

Vibrations

small angles: $\cos \theta = 1$
 $\sin \theta = \theta$
rad!

1. Equilibrium (sometimes)
2. Dynamic: $\text{defl} = \delta + \delta y$
3. ① into ②... form $\ddot{x} + \omega_n^2 x = 0$
4. ω_n
5. $\phi = \dots$
6. solve A, B / C

Free undamped Vibrations.

$$x: \Sigma F = ma$$

Performing for a single weight, single spring:

$$\ddot{x} + \omega_n^2 x = 0$$

y: Equilibrium:

$$-k \delta_{st} + mg = 0$$

$$\delta_{st} \text{ (static deflection)} = \frac{mg}{k}$$

Dynamics:

$$\Sigma F = ma \Rightarrow$$

$$-k \delta_{st} - ky + mg = m\ddot{y}$$

$$\ddot{y} + \omega_n^2 y = 0$$

Get into this form with methods above.

DE Solutions

$$(1) x = A \sin \omega_n t + B \cos \omega_n t$$

from initial conditions.

derive for \dot{x}, \ddot{x} and plug in to find A, B.

$$(2) x = C \sin (\omega_n t + \phi)$$

Amplitude

phase angle

from initial conditions

$$\text{natural, circular freq: } \omega_n = \sqrt{\frac{k}{m}}$$

$$\text{natural freq: } f = \frac{\omega_n}{2\pi} = \frac{1}{2\pi} \sqrt{\frac{k}{m}} = \frac{1}{T} \sim \text{period}$$

1. Equilibrium (y_{st})
 $\frac{\partial F_y}{\partial F_z} / \epsilon M$ 2. Dynamic
 $Disp = (y_{st} + y)$
 3. form $\ddot{y} + \omega_n^2 y = \frac{F_0}{m} \cos \omega t$
 4. $x_c; x_p$

Undamped forced vibrations:

(force acting: $F = F_0 \sin \omega_0 t$)

$$\ddot{x} + \omega_n^2 x = \frac{F_0}{m} \sin(\omega_0 t)$$

$$\omega_n = \sqrt{\frac{k}{m}}$$

DE Solution: $x = x_c + x_p$

Transient solution: $x_c = C \sin(\omega_n t + \phi)$

Steady state solution: $x_p = \left(\frac{F_0/k}{1 - (\omega_0/\omega_n)^2} \right) \sin \omega_0 t$

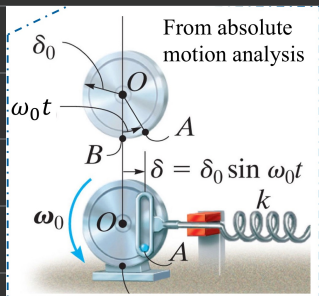
$$\gamma = \frac{2\pi}{\omega_0} \quad \text{Amp } |x| = \left| \frac{F_0/k}{1 - (\omega_0/\omega_n)^2} \right|$$

Magnification factor: $M = \frac{x}{F_0/k} = \frac{1}{1 - (\omega_0/\omega_n)^2}$

Resonance will occur when $\omega_0 \rightarrow \omega_n$



Support displacement:



$$\ddot{x} + \omega_n^2 x = \frac{k \delta_0}{m} \sin \omega_0 t \quad \frac{F_0}{k}$$

$$x = \left(\sin(\omega_n t + \phi) + \left[\frac{\delta_0}{1 - (\omega_0/\omega_n)^2} \right] \sin \omega_0 t \right) \frac{F_0}{k}$$

if we have
multiple spring/damper
th.s will change

1. Static (if there is static deflection)
2. Dynamic ($y_{st} + y$)
3. Form $m\ddot{y} + c\dot{y} + ky \rightarrow$
4. Find λ from $m\lambda^2 + c\lambda + k = 0$
5. c_c

Free, damped vibrations.

$$m\ddot{x} + c\dot{x} + kx = 0 \rightarrow m\lambda^2 + c\lambda + k = 0$$

where c is damping coefficient.

$$\lambda_{1,2} = \frac{-c}{2m} \pm \sqrt{\left(\frac{c}{2m}\right)^2 - \frac{k}{m}} \sim \Delta$$

If more than
1 spring / damper:
set $\Delta = 0$

critical damping coefficient: $c_c = 2m\omega_n = 2m\sqrt{\frac{k}{m}}$

\Rightarrow damping factor $\zeta = \frac{c}{c_c}$

Overdamp: $c > c_c$ ($\zeta > 1$)

$$x = A e^{\lambda_1 t} + B e^{\lambda_2 t}$$

(λ_1, λ_2 real)

no oscillations

Critically damped: $c = c_c$ ($\zeta = 1$)

$$x = (A + Bt)e^{-\omega_n t}$$

Underdamped: $c < c_c$ ($\zeta < 1$)

$$x = D e^{-\left(\frac{c}{2m}\right)t} \sin(\omega_d t + \phi)$$

(λ_1, λ_2 complex)

Damped natural freq: $\omega_d = \omega_n \sqrt{1 - \left(\frac{c}{c_c}\right)^2}$

period of damped vibration: $T_d = \frac{2\pi}{\omega_d}$

A general approach : ① if there is static deflection:

↳ Equilibrium

② Dynamics

↳ $\Sigma F_x / \Sigma F_y / \Sigma M$

③ using ① and ② find function
in std. form.

④ Derive / Use solutions.