

Continuous System

What does jello look like in space?



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Equations of Motion

Newton's Law:

$$d\mathbf{F} = \ddot{\mathbf{R}} dm$$

Force Vector:

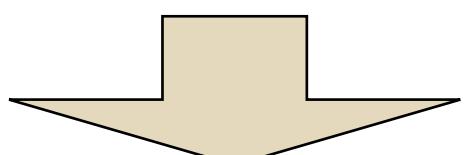
$$d\mathbf{F} = d\mathbf{F}_E + d\mathbf{F}_I$$

Total Force acting
on System:

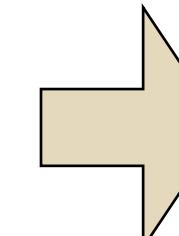
$$\mathbf{F} = \int_B d\mathbf{F} = \int_B d\mathbf{F}_E$$

Center of Mass:

$$M\mathbf{R}_c = \int_B \mathbf{R} dm = \int_{\mathcal{B}} (\mathbf{R}_c + \mathbf{r}) dm \rightarrow \int_{\mathcal{B}} \mathbf{r} dm = \mathbf{0}$$

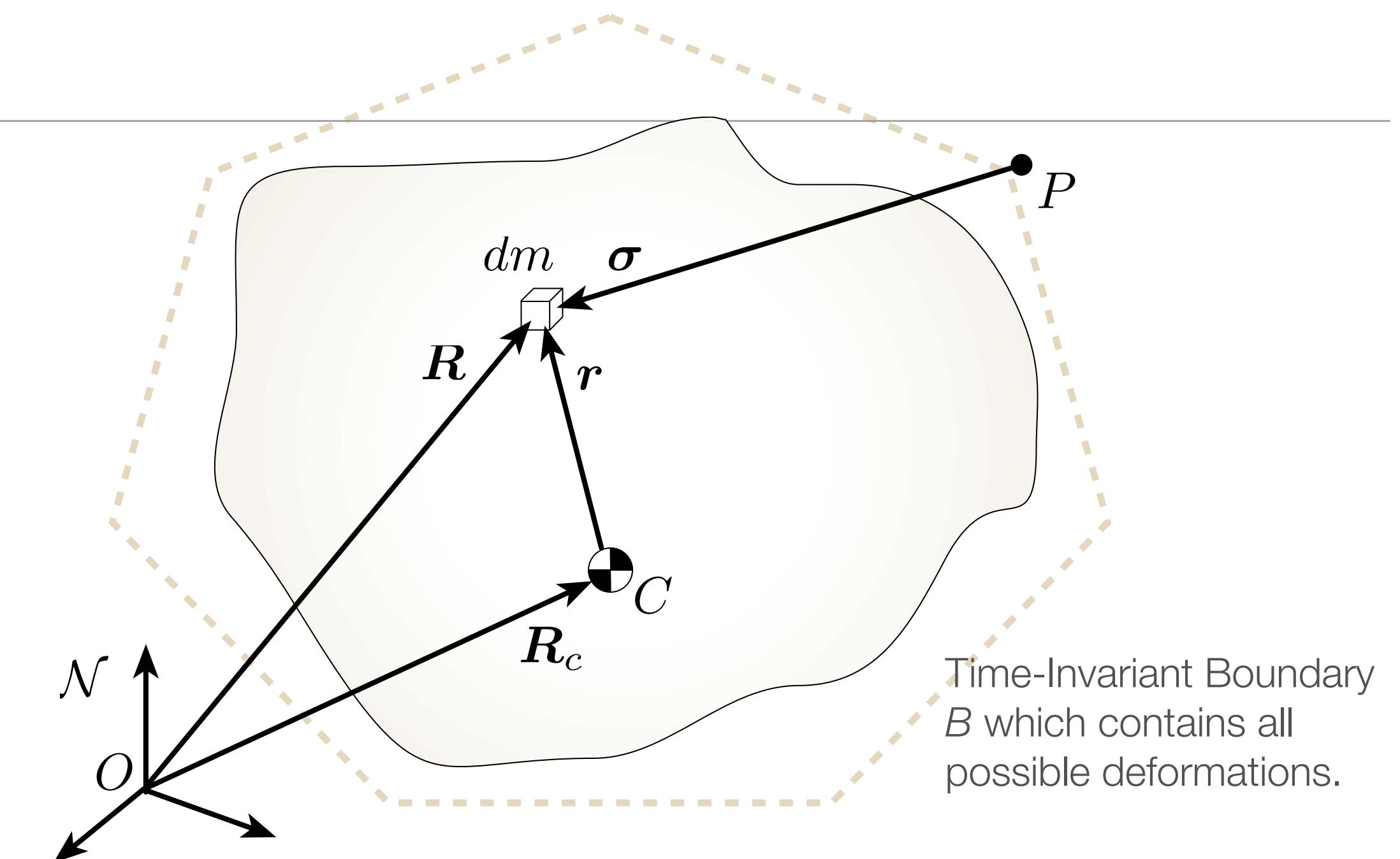


$$M\ddot{\mathbf{R}}_c = \int_B \ddot{\mathbf{R}} dm = \int_B d\mathbf{F}$$



$$M\ddot{\mathbf{R}}_c = \mathbf{F}$$

Super Particle Theorem



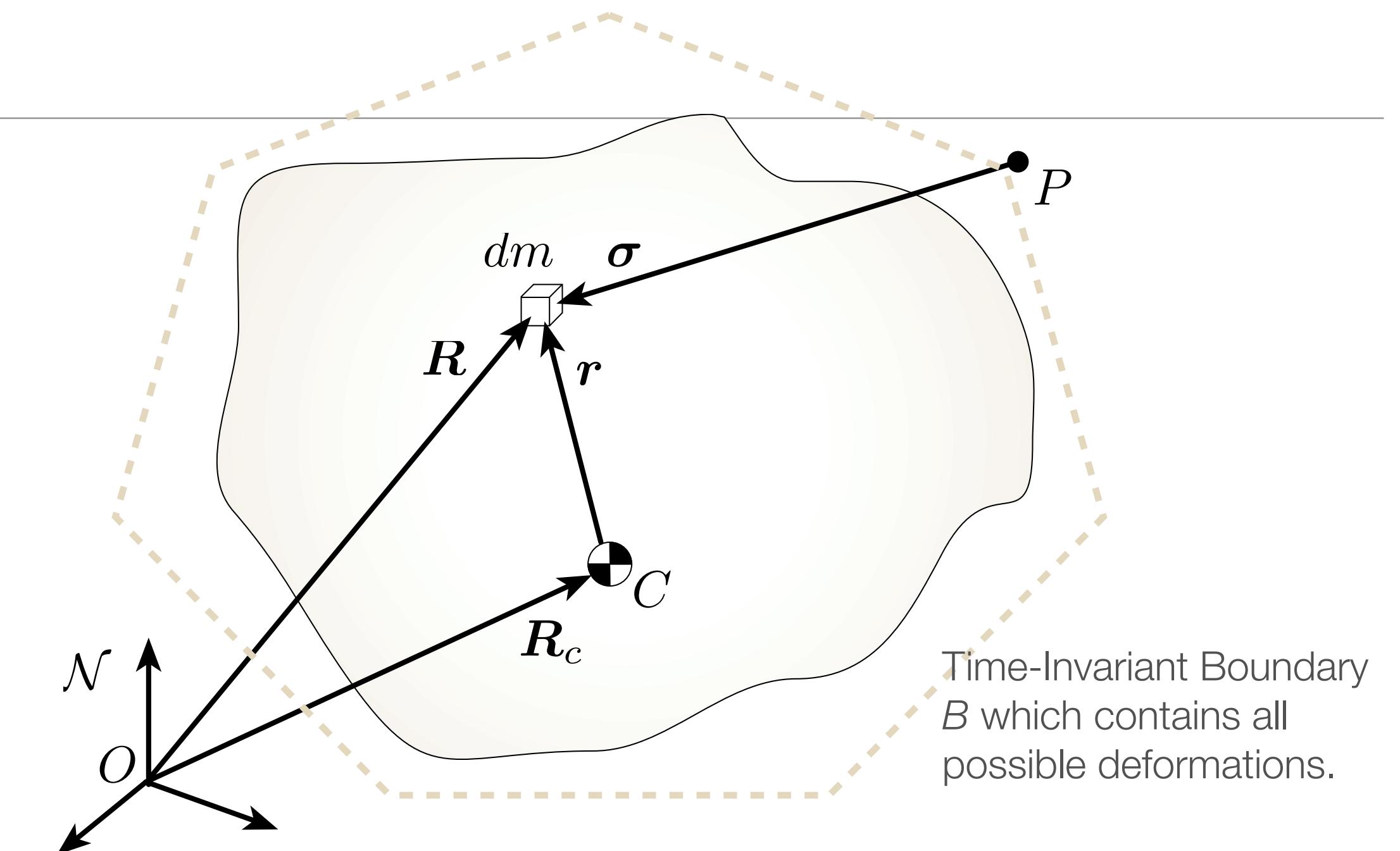
Kinetic Energy

Definition:

$$T = \frac{1}{2} \int_B \dot{\mathbf{R}} \cdot \dot{\mathbf{R}} dm$$

$$\dot{\mathbf{R}} = \dot{\mathbf{R}}_c + \dot{\mathbf{r}}$$

$$T = \frac{1}{2} \left(\int_B dm \right) \dot{\mathbf{R}}_c \cdot \dot{\mathbf{R}}_c + \cancel{\dot{\mathbf{R}}_c \cdot \cancel{\dot{\mathbf{r}} dm}} + \frac{1}{2} \int_B \dot{\mathbf{r}} \cdot \dot{\mathbf{r}} dm$$



$$T = \frac{1}{2} M \dot{\mathbf{R}}_c \cdot \dot{\mathbf{R}}_c + \frac{1}{2} \int_B \dot{\mathbf{r}} \cdot \dot{\mathbf{r}} dm$$

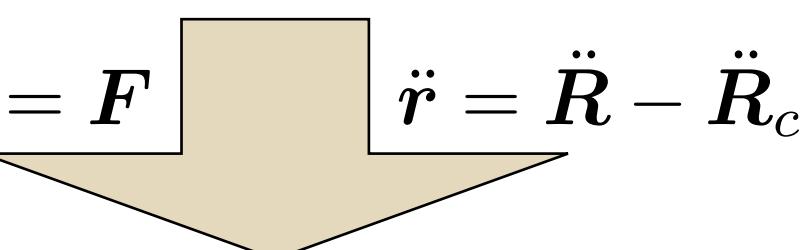
Energy of CM

Energy about CM

Work/Energy Principle

Differentiate Energy:

$$\frac{dT}{dt} = M \ddot{\mathbf{R}}_c \cdot \dot{\mathbf{R}}_c + \int_B \dot{\mathbf{r}} \cdot \ddot{\mathbf{r}} dm$$

$$M \ddot{\mathbf{R}}_c = \mathbf{F}$$

$$\ddot{\mathbf{r}} = \ddot{\mathbf{R}} - \ddot{\mathbf{R}}_c$$

$$\frac{dT}{dt} = \mathbf{F} \cdot \dot{\mathbf{R}}_c + \int_B (\ddot{\mathbf{R}} dm) \cdot \dot{\mathbf{r}} - \ddot{\mathbf{R}}_c \cdot \cancel{\int_B \dot{\mathbf{r}} dm}$$

C.M.

$$\frac{dT}{dt} = \mathbf{F} \cdot \dot{\mathbf{R}}_c + \int_B d\mathbf{F} \cdot \dot{\mathbf{r}}$$

$$T(t_2) - T(t_1) = \int_{\mathbf{R}(t_1)}^{\mathbf{R}(t_2)} \mathbf{F} \cdot \dot{\mathbf{R}}_c d\mathbf{R}_c + \int_{t_1}^{t_2} \int_{\mathbf{r}(t_B)}^{\mathbf{r}(t_2)} d\mathbf{F} \cdot d\mathbf{F} \cdot d\mathbf{r}$$

Work energy/principle for system of particles



Linear Momentum

Definition:

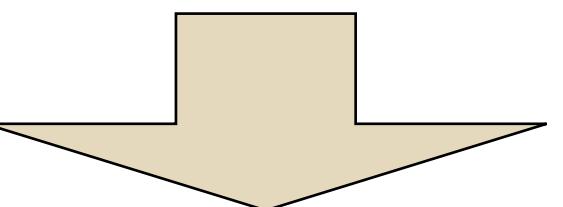
$$dp = \dot{R}dm$$

$$p = \int_{\mathcal{B}} dp = \int_{\mathcal{B}} \dot{R}dm = \int_{\mathcal{B}} (\dot{R}_c + \dot{r})dm = \left(\int_{\mathcal{B}} dm \right) \dot{R}_c + \cancel{\int_{\mathcal{B}} \dot{r}dm}$$

$$p = M \dot{R}_c$$

Linear Momentum
Rate:

$$\dot{p} = \int_{\mathcal{B}} \ddot{R}dm = \int_{\mathcal{B}} dF = F$$



$$F = \frac{N_d}{dt} (p)$$



Angular Momentum

Ang. Momentum about P : $\mathbf{H}_P = \int_B \boldsymbol{\sigma} \times \dot{\boldsymbol{\sigma}} dm$

$$\boldsymbol{\sigma} = \mathbf{R} - \mathbf{R}_P$$

Inertial Time Derivative: $\dot{\mathbf{H}}_P = \cancel{\int_B \dot{\boldsymbol{\sigma}} \times \dot{\boldsymbol{\sigma}} dm} + \int_B \boldsymbol{\sigma} \times \boxed{\ddot{\boldsymbol{\sigma}}} dm$

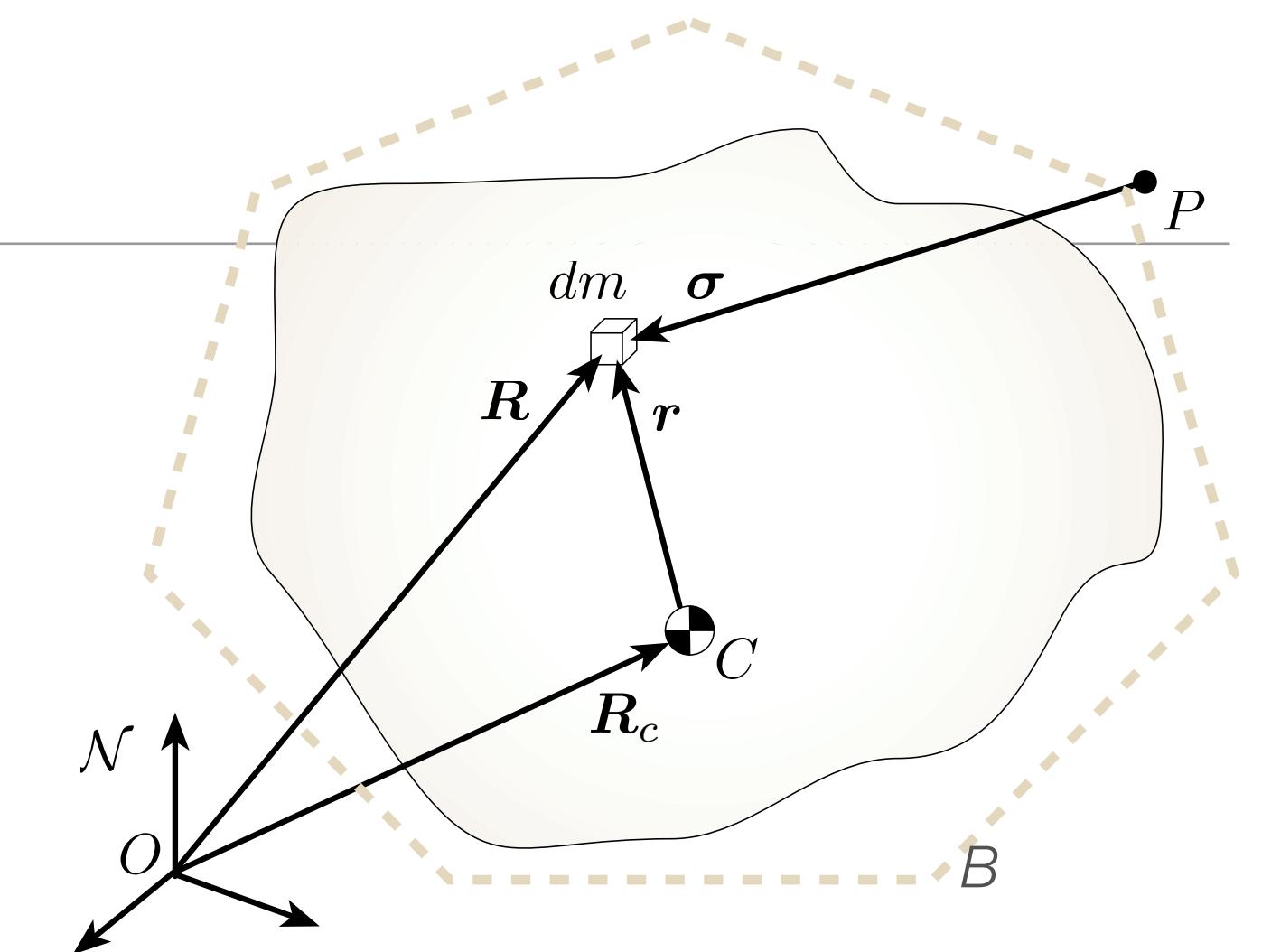
$$\dot{\mathbf{H}}_P = \boxed{\int_B \boldsymbol{\sigma} \times \ddot{\mathbf{R}} dm} - \boxed{\left(\int_B \boldsymbol{\sigma} dm \right)} \times \ddot{\mathbf{R}}_P$$

$$\int_B \boldsymbol{\sigma} dm = \int_B \mathbf{R} dm - \left(\int_B dm \right) \mathbf{R}_P = \boxed{M(\mathbf{R}_c - \mathbf{R}_P)}$$

Torque about P : $\mathbf{L}_P = \boxed{\int_B \boldsymbol{\sigma} \times \ddot{\mathbf{R}} dm} = \int_B \boldsymbol{\sigma} \times d\mathbf{F}$

$$\dot{\mathbf{H}}_P = \mathbf{L}_P + M \ddot{\mathbf{R}}_P \times (\mathbf{R}_c - \mathbf{R}_P)$$

$\Rightarrow \boxed{\dot{\mathbf{H}}_P = \mathbf{L}_P}$
If P is CM or Inertial



Rigid Body Dynamics

The 101 of spacecraft dynamics...



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General Angular Momentum

Definition:

$$\mathbf{H}_O = \int_B \mathbf{R} \times \dot{\mathbf{R}} dm$$

or

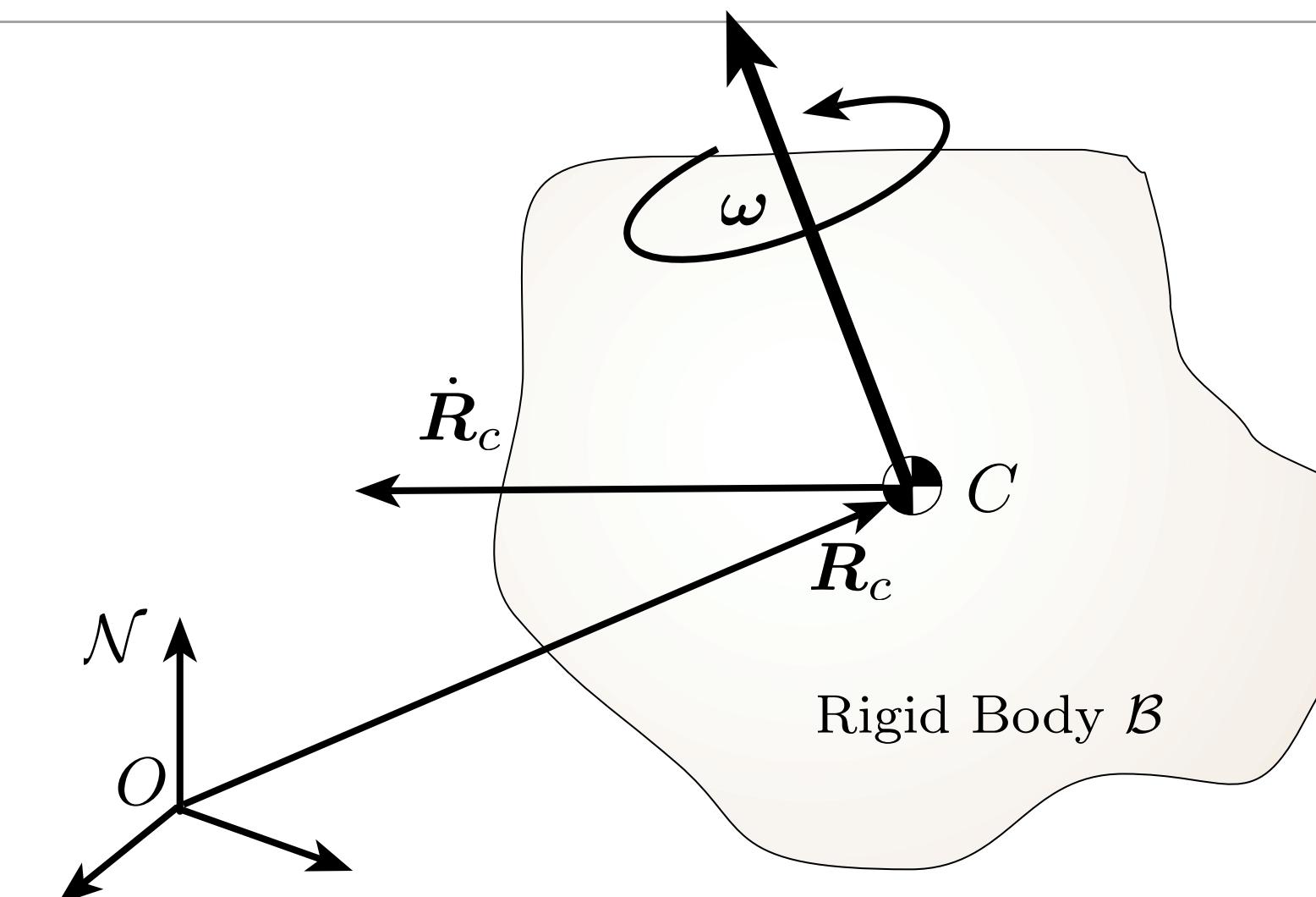
$$\mathbf{H}_O = \mathbf{R}_c \times M \dot{\mathbf{R}}_c + \int_B \mathbf{r} \times \dot{\mathbf{r}} dm$$

Momentum about CM:

$$\mathbf{H}_c = \int_B \mathbf{r} \times \dot{\mathbf{r}} dm$$

$$\dot{\mathbf{r}} = \frac{d\mathbf{r}}{dt} = \cancel{\frac{d\mathbf{r}}{dt}} + \omega \times \mathbf{r} = \omega \times \mathbf{r}$$

$$\mathbf{H}_c = \int_B \mathbf{r} \times (\omega \times \mathbf{r}) dm = \left(\int_B -[\tilde{\mathbf{r}}][\tilde{\mathbf{r}}] dm \right) \omega$$



Inertia Tensor Properties

Definition:

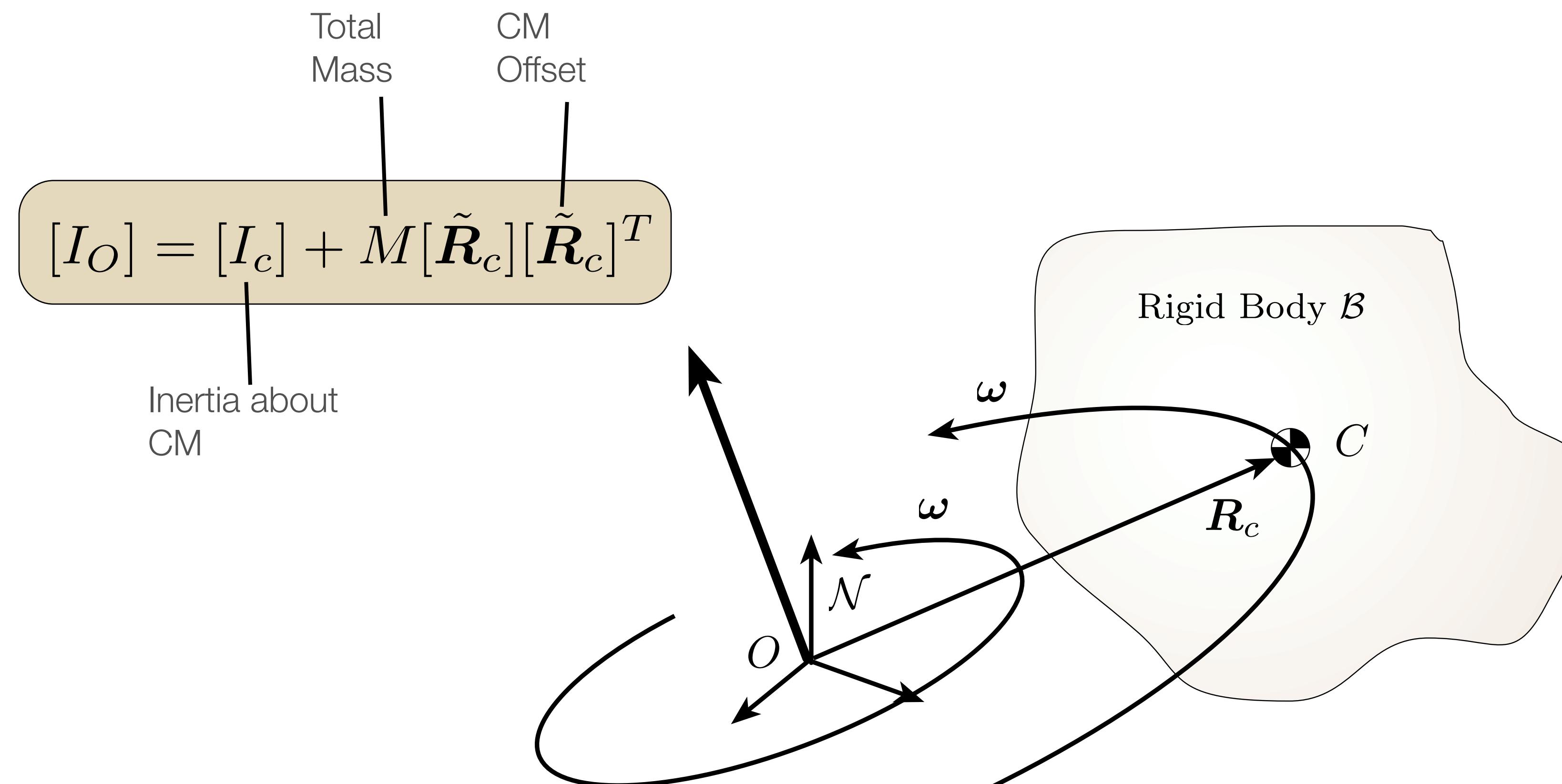
$$\mathcal{B}[I_c] = \int_B -[\tilde{\mathbf{r}}][\tilde{\mathbf{r}}]dm = \int_B \begin{bmatrix} r_2^2 + r_3^2 & -r_1r_2 & -r_1r_3 \\ -r_1r_2 & r_1^2 + r_3^2 & -r_2r_3 \\ -r_1r_3 & -r_2r_3 & r_1^2 + r_2^2 \end{bmatrix} dm$$

Angular Momentum Expression:

$$\mathbf{H}_c = \begin{pmatrix} \mathcal{B}(H_{c_1}) \\ \mathcal{B}(H_{c_2}) \\ \mathcal{B}(H_{c_3}) \end{pmatrix} = \int_B \begin{bmatrix} r_2^2 + r_3^2 & -r_1r_2 & -r_1r_3 \\ -r_1r_2 & r_1^2 + r_3^2 & -r_2r_3 \\ -r_1r_3 & -r_2r_3 & r_1^2 + r_2^2 \end{bmatrix} \begin{pmatrix} \mathcal{B}(\omega_1) \\ \mathcal{B}(\omega_2) \\ \mathcal{B}(\omega_3) \end{pmatrix} dm = [I_c]\boldsymbol{\omega}$$



Parallel Axis Theorem



Coordinate Transformation

$$\mathcal{F}[I] = [FB]^{\mathcal{B}}[I][FB]^T$$

B - Body Frame

F - 2nd Coordinate Frame

$$\begin{bmatrix} C_{11} & C_{12} & C_{13} \\ C_{21} & C_{22} & C_{23} \\ C_{31} & C_{32} & C_{33} \end{bmatrix}^{\mathcal{B}} \begin{bmatrix} I_{11} & I_{12} & I_{13} \\ I_{12} & I_{22} & I_{23} \\ I_{13} & I_{23} & I_{33} \end{bmatrix} = \begin{bmatrix} I_1 & 0 & 0 \\ 0 & I_2 & 0 \\ 0 & 0 & I_3 \end{bmatrix} \begin{bmatrix} C_{11} & C_{12} & C_{13} \\ C_{21} & C_{22} & C_{23} \\ C_{31} & C_{32} & C_{33} \end{bmatrix}$$

Rotation matrix [C]
contains the
eigenvectors of [I]

$$[C] = [V]^T = \begin{bmatrix} \mathbf{v}_1^T \\ \mathbf{v}_2^T \\ \mathbf{v}_3^T \end{bmatrix}$$

Principal inertia
matrix whose
diagonal entries
are the
eigenvalues of [I]



Kinetic Energy

Total Energy:

$$T = \frac{1}{2} M \dot{\mathbf{R}}_c \cdot \dot{\mathbf{R}}_c + \frac{1}{2} \int_B \dot{\mathbf{r}} \cdot \dot{\mathbf{r}} dm = T_{\text{trans}} + T_{\text{rot}}$$

Rotational Energy:

$$T_{\text{rot}} = \frac{1}{2} \int_B \dot{\mathbf{r}} \cdot \dot{\mathbf{r}} dm = \frac{1}{2} \int_B (\boldsymbol{\omega} \times \mathbf{r}) \cdot (\boldsymbol{\omega} \times \mathbf{r}) dm$$

$$T_{\text{rot}} = \frac{1}{2} \boldsymbol{\omega} \cdot \int_B \mathbf{r} \times (\boldsymbol{\omega} \times \mathbf{r}) dm = \frac{1}{2} \boldsymbol{\omega} \cdot \mathbf{H}_c = \frac{1}{2} \boldsymbol{\omega}^T [I] \boldsymbol{\omega}$$

Energy Rate:

$$\dot{T} = \mathbf{F} \cdot \dot{\mathbf{R}}_c + \mathbf{L}_c \cdot \boldsymbol{\omega}$$

Work/Energy Principle:

$$W = T(t_2) - T(t_1) = \int_{t_1}^{t_2} \mathbf{F} \cdot \dot{\mathbf{R}}_c dt + \int_{t_1}^{t_2} \mathbf{L}_c \cdot \boldsymbol{\omega} dt$$



Equations of Motion

Euler's equation:

$$\dot{\mathbf{H}}_c = \boxed{\frac{\mathcal{B}_d}{dt} (\mathbf{H}_c)} + \boldsymbol{\omega} \times \mathbf{H}_c = \mathbf{L}_c$$

$$\frac{\mathcal{B}_d}{dt} (\mathbf{H}_c) = \frac{\mathcal{B}_d}{dt} ([I]) \boldsymbol{\omega} + [I] \frac{\mathcal{B}_d}{dt} (\boldsymbol{\omega}) = [I] \dot{\boldsymbol{\omega}}$$

Euler's rotational
equations of motion:

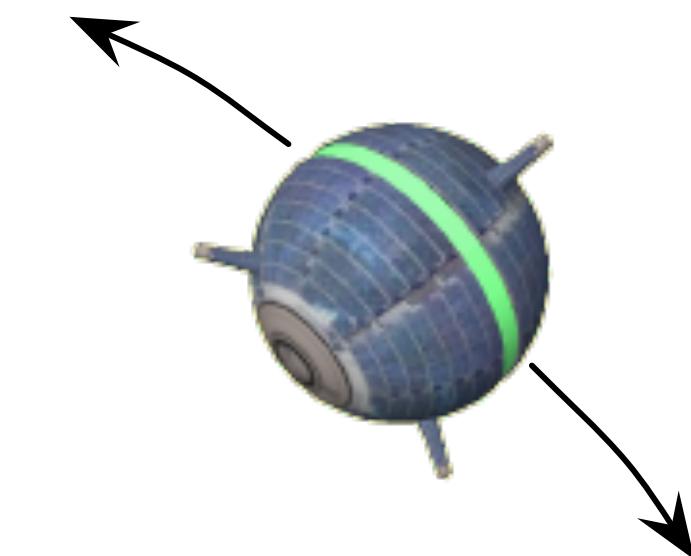
$$[I] \dot{\boldsymbol{\omega}} = -[\tilde{\boldsymbol{\omega}}] [I] \boldsymbol{\omega} + \mathbf{L}_c$$

Principal axis version of
rotational EOM:

$$I_{11} \dot{\omega}_1 = -(I_{33} - I_{22}) \omega_2 \omega_3 + L_1$$

$$I_{22} \dot{\omega}_2 = -(I_{11} - I_{33}) \omega_3 \omega_1 + L_2$$

$$I_{33} \dot{\omega}_3 = -(I_{22} - I_{11}) \omega_1 \omega_2 + L_3$$



Discuss how to integrate full EOM



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Example: Slender Rod Falling

Rod Inertia about CM: $I_c = \frac{m}{12}L^2$

Momentum about CM: $\mathbf{H}_c = I_c \dot{\theta} \hat{\mathbf{e}}_3$

Torque:

$$\mathbf{L}_c = \left(-\frac{L}{2} \hat{\mathbf{e}}_L \right) \times N \hat{\mathbf{n}}_2 = \frac{L}{2} N \sin \theta \hat{\mathbf{e}}_3$$

Euler's Eqn:

$$\dot{\mathbf{H}}_c = \mathbf{L}_c$$

$$\frac{m}{12} L^2 \ddot{\theta} - \frac{L}{2} N \sin \theta = 0$$

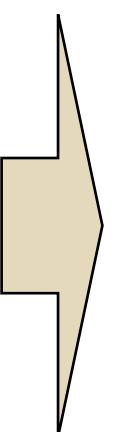
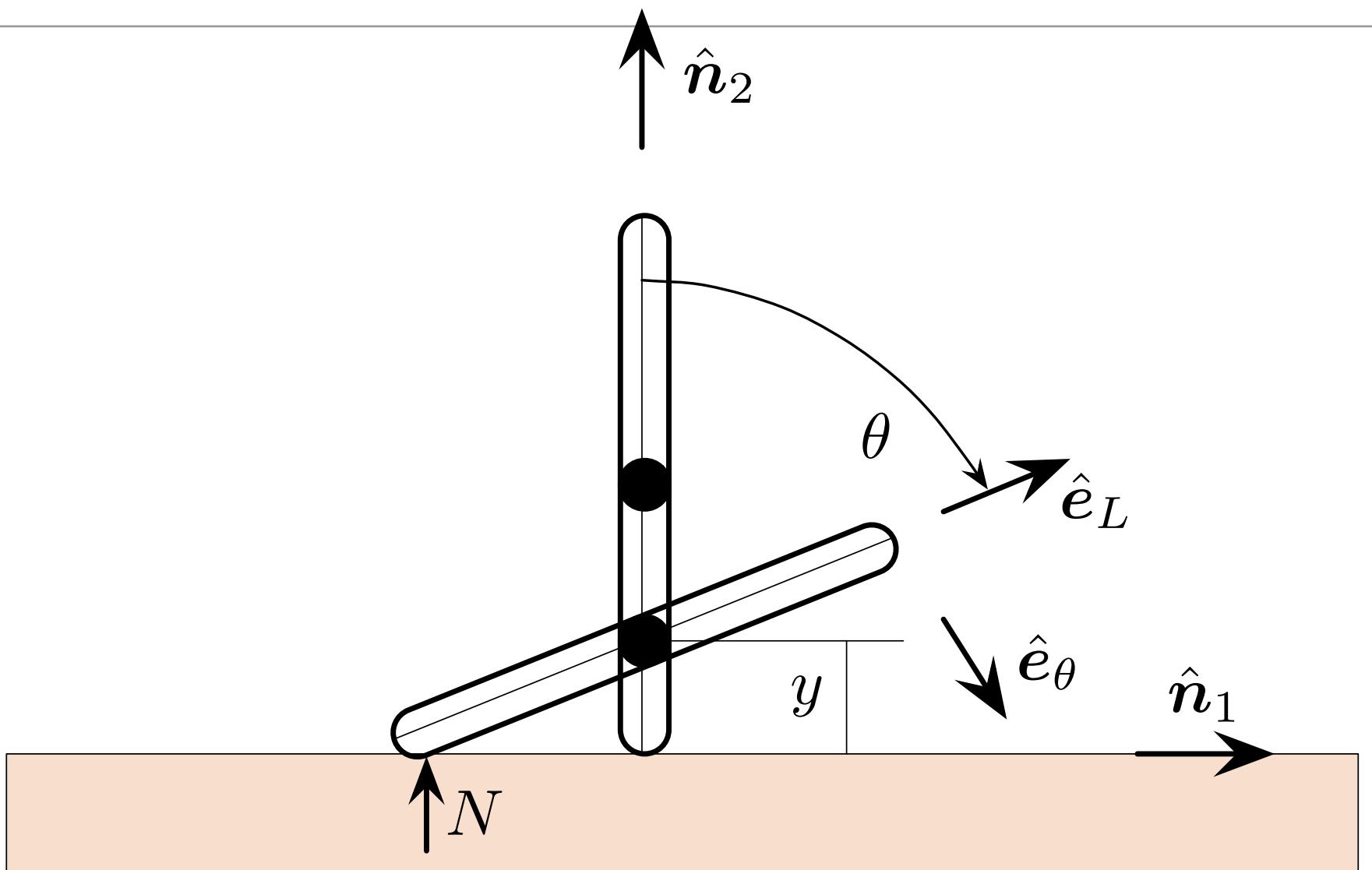
Newton's Eqn:

$$m \ddot{y} \hat{\mathbf{n}}_2 = (N - mg) \hat{\mathbf{n}}_2$$

$$y = \frac{L}{2} \cos \theta \quad \ddot{y} = -\frac{L}{2} \ddot{\theta} \sin \theta - \frac{L}{2} \dot{\theta}^2 \cos \theta$$

EOM:

$$\boxed{\frac{m}{12} L^2 \ddot{\theta} (1 + 3 \sin^2 \theta) + \frac{m}{4} L^2 \dot{\theta}^2 \sin \theta \cos \theta - \frac{m}{2} L g \sin \theta = 0}$$



$$N = mg - m \frac{L}{2} \ddot{\theta} \sin \theta - m \frac{L}{2} \dot{\theta}^2 \cos \theta$$



Example: Slender Rod Falling

Energy functions:

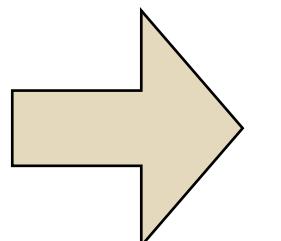
$$V(\theta) = mgy = mg\frac{L}{2} \cos \theta$$

$$T(\theta, \dot{\theta}) = \frac{m}{2}\dot{y}^2 + \frac{I_c}{2}\dot{\theta}^2 = \frac{mL^2}{24}(1 + 3\sin^2 \theta)\dot{\theta}^2$$

Initial energy level:

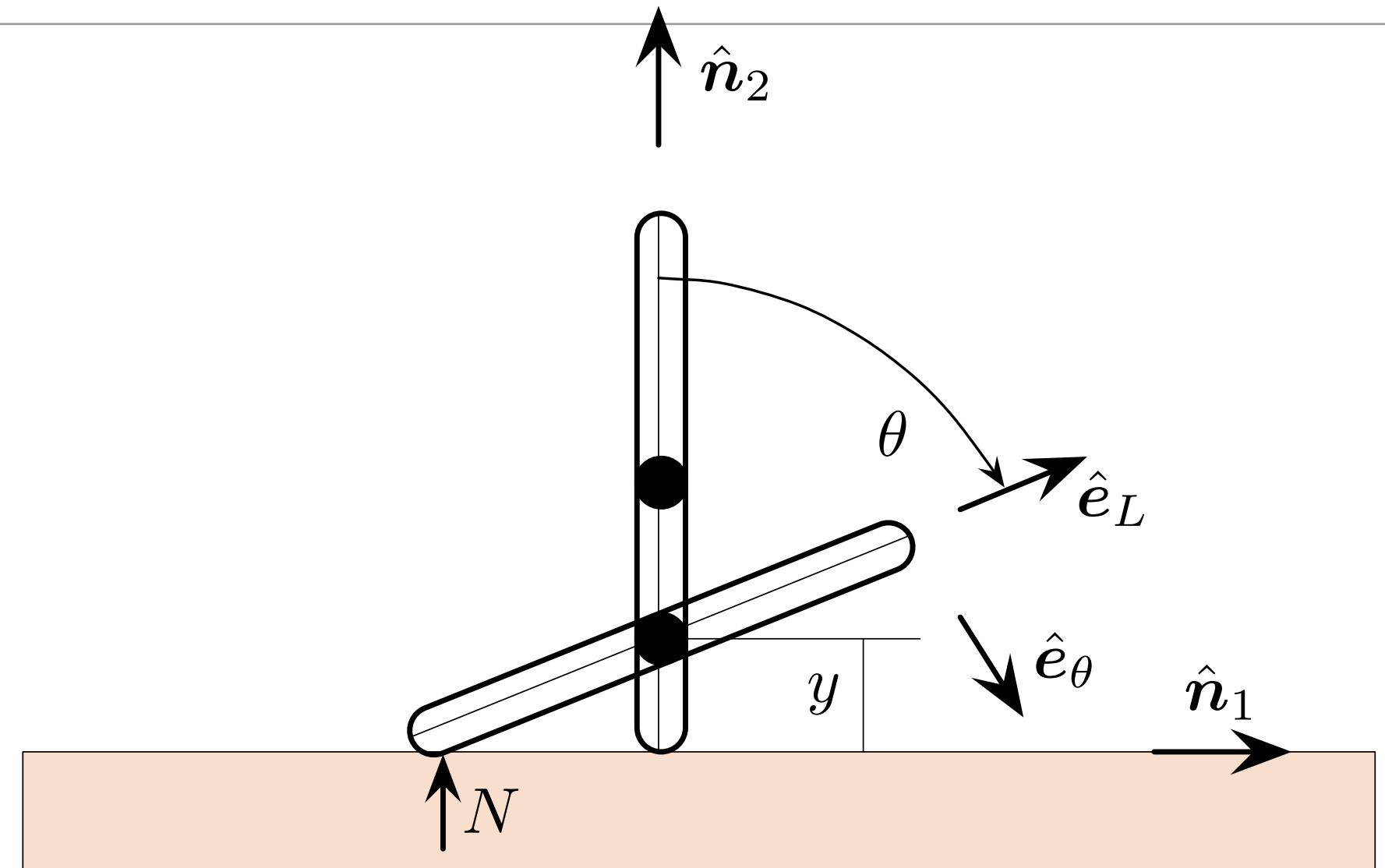
$$E(t_0) = T_0 + V_0 = mg\frac{L}{2}$$

$$T(\theta, \dot{\theta}) + V(\theta) = E(t_0)$$



$$\dot{\theta}^2 = \frac{12g(1 - \cos \theta)}{L(1 + 3\sin^2 \theta)}$$

Energy Conservation avoids having to solve ODE.



Momentum/Energy Surfaces

- Let's study a special class of rigid body motion where no external torque is acting on the body.
- In this case the kinetic energy and the angular momentum of the rigid body are conserved!
- In inertial frame vector components, we find

$$\mathbf{H} = {}^N\mathbf{H} = [BN]^T \mathcal{B}\mathbf{H}$$

$$\mathbf{H} = {}^N\mathbf{H} = \begin{bmatrix} c\theta_2c\theta_1 & c\theta_2s\theta_1 & -s\theta_2 \\ s\theta_3s\theta_2c\theta_1 - c\theta_3s\theta_1 & s\theta_3s\theta_2s\theta_1 + c\theta_3c\theta_1 & s\theta_3c\theta_2 \\ c\theta_3s\theta_2c\theta_1 + s\theta_3s\theta_1 & c\theta_3s\theta_2s\theta_1 - s\theta_3c\theta_1 & c\theta_3c\theta_2 \end{bmatrix} \begin{pmatrix} I_1\omega_1 \\ I_2\omega_2 \\ I_3\omega_3 \end{pmatrix}$$

$$\dot{\mathbf{H}} = 0 = \mathbf{f}(\theta_1, \theta_2, \theta_3, \omega_1, \omega_2, \omega_3, \dot{\omega}_1, \dot{\omega}_2, \dot{\omega}_3)$$



- Notice that the constant angular momentum condition can become very complicated and difficult to study!
- Instead of writing \mathbf{H} in inertial frame components, we chose to write it in the body frame where the inertia matrix is a constant for a rigid body.
- Assume the angular momentum vector \mathbf{H} is written in body frame components, and that principal axes were chosen for the body frame B .

$$\begin{aligned}\boldsymbol{\omega} &= \omega_1 \hat{\mathbf{b}}_1 + \omega_2 \hat{\mathbf{b}}_2 + \omega_3 \hat{\mathbf{b}}_3 \\ \mathbf{H} = {}^B\mathbf{H} &= H_1 \hat{\mathbf{b}}_1 + H_2 \hat{\mathbf{b}}_2 + H_3 \hat{\mathbf{b}}_3 \quad [I] = \begin{bmatrix} I_1 & 0 & 0 \\ 0 & I_2 & 0 \\ 0 & 0 & I_3 \end{bmatrix} \\ &= I_1 \omega_1 \hat{\mathbf{b}}_1 + I_2 \omega_2 \hat{\mathbf{b}}_2 + I_3 \omega_3 \hat{\mathbf{b}}_3\end{aligned}$$



- This allows us to write \mathbf{H} as:

$$\mathbf{H} = {}^{\mathcal{B}}\mathbf{H} = \begin{pmatrix} H_1 \\ H_2 \\ H_3 \end{pmatrix} = \begin{pmatrix} {}^{\mathcal{B}}(I_1\omega_1) \\ {}^{\mathcal{B}}(I_2\omega_2) \\ {}^{\mathcal{B}}(I_3\omega_3) \end{pmatrix}$$

- Because \mathbf{H} is constant, all possible rigid body angular velocities must lie on the surface of the following momentum ellipsoid:

$$H^2 = \mathbf{H}^T \mathbf{H} = I_1^2\omega_1^2 + I_2^2\omega_2^2 + I_3^2\omega_3^2 = \text{constant}$$

- Similarly, since the kinetic energy is conserved, all possible rigid body angular velocities must also lie on the surface of the following energy ellipsoid:

$$T = \frac{1}{2}I_1\omega_1^2 + \frac{1}{2}I_2\omega_2^2 + \frac{1}{2}I_3\omega_3^2$$

- The final admissible angular velocities will be on the intersection of these two ellipsoids.

- Using the momenta coordinates

$$H_1 = I_1\omega_1 \quad H_2 = I_2\omega_2 \quad H_3 = I_3\omega_3$$

- we can write the momentum magnitude constraint as

$$H^2 = H_1^2 + H_2^2 + H_3^2 \quad \rightarrow \text{Sphere}$$

- and the kinetic energy constraint as

$$1 = \frac{H_1^2}{2I_1T} + \frac{H_2^2}{2I_2T} + \frac{H_3^2}{2I_3T}$$

Compare to ellipsoid equation:

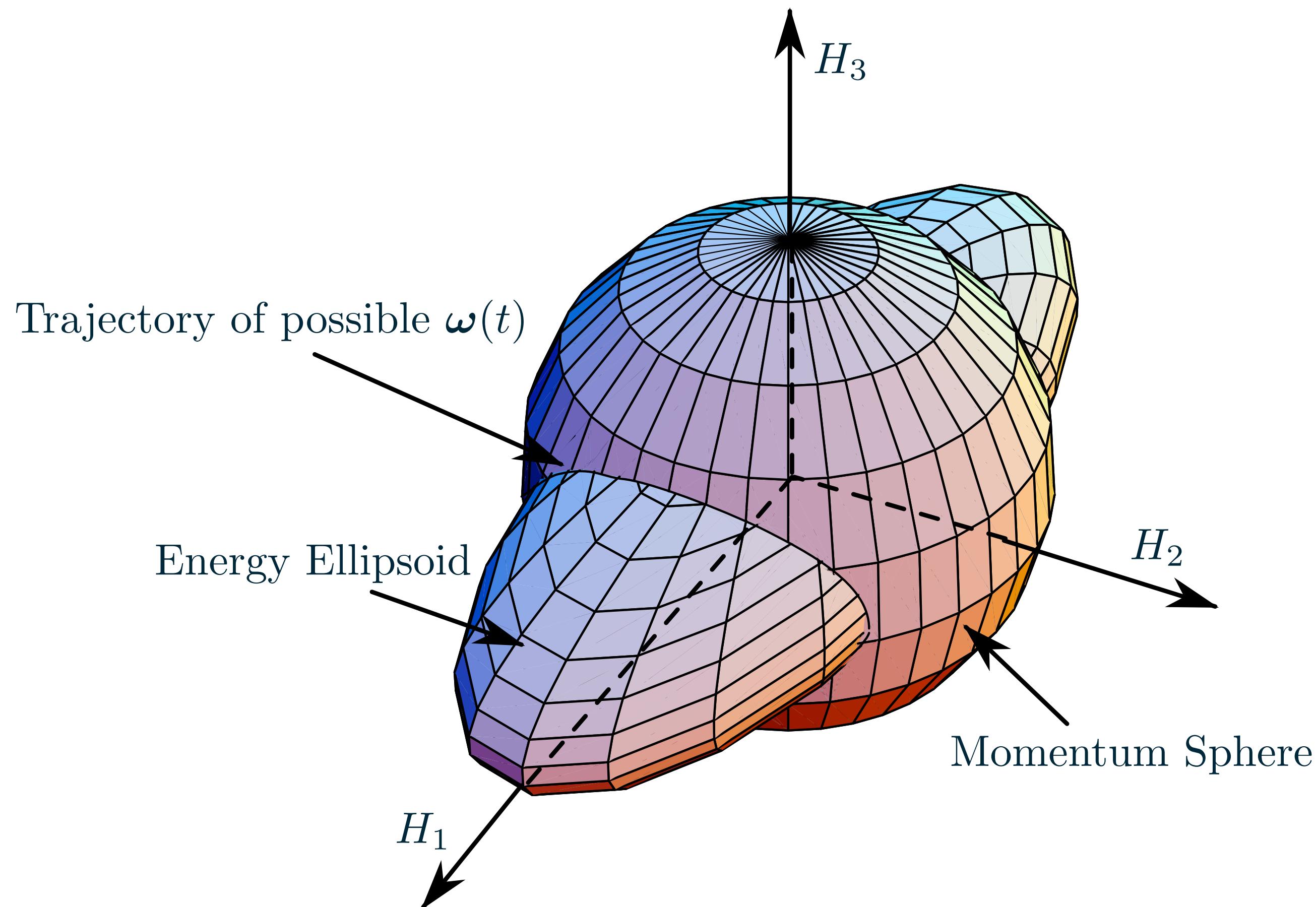
$$1 = \frac{x^2}{a^2} + \frac{y^2}{b^2} + \frac{z^2}{c^2}$$

$$\sqrt{2I_iT} \quad \rightarrow \text{semi-axes of ellipsoid}$$



- Clearly, for a given H , only a certain range of kinetic energies is possible.
- Let's assume the common notation:

$$I_1 \geq I_2 \geq I_3$$



- Let's look at the Minimum Energy Case:
- The surfaces will only intersect at:

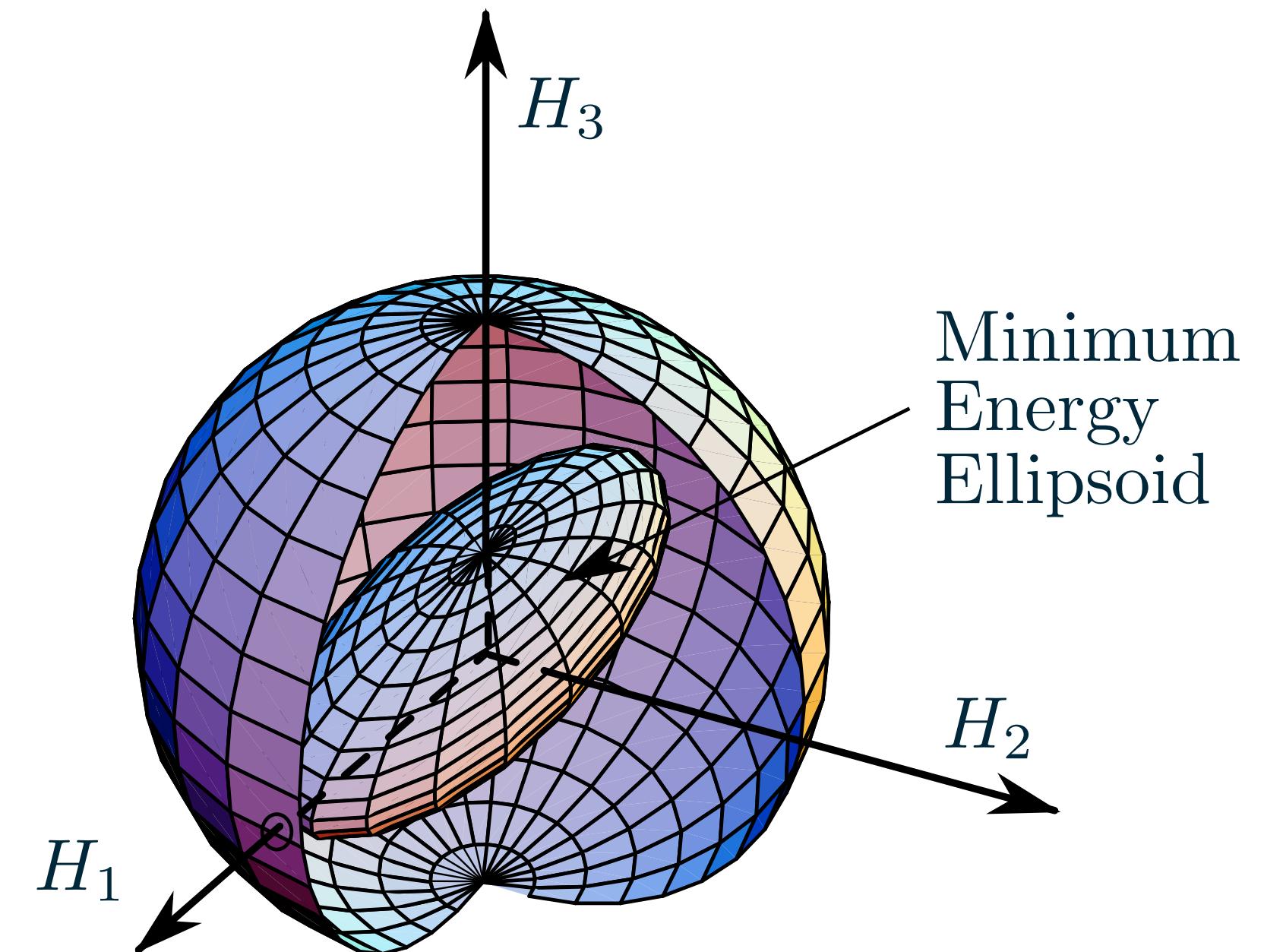
$${}^B\mathbf{H} = \pm H \hat{\mathbf{b}}_1$$

$$H_1 = H \quad H_2 = H_3 = 0$$

The kinetic energy is:

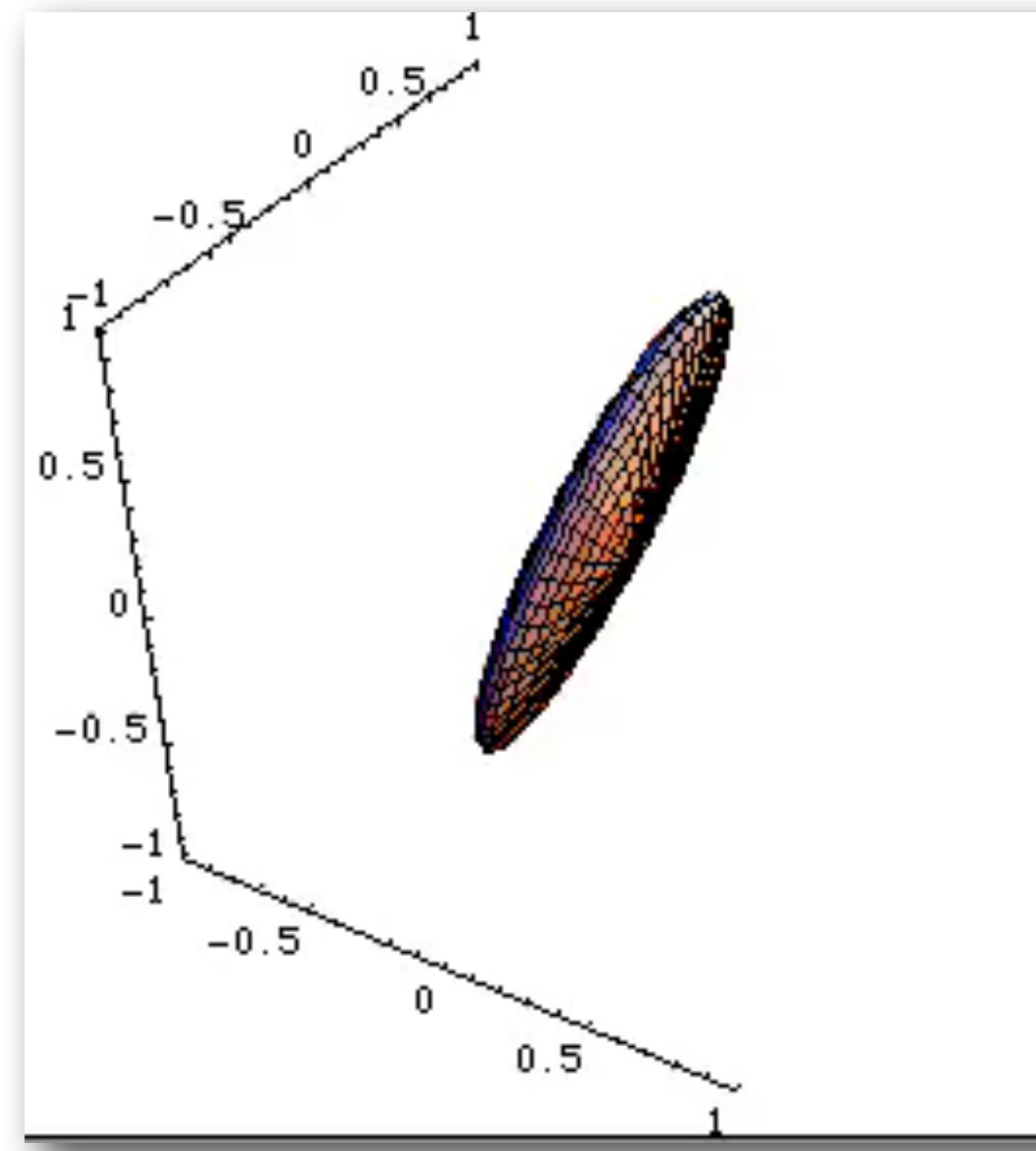
$$1 = \frac{H_1^2}{2I_1 T} + \frac{H_2^2}{2I_2 T} + \frac{H_3^2}{2I_3 T}$$

$$T_{\min} = \frac{H^2}{2I_1}$$



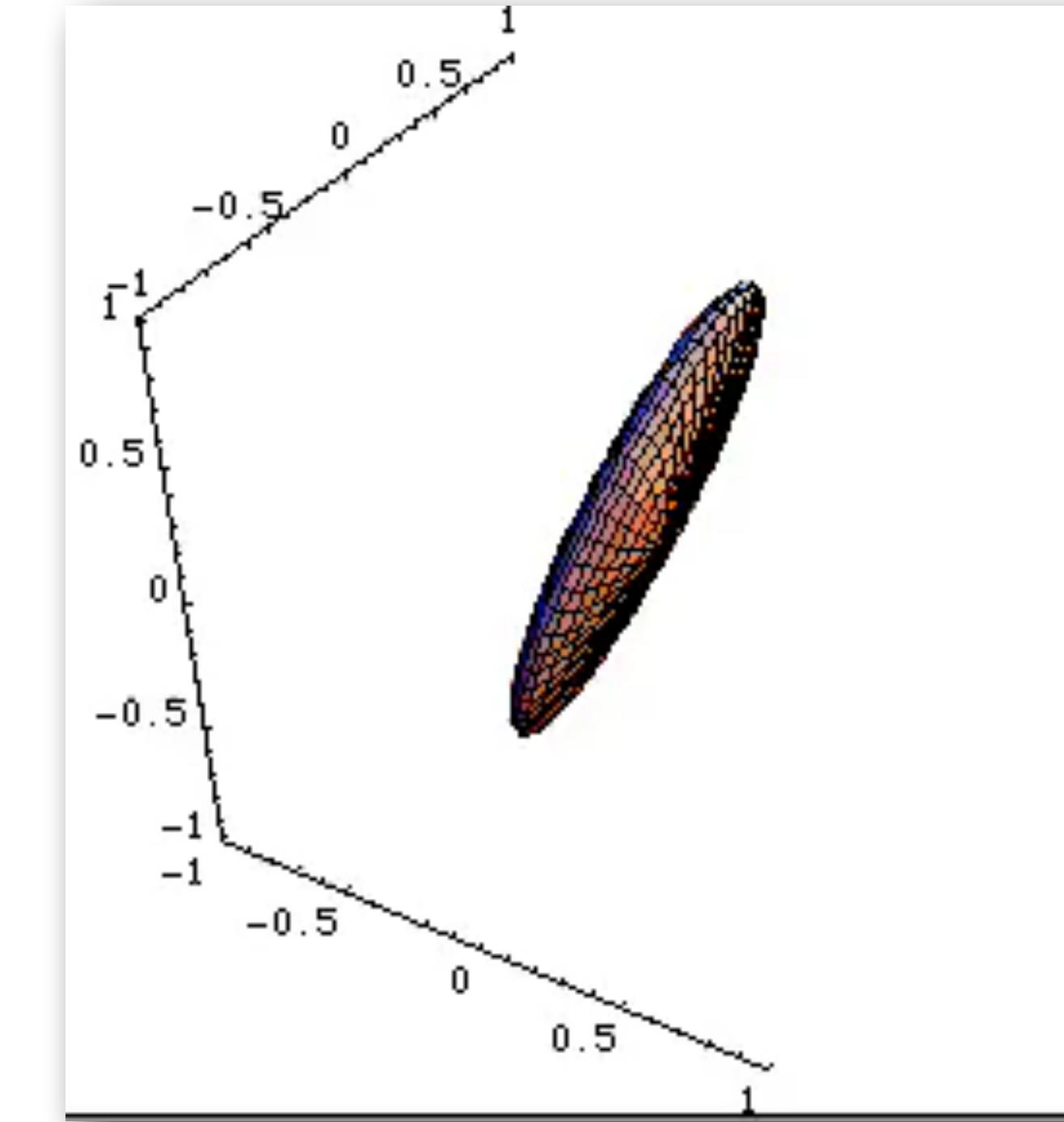
General Rotation of Rigid Body with

$$I_1 \geq I_2 \geq I_3$$



Pure Spin

$$\omega_0 = (10^\circ, 0^\circ, 0^\circ) / \text{s}$$



Slightly Off Spin

$$\omega_0 = (10^\circ, 0.5^\circ, 0.5^\circ) / \text{s}$$

- Let's look at the Intermediate Energy Case:

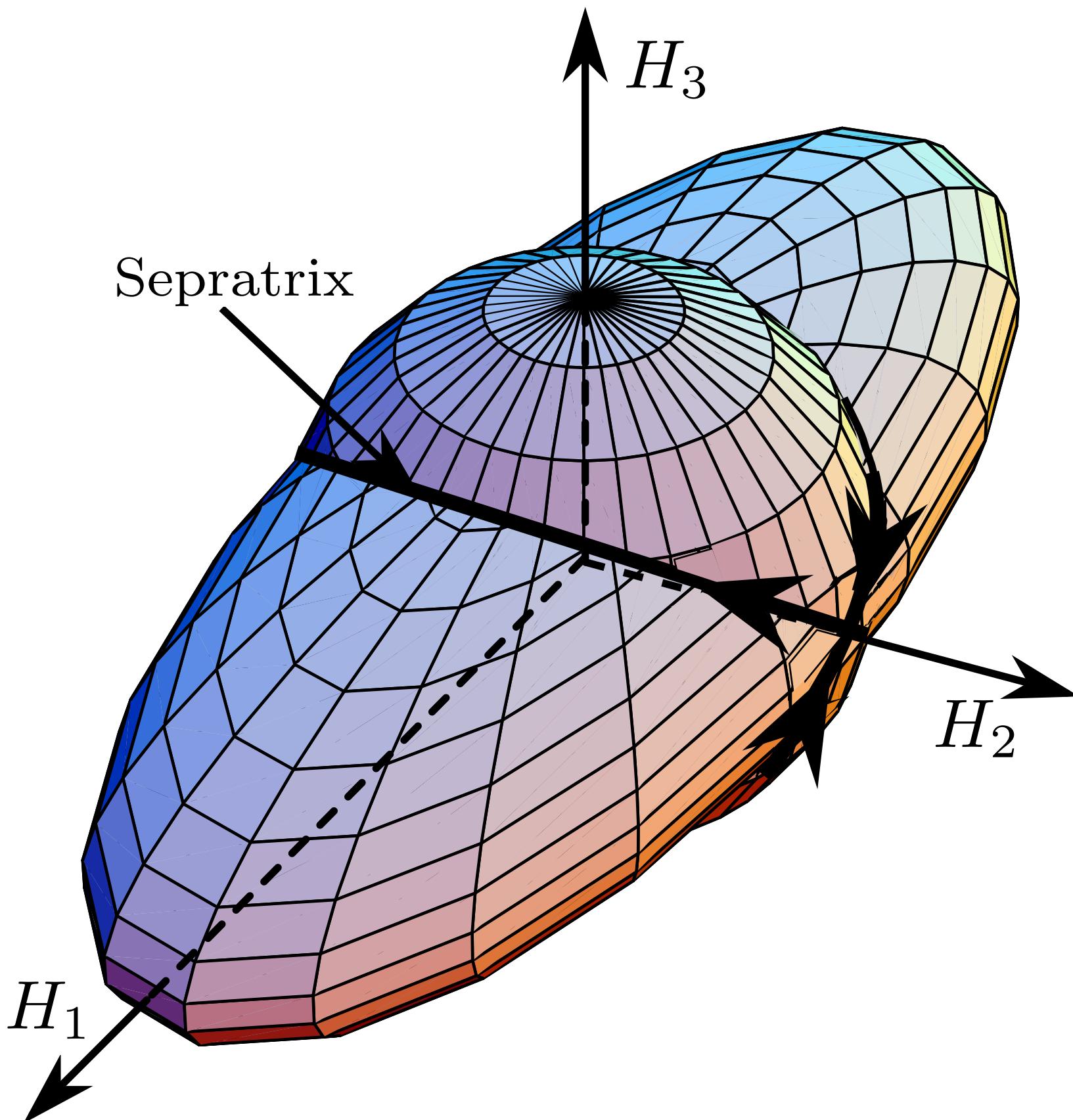
- The surfaces will only intersect at:

$${}^{\mathcal{B}}\boldsymbol{H} = \pm H \hat{\boldsymbol{b}}_2$$

The kinetic energy is:

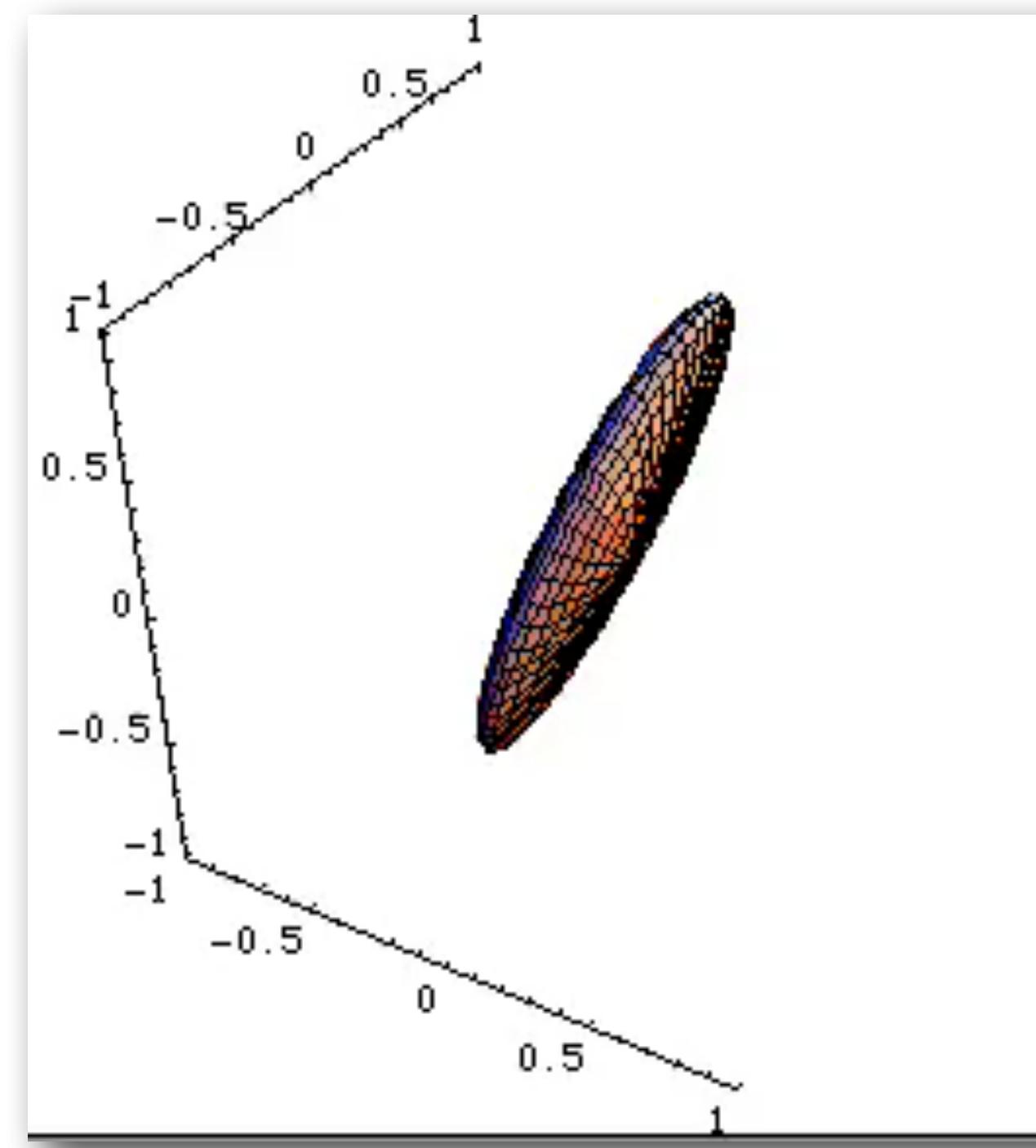
$$1 = \frac{H_1^2}{2I_1 T} + \frac{H_2^2}{2I_2 T} + \frac{H_3^2}{2I_3 T}$$

$$T_{\text{int}} = \frac{H^2}{2I_2}$$



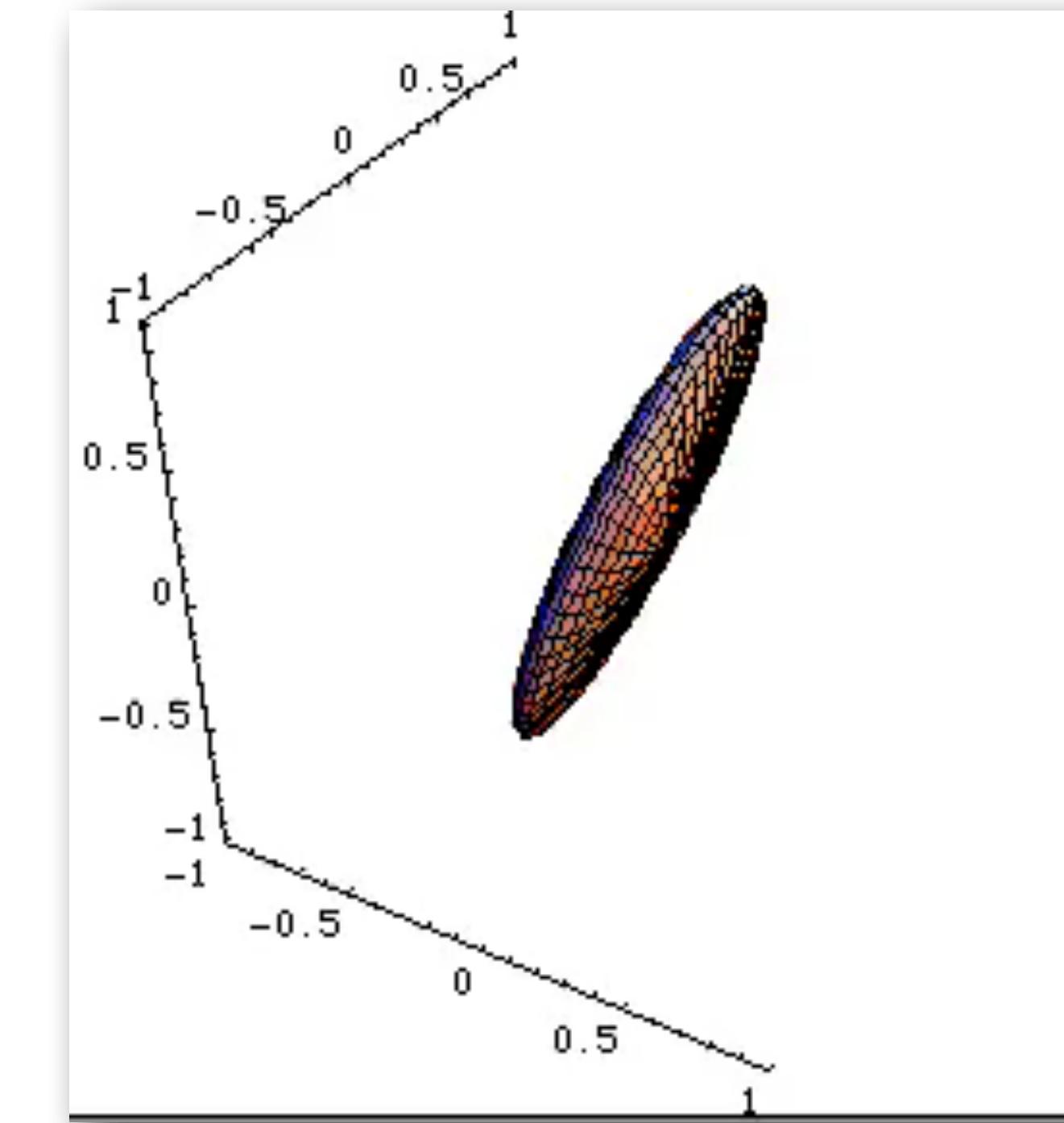
General Rotation of Rigid Body with

$$I_1 \geq I_2 \geq I_3$$



Pure Spin

$$\omega_0 = (0^\circ, 10^\circ, 0^\circ) / \text{s}$$



Slightly Off Spin

$$\omega_0 = (0.5^\circ, 10^\circ, 0.5^\circ) / \text{s}$$

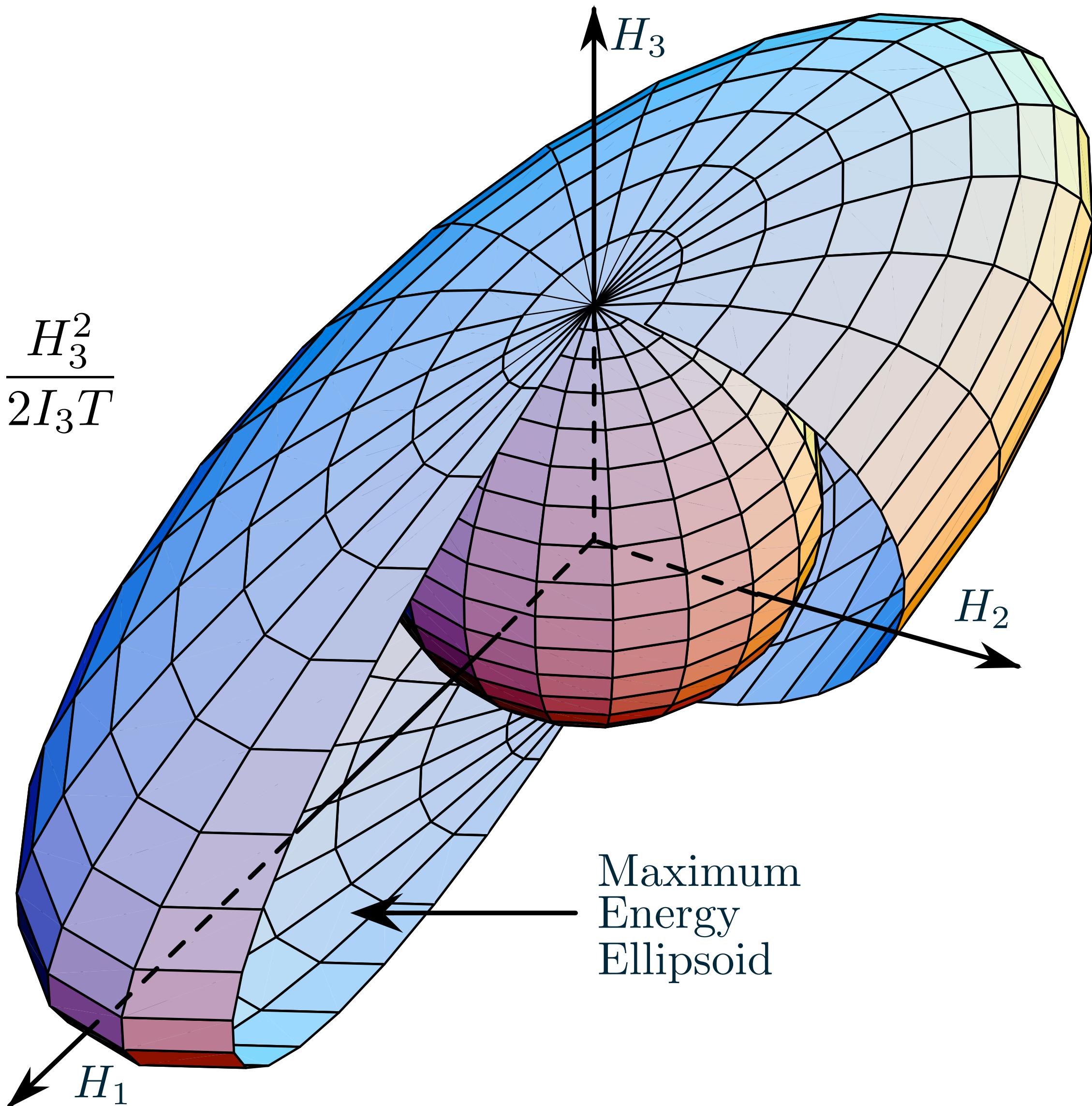
- Maximum Energy Case:

$${}^B H = H \hat{b}_3$$

The kinetic energy is:

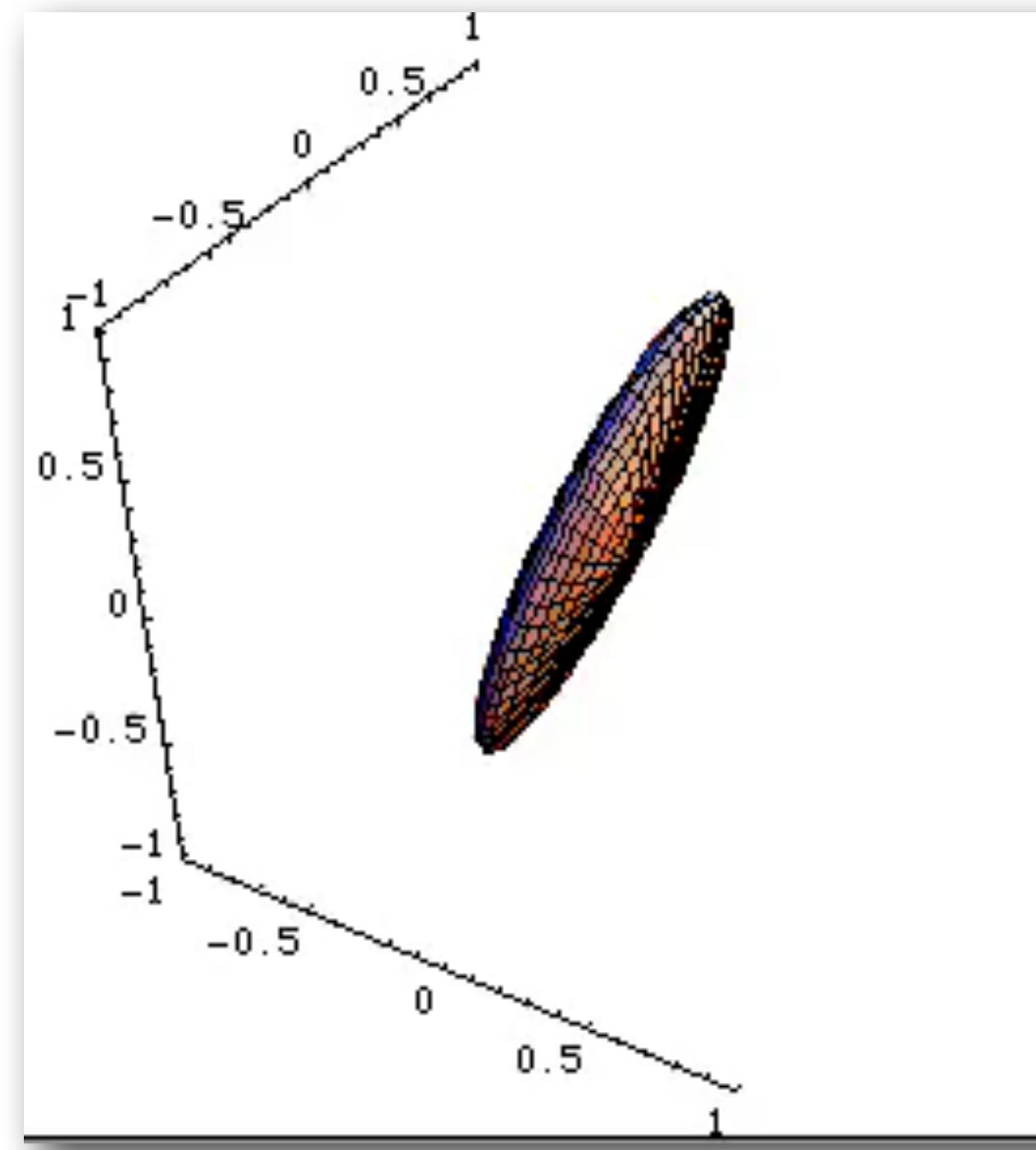
$$1 = \frac{H_1^2}{2I_1 T} + \frac{H_2^2}{2I_2 T} + \frac{H_3^2}{2I_3 T}$$

$$T_{\max} = \frac{H^2}{2I_3}$$



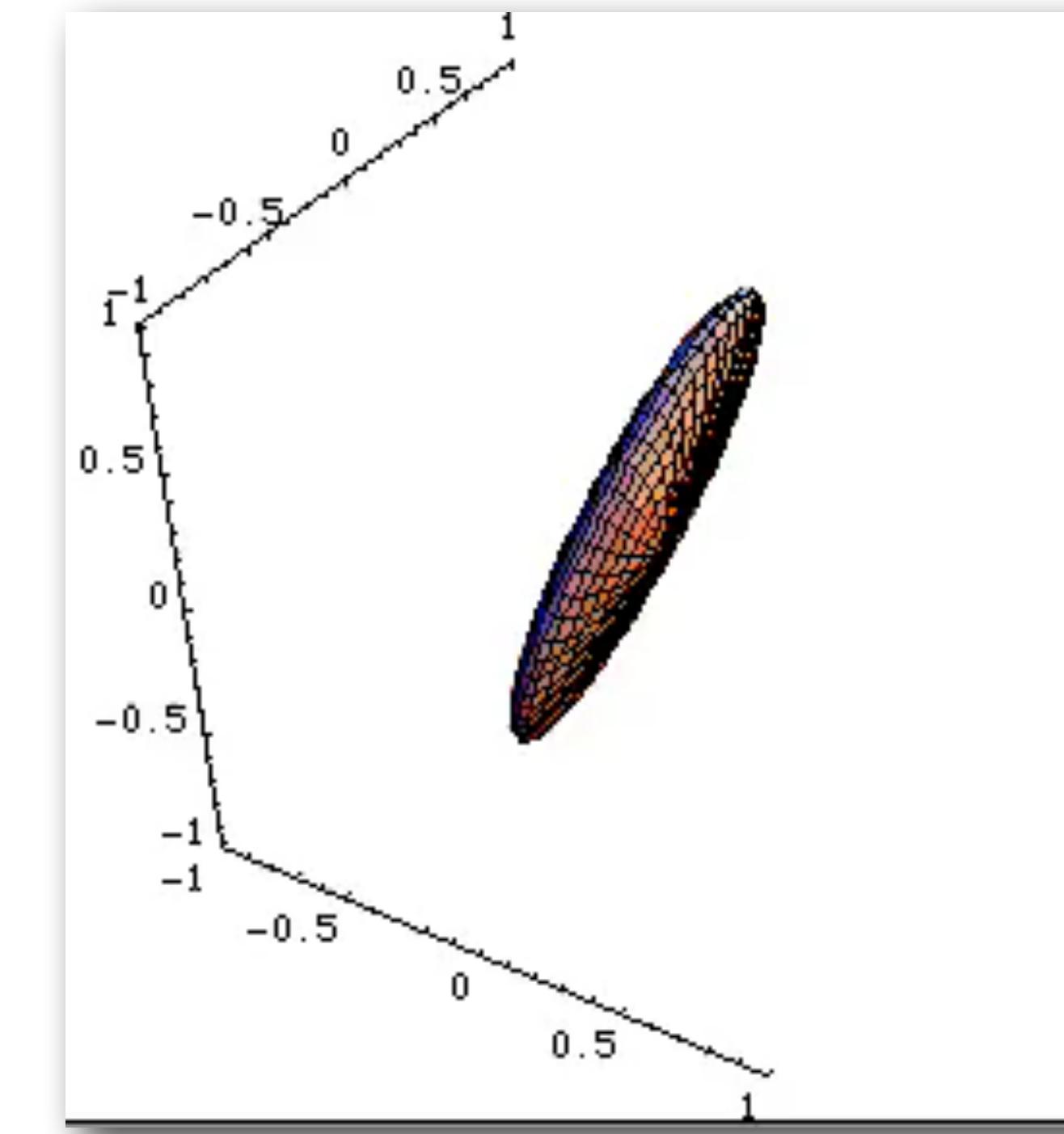
General Rotation of Rigid Body with

$$I_1 \geq I_2 \geq I_3$$



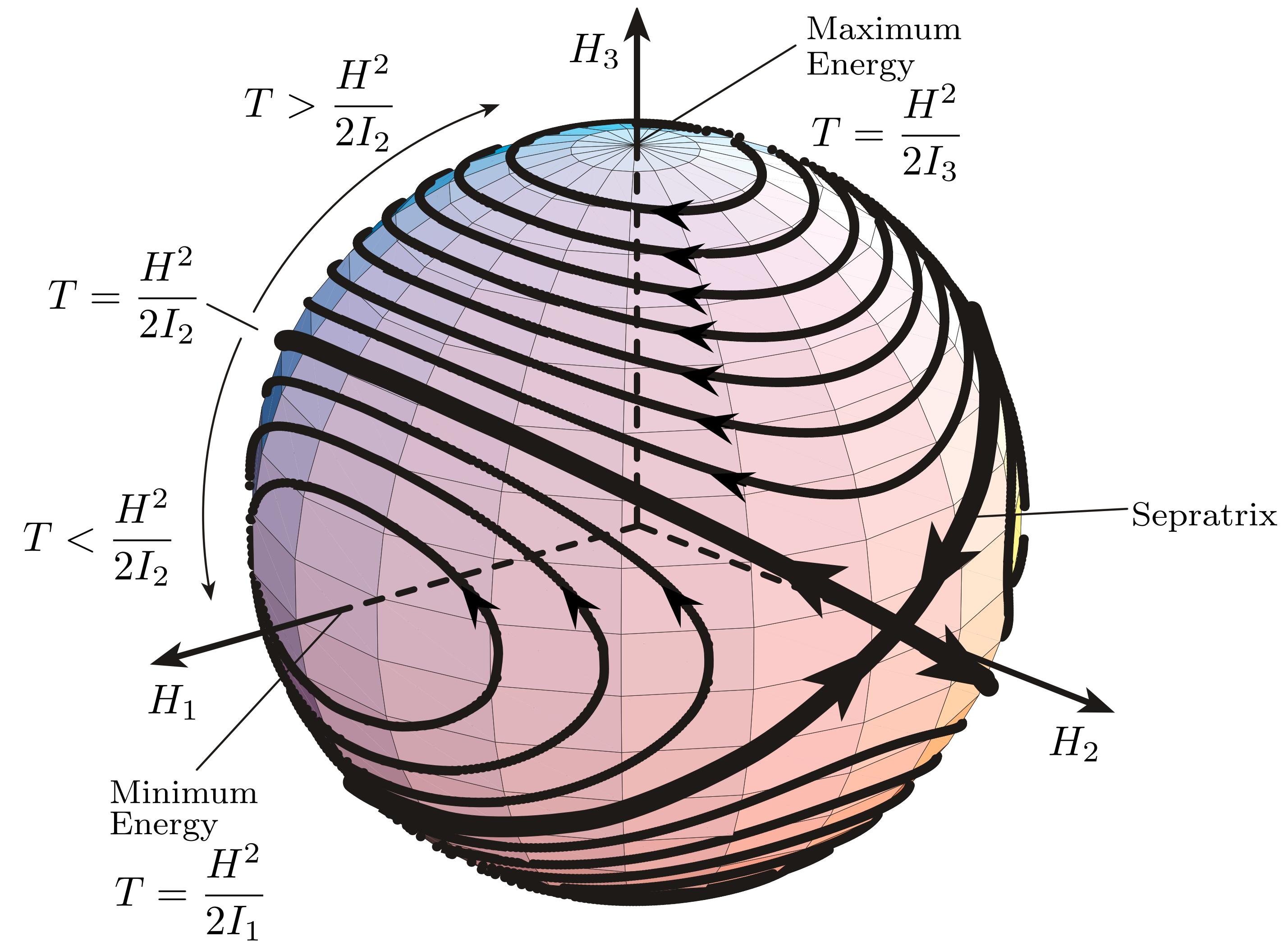
Pure Spin

$$\omega_0 = (0^\circ, 0^\circ, 10^\circ) / \text{s}$$

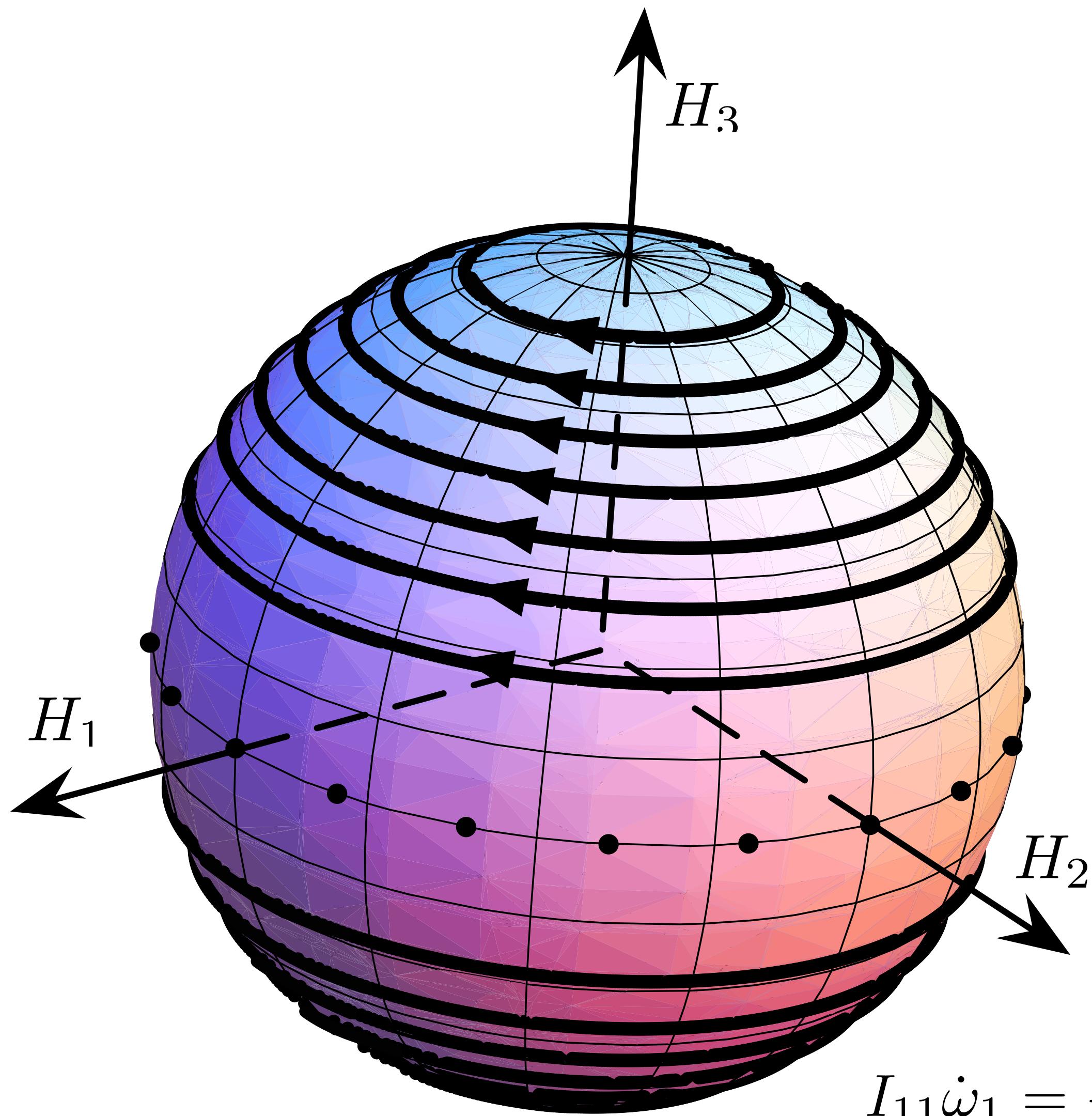


Slightly Off Spin

$$\omega_0 = (0.5^\circ, 0.5^\circ, 10^\circ) / \text{s}$$



Family of energy ellipsoid and momentum sphere intersections.

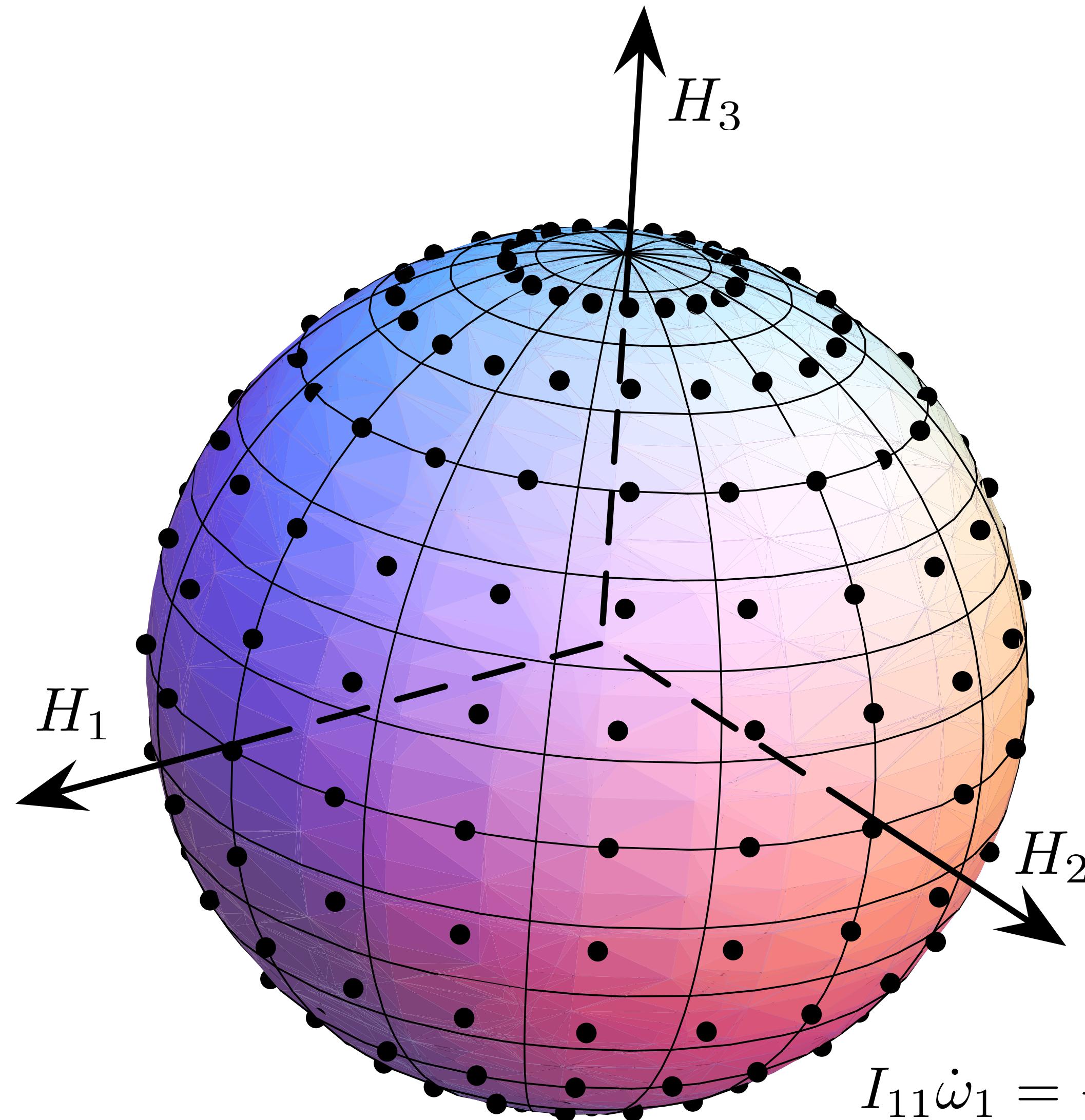


What type of spacecraft body would yield this?

$$I_{11}\dot{\omega}_1 = -(I_{33} - I_{22})\omega_2\omega_3$$

$$I_{22}\dot{\omega}_2 = -(I_{11} - I_{33})\omega_3\omega_1$$

$$I_{33}\dot{\omega}_3 = -(I_{22} - I_{11})\omega_1\omega_2$$



What type of spacecraft body would yield this?

$$I_{11}\dot{\omega}_1 = -(I_{33} - I_{22})\omega_2\omega_3$$

$$I_{22}\dot{\omega}_2 = -(I_{11} - I_{33})\omega_3\omega_1$$

$$I_{33}\dot{\omega}_3 = -(I_{22} - I_{11})\omega_1\omega_2$$

