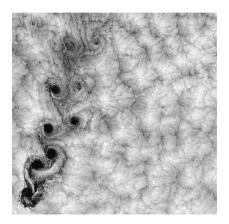


# Two-dimensional cylinder flow at low Reynolds numbers

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A canonical example of flow oscillators



A canonical example of flow oscillators

Its dynamics are governed by the Navier-Stokes equations

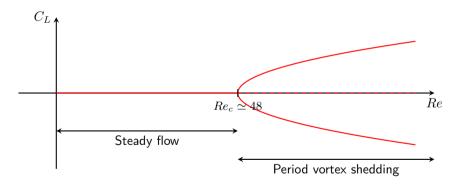
$$\frac{\partial \boldsymbol{u}}{\partial t} + \nabla \cdot (\boldsymbol{u} \otimes \boldsymbol{u}) = -\nabla p + \frac{1}{Re} \nabla^2 \boldsymbol{u}$$
$$\nabla \cdot \boldsymbol{u} = 0$$

Add DNS movie

where  $\boldsymbol{u}(\boldsymbol{x},t)$  is the velocity field and  $p(\boldsymbol{x},t)$  is the pressure field.

A canonical example of flow oscillators

Bifurcation diagram



Finding fixed points

$$abla \cdot (oldsymbol{u} \otimes oldsymbol{u}) = -
abla p + rac{1}{Re} 
abla^2 oldsymbol{u}$$

Define the state vector  $\mathbf{q} = (\mathbf{u}, p)^T$ . Reformulate the problem as a root-finding problem  $\mathcal{F}(\mathbf{q}, Re) = \mathbf{0}$  and use Newton's method (or variants) to solve it.

Finding fixed points

Add Evolution of the base flow

Linear stability analysis

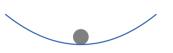
Denote by  $U_b(x, Re)$  the base flow and linearized around it to obtain the linearized system

$$oldsymbol{B} rac{doldsymbol{q}}{dt} = oldsymbol{L}oldsymbol{q}$$

and look for the eigenvalues and eigenvectors of the generalized eigenvalue problem

$$\lambda B \hat{q} = L \hat{q}$$

using numerical eigensolvers.

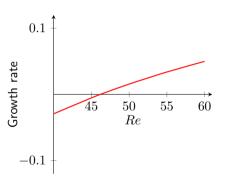


Stable equilibrium



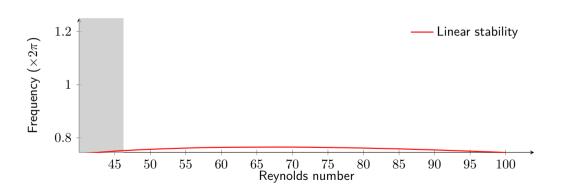
Unstable equilibrium

Linear stability analysis

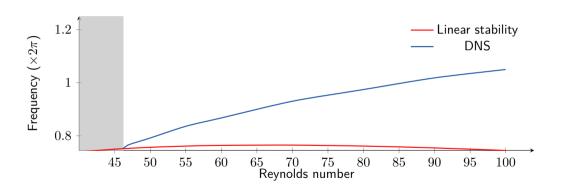


- Leading eigenvalues come in complex-conjugate pairs.
- Hopf bifurcation at  $Re \simeq 46.27$ .

Linear stability vs. real life



Linear stability vs. real life



Linear stability vs. Nonlinear evolution

Stability mode

POD mode





Base flow vs. mean flow

Base flow solution

Time-averaged solution

Modeling objectives

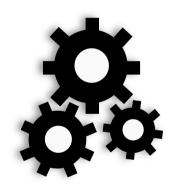
**Objective:** Simple model capturing the essence of the problem.

- 1. Linearly unstable nature of the fixed point.
- 2. Captures the transition to the limit cycle.
- 3. Explains why the base flow and mean flow are so different.
- 4. Explains why the frequency predictions are bad.
- 5. Capture the Reynolds number dependence.

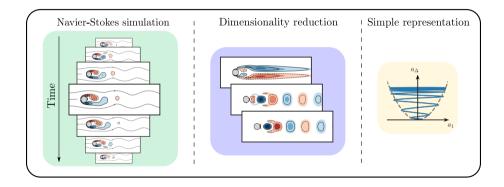


Modeling strategy

- Transform PDE into a handful of ODE.
  - → Dimensionality reduction, reduced-order modeling, . . .
- Statistical inference of the parameters.
  - → Least-squares, calibration techniques, interpolation, . . .
- Mathematical analysis of the model's properties.
  - $\hookrightarrow$  Linear and weakly nonlinear analyses, comparison with ground truth, ...



Dimensionality reduction

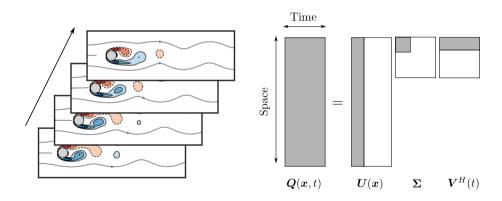


Dimensionality reduction

**Objective:** Find proxies for the vortex shedding's amplitude, phase and distortion between the base flow and the mean flow.

- Snapshots of the full state vector  $\{m{q}(m{x},t_k)\}$  are available :
- If only limited sensor measurements are available :
  - $\hookrightarrow$  Use time-delay embeddings to construct the proxies.

Dimensionality reduction



Dimensionality reduction

<u>Modes 1 and 2:</u> Spatial structure of the vortex shedding. Their time-dependant amplitudes provide our proxy variables to describe the evolution of the oscillations.

<u>Mode 3:</u> Distortion between the base flow and the mean flow. Its amplitude provides the remaining proxy variable for our model.

Low-dimensional representation

Low-order model

**Objective:** Obtain a dynamical system describing the evolution of our proxy variables.

#### Model

- If the original equations are known :

$$\dot{\boldsymbol{x}} = \boldsymbol{f}(\boldsymbol{x}, Re)$$

- If the original equations are unknown :

POD-Galerkin projection

Step 1 : Galerkin expansion of the velocity field as

$$\boldsymbol{u}(\boldsymbol{x},t) \simeq \boldsymbol{U}_b(\boldsymbol{x}) + \boldsymbol{u}_1(\boldsymbol{x})a_1(t) + \boldsymbol{u}_2(\boldsymbol{x})a_2(t) + \boldsymbol{u}_{\Delta}a_{\Delta}(t) + \cdots$$

**Step 2 :** Inject the Galerkin expansion into the Navier-Stokes equations and project onto the span of the POD modes.

$$oldsymbol{U}^T oldsymbol{U} rac{doldsymbol{a}}{dt} = oldsymbol{U}^T oldsymbol{f}(oldsymbol{U}oldsymbol{a}, Re)$$

**Step 3**: Inspect the model and use for rapid (approximate) simulations of the original system.

POD-Galerkin reduced-order model

#### Reduced-order model

$$\dot{x} = \sigma x - \omega y - xz - \alpha yz$$
$$\dot{y} = \omega x + \sigma y - yz + \alpha xz$$
$$\dot{z} = -z + x^2 + y^2$$

POD-Galerkin reduced-order model

Physical analysis

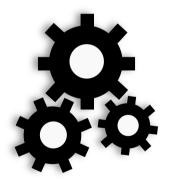
**Objective:** What can this model tell us about the physics of the problem and to what extent is it correct?

#### Physical consistency :

- → Does it respect the known physics?
- → Are its predictions consistent with the observations?

#### Improved understanding :

- What does it tells us about the problem which was not directly obvious?
- → What insights are to be gained?



Reduced-order model consistency

Property: The quadratic nonlinear term in Navier-Stokes equations is energy-preserving.

The kinetic energy is given by  $E(t) = \|\boldsymbol{a}(t)\|_2^2$  and we thus have

$$\begin{aligned} \frac{dE}{dt} &= \frac{1}{2} \boldsymbol{a}^T \dot{\boldsymbol{a}} \\ &= \frac{1}{2} (x\dot{x} + y\dot{y} + z\dot{z}) \\ &= \sigma(x^2 + y^2) - z^2 \end{aligned}$$

Only the linear terms in our model contribute to this energy budget.

Reduced-order model consistency

**Property:** The fixed point has a two-dimensional unstable subspace characterized by complex-conjugate eigenvalues.

The Jacobian matrix of the system reads

$$\boldsymbol{J} = \begin{bmatrix} \sigma - z & -\omega - \alpha z & -x - \alpha y \\ \omega + \alpha z & \sigma - z & -y + \alpha x \\ 2x & 2y & -1 \end{bmatrix}$$

For (x,y,z)=(0,0,0) and  $\sigma>0$ , its eigenvalues are  $\sigma\pm i\omega$  and -1.

What insights are to be gained?

What can this reduced-order model actually tell me about the two-dimensional cylinder flow ?

$$\dot{x} = \sigma x - \omega y - xz - \alpha yz$$
$$\dot{y} = \omega x + \sigma y - yz + \alpha xz$$
$$\dot{z} = -z + x^2 + y^2$$

$$\begin{split} \dot{x} &= \sigma x - \omega y - xz - \alpha yz \\ \dot{y} &= \omega x + \sigma y - yz + \alpha xz \\ \dot{z} &= -z + x^2 + y^2 \end{split}$$

$$\dot{\eta} = (\sigma + i\omega) \eta - \eta z + i\alpha z$$
$$\dot{z} = -z + |\eta|^2$$

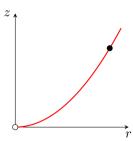
$$\dot{r} = (\sigma - z) r$$

$$\dot{\varphi} = \omega + \alpha z$$

$$\dot{z} = -z + r^{2}$$

What insights are to be gained?

Both the linearly unstable baseflow (r,z)=(0,0) and linearly stable mean flow  $(r,z)=(\bar{r},\bar{z})$  are fixed points of the phase-averaged equations.



What insights are to be gained?

Distortion eq:  $\dot{z} = -z + r^2$ 

As r increases, the amplitude z of the distortion increases. It does so until a balance is met where  $z=r^2$ . Here,  $r^2$  plays the role of the **Reynolds stesses** in the Navier-Stokes eqn.

Amplitude eq :  $\dot{r} = (\sigma - z) r$ 

 $\sigma-z$  is the **effective growth rate** of the instability. The amplitude of the vortex shedding grows until a balance is met where  $z=\sigma.$ 

Two-timing approximate solution

Assume that  $\sigma=\epsilon^2$  and introduce a multiple time-scale expansion with  $\tau=\epsilon^2 t$ . Expanding the solution in the vicinity of  $(r_0,z_0)=(0,0)$  yields

$$r(t,\epsilon) = \epsilon r_1(t,\tau) + \epsilon^2 r_2(t,\tau) + \epsilon^3 r_3(t,\tau) + \cdots$$
  
$$z(t,\epsilon) = \epsilon z_1(t,\tau) + \epsilon^2 z_2(t,\tau) + \epsilon^3 z_3(t,\tau) + \cdots$$

We can now use **regular perturbation theory** to obtain an approximation of the evolution of r(t) and z(t).

Two-timing approximate solution

After some algebraic manipulations, we obtain that the vortex shedding's amplitude obeys  $\dot{}$ 

$$\frac{dr}{dt} = \sigma r - r^3$$

while the evolution of the distortion is given by

$$z(t) = Ae^{-t} + r^{2}(t) (1 - e^{-t}) + \mathcal{O}(\epsilon^{3}).$$

and so, very rapidly we have  $z(t) \approx r^2(t)$ .

Further reducing the model's complexity...

$$\dot{r} = \sigma r - r^3$$

$$\dot{\varphi} = \omega + \alpha z$$

$$z = r^2$$

Piecing everything together

The power of mathematical modeling

Our model explains most of the dynamics observed in the flow :

- Saturation mechanism for the vortex shedding's amplitude,
- The baseflow gets distorted into the mean flow through the Reynold stresses,
- This distortion simultaneously induces a frequency shift.

To date, this is the simplest yet most accurate reduced-order model of the cylinder flow.

What next?

Despite its accuracy and interpretability, our model leaves some questions unanswered, e.g.

- What is the physical mechanism responsible for the instability in the first place ?
- How exactly does the spatial support of the different structures evolves as their amplitude grows?
- To what extent is our model generic and applicable to other flows?

This is where we leave the realm of dynamical systems and enter that of classical fluid mechanics.