

## Journal of Statistical Computation and Simulation



Date: 18 April 2016, At: 08:48

ISSN: 0094-9655 (Print) 1563-5163 (Online) Journal homepage: http://www.tandfonline.com/loi/gscs20

# New tables of coefficients and percentage points for the w test for normality

Rudolph S. Parrish

**To cite this article:** Rudolph S. Parrish (1992) New tables of coefficients and percentage points for the w test for normality, Journal of Statistical Computation and Simulation, 41:3-4, 169-185, DOI: <u>10.1080/00949659208811399</u>

To link to this article: <a href="http://dx.doi.org/10.1080/00949659208811399">http://dx.doi.org/10.1080/00949659208811399</a>



Full Terms & Conditions of access and use can be found at http://www.tandfonline.com/action/journalInformation?journalCode=gscs20

### NEW TABLES OF COEFFICIENTS AND PERCENTAGE POINTS FOR THE W TEST FOR NORMALITY

#### RUDOLPH S. PARRISH

Computer Sciences Corporation, c/o U.S. Environmental Protection Agency, College Station Road, Athens, GA 30613 U.S.A.

(Received 20 July 1989; in final form 14 August 1991)

Recent work has made available new tables of expected values, variances, and covariances of normal order statistics to higher precision and greater accuracy than existing tables. The coefficients associated with calculation of the Shapiro-Wilk W statistic used in testing departure from normality are based upon expressions involving expected values of normal order statistics and the corresponding variance-covariance matrix. These coefficients have been calculated on the basis of the new tables for sample sizes up to 50. Percentage points of the distribution of W are evaluated via simulation using the new coefficients, and an approximation is provided. The first and half moments of W also are given.

KEY WORDS: normal order statistics, Shapiro-Wilk W statistic, test of normality, W test.

#### 1. INTRODUCTION

Since the introduction of the W test of normality by Shapiro and Wilk (1965), many authors have applied and extended the technique. The computation of W usually has been based on tables of coefficients provided originally by Shapiro and Wilk which, in turn, were based on variances and covariances of normal order statistics as provided by Sarhan and Greenberg (1956) and also appearing in Sarhan and Greenberg (1962). The moments were given to ten decimal places (d.p.) for sample sizes n up to 20. For larger sample sizes, approximations were used for the coefficient calculations. Recently, Parrish (1992a, 1992b) computed high-precision values for the expected values, variances, and covariances of normal order statistics. Expected values and standard deviations were computed to 25 d.p. for n up to 500. Variances and covariances were computed to 25 d.p. for n = 2(1)20, to 20 d.p. for n = 21(1)30, to 15 d.p. for n = 31(1)40, and to 10 d.p. for n = 41(1)50. A brief summary of the computational techniques is provided in the Appendix. These values can be utilized to calculate with higher accuracy the coefficients used for computing W for sample sizes up to 50. In addition, percentage points of the distribution of W and low-order moments also can be computed with better accuracy. The percentage points presented here differ somewhat from those reported by Shapiro and Wilk and also from those based on code by Royston (1982b).

#### 2. COEFFICIENTS FOR CALCULATION OF W

For a random sample of n observations, the W test statistic is defined by

$$W = \frac{(a'y)^{2}}{\sum_{i=1}^{n} (y_{i} - \overline{y})^{2}}$$

where y represents the vector of ordered observations with elements  $y_i$  ( $i = 1, \ldots, n$ ) having mean value  $\overline{y}$ , and where a' represents a set of corresponding coefficients. Of course, the numerator for W may be written as  $(\sum a_i y_i)^2$ , where the summation extends over  $i = 1, \ldots, n$ . Note also that the bounds on W are from  $na_i^2/(n-1)$  to 1.

The coefficients are determined on the basis of the expected values, variances, and covariances of order statistics for a sample of size n from the unit normal distribution. Using  $\mu$  to denote the vector of expected values and  $\Sigma$  to denote the variance-covariance matrix, the coefficients are given by

$$a' = \frac{\mu' \Sigma^{-1}}{(\mu' \Sigma^{-1} \Sigma^{-1} \mu)^{-1/2}}$$

The values of  $a_i$  for n = 2(1)50 were calculated using the values given by Parrish; these are presented in Table 1. The table contains values for  $-a_i$ , noting that  $a_{n-i+1} = -a_i$ .

By definition,  $\mathbf{a}'\mathbf{a} = 1$  for each sample size. As a numerical check, this identity holds to at least 31 d.p. for all cases reported. The identity  $\mu' \Sigma^{-1} \mathbf{1} = 0$  holds also to at least 31 d.p. In comparison to the 4-d.p. table of coefficients of Shapiro and Wilk (1965), there is uniform agreement up to sample size 20. Thereafter, however, there are several instances of relatively large differences between the two sets of values.

Royston (1982a) described an algorithm for approximating these coefficients with emphasis on higher sample sizes. Royston's computed values agree very well with those of Shapiro and Wilk for n between 21 and 50, being based partly on the same technique of approximation. In comparison to current values, however, maximum absolute (relative) differences observed for  $a_i$  values were 0.0087 (2.1%), 0.0176 (4.6%), and 0.0243 (6.9%) for n equal to 30, 40, and 50, respectively. The maximum differences all occur for  $a_1$ , which is the weight applied to the most extreme observations in the sample.

#### 3. LOW-ORDER MOMENTS OF W

The expected value of W is given by

$$E(W) = \frac{(\boldsymbol{\mu}' \boldsymbol{\Sigma}^{-1} \boldsymbol{\mu}) (\boldsymbol{\mu}' \boldsymbol{\Sigma}^{-1} \boldsymbol{\mu} + 1)}{(n-1)(\boldsymbol{\mu}' \boldsymbol{\Sigma}^{-1} \boldsymbol{\Sigma}^{-1} \boldsymbol{\mu})}$$

and the first half-moment is

$$E(W^{1/2}) = \frac{\Gamma[(n-1)/2](\mu' \Sigma^{-1} \mu)^2}{2^{1/2} \Gamma(n/2)(\mu' \Sigma^{-1} \Sigma^{-1} \mu)^{1/2}}$$

(see Shapiro and Wilk, 1965). Computed values of these moments for n = 2(1)50 are given in Table 2 to 20 d.p. In comparison to the values given by Shapiro and Wilk for n = 3(1)20, there are some discrepancies in the fourth decimal digit.

#### 4. PERCENTAGE POINTS OF W

Simulation techniques were employed to obtain empirical percentage points for the distribution of W. For each size n, 100,000 random normal samples of size n were generated using an inverse CDF technique; see routine RNNOR of IMSL (1987). For each sample, the value of W was computed. Percentage points of the resulting empirical distributions were calculated according to the quantile estimator given by

$$\hat{\mu}_p = (0.5 + i - np)W_{(i)} + (0.5 - i + np)W_{(i+1)}$$

where  $\mu_p$  represents the 100*p*-th percentile, n=100,000, i=[np+0.5] (an integer), and where  $W_{(i)}$  is the *i*th order statistic of the set of *W* values; see Parrish (1990). Percentage points were computed for  $p=0.005,\,0.01,\,0.02,\,0.025,\,0.05,\,0.10,\,0.15,\,0.20,\,0.25,\,0.30,\,0.40,\,0.50,\,0.60,\,0.70,\,0.75,\,0.80,\,0.85,\,0.90,\,0.95,\,0.975,\,0.98,\,0.99$ , and 0.995. These results are presented in Table 3. The reported values were convergent to within one digit in the third decimal place.

The Q-Q plot of cumulative distribution function values in Figure 1 shows the relationship between the empirical percentage points  $W_p$  calculated on the basis of the high-precision coefficient values and those produced by Royston's approximate technique, for the case of n=50. This indicates that the empirical values are consistently greater than those of Royston. For values of n below 20, there is very little difference between the values. For values of n=30, 40, and 50, however, the maximum differences are 3.1%, 5.3%, and 9.2%, respectively, when expressed relative to the 99% empirical quasi-range ( $W_{0.995}-W_{0.005}$ ).

Royston (1982) described an effective technique for approximating percentiles of the distribution of W, based on a power transformation of the form  $Y = (1 - W)^{\tau}$ . For appropriate values of  $\tau$ , Y has approximately a normal distribution. Thus, an approximation of a percentage point of W can be obtained by applying the inverse transformation using the corresponding percentage point of the normal distribution, provided the mean and strandard deviation are known. By using simulation, Royston determined a value of  $\tau$  for each n that maximized the coefficient of determination for a weighted regression of empirical percentage points of W on corresponding values of the normal distribution. Polynomials then were used to obtain an approximation for  $\tau$  as a function of n. Using high-precision

 Table 1
 Coefficients for the W test of normality

	Sample size n			_	
i		2	3	4	5
1 2 3		0.7071067812	0.7071067812 0.00000000000	0.6871551280 0.1667867802	0.6646474775 0.2413373793 0.00000000000
	6	7	8	9	10
1 2 3 4 5	0.6431054172 0.2806345383 0.0875195881	0.6232895333 0.3031014983 0.1401414979 0.00000000000	0.6052472633 0.3164469157 0.1743201616 0.0561211289	0.5888321091 0.3244228324 0.1976490410 0.0946648285 0.00000000000	0.5738570793 0.3290504445 0.2141165910 0.1223707080 0.0399168226
			13	14	15
1 2 3 4 5	0.5601422499 0.3315011888 0.2260112813 0.1429441989 0.0695232230 0.00000000000	0.5475281705 0.3324925825 0.2347342583 0.1585949356 0.0921573545 0.0302668380	0.5358777533 0.3324834790 0.2411873679 0.1707215330 0.1098628215 0.0538770994	0.5250744090 0.3317775940 0.2459746345 0.1802509537 0.1239635841 0.0726976454	0.5150192099 0.3305816528 0.2495139501 0.1878205734 0.1353555195 0.0879586645
7 8	0.000000000	0.0302006360	0.0000000000	0.0239718197	0.0433516067 0.00000000000
	16	17	18	19	20
1 2 3 4 5	0.5056280678 0.3290396258 0.2521023330 0.1938820587 0.1446662435 0.1005055905	0.4968292406 0.3272536929 0.2539557503 0.1987636435 0.1523481263 0.1109391506	0.4885612340 0.3252975150 0.2552343204 0.2027090203 0.1587350801 0.1196979973	0.4807710708 0.3232248788 0.2560587664 0.2059024776 0.1640786216 0.1271098197	0.4734128767 0.3210754680 0.2565214513 0.2084856299 0.1685715416 0.1334242040
7 8 9 10	0.0592758746 0.0195963678	0.0725350058 0.0358670219 0.00000000000	0.0836968501 0.0495487472 0.0164092927	0.0931803327 0.0611755362 0.0303185106 0.00000000000	0.1013014106 0.0711446023 0.0422290548 0.0140026086
	21	22	23	24	25
1 2 3 4 5	0.4664467268 0.3188787999 0.2566939530 0.2105688392 0.1723638838	0.4598377036 0.3166569623 0.2566323737 0.2122391882 0.1755739987	0.4535551262 0.3144265488 0.2563811303 0.2135661558 0.1782963546	0.4475719153 0.3122000466 0.2559757039 0.2146057276 0.1806071621	0.4418640698 0.3099868465 0.2554446647 0.2154034217 0.1825684929
6 7 8 9 10 11 12 13	0.1388344530 0.1083028893 0.0797578651 0.0525164046 0.0260695452 0.00000000000	0.1434924768 0.1143743953 0.0872490460 0.0614677911 0.0365554708 0.0121324451	0.1475191999 0.1196661221 0.0938019389 0.0693069211 0.0457331335 0.0227298981 0.00000000000	0.1510119860 0.1242985139 0.0995630671 0.0762107318 0.0538160456 0.0320512598 0.0106449407	0.1540500328 0.1283692276 0.1046506560 0.0823210553 0.0609739073 0.0403000747 0.0200482635 0.00000000000

Table 1 (continued)

Laute 1	(commueu)				
	26	27	28	29	30
1	0.4364102318	0.4311913235	0.4261902430	0.4213916082	0.4167815395
2	0.3077939859	0.3056267018	0.3034888455	0.3013831975	0.2993117080
3	0.2548111830	0.2540941704	0.2533091512	0.2524689344	0.2515841371
4	0.2159965457	0.2164159026	0.2166870959	0.2168315372	0.2168672338
5	0.1842313407	0.1856379285	0.1868234674	0.1878175140	0.1886450282
6	0.1566983562	0.1590107760	0.1610321820	0.1628002757	0.1643469233
7	0.1319582284	0.1351315786	0.1379442958	0.1404425356	0.1426652801
8	0.1091611237	0.1131738590	0.1167547950	0.1199591189	0.1228333526
9	0.0877529291	0.0926006375	0.0969421793	0.1008426256	0.1043566768
10	0.0673433859	0.0730358257	0.0781428732	0.0827406551	0.0868929286
11	0.0476387943	0.0541987726	0.0600874378	0.0653935408	0.0701910651
12	0.0284039853	0.0358675038	0.0425649038	0.0485996488	0.0540574905
13	0.0094386991	0.0178561866	0.0254011137	0.0321944514	0.0383357562
14		0.0000000000	0.0084444544	0.0160369307	0.0228935039
15				0.0000000000	0.0076134408
	31	32	33	34	35
1	0.4123474753	0.4080780148	0.4039627823	0.3999923112	0.3961579430
2	0.2972756810	0.2952759175	0.2933128271	0.2913865147	0.2894968487
3	0.2506635954	0.2497146895	0.2487436027	0.2477555297	0.2467548445
4	0.2168094072	0.2166709859	0.2164629985	0.2161948911	0.2158747843
5	0.1893272049	0.1898821345	0.1903253306	0.1906701564	0.1909281695
6	0.1656992159	0.1668803105	0.1679100996	0.1688057516	0.1695821477
7	0.1446456552	0.1464119710	0.1479885486	0.1493963843	0.1506536862
8	0.1254169698	0.1277436640	0.1298423546	0.1317379895	0.1334521932
9	0.1075306355	0.1104039444	0.1130103996	0.1153791146	0.1175352940
10	0.0906534904	0.0940680413	0.0971756462	0.1000098881	0.1025997896
11	0.0745421847	0.0784995325	0.0821079619	0.0854059298	0.0884265934
12	0.0590101353	0.0635180246	0.0676324729	0.0713973324	0.0748503029
13	0.0439077750	0.0489798916	0.0536107452	0.0578502486	0.0617411619
14	0.0291099437	0.0347660481	0.0399288904	0.0446552907	0.0489937246
15	0.0145072955	0.0207737038	0.0264896074	0.0317198175	0.0365193539
16	0.0000000000	0.0069104320	0.0132065399	0.0189625234	0.0242410031
17			0.0000000000	0.0063094121	0.0120893874
18					0.0000000000
	36	37	38	39	40
1	0.3924517404	0.3888664111	0.3853952412	0.3820320373	0.3787710751
2	0.2876435153	0.2858260608	0.2840439256	0.2822964709	0.2805830004
3	0.2457452368	0.2447298236	0.2437112409	0.2426917189	0.2416731446
4	0.2155096836	0.2151056517	0.2146679507	0.2142011605	0.2137092772
5	0.1911094042	0.1912226036	0.1912754110	0.1912745293	0.1912258537
6	0.1702522385	0.1708273376	0.1713173630	0.1717310383	0.1720760607
7	0.1517763111	0.1527781229	0.1536712875	0.1544665180	0.1551732792
8	0.1350037920	0.1364092438	0.1376829911	0.1388377541	0.1398847738
9	0.1195008598	0.1212949605	0.1229343895	0.1244339305	0.1258066434
10	0.1049705543	0.1071441683	0.1091398918	0.1109746636	0.1126634352

Table 1	(continued)				
11	0.0911986879	0.0937472355	0.0960941216	0.0982585671	0.1002575176
12	0.0780239734	0.0809466579	0.0836430716	0.0861348820	0.0884411623
13	0.0653203350	0.0686196961	0.0716670478	0.0744867118	0.0771000561
14	0.0529858135	0.0566675032	0.0600700041	0.0632205491	0.0661430081
15	0.0409352519	0.0450079774	0.0487725460	0.0522594182	0.0554952212
16	0.0290952390	0.0335708457	0.0377071373	0.0415381925	0.0450937076
17	0.0174004411	0.0222941283	0.0268146765	0.0310002662	0.0348840459
18	0.0057907930	0.0111214682	0.0160419397	0.0205950910	0.0248179962
19		0.0000000000	0.0053395736	0.0102762695	0.0148516753
20				0.0000000000	0.0049440918
	41	42	43	44	45
1	0.3756070541	0.3725350582	0.3695505198	0.3666491887	0.3638271034
2	0.2789027767	0.2772550356	0.2756389962	0.2740538696	0.2724988661
3	0.2406571144	0.2396449769	0.2386378700	0.2376367512	0.2366424238
4	0.2131957957	0.2126637789	0.2121159166	0.2115545751	0.2109818394
5	0.1911345836	0.1910053165	0.1908421272	0.1906486361	0.1904280663
6	0.1723592414	0.1725866244	0.1727635870	0.1728949253	0.1729849265
7	0.1557999582	0.1563540092	0.1568420751	0.1572700910	0.1576433729
8	0.1408340158	0.1416943414	0.1424736528	0.1431790153	0.1438167624
9	0.1270641038	0.1282166039	0.1292733215	0.1302424635	0.1311313880
10	0.1142194504	0.1156544773	0.1169790060	0.1182024131	0.1193331038
11	0.1021059670	0.1038172270	0.1054031535	0.1068743374	0.1082402661
12	0.0905787649	0.0925626332	0.0944060615	0.0961209143	0.0977178112
13	0.0795259282	0.0817810149	0.0838801407	0.0858365195	0.0876619648
14	0.0688583927	0.0713852704	0.0737401095	0.0759375664	0.0779907276
15	0.0585033361	0.0613043797	0.0639166017	0.0663562150	0.0686376715
16	0.0483996851	0.0514789947	0.0543518343	0.0570361104	0.0595477552
17	0.0384949462	0.0418583377	0.0449965676	0.0479294009	0.0506743847
18	0.0287428900	0.0323979447	0.0358079007	0.0389945792	0.0419773060
19	0.0191017927	0.0230579646	0.0267476195	0.0301948747	0.0334210285
20	0.0095330456	0.0138018277	0.0177809160	0.0214970133	0.0249736258
21	0.0000000000	0.0045951585	0.0088753544	0.0128702296	0.0166057823
22			0.0000000000	0.0042854453	0.0082900138
23					0.0000000000
	46	47	48	49	50
1	0.3610805671	0.3584061243	0.3558005410	0.3532607867	0.3507840182
2	0.2709731999	0.2694760935	0.2680067810	0.2665645105	0.2651485459
3	0.2356555587	0.2346767133	0.2337063471	0.2327448354	0.2317924810
4	0.2103995493	0.2098093308	0.2092126222	0.2086106971	0.2080046843
5	0.1901832932	0.1899168868	0.1896311485	0.1893281424	0.1890097226
6	0.1730374321	0.1730558909	0.1730434054	0.1730027722	0.1729365164
7	0.1579666933	0.1582443460	0.1584802025	0.1586777604	0.1588401854
8	0.1443925851	0.1449116092	0.1453784606	0.1457973238	0.1461719907
9	0.1319467089	0.1326943841	0.1333797949	0.1340078086	0.1345828412
10	0.1203786312	0.1213458006	0.1222407543	0.1230690568	0.1238357434
11	0.1095094625	0.1106895990	0.1117876072	0.1128097444	0.1137617138
12	0.0992062826	0.1005949091	0.1018914211	0.1031028353	0.1042354485

Table	1 (continued)				
13	0.0893670710	0.0909613579	0.0924534230	0.0938509919	0.0951611725
14	0.0799113106	0.0817098458	0.0833957951	0.0849777624	0.0864633642
15	0.0707738969	0.0727764767	0.0746558557	0.0764213781	0.0780817119
16	0.0619009901	0.0641085570	0.0661818771	0.0681313152	0.0699659895
17	0.0532471542	0.0556616808	0.0579305124	0.0600648517	0.0620750784
18	0.0447732600	0.0473977700	0.0498645416	0.0521859361	0.0543728771
19	0.0364449666	0.0392834958	0.0419516359	0.0444628060	0.0468292242
20	0.0282315360	0.0312891934	0.0341630315	0.0368677677	0.0394164990
21	0.0201049228	0.0233879277	0.0264728170	0.0293756506	0.0321108620
22	0.0120390223	0.0155548020	0.0188571357	0.0219636245	0.0248899521
23	0.0040090437	0.0077663449	0.0112936741	0.0146103332	0.0177335170
24		0.0000000000	0.0037611431	0.0072956146	0.0106222495
25				0.0000000000	0.0035377912

coefficient values, the present author followed a similar approach and obtained values of  $\tau$  for n=7(1)50; these are plotted in Figure 2. Royston's results exhibited a discontinuity at n=20, which apparently was due to the use of approximate coefficients above this level, and the values tended to increase above n=20. In contrast, current values showed no discontinuity and showed a consistently declining exponential trend up to n=50. Implementation of this approximation also requires calculation of the mean and standard deviation of the approximating normal distribution. Royston obtained these by conducting further simulations using  $\tau$  values calculated from the polynomial function, and, similarly, the mean and standard deviation were fitted using polynomials. For this study, the mean and standard deviation were computed for n=7(1)50 on the basis of the regression of empirical percentage points  $W_p$  versus standard normal percentage points for p ranging from 0.005 to 0.995.  $R^2$  values for all cases were at least 0.999. Plots of the mean and standard deviation so obtained are given in Figures 3 and 4.

Approximations for the mean  $\mu$ , the standard deviation  $\sigma$ , and the exponent  $\tau$ , as functions of n, were obtained by using the following model forms:

$$\mu = A_0 - A_1 e^{-c_1 n} - A_2 e^{-c_2 n},$$

$$\sigma = A_3 e^{-c_3 n},$$

$$\tau = A_4 e^{-c_4 n} + A_5 e^{-c_5 n}.$$

The parameters  $A_i$  and  $C_i$  were estimated by using nonlinear least squares to minimize the function

$$\sum_{n} \sum_{p} \left( \frac{(1 - W_p)^r - \mu}{\sigma} - Z_p \right)^2$$

 Table 2
 Low-order moments of the Shapiro-Wilk W statistic

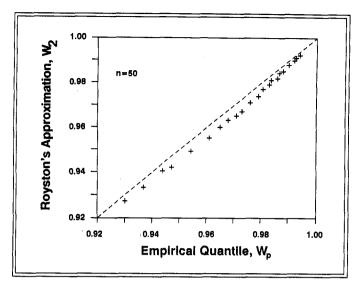
	Expected value	Half-moment
2 3	1.0000000000000000000000	1.000000000000000000000000000000000000
3	0.91349667156634403713	0.95492965855137201461
4	0.90134519044754513483	0.94860607100455176481
5	0.90260843946125172617	0.94940601433948222235
6	0.90714614811641694356	0.95190950844072190868
7	0.91234611623600380971	0.95472848337660872056
8	0.91741539192094758982	0.95745045124918655928
9	0.92211342347220650495	0.95995593518890414679
10	0.92638807705246033976	0.96222346577841627740
11	0.93025382416783535182	0.96426509595203587480
12	0.93374706814312365772	0.96610316450704737430
13	0.93690901753580717613	0.96776161652006365754
14	0.93977917406865121558	0.96926284465681634435
15	0.94239310007495775322	0.97062670877930646601
16	0.94478193531821190766	0.97187041788235817517
17	0.94697260747540038439	0.97300873535868117156
18	0.94898828567435564682	0.97405428331057649864
19	0.95084888532062159215	0.97501785408068273388
20	0.95257154612940791482	0.97590869412744424108
21	0.95417105567720966067	0.97673474988580386552
22	0.95566021282936844758	0.97750287549381897308
23	0.95705013453551454870	0.97821900616304097490
24	0.95835051274254200149	0.97888830207528633362
25	0.95956982881124831504	0.97951526761339007590
26	0.96071553235951415086	0.98010385021201581895
27	0.96179419059883489611	0.98065752247435142336
28	0.96281161330195789883	0.98117935058079124809
29	0.96377295767263980247	0.98167205146856415872
30	0.96468281663238855126	0.98213804079942762298
31	0.96554529340195746272	0.98257947335199262952
32	0.96636406472883727551	0.98299827716580251738
33	0.96714243468154719357	0.98339618251445152654
34	0.96788338058167134825	0.98377474658398625977
35	0.96858959236100004900	0.98413537457120792105
36	0.96926350640141707580	0.98447933778647664352
37	0.96990733472896596327	0.98480778924085681398
38	0.97052309028234917024	0.98512177711283064956
39	0.97111260885310429550	0.98542225642127860286
40	0.97167756819435038516	0.98571009917574988482
41	0.97221950471289455497	0.98598610322966457887
42	0.97273982809210959919	0.98625100002497102641
43	0.97323983413752123150	0.98650546138631832536
44	0.97372071609123614432	0.98675010549771871360
45	0.97418357462334380940	0.98698550217392305224
46	0.97462942667689210948	0.98721217752155076934
47	0.97505921331670195411	0.98743061807070342071
48	0.97547380670972191675	0.98764127444557188837
49	0.97587401634656281830	0.98784456463277569408
50	0.97626059459539153246	0.98804087689639025830

 Table 3
 Empirical percentage points of the Shapiro-Wilk W statistic

			·	U .								
N	0.005	0.010	0.020	0.025	0.050	0.100	0.150	0.200	0.250	0.300	0.400	0.500
3	0.752	0.755	0.759	0.761	0.772	0.794	0.815	0.835	0.854	0.872	0.905	0.933
4	0.674	0.692	0.716	0.726	0.761	0.800	0.826	0.846	0.860	0.872	0.893	0.914
5	0.671	0.700	0.732	0.743	0.777	0.813	0.835	0.853	0.867	0.879	0.899	0.915
,							0.055					
6	0.691	0.720	0.750	0.760	0.793	0.828	0.849	0.864	0.877	0.887	0.905	0.919
7	0.709	0.737	0.768	0.778	0.809	0.840	0.860	0.874	0.885	0.894	0.910	0.923
8	0.726	0.754	0.784	0.793	0.821	0.851	0.869	0.882	0.892	0.901	0.915	0.927
9	0.745	0.772	0.799	0.808	0.835	0.863	0.879	0.890	0.899	0.907	0.920	0.932
10	0.760	0.786	0.812	0.821	0.845	0.871	0.886	0.897	0.906	0.913	0.925	0.935
11	0.773	0.798	0.823	0.830	0.854	0.879	0.893	0.903	0.911	0.918	0.929	0.939
12	0.786	0.809	0.832	0.840	0.862	0.885	0.898	0.908	0.916	0.922	0.933	0.942
13	0.797	0.819	0.840	0.847	0.869	0.891	0.904	0.913	0.920	0.926	0.936	0.944
14	0.805	0.827	0.848	0.854	0.875	0.896	0.908	0.917	0.924	0.930	0.939	0.947
15	0.813	0.836	0.856	0.863	0.882	0.902	0.913	0.921	0.928	0.933	0.942	0.949
16	0.823	0.843	0.863	0.869	0.887	0.905	0.916	0.924	0.930	0.935	0.944	0.951
17	0.831	0.850	0.869	0.875	0.892	0.910	0.920	0.928	0.934	0.938	0.946	0.953
18	0.840	0.857	0.874	0.880	0.897	0.913	0.924	0.931	0.936	0.941	0.948	0.955
19	0.844	0.861	0.879	0.884	0.900	0.917	0.926	0.933	0.939	0.943	0.950	0.956
20	0.850	0.867	0.883	0.888	0.905	0.920	0.929	0.936	0.941	0.945	0.952	0.958
21	0.857	0.873	0.888	0.893	0.908	0.923	0.932	0.938	0.943	0.947	0.954	0.959
22	0.861	0.876	0.891	0.896	0.911	0.926	0.934	0.940	0.945	0.949	0.955	0.961
23	0.865	0.880	0.894	0.900	0.914	0.928	0.936	0.942	0.947	0.950	0.957	0.962
24	0.870	0.885	0.899	0.903	0.917	0.930	0.938	0.944	0.948	0.952	0.958	0.963
25	0.875	0.888	0.902	0.906	0.919	0.932	0.940	0.945	0.950	0.953	0.959	0.964
23	0.673	0.000	0.902		0.919	0.932	0.940	0.943	0.930	0.933	0.939	
26	0.877	0.892	0.905	0.909	0.922	0.934	0.942	0.947	0.951	0.955	0.960	0.965
27	0.881	0.895	0.908	0.912	0.924	0.936	0.944	0.949	0.953	0.956	0.961	0.966
28	0.885	0.898	0.910	0.914	0.926	0.938	0.945	0.950	0.954	0.957	0.962	0.967
29	0.888	0.900	0.912	0.916	0.928	0.939	0.946	0.951	0.955	0.958	0.963	0.968
30	0.892	0.904	0.916	0.919	0.930	0.942	0.948	0.953	0.956	0.959	0.964	0.969
31	0.894	0.906	0.917	0.921	0.932	0.943	0.949	0.954	0.957	0.960	0.965	0.969
32	0.897	0.908	0.919	0.923	0.934	0.944	0.951	0.955	0.958	0.961	0.966	0.970
33	0.899	0.910	0.921	0.925	0.935	0.945	0.952	0.956	0.959	0.962	0.967	0.971
34	0.901	0.912	0.923	0.926	0.937	0.947	0.953	0.957	0.960	0.963	0.968	0.971
35	0.904	0.915	0.925	0.928	0.938	0.948	0.954	0.958	0.961	0.964	0.968	0.972
	0.908	0.917	0.927	0.930	0.940	0.949	0.955	0.959	0,962	0.965	0.969	0.973
36	0.908	0.917	0.927	0.930	0.940	0.949	0.955	0.960	0.963	0.965	0.909	0.973
37												
38	0.911	0.920	0.930	0.933	0.942	0.951	0.957	0.960	0.964	0.966	0.970	0.974
39	0.912	0.922	0.931	0.934	0.943	0.952	0.958	0.961	0.964	0.967	0.971	0.974
40	0.913	0.924	0.932	0.935	0.944	0.953	0.958	0.962	0.965	0.967	0.971	0.975
41	0.916	0.925	0.935	0.938	0.946	0.954	0.959	0.963	0.966	0.968	0.972	0.975
42	0.917	0.926	0.935	0.938	0.947	0.955	0.960	0.964	0.967	0.969	0.973	0.976
43	0.919	0.928	0.936	0.939	0.948	0.956	0.961	0.964	0.967	0.969	0.973	0.976
44	0.920	0.929	0.938	0.940	0.949	0.957	0.962	0.965	0.968	0.970	0.973	0.976
45	0.922	0.930	0.939	0.942	0.950	0.958	0.962	0.966	0.968	0.970	0.974	0.977
	0.924	0.932	0.940	0.943	0.951	0.958	0.963	0.966	0.969	0.971	0.974	0.977
46	0.924			0.943	0.951	0.956	0.963	0.967	0.969	0.971	0.974 $0.975$	0.977
47		0.933	0.941 0.942					0.967	0.969	0.971 $0.972$	0.975	0.978
48	0.927	0.935		0.945	0.953	0.960	0.964					
49	0.928	0.936	0.943	0.946	0.953	0.961	0.965	0.968	0.970	0.972	0.976	0.978 $0.979$
50	0.930	0.937	0.944	0.947	0.954	0.961	0.965	0.968	0.971	0.973	0.976	0.979

Table 3 (continued)

3         0.957         0.976         0.983         0.989         0.994         0.997         0.999         1.000         1.000         1.3           4         0.933         0.950         0.958         0.967         0.975         0.983         0.992         0.996         0.997         0.95           5         0.930         0.945         0.953         0.960         0.968         0.975         0.984         0.990         0.992         0.9           6         0.932         0.945         0.951         0.958         0.965         0.972         0.981         0.986         0.988         0.9           7         0.935         0.946         0.952         0.958         0.964         0.971         0.979         0.985         0.986         0.9           8         0.938         0.948         0.953         0.959         0.964         0.971         0.979         0.984         0.985         0.986         0.9           9         0.941         0.951         0.955         0.960         0.965         0.971         0.978         0.983         0.984         0.9           10         0.944         0.953         0.957         0.961         0.966         0.	990 0.995 000 1.000 998 0.999 995 0.997
4       0.933       0.950       0.958       0.967       0.975       0.983       0.992       0.996       0.997       0.95         5       0.930       0.945       0.953       0.960       0.968       0.975       0.984       0.990       0.992       0.96         6       0.932       0.945       0.951       0.958       0.965       0.972       0.981       0.986       0.988       0.7         7       0.935       0.946       0.952       0.958       0.964       0.971       0.979       0.985       0.986       0.8         8       0.938       0.948       0.953       0.959       0.964       0.971       0.979       0.984       0.985       0.98         9       0.941       0.951       0.955       0.960       0.965       0.971       0.978       0.983       0.984       0.9         10       0.944       0.953       0.957       0.961       0.966       0.972       0.978       0.983       0.984       0.9         11       0.947       0.955       0.959       0.963       0.968       0.972       0.979       0.983       0.984       0.9         12       0.949       0.957 <t< th=""><th>998 0.999</th></t<>	998 0.999
5         0.930         0.945         0.953         0.960         0.968         0.975         0.984         0.990         0.992         0.4           6         0.932         0.945         0.951         0.958         0.965         0.972         0.981         0.986         0.988         0.4           7         0.935         0.946         0.952         0.958         0.964         0.971         0.979         0.985         0.986         0.4           8         0.938         0.948         0.953         0.959         0.964         0.971         0.979         0.984         0.985         0.986           9         0.941         0.951         0.955         0.960         0.965         0.971         0.978         0.983         0.984         0.1           10         0.944         0.953         0.957         0.961         0.966         0.972         0.978         0.983         0.984         0.1           11         0.947         0.955         0.959         0.963         0.968         0.972         0.979         0.983         0.984         0.1           12         0.949         0.957         0.961         0.966         0.968         0.973 <th< th=""><td></td></th<>	
5         0.930         0.945         0.953         0.960         0.968         0.975         0.984         0.990         0.992         0.96           6         0.932         0.945         0.951         0.958         0.965         0.972         0.981         0.986         0.988         0.9           7         0.935         0.946         0.952         0.958         0.964         0.971         0.979         0.985         0.986         0.9           8         0.938         0.948         0.953         0.959         0.964         0.971         0.979         0.984         0.985         0.9           9         0.941         0.951         0.955         0.960         0.965         0.971         0.978         0.983         0.984         0.9           10         0.944         0.953         0.957         0.961         0.966         0.972         0.978         0.983         0.984         0.9           11         0.947         0.955         0.959         0.963         0.968         0.972         0.979         0.983         0.984         0.9           12         0.949         0.957         0.961         0.964         0.968         0.973	995 0.997
7         0.935         0.946         0.952         0.958         0.964         0.971         0.979         0.985         0.986         0.98           8         0.938         0.948         0.953         0.959         0.964         0.971         0.979         0.984         0.985         0.9           9         0.941         0.951         0.955         0.960         0.965         0.971         0.978         0.983         0.984         0.9           10         0.944         0.953         0.957         0.961         0.966         0.972         0.978         0.983         0.984         0.9           11         0.947         0.955         0.959         0.963         0.968         0.972         0.979         0.983         0.984         0.9           12         0.949         0.957         0.961         0.964         0.968         0.973         0.979         0.983         0.984         0.9           13         0.951         0.958         0.962         0.966         0.969         0.974         0.979         9.983         0.984         0.9           14         0.954         0.960         0.964         0.967         0.971         0.975 <t< th=""><td></td></t<>	
7         0.935         0.946         0.952         0.958         0.964         0.971         0.979         0.985         0.986         0.98           8         0.938         0.948         0.953         0.959         0.964         0.971         0.979         0.984         0.985         0.9           9         0.941         0.951         0.955         0.960         0.965         0.971         0.978         0.983         0.984         0.9           10         0.944         0.953         0.957         0.961         0.966         0.972         0.978         0.983         0.984         0.9           11         0.947         0.955         0.959         0.963         0.968         0.972         0.979         0.983         0.984         0.9           12         0.949         0.957         0.961         0.964         0.968         0.973         0.979         0.983         0.984         0.9           13         0.951         0.958         0.962         0.966         0.969         0.974         0.979         9.983         0.984         0.9           14         0.954         0.960         0.964         0.967         0.971         0.975 <t< th=""><td>991 0.994</td></t<>	991 0.994
8         0.938         0.948         0.953         0.959         0.964         0.971         0.979         0.984         0.985         0.99           9         0.941         0.951         0.955         0.960         0.965         0.971         0.978         0.983         0.984         0.7           10         0.944         0.953         0.957         0.961         0.966         0.972         0.978         0.983         0.984         0.7           11         0.947         0.955         0.959         0.963         0.968         0.972         0.979         0.983         0.984         0.7           12         0.949         0.957         0.961         0.964         0.968         0.972         0.979         0.983         0.984         0.7           13         0.951         0.958         0.962         0.964         0.968         0.973         0.979         0.983         0.984         0.9           14         0.954         0.960         0.964         0.967         0.971         0.975         0.980         0.984         0.985         0.9           15         0.956         0.962         0.965         0.968         0.972         0.976         <	989 0.992
9         0.941         0.951         0.955         0.960         0.965         0.971         0.978         0.983         0.984         0.10           10         0.944         0.953         0.957         0.961         0.966         0.972         0.978         0.983         0.984         0.73           11         0.947         0.955         0.959         0.963         0.968         0.972         0.979         0.983         0.984         0.73           12         0.949         0.957         0.961         0.964         0.968         0.973         0.979         0.983         0.984         0.74           13         0.951         0.958         0.962         0.966         0.969         0.974         0.979         0.983         0.984         0.74           14         0.954         0.960         0.966         0.969         0.974         0.979         9.983         0.984         0.985           15         0.956         0.962         0.965         0.968         0.972         0.975         0.980         0.984         0.985         0.985           16         0.957         0.963         0.966         0.969         0.973         0.976         0.981	988 0.991
10         0.944         0.953         0.957         0.961         0.966         0.972         0.978         0.983         0.984         0.71           11         0.947         0.955         0.959         0.963         0.968         0.972         0.979         0.983         0.984         0.71           12         0.949         0.957         0.961         0.964         0.968         0.973         0.979         0.983         0.984         0.71           13         0.951         0.958         0.962         0.966         0.969         0.974         0.979         9.983         0.984         0.94           14         0.954         0.960         0.966         0.969         0.974         0.979         9.983         0.984         0.981           15         0.956         0.960         0.967         0.971         0.975         0.980         0.984         0.985         0.981           16         0.957         0.963         0.966         0.969         0.973         0.976         0.981         0.984         0.985         0.985           17         0.959         0.965         0.967         0.970         0.973         0.977         0.982         0.985 <td></td>	
11         0.947         0.955         0.959         0.963         0.968         0.972         0.979         0.983         0.984         0.71           12         0.949         0.957         0.961         0.964         0.968         0.973         0.979         0.983         0.984         0.71           13         0.951         0.958         0.962         0.966         0.969         0.974         0.979         9.983         0.984         0.91           14         0.954         0.960         0.967         0.971         0.975         0.980         0.984         0.985         0.981           15         0.956         0.962         0.965         0.968         0.972         0.976         0.980         0.984         0.985         0.985           16         0.957         0.963         0.966         0.969         0.973         0.976         0.981         0.984         0.985         0.985           17         0.959         0.965         0.967         0.970         0.973         0.977         0.982         0.985         0.986         0.986         0.977         0.977         0.982         0.985         0.986         0.         0.974         0.978         0.98	987 0.989
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	987 0.989
13         0.951         0.958         0.962         0.966         0.969         0.974         0.979         9.983         0.984         0.71           14         0.954         0.960         0.964         0.967         0.971         0.975         0.980         0.984         0.985         0.71           15         0.956         0.962         0.965         0.968         0.972         0.976         0.980         0.984         0.985         0.71           16         0.957         0.963         0.966         0.969         0.973         0.976         0.981         0.984         0.985         0.71           17         0.959         0.965         0.967         0.970         0.973         0.977         0.982         0.985         0.986         0.986           18         0.960         0.966         0.969         0.971         0.974         0.978         0.982         0.985         0.986         0.           19         0.962         0.967         0.969         0.972         0.975         0.978         0.982         0.985         0.986         0.           20         0.963         0.968         0.970         0.973         0.976         0.979	987 0.989
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	
15         0.956         0.962         0.965         0.968         0.972         0.976         0.980         0.984         0.985         0.7           16         0.957         0.963         0.966         0.969         0.973         0.976         0.981         0.984         0.985         0.7           17         0.959         0.965         0.967         0.970         0.973         0.977         0.982         0.985         0.986         0.           18         0.960         0.966         0.969         0.971         0.974         0.978         0.982         0.985         0.986         0.           19         0.962         0.967         0.969         0.972         0.975         0.978         0.982         0.985         0.986         0.           20         0.963         0.968         0.970         0.973         0.976         0.979         0.983         0.986         0.986         0.           21         0.964         0.969         0.971         0.974         0.976         0.979         0.983         0.986         0.987         0.           22         0.965         0.970         0.972         0.975         0.977         0.980         0	
16         0.957         0.963         0.966         0.969         0.973         0.976         0.981         0.984         0.985         0.7           17         0.959         0.965         0.967         0.970         0.973         0.977         0.982         0.985         0.986         0.           18         0.960         0.966         0.969         0.971         0.974         0.978         0.982         0.985         0.986         0.           19         0.962         0.967         0.969         0.972         0.975         0.978         0.982         0.985         0.986         0.           20         0.963         0.968         0.970         0.973         0.976         0.979         0.983         0.986         0.986         0.           21         0.964         0.969         0.971         0.974         0.976         0.979         0.983         0.986         0.987         0.           22         0.965         0.970         0.972         0.975         0.977         0.980         0.983         0.986         0.987         0.           23         0.966         0.971         0.973         0.975         0.978         0.981         0.	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	988 0.990
19     0.962     0.967     0.969     0.972     0.975     0.978     0.982     0.985     0.986     0.       20     0.963     0.968     0.970     0.973     0.976     0.979     0.983     0.986     0.986     0.       21     0.964     0.969     0.971     0.974     0.976     0.979     0.983     0.986     0.987     0.       22     0.965     0.970     0.972     0.975     0.977     0.980     0.983     0.986     0.987     0.       23     0.966     0.971     0.973     0.975     0.978     0.981     0.984     0.987     0.987     0.       24     0.967     0.972     0.974     0.976     0.978     0.981     0.984     0.987     0.988     0.	988 0.990
20     0.963     0.968     0.970     0.973     0.976     0.979     0.983     0.986     0.986     0.       21     0.964     0.969     0.971     0.974     0.976     0.979     0.983     0.986     0.987     0.       22     0.965     0.970     0.972     0.975     0.977     0.980     0.983     0.986     0.987     0.       23     0.966     0.971     0.973     0.975     0.978     0.981     0.984     0.987     0.987     0.       24     0.967     0.972     0.974     0.976     0.978     0.981     0.984     0.987     0.988     0.	988 0.990
21     0.964     0.969     0.971     0.974     0.976     0.979     0.983     0.986     0.987     0.       22     0.965     0.970     0.972     0.975     0.977     0.980     0.983     0.986     0.987     0.       23     0.966     0.971     0.973     0.975     0.978     0.981     0.984     0.987     0.987     0.       24     0.967     0.972     0.974     0.976     0.978     0.981     0.984     0.987     0.988     0.	988 0.990
22     0.965     0.970     0.972     0.975     0.977     0.980     0.983     0.986     0.987     0.       23     0.966     0.971     0.973     0.975     0.978     0.981     0.984     0.987     0.987     0.       24     0.967     0.972     0.974     0.976     0.978     0.981     0.984     0.987     0.988     0.	989 0.990
23     0.966     0.971     0.973     0.975     0.978     0.981     0.984     0.987     0.987     0.       24     0.967     0.972     0.974     0.976     0.978     0.981     0.984     0.987     0.988     0.	989 0.990
24  0.967  0.972  0.974  0.976  0.978  0.981  0.984  0.987  0.988  0.	989 0.990
	989 0.990
	989 0.991
20 01200 01212 01210 01211 01212 01201 01201 01200 01	990 0.991
26 0.969 0.973 0.975 0.977 0.979 0.982 0.985 0.987 0.988 0.	990 0.991
27 0.970 0.974 0.976 0.978 0.980 0.982 0.985 0.988 0.988 0.	990 0.991
	990 0.991
	990 0.992
	990 0.992
31 0.973 0.976 0.978 0.980 0.982 0.984 0.987 0.989 0.989 0.	991 0.992
	991 0.992
	991 0.992
	991 0.992
	991 0.992
36 0.976 0.979 0.980 0.982 0.983 0.985 0.988 0.990 0.990 0.	991 0.992
	992 0.993
	992 0.993
	992 0.993
	992 0.993
	992 0.993 992 0.993
	992 0.993
	992 0.993
	993 0.993
	993 0.993 993 0.994
47 0.980 0.983 0.984 0.985 0.986 0.988 0.990 0.991 0.992 0.	
	993 0.994
50 0.981 0.983 0.984 0.986 0.987 0.988 0.990 0.992 0.992 0.	993 0.994 993 0.994



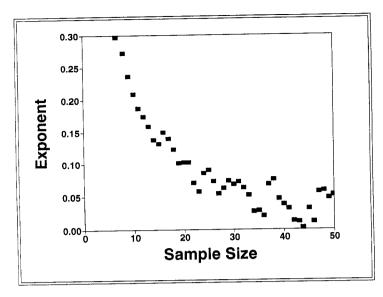
**Figure 1** Quantile-quantile plot for Shapiro-Wilk W statistic based on empirical values  $(W_p)$  and on Royston's approximation  $(W_2)$ , for sample size n = 50.

where  $W_p$  represents an empirical percentage point and  $Z_p$  represents that of the standard normal. The summations extend over n=7(1)50 and  $p=0.005,\,0.01,\,0.02,\,0.025,\,0.05,\,0.10,\,0.15,\,0.20,\,0.25,\,0.30,\,0.40,\,0.50,\,0.60,\,0.70,\,0.75,\,0.80,\,0.85,\,0.90,\,0.95,\,0.975,\,0.98,\,0.99,\,$  and 0.995. The final estimates are given in Table 4. Using the estimated values, simulations were conducted to evaluate the first four moments of the the function  $[(1-W_p)^\tau-\mu]/\sigma$ ; results are given in Table 5. The moment values are in close agreement with those of the standard normal (i.e., 0,1,0,3) in all cases. Thus, percentage points of W are given approximately by

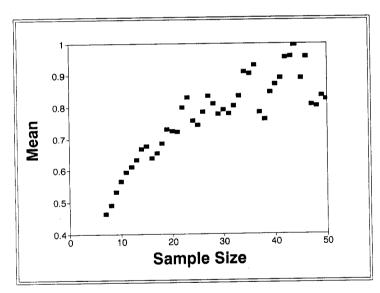
$$W_p \approx 1 - (\mu + \sigma Z_p)^{1/\tau}$$

for  $7 \le n \le 50$ .

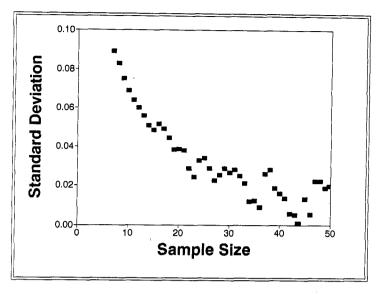
For n greater than 20, percentage points developed using the present technique generally are closer to empirical values than are those based on Royston's method. In Table 6, percentage points calculated using the two approximation methods are summarized for n = 10(10)50. The table contains empirical percentage points  $(W_p)$ , approximations based on the present method  $(W_1)$ , and approximations based on Royston's method  $(W_2)$ . Also, given in the table is the percent absolute difference  $(RE_1 \text{ and } RE_2)$  between each approximation and the empirical values, expressed relative to the 99% empirical quasi-range. Small values of RE indicate closer agreement with empirical values. The values in Table 6 show that the two methods perform about equally well for smaller values of n. For larger values of n, the present method is uniformly better. In several cases, the difference in relative errors is more than 8%.



**Figure 2** Plot of exponent versus sample size used in the normalizing power transformation  $(1-W)^{-1}$  derived from regression of empirical quantiles versus standard normal quantiles.



**Figure 3** Plot of mean versus sample size used in the transformation  $[(1 - W)^2 - \mu]/\sigma$  derived from regression of empirical quantiles versus standard normal quantiles.



**Figure 4** Plot of standard deviation versus sample size used in the transformation  $[(1 - W)^{\tau} - \mu]/\sigma$  derived from regression of empirical quantiles versus standard normal quantiles.

 Table 4
 Coefficients used in approximations based on normalizing transformations

$A_0 = 1.00317$	
$A_1 = 0.25318$	$C_1 = 0.05687$
$A_2 = 0.64930$	$C_2 = 0.06740$
$A_3 = 0.14761$	$C_3 = 0.07159$
$A_4 = 0.34797$	$C_4 = 0.07322$
$A_5 = 0.50182$	$C_5 = 0.20230$

**Table 5** Moments of transformed W values obtained in a simulation of 10,000 samples from a standard normal distribution

n	μ	$\sigma^2$	$oldsymbol{eta}_1^{1/2}$	$eta_2$
10	0.004	1.006	-0.005	2.943
15	-0.004	0.992	0.002	3.020
20	0.000	0.992	-0.007	3.058
25	0.003	0.995	0.020	3.086
30	0.001	1.000	-0.021	3.122
35	0.007	0.998	-0.008	3.073
40	-0.003	0.994	-0.002	3.110
45	0.010	0.991	-0.011	3.006
50	0.003	0.985	0.013	3.082

Table 6 Selected empirical quantiles and approximations based on two methods

$p$ 0.0005         0.0101         0.020 $W$ 0.760         0.786         0.812 $W_1$ 0.762         0.783         0.812 $R_2$ 0.4759         0.787         0.812 $R_2$ 0.1         0.2         0.2 $R_2$ 0.1         0.2         0.2 $R_2$ 0.1         0.2         0.2 $R_2$ 0.1         0.2         0.2 $R_2$ 0.4         0.2         0.3 $R_2$ 0.5         0.3         0.3 $R_2$ 0.5         0.3         0.3 $R_2$ 0.5         0.3         0.3 $R_2$ 0.3         0.3         0.3 $R_2$ 0.3         0.3         0.3 $R_2$	0 0.025 0.821 0.821 0.820 0.7 0.7 0.5 0.888 3 0.888 3 0.888 3 0.888 3 0.888 3 0.888 3 0.888 3 0.888 3 0.888 3 0.888	0.050 0.845 0.844 0.33 0.3 0.944 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994 0.994	0.100 0.877 0.877 0.7 0.3 0.100 0.930 0.930 0.919	0.150 0.886 0.887 0.887	0.200 0.897 0.896 0.898	0.250	0.913	0,400	0.935		- !				006.0	0.950	€/6.0 - :	0.980	10.000 O	S
0.760 0.786 0.812 0.772 0.778 0.812 0.759 0.778 0.812 0.11 0.4 0.2 0.4 0.2 0.2 0.4 0.2 0.2 0.4 0.2 0.2 0.408 0.000 0.000 0.850 0.867 0.883 0.850 0.867 0.883 0.851 0.904 0.902 0.891 0.902 0.914 0.903		0.845 0.846 0.3 0.3 0.30 0.904 0.904 0.904 0.904 0.904 0.904 0.904 0.904						0.925		0.944	0.953								C 087	
0.762 0.787 0.812 0.759 0.785 0.812 1.1 0.4 0.2 0.4 0.2 0.2 0.4 0.2 0.2 0.850 0.867 0.883 0.850 0.867 0.883 0.850 0.867 0.883 0.851 0.883 0.883 0.892 0.994 0.996 0.892 0.994 0.996 0.891 0.902 0.991 0.891 0.992 0.993 0.913 0.924 0.933 0.913 0.924 0.933 0.914 0.924 0.933 0.916 0.900 0.020 0.506 0.914 0.933 0.917 0.924 0.933 0.918 0.924 0.933 0.918 0.924 0.933 0.918 0.924 0.933		0.844 0.33 0.3 0.915 0.904 0.904 0.904 0.904 0.904 0.904 0.904 0.904 0.904 0.904 0.904 0.904 0.904 0.904 0.904 0.904						1000							0.972		0.985	186.0	102.70	0.989
0.759 0.785 0.812  1.1 0.4 0.2  0.4 0.2 0.2  0.4 0.2 0.2  0.005 0.010 0.020  0.850 0.887 0.883  0.850 0.887 0.883  0.850 0.887 0.883  0.850 0.904 0.916  0.891 0.902 0.916  0.891 0.902 0.916  0.991 0.992 0.993  0.914 0.924 0.932  0.914 0.924 0.933  0.918 0.900 0.020  0.919 0.920 0.990  0.910 0.020  0.910 0.920 0.990  0.911 0.924 0.933  0.912 0.990  0.916 0.927 0.990  0.917 0.924 0.933  0.918 0.929 0.990  0.918 0.929 0.990  0.919 0.937 0.990		0.846 0.3 0.3 0.915 0.915 0.914 0.914 0.914 0.914 0.916 0.916 0.916	!					±.75		176.0	0.952	0.957	196.0	0.966	176.0		0.983	186.0	0.987	066.0
0.4 0.2 0.2 0.4 0.2 0.2 0.40 0.20 0.20 0.850 0.867 0.883 0.850 0.867 0.883 0.850 0.867 0.883 0.850 0.804 0.905 0.2 0.1 0.0 1.5 0.6 0.3 0.892 0.904 0.916 0.891 0.902 0.916 0.891 0.902 0.916 0.991 0.992 0.993 0.914 0.924 0.993 0.914 0.924 0.993 0.913 0.924 0.993 0.914 0.924 0.993 0.918 0.903 0.993 0.918 0.903 0.993 0.918 0.903 0.994 0.908 0.903 0.994 0.908 0.903 0.994		0.3 0.3 0.905 0.904 0.904 0.7 1.0						0.927		976'0	0.954	0.958			0.972		0.983	186.0	0.987	686.0
0.005 0.010 0.020 0.850 0.867 0.883 0.850 0.867 0.883 0.850 0.867 0.883 0.2 0.1 0.0 1.5 0.6 0.3 0.891 0.903 0.915 0.891 0.903 0.915 0.891 0.903 0.915 0.904 0.904 0.906 0.914 0.924 0.936 0.913 0.924 0.932 0.914 0.924 0.933 0.913 0.924 0.933 0.913 0.924 0.933 0.913 0.924 0.933 0.913 0.924 0.933 0.914 0.924 0.933 0.914 0.924 0.933 0.915 0.904 0.933 0.906 0.907 0.904		0.030 0.0904 0.904 0.77 1.0										-		0.5		0	-0	0.0	1.0	6.3
0.005 0.010 0.020 0.850 0.867 0.883 0.850 0.867 0.883 0.2 0.1 0.0 1.5 0.6 0.3 0.005 0.010 0.020 0.891 0.902 0.915 0.891 0.902 0.915 0.891 0.902 0.915 0.891 0.902 0.915 0.891 0.902 0.916 0.891 0.902 0.916 0.891 0.902 0.916 0.991 0.922 0.933 0.913 0.924 0.933 0.913 0.924 0.933 0.913 0.924 0.933 0.914 0.924 0.933 0.915 0.910 0.020 0.936 0.937 0.944		0.050 			0.6	0.5	0.7	0.7	0.7	0.7	7	0.5	0.6	6.4	1.0	=	=	0.1	0.0	0.1
0.005 0.010 0.020 0.850 0.867 0.883 0.850 0.867 0.883 0.850 0.867 0.883 0.2 0.1 0.0 1.5 0.6 0.3 0.891 0.991 0.991 0.991 0.992 0.993 0.914 0.924 0.933 0.915 0.904 0.933 0.914 0.934 0.933 0.915 0.900 0.020 0.916 0.934 0.933 0.917 0.608 0.900 0.903 0.918 0.920 0.990 0.918 0.920 0.990 0.918 0.920 0.990 0.908 0.900 0.930 0.908 0.900 0.930		0.050 																		
0.005 0.010 0.020 0.850 0.867 0.883 0.850 0.867 0.883 0.852 0.886 0.883 0.852 0.886 0.883 0.892 0.011 0.0 0.892 0.014 0.020 0.891 0.090 0.0913 0.913 0.924 0.933 0.913 0.924 0.933 0.913 0.924 0.933 0.913 0.926 0.910 0.913 0.920 0.930 0.914 0.923 0.930 0.936 0.938 0.930 0.936 0.938 0.938 0.939		0.050 0.905 0.904 0.904 0.7 1.0	!												9	0.00				5000
0.850 0.867 0.883 0.853 0.867 0.883 0.850 0.867 0.883 0.883 0.882 0.91 0.00 0.00 0.881 0.902 0.91 0.902 0.914 0.924 0.925 0.906 0.926 0.936 0.906 0.926 0.93		6.936 6.944 6.77 6.050		0.150	0.200	0.250	0.300	0010	0.500	0.600	0.700	0.750	0.800	0.850	0,978)	0.950	(1.97)	1.980	(). (A.K)	S 1
0.25 0.367 0.383 0.2 0.1 0.0 1.5 0.6 0.3 0.005 0.010 0.020 0.892 0.091 0.916 0.891 0.903 0.915 0.891 0.903 0.915 0.891 0.903 0.915 0.891 0.903 0.915 0.891 0.903 0.915 0.891 0.903 0.915 0.891 0.903 0.913 0.993 0.993 0.993 0.994 0.994 0.993 0.994 0.994 0.994 0.996 0.994 0.994 0.996 0.997 0.994 0.996 0.997 0.994		0.904 0.914 0.7 1.0		6.929										9260	0.979	0.983			0.989	0.990
0.852 0.868 0.2 0.1 0.0 1.5 0.6 0.3 0.2 0.1 0.0 0.892 0.904 0.916 0.891 0.902 0.918 0.891 0.902 0.918 0.918 0.912 0.913 0.918 0.924 0.933 0.914 0.934 0.933 0.914 0.934 0.938 0.918 0.904 0.938 0.918 0.904 0.938 0.918 0.904 0.938 0.918 0.904 0.938 0.908 0.908 0.904 0.938 0.938 0.994		0.904 0.7 1.0 0.050		676								0.971	0.973	0.976	0.979	0.983	0.986		0.989	0.990
0.005 0.1 0.0 1.5 0.6 0.3 0.005 0.010 0.020 0.891 0.902 0.915 0.891 0.902 0.915 0.901 0.924 0.933 0.913 0.924 0.933 0.914 0.924 0.933 0.913 0.924 0.933 0.914 0.934 0.934 0.915 0.000 0.020 0.005 0.000 0.020 0.005 0.000 0.020 0.005 0.000 0.020 0.006 0.037 0.944 0.938 0.938 0.934		0.7 1.0 0.030		826.0	0.935	0.940	176.0	0.951	0.957	0.963	896.0			9/6.0	0.979	0.983			886.0	0.900
0.005 0.010 0.020 0.891 0.992 0.993		0.7 1.0 0.050		-							,			9	-	9	ć	-	-	=
0.005 0.000 0.020 0.892 0.994 0.916 0.891 0.902 0.915 0.891 0.902 0.913 1.5 1.3 1.4 0.9 1.7 2.6 0.005 0.010 0.020 0.914 0.924 0.933 0.914 0.924 0.933 0.914 0.924 0.933 0.915 3.0 2.8		0.050		0.7	99	1.8	970	17.0	6.5	6.2	5.0		1.0	0.3	0.2	0.2	0.3	0.3	<del>1</del> 0	0
0.005 0.001 0.000 0.891 0.901 0.915 0.891 0.902 0.915 0.891 0.902 0.915 0.991 1.7 2.6 0.005 0.010 0.020 0.914 0.924 0.933 0.904 0.932 0.930 0.506 1.0 0.508 0.904 0.934		0.050																		
0.892 0.904 0.916 0.891 0.905 0.915 0.891 0.902 0.915 0.99 1.7 2.6 0.005 0.001 0.020 0.913 0.924 0.933 0.914 0.924 0.933 0.918 0.924 0.933 0.918 0.924 0.933 0.918 0.924 0.933 0.918 0.924 0.933 0.918 0.924 0.934 0.938 0.936 0.944			0.100	0.150	0.200	0.250	0.300	00110	0.500	0.600	0.700	0.750	0.800	0.850	006.0				0.990	5(66.0)
0.005 0.004 0.916 0.891 0.904 0.915 0.891 0.902 0.913 0.903 0.904 0.903 0.914 0.904 0.903 0.914 0.904 0.903 0.915 0.904 0.903 0.916 0.904 0.903 0.906 0.906 0.900 0.906 0.906 0.900 0.906 0.907 0.904 0.906 0.907 0.904		820		i				Ì	ĺ					100 0	1				0000	1 00
0.005 0.0010 0.020 0.005 0.010 0.020 0.015 0.010 0.020 0.014 0.924 0.933 0.913 0.922 0.903 0.913 0.923 0.920 0.006 0.037 0.944 0.936 0.030 0.020		0.50.0												106.0					0.000	000
1.5 1.3 1.4 2.6 0.005 0.000 0.		06.6.0 86.0.0	0.040	0.945	0.950	0.6.0	756.0	596°D	0.509	27670	0.974	0.976	0.979	186.0	0.963	0.986	986.0	986.0	0660	166.0
1.5 1.3 1.4 0.9 1.7 2.6 0.005 0.000 0.020 0.913 0.924 0.933 0.914 0.924 0.933 0.913 0.924 0.933 0.913 0.92 0.930 1.3 0.6 1.0 0.5 3.0 2.8 0.005 0.001 0.020 0.93 0.936 0.944		07.													١.					
0.9 1.7 2.6 0.005 0.010 0.020 0.913 0.924 0.933 0.914 0.924 0.933 0.913 0.924 0.933 0.915 0.920 1.3 0.6 1.0 0.5 3.0 2.8 0.005 0.910 0.020 0.936 0.937 0.944	0.7	0.2	<u> </u>	0.3	0.0	0.1	0.2	0.3	0.5	0.3	0.2	6.5	<del>†</del> .0	0.3	6.5	0.3	0.3	- - -	<del>†</del> .	<u>C</u>
0.005 0.010 0.020 0.913 0.924 0.932 0.914 0.924 0.933 0.913 0.920 0.930 0.913 0.622 0.930 0.55 3.0 2.8 0.030 0.937 0.944 0.928 0.936 0.944		2.1		2.5						<del></del>					0.5	5.0	0.2	9.0	0.0	0.7
0.005 0.010 0.020 0.913 0.934 0.935 0.914 0.924 0.933 0.913 0.92 0.930 1.3 0.6 1.0 0.5 3.0 2.8 0.005 0.010 0.020 0.930 0.937 0.944																				
0.913 0.934 0.932 0.914 0.924 0.933 0.913 0.922 0.930 1.3 0.6 1.0 0.5 3.0 2.8 0.005 0.010 0.020 0.930 0.937 0.944	9 0.25	050.0	0.100	0.150	0.200	0.250	0.300	0.400	0.500	0.600	0.700	0.750	0.800	05870	0.900	056.0	0.975	0.980	0,990	0.995
0.914 0.924 0.933 0.913 0.925 0.930 0.930 0.930 0.930 0.930 0.930 0.930 0.934 0.938 0.934 0.938 0.934 0.934	2 0.935	0.944		0.958	0.962		İ	176.0	1	876.0	086.0	0.982	0.983	0.985	0.986	0.989	0.90	- 166.0 0.991	0.992	0.93
0.913 0.922 0.930 1.3 0.6 1.0 0.5 3.0 2.8 0.005 0.010 0.020 0.930 0.937 0.944 0.928 0.936 0.944	3 0.936	0.945		0.959	0.962			0.971		876.0	086.0	0.982	0.983	0.985	0.986	686.0	066.0	166.0	0.992	0.993
0.5 3.0 2.8 0.5 3.0 2.8 0.005 0.010 0.020 0.930 0.937 0.944 0.928 0.936 0.944	0 0.932	0.941	0.949	0.954	0.958	196.0	0.963	0.967	0.971	0.974	7.20	6/6/0	0.980	0.982	0.984	786.0	686.0	0.989	166'0	0.992
0.005 3.0 0.005 0.010 0.930 0.937 0.928 0.936		8.0		0.7									0.2	<b>1</b> .0	0.5	0.5	0.3	0.4	0.2	0.3
0.005 0.010 0.930 0.937 0.928 0.936	3.3	4.2	6.4	4.9	5.2	5.3	4.6	4.4	5.0	4.7	3.4	3.9	3.2	3.5	2.2	2.7	1.5	2.0	5:1	1.3
0.005 0.010																				
0.930 0.937		0.050	0.100	0.150	0.200	0.250	0.300	0,400	0.500	0.600	0.700	0.750	0.800	0.850	0.900	0.950	6.975	0.980	0.990	0.995
0.928 0.936	4 0.947	156.0		0.965	l				 	0.981	0.983	0.984	0.986	0.987	0.988	066.0	0.992	0.992	0.993	96.0
		0.953	196.0	0.965	0.968	176.0	0.973	0.976	0.979	186.0	0.983	0.985	986.0	0.987	0.988	0.990	0.992	0.992	0,993	66.0
0.927 0.933		0.949		0.96.0						776.0	6/6'0	186.0	0.982	186.0	0.985	886.0	066.0	066.0	166.0	0.00
RE <sub>1</sub> 3.3 1.8 0.6	1.5	8.0	6.3	0.2	0.3	9.0	9.0	0.1	0.5	0.1	9.0	8.0	0.5	0.0	9.0	0.4	9.0	0.0	0.0	0.4
4.6 5.6		8.5		8.5	¥.¥	9.2		1		7.0	6.5	5.3	6.2	5.3	4.1	3.5	3.8	3.0	2.5	4.7

Cumulative probabilities for W can be approximated according to

$$P(W \le w) \approx P\left(Z \ge \frac{(1-w)^{\tau} - \mu}{\sigma}\right)$$

for  $7 \le n \le 50$ , where Z is a standard normal variable.

#### 5. SUMMARY

The tables of coefficients presented here were developed on the basis of expected values, variances, and covariances of normal order statistics that recently were computed to high precision. The availability of these values made it possible to compute to high precision the coefficients used in the Shapiro-Wilk W statistic. Previous values were of limited precision, and those for higher values of n had been based on approximations. Similarly, the first and half moments of W were computed. Percentage points were developed using simulation methodology with calculations of W being based on the higher precision coefficients. Simple functional approximations were developed for the power transformation coefficients and the corresponding mean and standard deviation that are used to compute percentage points of W. The resulting approximations for the percentage points were shown to be more precise than previously available values for sample sizes between 25 and 50. The present technique can be implimented as easily as the method based on polynomial approximations. Inasmuch as the general relationships for  $\tau$ ,  $\mu$ , and  $\sigma$  (as functions of n) differ from those reported by Royston (1982), it would be of interest to investigate further these approximations for sample sizes above n = 50.

#### References

Godwin, H. J. (1949). Some low moments of order statistics. Annals of Mathematical Statistics 20, 279–285.

IMSL User's Manual: STAT/Library. IMSL, Inc., Houston, TX. 1987. 1232 pp.

Parrish, R. S. (1990). Comparison of quantile estimators in normal sampling. *Biometrics* 46, 247–257. Parrish, R. S. (1992a). Computing expected values of normal order statistics. *Communications in* 

Parrish, R. S. (1992a). Computing expected values of normal order statistics. *Communications in Statistics* (B)—Simulation and Computation 21, to appear.

Parrish, R. S. (1992b). Computing variances and covariances of normal order statistics. *Communications in Statistics (B)—Simulation and Computation 21*, to appear.

Royston, J. P. (1982a). An extension of Shapiro and Wilk's W test for normality to large samples. Applied Statistics 31, 115-124.

Royston, J. P. (1982b). Algorithm AS181: The W test for normality. Applied Statistics 31, 176-180.

Sarhan, A. E. and B. G. Greenberg (1956). Estimation of location and scale parameters by order statistics from singly and doubly censored samples. *Ann. Math. Statis.* 27, 427-451.

Sarhan, A. E. and B. G. Greenberg. *Contributions to Order Statistics*, Wiley, New York, 1962. 482 pp.

Shapiro, S. S. and R. S. Francia (1972). An approximate analysis of variance test for normality. *JASA* 67, 215–216.

Shapiro, S. S. and M. B. Wilk (1965). An analysis of variance test for normality (complete samples). *Biometrika* 52, 591-611.

#### **APPENDIX**

Computation of expected values, variances, and covariances of normal order statistics

Parrish (1992a) used the following approximations for computing the first two noncentral moments of the ith order statistic in a normal sample of size n. Numerical computations are based on Gauss-Legendre quadrature.

$$E[X_{im}^r] = K_{in} \int_{-\infty}^{\infty} x^r f(x) [F(x)]^{i-1} [1 - F(x)]^{n-i} dx$$

$$= K_{in} \int_{-12.2}^{12.2} x^r f(x) [F(x)]^{i-1} [1 - F(x)]^{n-i} dx + e_{in}$$

$$\approx K_{in} \sum_{j=1}^{N} w_j x_j^r f(x_j) [F(x_j)]^{i-1} [1 - F(x_j)]^{n-i}$$

for r = 1,2, where N is a predetermined number of integration points,  $x_i$  and  $w_i$  are Gaussian points and weights, respectively,

$$K_m = \frac{n!}{(n-i)!(i-1)!},$$

$$f(x) = \frac{1}{\sqrt{2\pi}} e^{-1/2x^2},$$

and

$$F(x) = \int_{-\infty}^{x} f(t)dt.$$

This method provided more than 25 decimal places of precision for expected values and variances.

Covariance computations were based on a similar approach. Noncentral product moments for the *i*th and *j*th order statistics from a normal sample of size *n* may be written as follows.

$$E[X_{i|n}X_{j|n}] = K_{ijn} \int_{-\infty}^{\infty} \int_{-\infty}^{y} xyf(x)f(y)[F(x)]^{i-1}$$

$$\times [1 - F(y)]^{n-j}[F(y) - F(x)]^{j-i-1} dx dy$$

$$= K_{ijn} \sum_{r=0}^{j-i-1} \sum_{s=0}^{j-i-1-r} \frac{(-1)^{r+s}(j-i-1)!}{r!s!(j-i-1-r-s)!} \gamma_{i+r,n-j+s+1}$$

where

$$K_{ijn} = \frac{n!}{(i-1)!(n-j)!(j-i-1)!},$$

$$\gamma_{i,j} = \frac{1}{ij} (\alpha_{i,j} + i\beta_{i-1,j} - \psi_{i,j}),$$

$$\alpha_{i,j} = \int_{-\infty}^{\infty} x[F(x)]^{j}[1 - F(x)]^{j} dx,$$

$$\beta_{i,j} = \int_{-\infty}^{\infty} x^{2}f(x)[F(x)]^{j}[1 - F(x)]^{j} dx,$$

and

$$\Psi_{i,j} = \int_{-\infty}^{\infty} [F(x)]^{i} \int_{x}^{\infty} [1 - F(y)]^{j} dy dx;$$

see Godwin (1949). By using finite limits of -12.2 to 12.2 in each integral and applying Gauss-Legendre integration techniques, the following approximations were obtained.

$$\alpha_{i,j} \approx \sum_{k=1}^{N} w_k x_k [F(x_k)]^{i} [1 - F(x_k)]^{i},$$

$$\beta_{i,j} \approx \sum_{k=1}^{N} w_k x_k^2 f(x_k) [F(x_k)]^{i} [1 - F(x_k)]^{i},$$

$$\Psi_{i,j} \approx \sum_{k=1}^{N} \sum_{m=1}^{N} w_{km} [F(x_k)]^{i} [F(x_m)]^{i}.$$

These approximations enable the computation of product moments to high precision. Using these results, high-precision values for covariances can be obtained.