

Solutions to *The Art of Electronics 3rd Edition*

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# Solutions for Chapter 2

## Exercise 2.1

In order to solve this problem, many assumptions must be made. Different people may assume slightly different values for parameters. This is OK. What is important is making good assumptions and checking our conclusions to make sure they are reasonable.

To solve for the current in the LED, let us assume we know the LED is red, so it follows the red LED curve from Figure 2.8 in the book. Let us also assume the transistor is acting like a closed switch, so the collector voltage of Q1 is close to 0 V. Let us also assume the LED is ON, so its voltage is approximately  $V_{\text{LED}} = 2 \text{ V}$ . From the preceding assumptions, we can calculate that the LED current is

$$I_{\text{LED}} = \frac{3.3 \text{ V} - 2 \text{ V}}{330 \Omega} = \frac{1.3 \text{ V}}{330 \Omega} \approx 3.94 \text{ mA}$$

If we use Figure 2.8 (from the textbook) to check our numbers, we see that a current of 3.94 mA roughly correlates to an LED voltage of  $V_{\text{LED}} = 1.7 \text{ V}$ . We will run the same calculation again to reduce our error.

$$I_{\text{LED}}^* = \frac{3.3 \text{ V} - 1.7 \text{ V}}{330 \Omega} = \frac{1.6 \text{ V}}{330 \Omega} \approx \boxed{4.85 \text{ mA}}$$

In order to determine the minimum current gain required from our transistor, we must calculate the base current. Let us assume we know the base-emitter voltage  $V_{\text{BE}} = 0.6 \text{ V}$ . Therefore

$$I_{\text{B}} = \frac{3.3 \text{ V} - 0.6 \text{ V}}{10 \text{ k}\Omega} = 270 \mu\text{A}$$

So the minimum current gain must be

$$\beta_{\text{min}} = \frac{I_{\text{LED}}^*}{I_{\text{B}}} \approx \frac{4.85 \text{ mA}}{270 \mu\text{A}} \approx \boxed{18.0}$$

## Exercise 2.2

When  $Q_1$  goes is in saturation, the base voltage of  $Q_2$  equals the opposite of the voltage on the capacitor  $C_1$  at  $t = 0 \text{ s}$ ,  $V_0 = 4.4 \text{ V}$  and  $Q_2$  is then cutoff.  $V_{\text{out}}$  will be equal to 5 V until  $Q_2$  is brought in saturation again. This happens when its base voltage gets higher or equal to the  $Q_2$  threshold voltage (0.6 V). As soon as  $Q_1$  is brought in saturation,  $C_1$  starts to discharge into the resistor  $R_3$  and the equivalent circuit, valid until  $Q_2$  is cutoff, is then:

Figure 1.1: Equivalent  $C_1$  discharging circuit.

The time evolution of the voltage across the capacitor  $C_1$  is given by:

$$V_C(t) = (V_0 - V_\infty) e^{-\frac{t}{R_3 C_1}} + V_\infty$$

where  $V_\infty$  is the steady-state voltage on the capacitor  $C_1$  and equals  $-5\text{ V}$ . Given the considerations above, we have that  $V_C(t = T_{\text{pulse}}) = -0.6\text{ V}$ . Solving for  $t$  gives:

$$T_{\text{pulse}} = -R_3 C_1 \ln \left( \frac{-0.6\text{ V} - V_\infty}{V_0 - V_\infty} \right) = \boxed{0.76 R_3 C_1 = 76\text{ }\mu\text{s}}$$

### Exercise 2.3

The output voltage is now influenced by  $R_5$  that goes in series with  $R_4$ , and by the  $V_{\text{BE}}$  of  $Q_3$  which is equal to  $0.6\text{ V}$  when the transistor is in saturation. Therefore:

$$V_{\text{out}} = \frac{R_5}{R_5 + R_4} (5\text{ V} - 0.6\text{ V}) + 0.6\text{ V} = \boxed{4.79\text{ V}}$$

The minimum value of  $\beta$  of  $Q_3$  can be obtained looking at the maximum value of the current flowing through the collector of  $Q_3$ ,  $I_c^{Q_3}$ . As soon as  $Q_1$  goes in saturation, the capacitor  $C_1$  starts to discharge and its current is given by  $C_1 dV_C/dt$ . With reference to the variables introduced in the previous exercise (2.2):

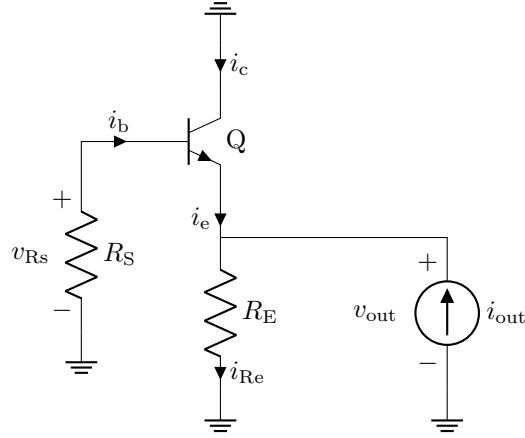
$$I_c^{Q_3}(t) = \frac{5\text{ V}}{R_2} - I_{C_1}(t) = \frac{5\text{ V}}{R_2} + C_1 \frac{1}{R_3 C_1} (V_0 - V_\infty) e^{-\frac{t}{R_3 C_1}}$$

Therefore:

$$\beta_{\min} = \frac{I_c^{Q_3}(t)|_{\max}}{I_b^{Q_3}} = \frac{I_c^{Q_3}(t=0\text{ s})}{I_b^{Q_3}} = \boxed{27}$$

## Exercise 2.4

Figure 1.2: Emitter follower circuit used for computing the output resistance



Applying the KCL on the Q transistor:

$$i_e = i_b + i_c = i_b (\beta + 1)$$

The current flowing through the emitter resistor  $R_E$  is equal to:

$$i_{Re} = i_e + i_{out} = i_b (\beta + 1) + i_{out}$$

Since for the emitter follower  $v_{Rs} = v_{out}$ :

$$[i_b (\beta + 1) + i_{out}] R_E = v_{out}$$

Since:

$$i_b = -\frac{v_{Rs}}{R_S} = -\frac{v_{out}}{R_S}$$

we can write:

$$\left[ -\frac{v_{out}}{R_S} (\beta + 1) + i_{out} \right] R_E = v_{out}$$

Therefore:

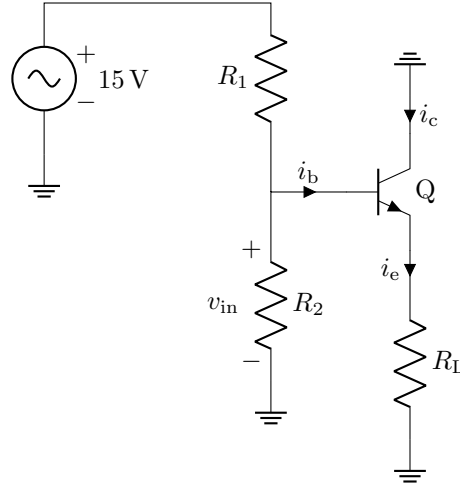
$$R_{out} = \frac{v_{out}}{i_{out}} = \frac{R_E R_S}{R_S + (\beta + 1) R_E}$$

If  $R_E \gg R_S/(\beta + 1)$ :

$$R_{out} \approx \frac{R_S}{(\beta + 1)}$$

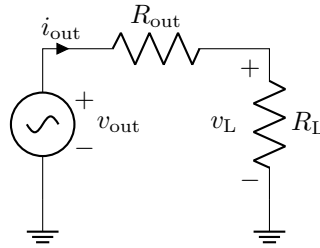
## Exercise 2.5

Figure 1.3: Small signal circuit



In order to achieve a maximum voltage change of 5% for a maximum current to the load ( $R_L$ ) equal to 25 mA, we can make reference to the equivalent circuit of Figure 1.4:

Figure 1.4: Output equivalent circuit



obtaining:

$$\left. \frac{v_{\text{out}} - v_L}{v_{\text{out}}} \right|_{i_{\text{out}} = 25 \text{ mA}} = 0.05$$

Since

$$v_{\text{out}} - R_{\text{out}} i_{\text{out}} = v_L$$

and for an emitter follower  $v_{\text{out}} = v_{\text{in}} = 5 \text{ V}$  we can write:

$$\frac{R_{\text{out}} 25 \text{ mA}}{5 \text{ V}} = 0.05$$

obtainin the following condition on  $R_{\text{out}}$ :

$$R_{\text{out}} = \frac{0.05 \cdot 5 \text{ V}}{25 \text{ mA}}$$



For the emitter follower configuration:

$$R_{\text{out}} = \frac{R_{\text{in}}}{\beta + 1}$$

and we see from the circuit of Figure 1.3 that  $R_{\text{in}}$  is given by the parallel between  $R_1$  and  $R_2$ :

$$R_{\text{in}} = \frac{R_1 R_2}{R_1 + R_2}$$

In order to achieve  $v_{\text{in}} = 5 \text{ V}$ , the following condition must be verified for the values of  $R_1$  and  $R_2$ :

$$\frac{R_2}{R_1 + R_2} = \frac{5 \text{ V}}{15 \text{ V}}$$

Assuming  $\beta = 100$ , we can finally obtain:

$$\boxed{R_1 = 30 \Omega, R_2 = 15 \Omega}$$

## Exercise 2.6

The minimum current flowing through the  $R$  resistor has to be at least equal to the maximum current to the load plus the minimum current to the zener:

$$I_{\text{min},R} = \frac{20 \text{ V} - 10 \text{ V}}{R} \geq 100 \text{ mA} + 10 \text{ mA}$$

Therefore:

$$R \leq \frac{10 \text{ V}}{110 \text{ mA}} = \boxed{91 \Omega}$$

It follows that the maximum power to the zener, selecting  $R = 91 \Omega$ , is equal to

$$P_{\text{max},z} = \left( \frac{25 \text{ V} - 10 \text{ V}}{91 \Omega} - 0 \text{ A} \right) 10 \text{ V} = \boxed{1.65 \text{ W}}$$

## Exercise 2.7

With reference to figure 2.21 of the book, neglecting the current entering the base of the transistor  $Q$ , in order to have at least 10 mA flowing through the zener, the resistor  $R$  should comply with the following condition:

$$\frac{20 \text{ V} - 10 \text{ V}}{R} \geq 10 \text{ mA}$$

which results in:

$$\boxed{R \leq 1 \text{ k}\Omega}$$

In order to avoid the transistor to be saturated, we want the collector-base voltage to be always higher than zero. This translates in:

$$R_C < R \frac{10 \text{ mA}}{100 \text{ mA}} = 100 \Omega$$

Selecting a conservative value of  $R_C$  equal to  $\boxed{20 \Omega}$ , we can compute the maximum power dissipated by the zener,  $P_{\text{max},z}$  and the transistor,  $P_{\text{max},Q}$  as:

$$P_{\text{max},z} = \left( \frac{25 \text{ V} - 10 \text{ V}}{1 \text{ k}\Omega} \right) 10 \text{ V} = \boxed{0.15 \text{ W}}$$

$$P_Q = (25 \text{ V} - 20 \Omega I_{\text{load}}) I_{\text{load}}$$

The maximum power dissipated by the transistor is obtained for a collector current equal to 625 mA which is higher than the maximum load current. Therefore, in our case, the maximum power dissipated by  $Q$  will be obtained for  $I_{\text{load,max}} = 100 \text{ mA}$ :

$$P_{\text{max,Q}} = (25 \text{ V} - 20 \Omega I_{\text{load,max}}) I_{\text{load,max}} = \boxed{2.3 \text{ W}}$$

Comparing the results with those of the previous exercise, we notice that the power dissipated by the zener diode significantly decreased but we have an additional power dissipated by the transistor which is higher than the power that the zener diode dissipated in the circuit of the previous exercise. However this power can be decreased by increasing the value of  $R_C$ .

## Exercise 2.8

In order to keep the emitter voltage  $V_E$  in the half range of the dc supply, considering the quiescent current of 5 mA we have:

$$V_E = \frac{15 \text{ V} - (-15 \text{ V})}{2} = 15 \text{ V}$$

and the emitter resistor  $R_E$ :

$$R_E = \frac{15 \text{ V}}{5 \text{ mA}} = \boxed{3 \text{ k}\Omega}$$

Since the input impedance to the transistor, under the assumption of a load resistance much larger than the emitter resistance, is:

$$R_{\text{in}} = \beta R_E = 300 \text{ k}\Omega$$

in order to have the 3 dB point below the lowest frequency of 20 Hz, the capacitor  $C_1$  has to be:

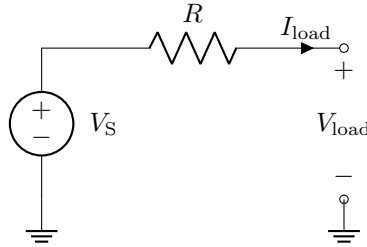
$$\frac{1}{R_{\text{in}} C_1} \leq 20 \text{ Hz}$$

meaning that:

$$\boxed{C_1 \geq 0.17 \mu\text{F}}$$

## Exercise 2.9

Figure 1.5: Current source circuit



We want:

$$\frac{I_{\text{load}}^{\text{max}} - I_{\text{load}}^{\text{min}}}{I_{\text{load}}^{\text{max}}} = \frac{V_S - 0 \text{ V} - (V_S - 10 \text{ V})}{V_S - 0 \text{ V}} = 0.01$$

from which it follows:

$$\boxed{V_S = 1 \text{ kV}}$$

## Exercise 2.10

With reference to Figure 1.5, we assume that  $I_{\text{load}}$  is equal to 10 mA if  $V_{\text{load}}$  is equal to 0 V, which means  $R_{\text{load}}$  is equal to 0  $\Omega$ . We can therefore calculate  $R$  as:

$$R = \frac{V_S}{10 \text{ mA}} = 100 \text{ k}\Omega$$

In this case we have:

$$P_{\text{load}} = 0 \text{ W}, P_R = I_{\text{load}}^2 R = 10 \text{ W}$$

If  $V_{\text{load}} = 10 \text{ V}$ , from the condition of the previous exercise, we have:

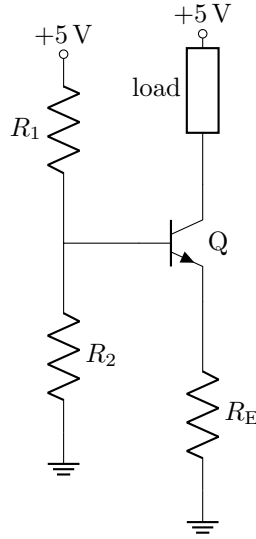
$$I_{\text{load}} = (1 - 0.01)10 \text{ mA} = 9.9 \text{ mA}$$

Therefore:

$$P_{\text{load}} = 10 \text{ V} I_{\text{load}} = 0.1 \text{ W}, P_R = I_{\text{load}}^2 R = 9.8 \text{ W}$$

## Exercise 2.11

Figure 1.6: Current sink



In order to have an emitter current equal to 5 mA, the following condition has to be verified:

$$\frac{R_2}{R_1 + R_2} 5 \text{ V} - 0.6 \text{ V} = R_E 5 \text{ mA}$$

Furthermore, the transistor shouldn't sensibly load the voltage divider, therefore:

$$\frac{R_1 R_2}{R_1 + R_2} \ll R_E \beta$$

Since we have a dc voltage of 5 V, we want the voltage on  $R_2$  to be lower or equal to this value:

$$R_E 5 \text{ mA} + 0.6 \text{ V} \leq 5 \text{ V}$$

leading to:

$$R_E \leq 880 \, \Omega$$

A good guess value for  $R_E$  could be:

$$R_E = 200 \, \Omega$$

The base voltage will be given by:

$$V_B = R_E 5 \, \text{mA} + 0.6 \, \text{V} = 1.6 \, \text{V}$$

Selecting  $R_1 = 1 \, \text{k}\Omega$  it is possible to compute  $R_2$ :

$$R_2 = 470 \, \Omega$$

The impedance seen by the input of the transistor is equal to  $320 \, \Omega$  and the input impedance of the transistor, considering  $\beta = 100$ , is  $R_E \beta = 20 \, \text{k}\Omega$  with the former much lower than the latter. Finally, considering a maximum  $V_{CE}$  voltage of the transistor equal to  $0.2 \, \text{V}$  before it saturates, we obtain the compliance voltage on the load as:

$$V_{\text{comp}} = 5 \, \text{V} - (0.2 \, \text{V} + R_E 5 \, \text{mA}) = 3.8 \, \text{V}$$

Exercise 2.12 **TODO: write solution**

Exercise 2.13 **TODO: write solution**

Exercise 2.14 **TODO: write solution**

Exercise 2.15 **TODO: write solution**

Exercise 2.16 **TODO: write solution**

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Exercise 2.30 **TODO: write solution**