3$) $\rightarrow \varepsilon_{xx} = 0.3\%$ from analytics



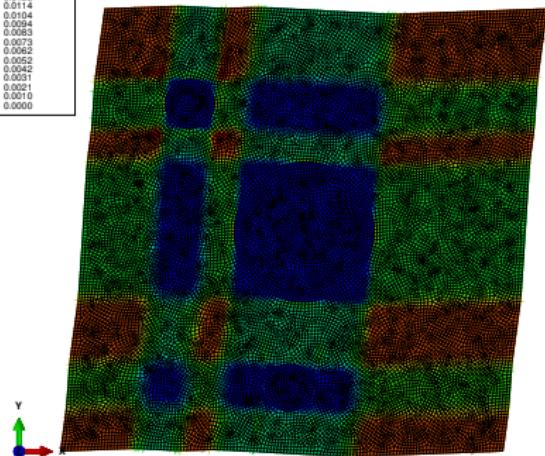
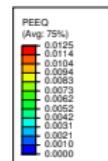
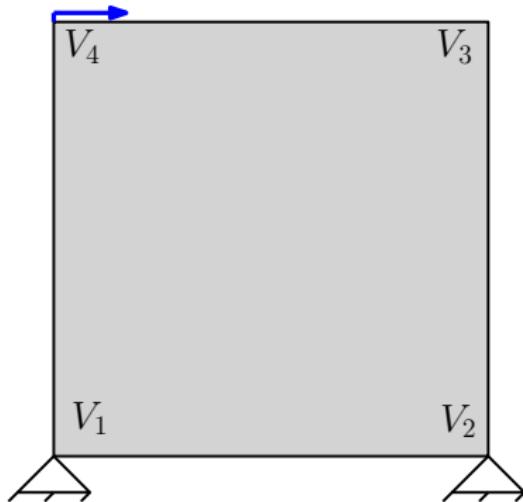
Complex tension test (Y-Dir)



Complex tension test (X-Dir)



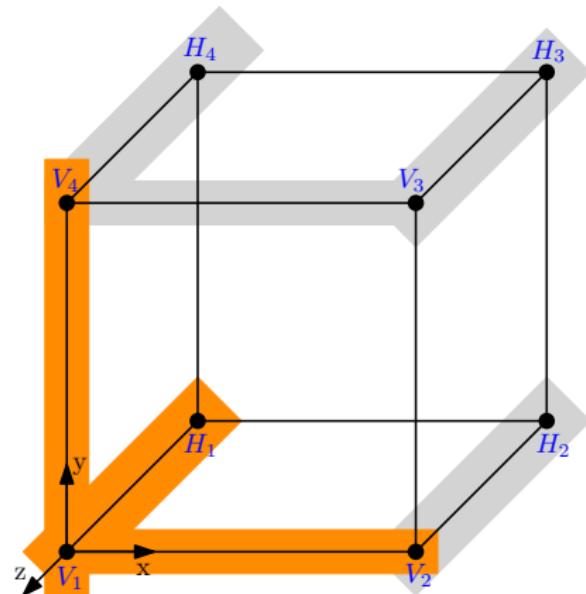
Shear test



Periodic boundary conditions - Abaqus implementation 3D

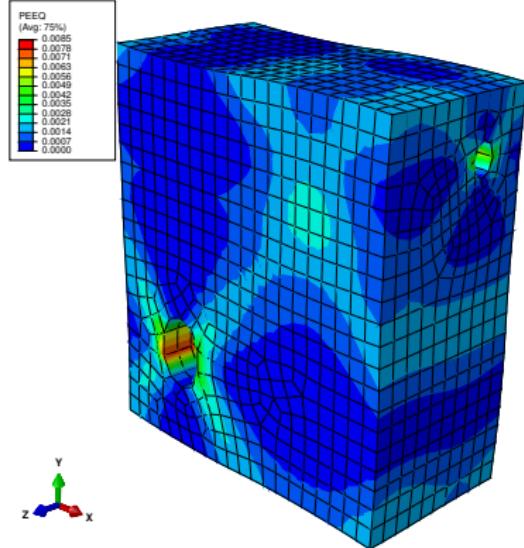
Procedure

- ▶ All surface nodes have to be coupled to opposite surface
- ▶ Special treatment for edge nodes and vertex nodes to avoid overconstraining
- ▶ Orange system is independent and deformation gradient can be prescribed
- ▶ Grey system is dependent and follows the applied deformation

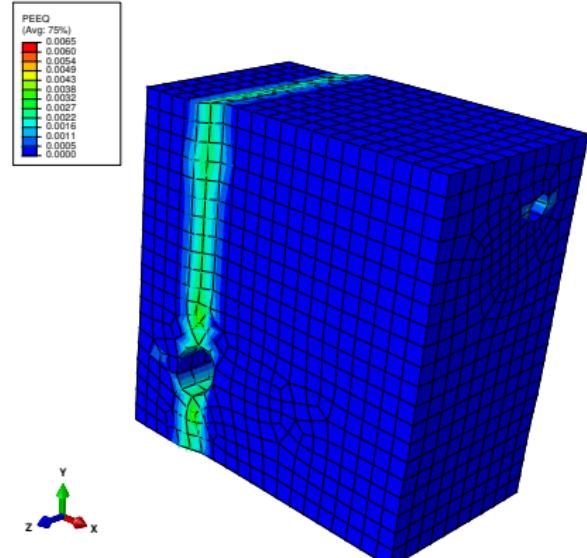


3D Applications

Tension test

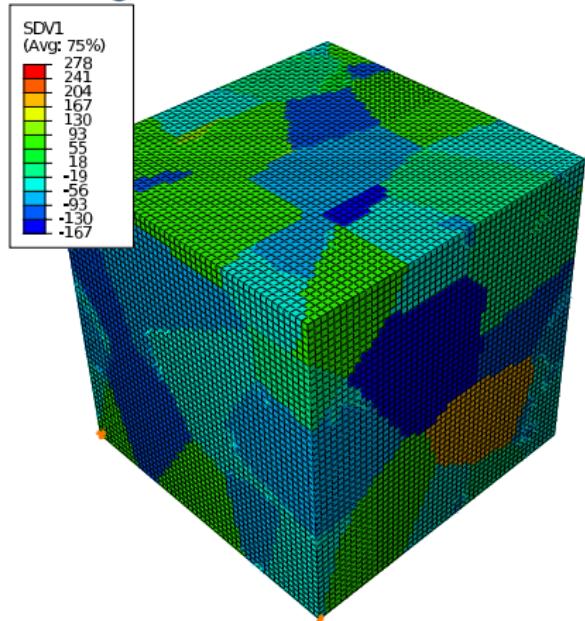


Shear test

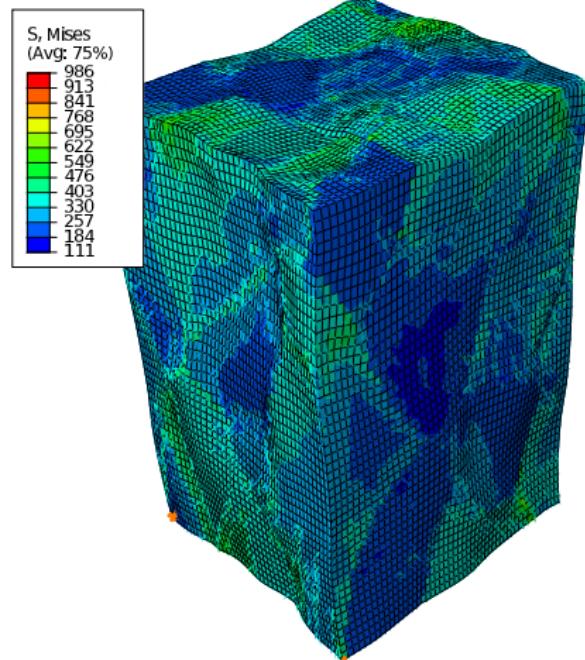


Periodic RVE

Initial grain orientation



Mises stress



Homogenisation approach

Averaged stress tensor

$$\bar{\sigma}_{\text{RVE}} = \frac{1}{V_{\text{RVE}}} \int_{\mathbf{y} \in V_{\text{RVE}}} \boldsymbol{\sigma}(\mathbf{y}) dV \quad (1)$$

$$\bar{\sigma}_{\text{RVE}} = \frac{1}{A} \text{sym} \left[(\mathbf{u}^{V4} - \mathbf{u}^{V1}) \mathbf{f}^{V4} + (\mathbf{u}^{V2} - \mathbf{u}^{V1}) \mathbf{f}^{V2} \right] \quad (2)$$