KNOWLES ELECTRONICS COMPANY

TECHNICAL NOTES ON THE USE OF THE BU 1771 ACCELEROMETER CARTRIDGE

These notes are intended as a guide to the use of the BU 1771 accelerometer cartridge. They should not be taken as a specification of this product.

1.0 <u>CONSTRUCTION</u>

The BU is a small, low mass accelerometer designed for use on light-weight structures. The inbuilt FET amplifier and high shock resistance also make this device, if mechanically protected, suitable for industrial applications.

The outer casing is type 305 stainless steel, epoxy sealed and with solder pad terminations. It may be safely "potted" with epoxy if required (provided that the temperatures resulting from exothermic reactions are maintained below 100°C).

Most other accelerometers use a high active mass to produce acceptable sensitivity to overcome problems of high impedance amplifiers on the end of long cables. Such a high mass can cause problems with a) weight b) shock susceptibility and c) change in mounted response.

The low mass piezo-electric element and integral FET amplifier overcomes such problems;

- 1) it withstands shocks in excess of 10,000g (half sine wave for $100 \, \mu \text{sec.}$)
- and 2) the dynamic (moving) mass is small (less than 10mgm) compared with the total BU mass (300mgm) so its resonance is little affected by the mass of the object upon which it is mounted.

Below 5KHz the transverse sensitivity is at least 20 dB below the main axis sensitivity.

2.0 MECHANICAL

2.1 <u>Use on Lightweight Structures</u> e.g. Circuit boards, body panels, windows, medical etc.

Use BU unencapsulated to keep low mass. Take care with soldering; use a low powered soldering iron with controlled temperature of 290° - 345°C. It may be necessary to strengthen the lead connections with epoxy adhesive.

Mounting

For use up to 5KHz, double sided tape is adequate. Above 5KHz cyanoa temperature beeswax is sufficient.

2.2 <u>Use for Machinery Monitoring</u>

The BU should be encapsulated in bubble-free epoxy in a metal housing with suitable mounting facilities.

It is recommended that the source follower mode is used for high accelerations; resistor R (voltage divider circuit) is encapsulated with the BU in the secondary housing which may be earthed. The BU in this application must be electrically insulated from the secondary housing.

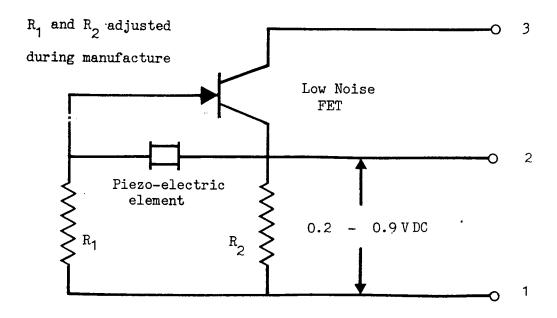
3.0 EFFECTS OF TEMPERATURE

The BU will operate at 70°C with a nominal 10% increase in sensitivity. It may be stored at 120°C without permanent degradation (it will not operate at this temperature), but care should be taken to avoid rapid temperature changes since these may set up stresses in the piezo-electric beam which will affect sensitivity.

4.0 <u>ELECTRICAL</u>

4.1 General

The piezo-electric element is connected internally to an FET amplifier as shown below



The case is electrically connected to terminal (1) via a resistance of less than 100Ω .

The transducer requires an external power supply which must be free from electrical noise. For the FET to operate, the voltage between terminals 1 and 3 must be greater than 1.1V; it may be destroyed by voltages in excess of 20V.

The power requirement is low and could be supplied by a battery. The put impedance of the BU is dependent upon mode of operation but generally it is low enough to drive several feet of cable without special amplifiers.

Three common methods of use are:

1) 3-wire mode

- simple connection of DC supply across terminals 1 and 3 then output taken from terminal 2 - high sensitivity mode.

2) 2-wire mode

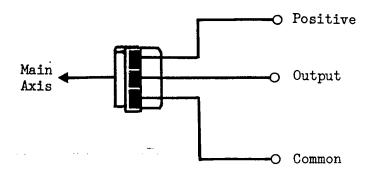
- uses only terminals 1 and 3, for situations where only two connecting wires to the transducer are available.

3) Source - follower mode

- for measurements of high accelerations.

BU 1771 is tested and specified in 2-wire mode, its sensitivity and spread in sensitivity will change for other modes of operation.

4.2 3-Wire Mode - typical performance



N.B. $g = 981 \text{ cm/sec}^2$

- 1. Supply voltage: 1.5V DC (range 1.1 to 20V)
- 2. Standing Current: 30 μA DC (range 20 50 μA)
- 3. Output Impedance: 13KΩ (range 8 22KΩ)
- 4. Response : See Section 6.
- 5. Sensitivity at 1KHz: 30 mV/g, i.e. 30 mV/g. Appical
- 6. Typical Minimum g : at 1KHz for 6 dB signal to noise .003 g or 3 cm/sec²
- 7. Typical Maximum g (peak) : limited by electrical "clipping". The maximum negative electrical excursion of the output may be typically 0.3V (range 0.2 to 0.9V and governed by production tolerances).

The signal will begin to 'clip' on a negative going acceleration of 0.3V which is typically 10g. sensitivity

At resonance the sensitivity is 40 dB higher so clipping occurs (in this instance) at 0.10g.

The FET will cease operation when the voltage across it is reduced below nominally 0.2V.

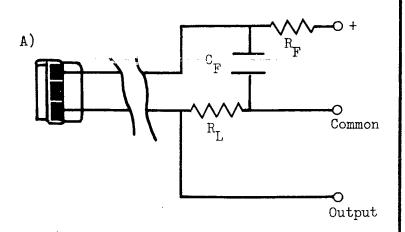
The maximum positive excursion is therefore

$$V_{\text{supply}} - (0.3 + 0.2) = 1V$$

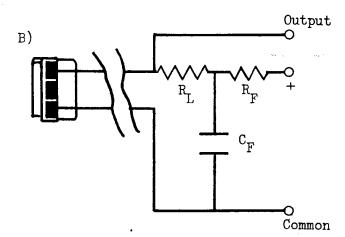
8. Phase Acceleration directed to the arrowed direction of the main axis results in a positive output.

4.3 <u>2-Wire Mode</u>

- Where only two connecting leads are available.



Same phase as 3 wire mode Case must not be grounded



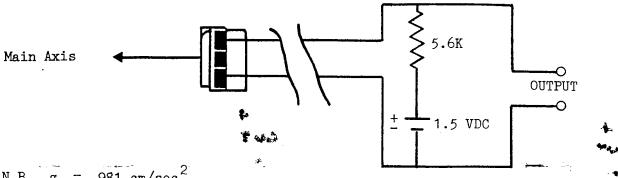
Reversed phase Case grounded Power supply 'feed through' is higher.

$$R_{_{\rm F}}$$
 $\, \leqslant \,$ 2K $\! \Omega$, $\,$ $\,$ $\,$ $\,$ $\,$ C $_{_{\rm F}}$ $\, \geqslant$ 1 $\,\mu f$, $\,$ R $_{_{\rm T}}$ $\,$ $\,$ $\,$ 20K $\! \Omega$ (typically 4K $\! \Omega$)

A change to $\mathbf{R}_{\text{T.}}$ will alter the sensitivity of the circuit.

 $\rm R_F$ and $\rm C_F$ decouple the power supply and are not necessary if battery powered, or supply ripple is very low.

Typical results for 2-wire (type B) connection



 $g = 981 \text{ cm/sec}^2$

1. Supply Voltage 1.5V DC. (range 1.1 to 20V)

2. Standing Current 30 µA DC (range 20 to 50 µA)

3. Output Impedance 5.2K Ω (range 4.9K Ω to 5.5K Ω)

4. Response See section 6.

5. Sensitivity at 1KHz nominal -45 dB re 1V/g i.e. 5.6 mV/g range -49.5 to -40.4 dB i.e. 3.3 to 9.4 ml/g

6. Noise (A weighted) -103 dB max re 1V i.e. $7 \mu V$ max.

at 1KHz for 6 dB signal to noise 7. Typical Minimum g .003 g i.e. 3 cm/sec^2

8. Typical Maximum g (peak) limited by electrical "clipping"

For a standing current of 30 µA (governed by production tolerances) and a load resistor of $5.6 \mathrm{K}\Omega$ the maximum positive electrical excursion of the output will be

$$30 \times 10^{-6} \times 5.6 \times 10^{3} = 0.168V$$

The negative excursion is limited by the internal 22KO resistance (and the approximately 0.2 minimum voltage across the transistor) for this device the maximum negative excursion will be

$$\left(\frac{1.5 - 0.2}{22000 + 5600} - 3 \times 10^{-6}\right) \qquad 5600 = 0.095V$$

The signal will begin to 'clip' on negative excursions of

$$\frac{0.095}{\text{sensitivity}} = 17 \text{ g (peak)}$$

At resonance the sensitivity is 40 dB higher so in this instance clipping will occur at 0.17 g.

9. Acceleration directed to the arrowed direction of the Phase

4.4. <u>Source-follower Mode</u>

This method of connection overcomes the problem of electrically limiting the output due to the operating point of the FET amplifier.

Two examples are:

V/2

A)

Output

3

V/2

V/2

Common

Common

Dual Supply

Case earthed

Voltage Divider

Case not earthed. Adjust R_2 until half the DC supply volts appear at terminal 3. R_4 typically $47K\Omega$

Typical results for voltage divider connection

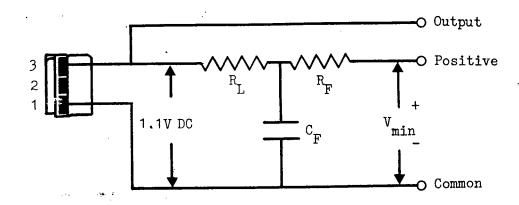
- 1. Supply (V) 20VDC (range 1.1 to 20V)
- 2. $R_1 = 47K\Omega$
- 3. When 10V at terminal 3 $R_2 \sim 20 \mathrm{K}\Omega$
- 4. Response : See section 6.
- 5. Sensitivity at 1KHz -45 dB re lV/g i.e. 5.6 mV/g
- 6. Noise : From the transducer 7µV max. but care must be taken with screening because case is not earthed.
- 7. Maximum g (peak) : before electrical "clipping"

Electrically the output may move by $\frac{\pm}{V/2}$.

Maximum g before clipping = $\frac{V/2}{\text{sensitivity}}$ which in this case is 1780 g at 1KHz and 17 g at resonance.

5.0 Supply Voltage

DC potential between terminals 1 and 3 should be greater than 1.1V for satisfactory operation.



Consider the above 2 wire circuit. Maximum standing current is 50 μA then the supply volts V_{\min} to give 1.1V across the BU is given by

If
$$R_{T_{.}} = 4K\Omega$$
 and $R_{F} = 2K\Omega$

then

$$V_{min} = 1.1 + 50 \times 10^{-6} (R_F + R_L)$$

= 1.4V typically

In practice BU will draw less than 50 μA therefore it could operate on lower supplies.

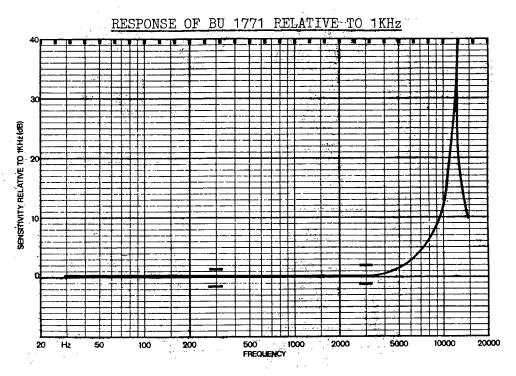
Little direct benefit may be gained by increasing the supply voltage above V because the sensitivity will be nominally unaltered.

However if both ${\bf R}_{\rm L}$ and the supply voltage are increased the sensitivity may be raised substantially, but it should be noted that the 'g' for overload will not be appreciably altered. For this type of operation ${\bf R}_{\rm L}$ is adjusted so that approximately $V/_2$ appears between terminals 1 and 3. The output impedance is then slightly less than ${\bf R}_{\rm L}$.

6.0 RESPONSE

Device Conformity (2 wire Mode)

Frequency (Hz) 300	Range of Deviation from 1KHz(dB)-	
	- 1.5	+ 1.5
1000	0	0
3000	- 1.0	+ 2.0



Sensitivity (at 1KHz)

2 wire connection with 5.6K source

nominal

5.6 mV/g

minimum

3.3 mV/g

maximum

9.4 mV/g