

Lecture Presentation
Nuclear Magnetic Resonance Logging

PGE385(M,K)

**Petrophysics of Nuclear
Magnetic Resonance
Measurements**

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Petrophysical Applications of NMR Data

- ▣ Mineralogically-Independent Porosities (**Total & Effective**)
- ▣ Clay-Bound Water Volume
- ▣ Capillary-Bound Water & Free Fluid Volumes
- ▣ Pore Size Distribution (**Single Phase Fluid Saturation**)
- ▣ Permeability (**With calibration to core or test data**)
- ▣ Shale Volume & Distribution
- ▣ Flushed Zone Fluid Saturations (**DTW analysis**)
- ▣ Hydrocarbon Viscosity (**DTE analysis**)
- ▣ Electrical Properties & Water Saturation (**Integrated Products**)

Basic NMR Data

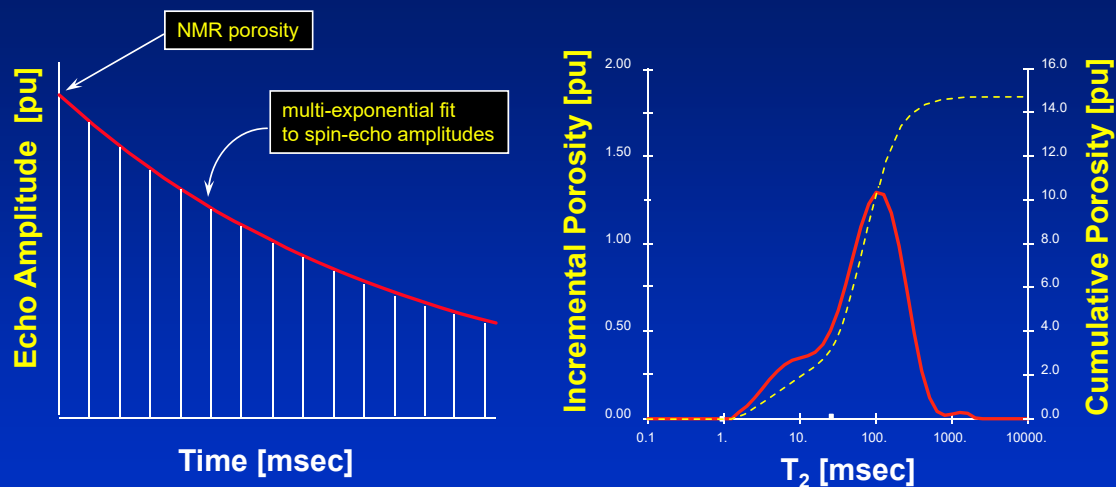
NMR measurements provide:

- Echo Amplitudes
- Echo Decay Rates

Calibrated transforms provide:

- Mineralogically Independent Porosities.
- Clay Bound Water
- Capillary Bound Water & Free Fluid Volumes
- Permeability

Echo Train Inversion Processing

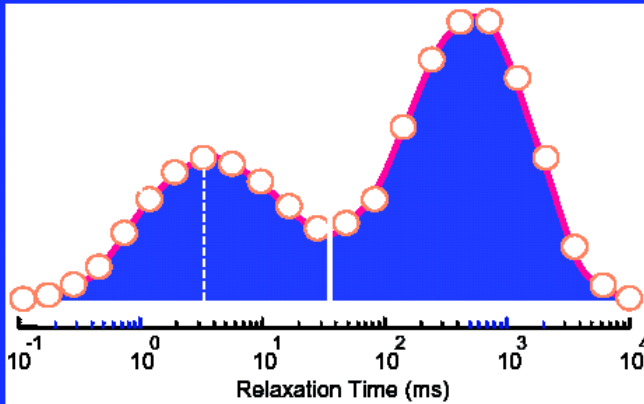


Acquisition Time Domain

Inversion
Processing

T_2 Relaxation Time Domain

Calculation of Petrophysical Parameters from the NMR T2 distribution



$$\phi = \sum_{j=1}^N a_j$$

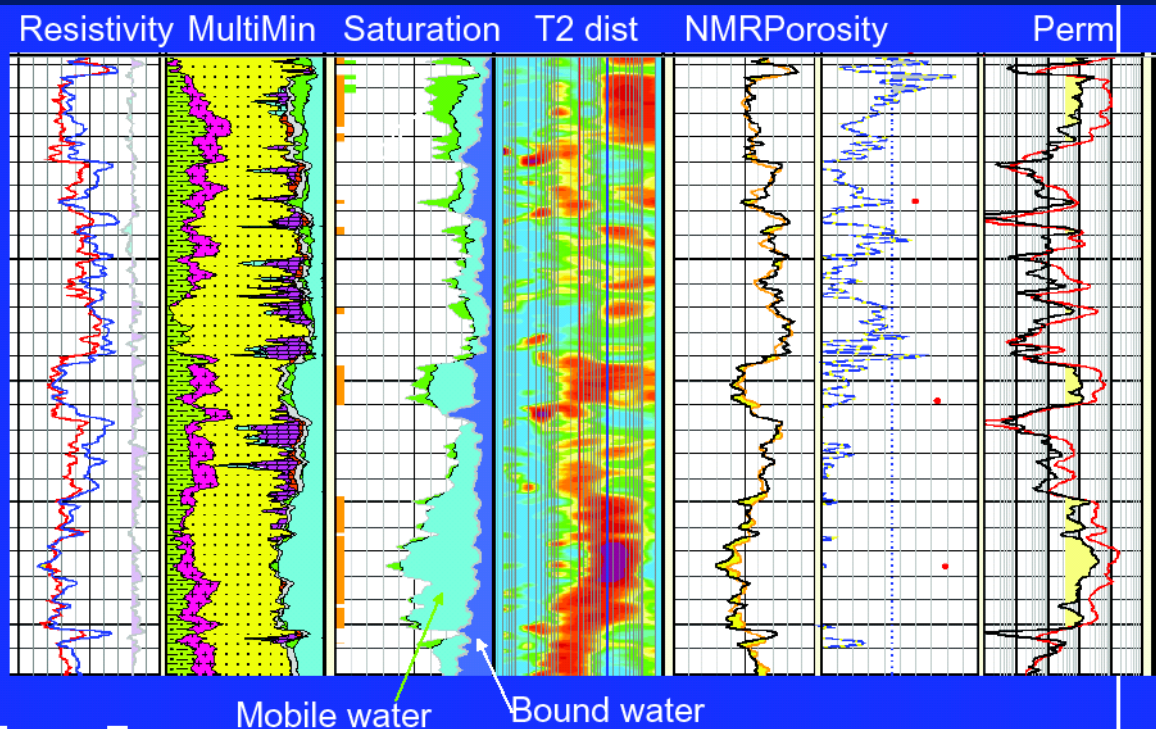
$$BVI = \sum_{j=1}^{N_{cut}} a_j$$

$$FFI = \sum_{j=N_{cut}+1}^N a_j$$

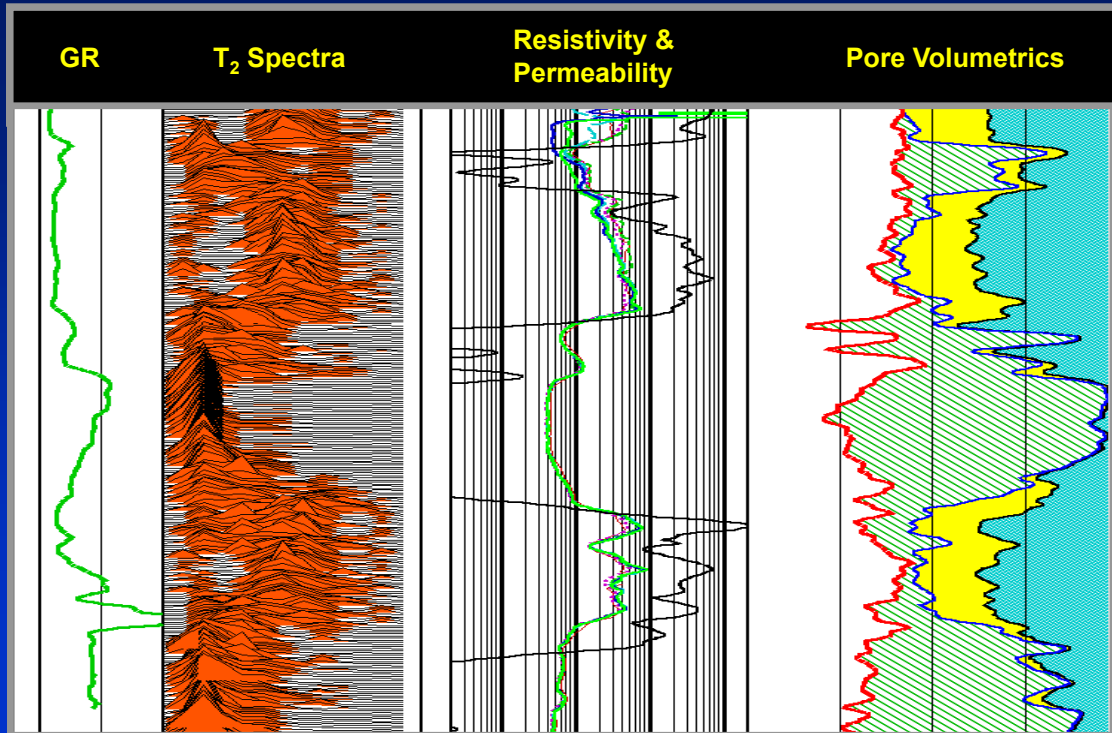
$$\kappa = \left[\left(\frac{\phi}{10} \right)^2 \frac{FFI}{BVI} \right]^2$$

$$\eta = aT/T_{2G}^{oil}$$

EXAMPLE



Basic NMR Field Deliverable

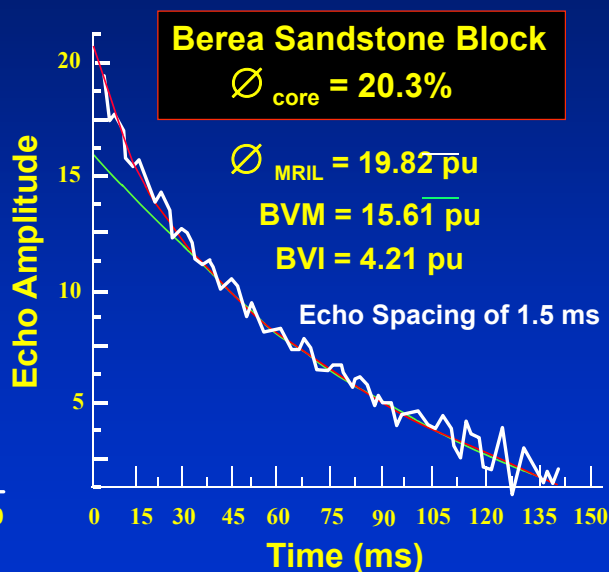
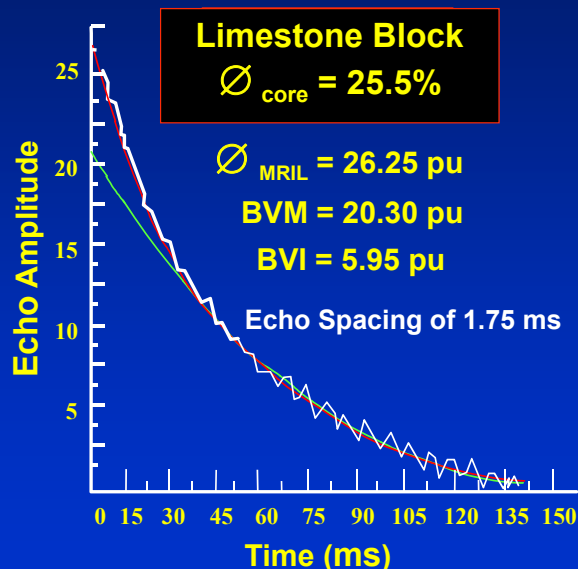


NMR Porosity Definitions

- **Effective \emptyset** - Pore volume excluding clay bound water.
- **Total \emptyset** - Pore volume including clay bound water.
- **CBW** - Clay bound water, which represents anion-free water adsorbed within clay inter-layers.
- **BVI** - Bulk volume irreducible water which includes water retained by capillary forces in small pores, and water wetting pore surfaces.
- **BVM** - Free-fluid volume which is available for hydrocarbon storage and fluid flow.

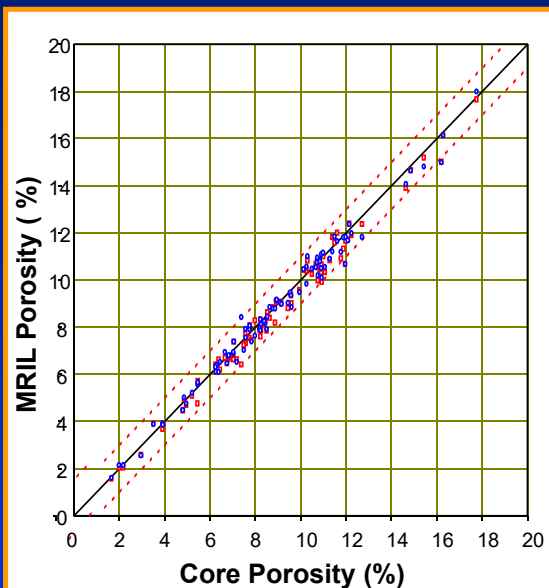
MRIL Porosity - Test Pit Verification

— Echo Amplitude — Complete Echo Fit Results — BVM Fit Results

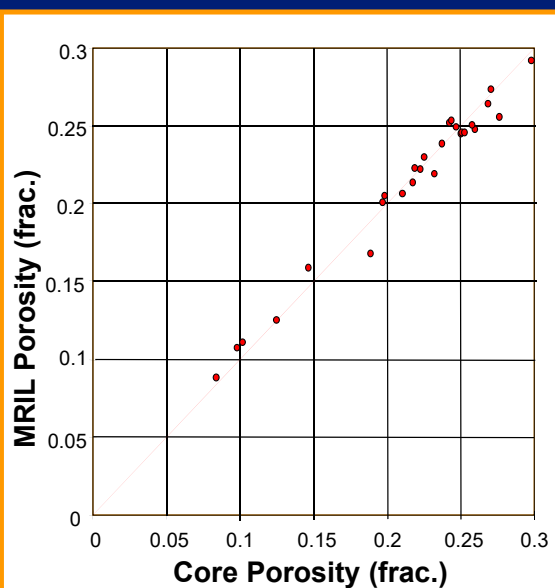


Mineralogy-Independent Porosity

Gulf of Mexico Sandstone



Middle East Carbonate



Porosity Considerations

Although NMR porosity is mineralogically Independent, it is not fluid independent.

NMR porosity can be too low when :

- Hydrogen Index of reservoir fluids < 1.0
- Reservoir fluids with long T_1 are only partially polarized due to insufficient acquisition wait time (TW)
- “Solid hydrocarbons” (tar) are present with relaxation rates faster than the measurement time window
- Internal gradients caused from magnetic minerals accelerate NMR echo decay to below measurement time window

COMPARISON OF DISTRIBUTIONS

Sandstone

$K_{air} = 2.15$ md

Porosity = 9.7 p.u.

$\rho_e = 23.0$ $\mu\text{m}/\text{sec}$.

Dolomite

$K_{air} = 7.41$ md

Porosity = 15.8 p.u.

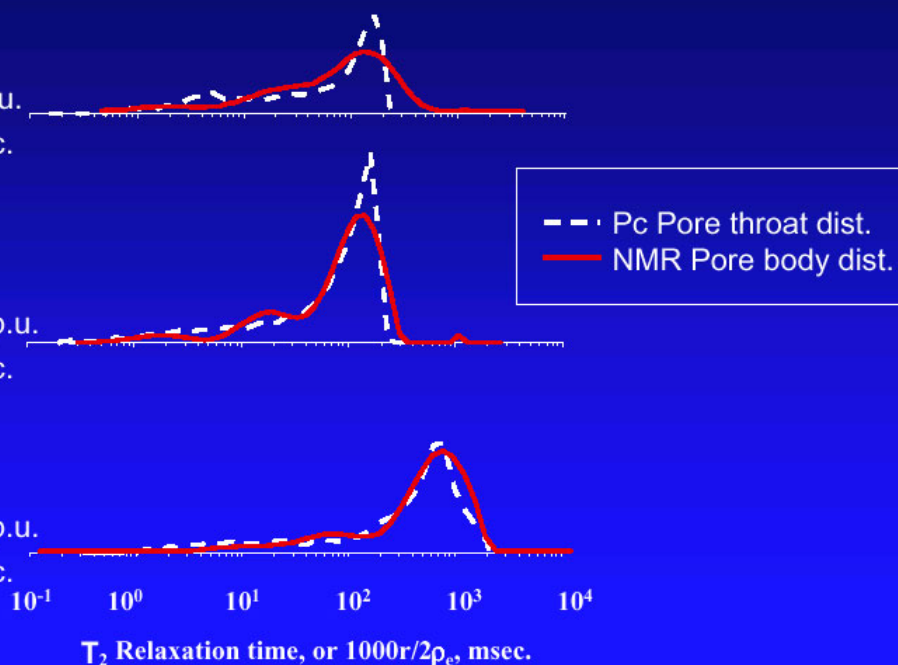
$\rho_e = 5.35$ $\mu\text{m}/\text{sec}$.

Limestone

$K_{air} = 12.3$ md

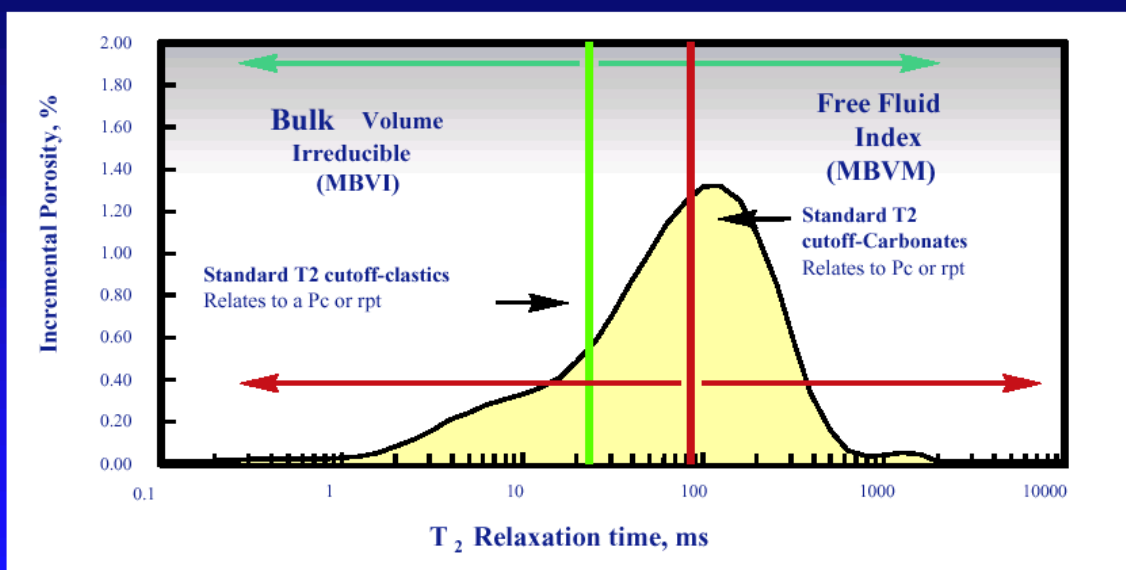
Porosity = 10.5 p.u.

$\rho_e = 3.16$ $\mu\text{m}/\text{sec}$.

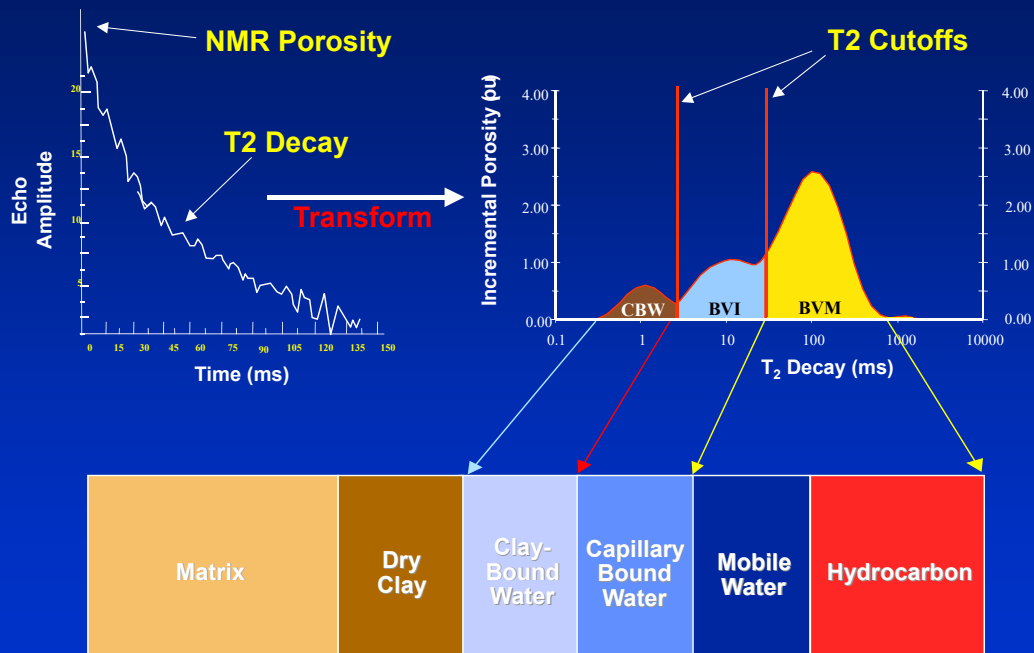


FLUID SATURATION DATA AND NMR MEASUREMENTS

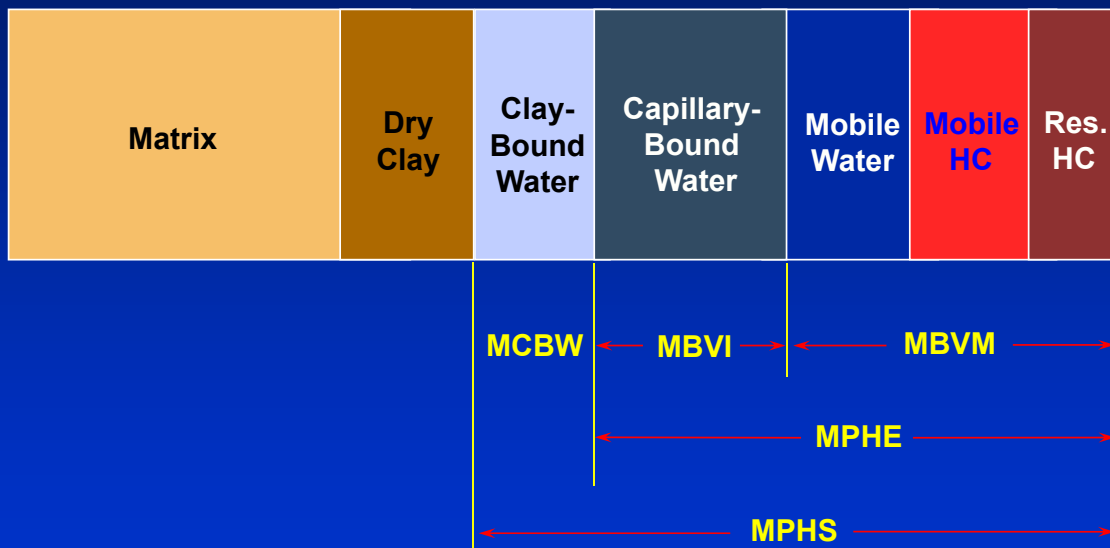
STANDARD METHOD TO DETERMINE MBVI



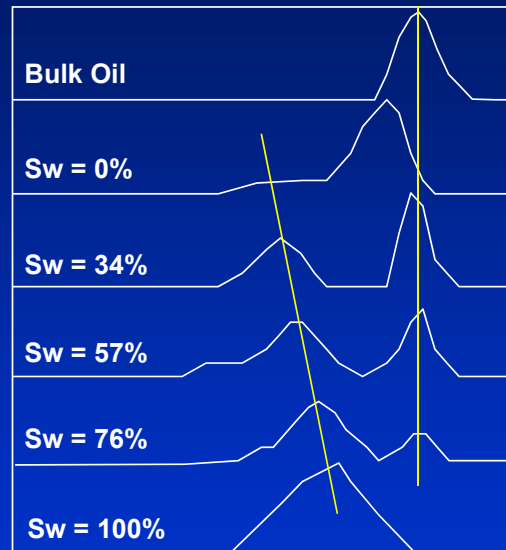
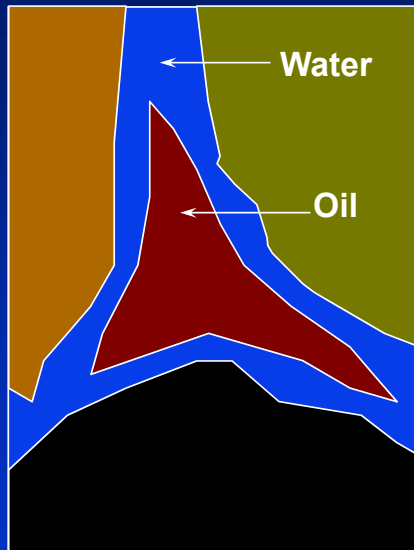
Pore Volumetric Distribution



Bulk Volumetrics - Light HC



Effect of Oil Saturation & T₂ Spectra



T₂

Adapted from Straley et al, Log Analyst (Jan. 1995)

T₂ Decay in a 2-Phase System

Wetting Phase Relaxivity

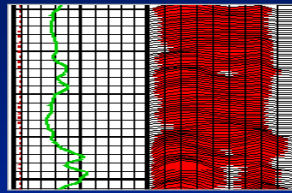
$$\frac{1}{T_{2b_{\text{water}}}} = \rho \frac{S}{V} + (S_w - \lambda \frac{S}{V}) \frac{1}{T_{2b_{\text{water}}}} + \frac{1}{T_{2D_{\text{water}}}}$$

Non-Wetting Phase Relaxivity

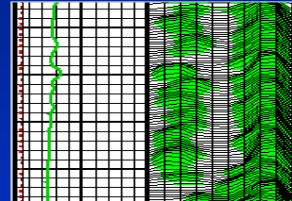
$$\frac{1}{T_{2_{hc}}} = \frac{1}{T_{2b_{hc}}} + \frac{1}{T_{2D_{hc}}}$$

T2 Spectra for Various Fluid Types

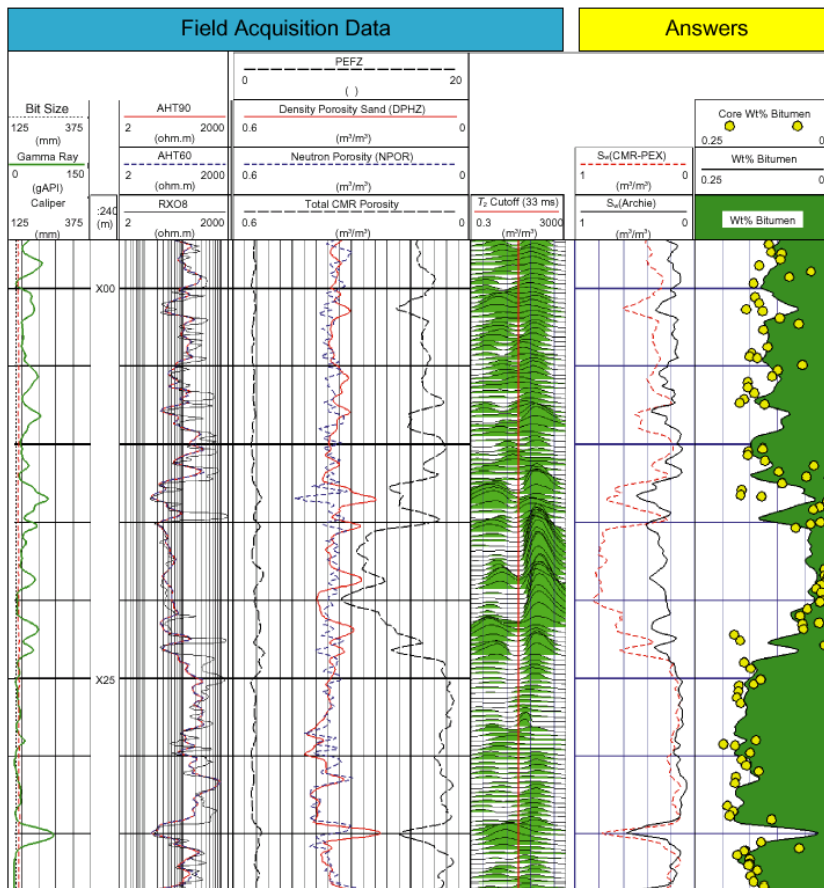
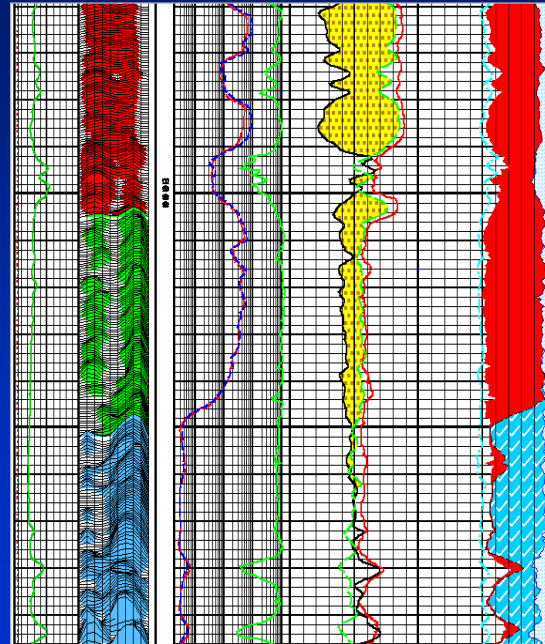
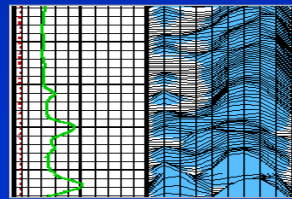
Gas



Oil



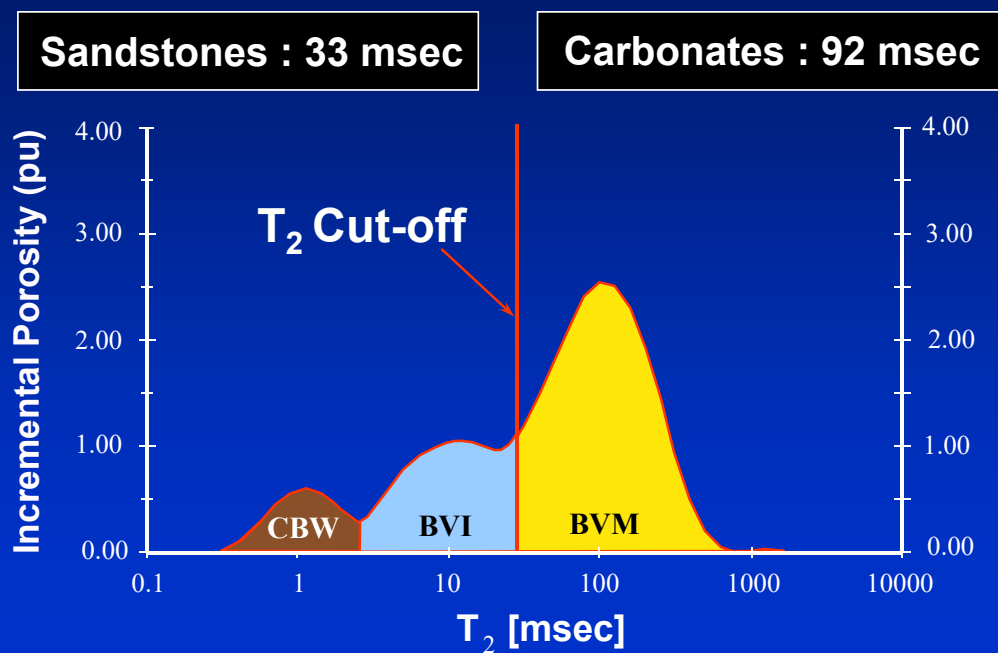
Water



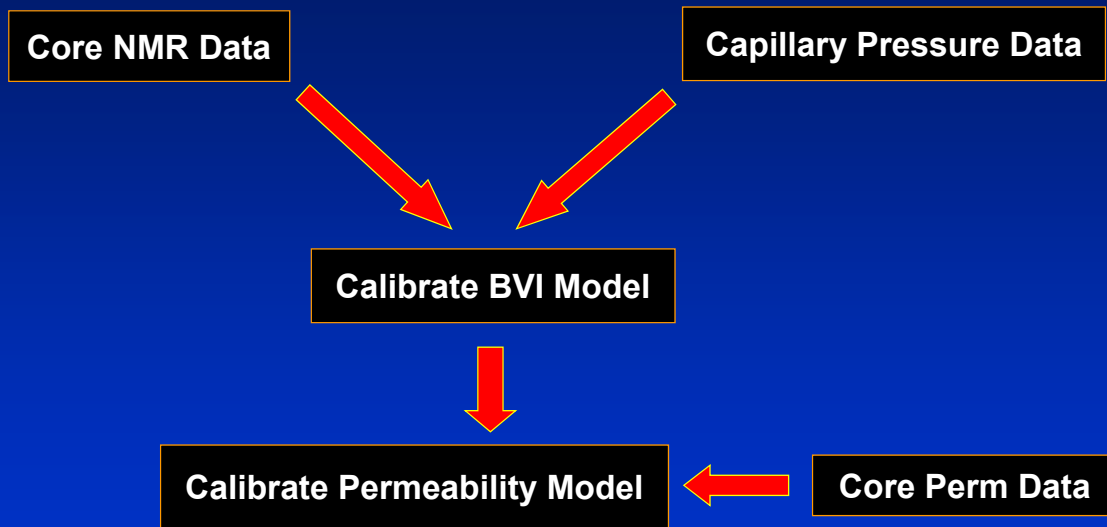
HYDROCARBON
VOLUME

CORE DATA AND NMR MEASUREMENTS

Default T_2 Cut-off Values



Core - Calibration Process



Core BVI Considerations

$$BVI_{core} = Swir_{core} \cdot \varnothing_{core}$$

- If \varnothing_{core} was determined after humidity drying:

$$BVI_{core} \approx BVI_{effective}$$

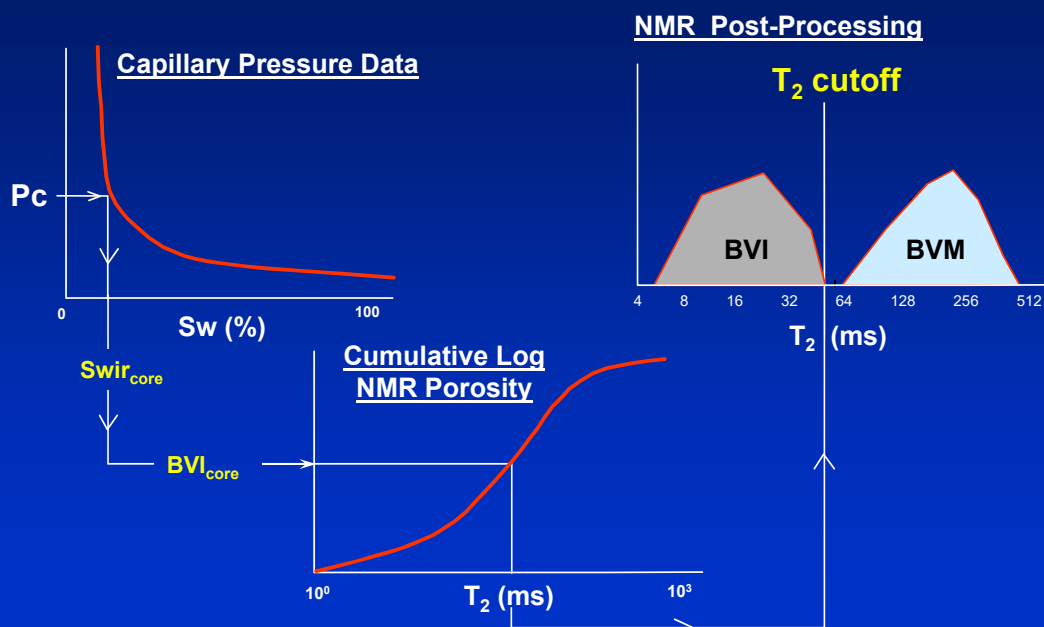
- If \varnothing_{core} was determined after oven drying:

$$BVI_{core} = BVI_{total} = BVI_{effective} + \text{Clay Bound Water}$$

Core NMR BVI Model Considerations

- Standard T_2 cut-off and SBVI models are constructed based on a correlation of T_2 spectra at irreducible water saturation to T_2 spectra at 100% water saturation. These these BVI models are only appropriate for application to T_2 spectra which reflect flushed zone conditions of $S_{xo} = 1.0$.
- If an oil-based mud filtrate is present in the flushed zone, then an oil-based mud filtrate de-saturation should be performed and used as the reference to construct the T_2 cut-off or SBVI model. These BVI models are only appropriate for application to T_2 spectra reflecting flushed zone conditions of $S_{xo} = S_{wir}$.
- T_2 cut-offs and SBVI models determined from core NMR may be inappropriate for application to NMR logs due to noise-induced positive shift of log T_2 spectra.

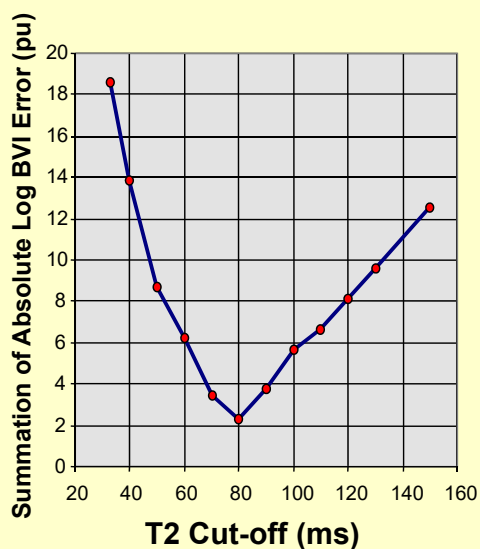
T_2 Cut-off from P_c & Log NMR Data



T₂ Cut-off from Pc & Log NMR Data

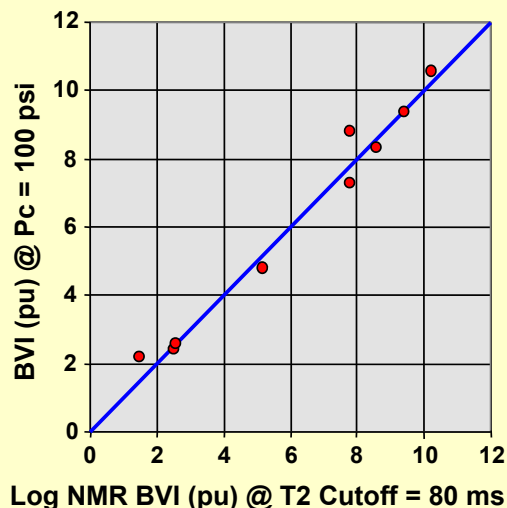
Error Minimization Plot

Summation of BVI Error vs. T2 Cut-off



Core- Calibrated Results

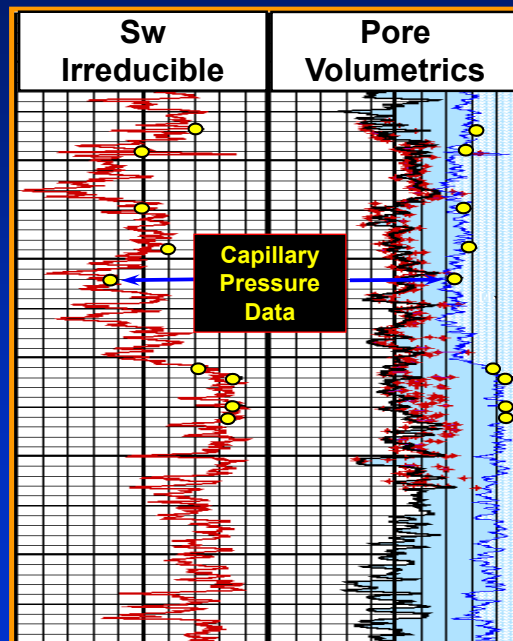
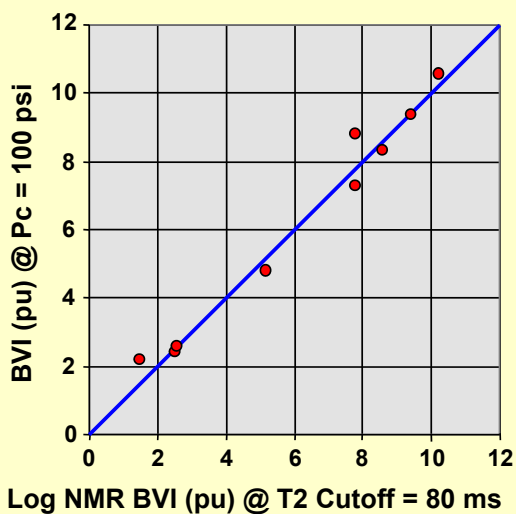
Calibrated Log BVI vs. Core BVI



T₂ Cut-off from Pc & Log NMR Data

Core- Calibrated Results

Calibrated Log BVI vs. Core BVI



NMR Connection to Capillary Pressure

Model Assumptions:

- T_2 is related to pore size
- P_c is controlled by pore throats
- Pore body radius and pore throat radius are proportional
- P_c can be approximated by T_2

$$P_c = \frac{2\sigma \cos(\theta)}{r_{throat}}$$

$$r_{throat} = \frac{106.4}{P_c} [\text{micron} / \text{psi}]$$

$$\frac{1}{T_2} \cong \rho \frac{S}{V}$$

$$\cong \rho \frac{F_s}{R_{body}}$$

where
 ρ = killing strength
 F_s = Shape Factor

$$R_{body} = T_2 \rho F_s$$

$$\Gamma = \frac{r_{throat}}{R_{body}}$$

$$r_{throat} = \Gamma F_s \rho T_2$$

$$P_c = \frac{106.4 [\text{microns/psi}]}{\Gamma F_s \rho T_2} \approx (7 - 50) \frac{1}{T_2}$$

where T_2 is in seconds

Pseudo- P_c curves from NMR T_2 Spectra

Model Core-Calibration

$$\frac{1}{T_2} = \frac{1}{T_{2b}} + \rho_2 \frac{S}{V}$$

$$P_c = \frac{2\sigma \cos(\theta)}{r_{pt}}$$

$$\frac{S}{V} = \frac{F_s}{r_b}$$

$$\frac{1}{P_c} = \frac{\rho_2}{2\sigma \cos(\theta)} \frac{r_{pt}}{r_b} F_s T_2$$

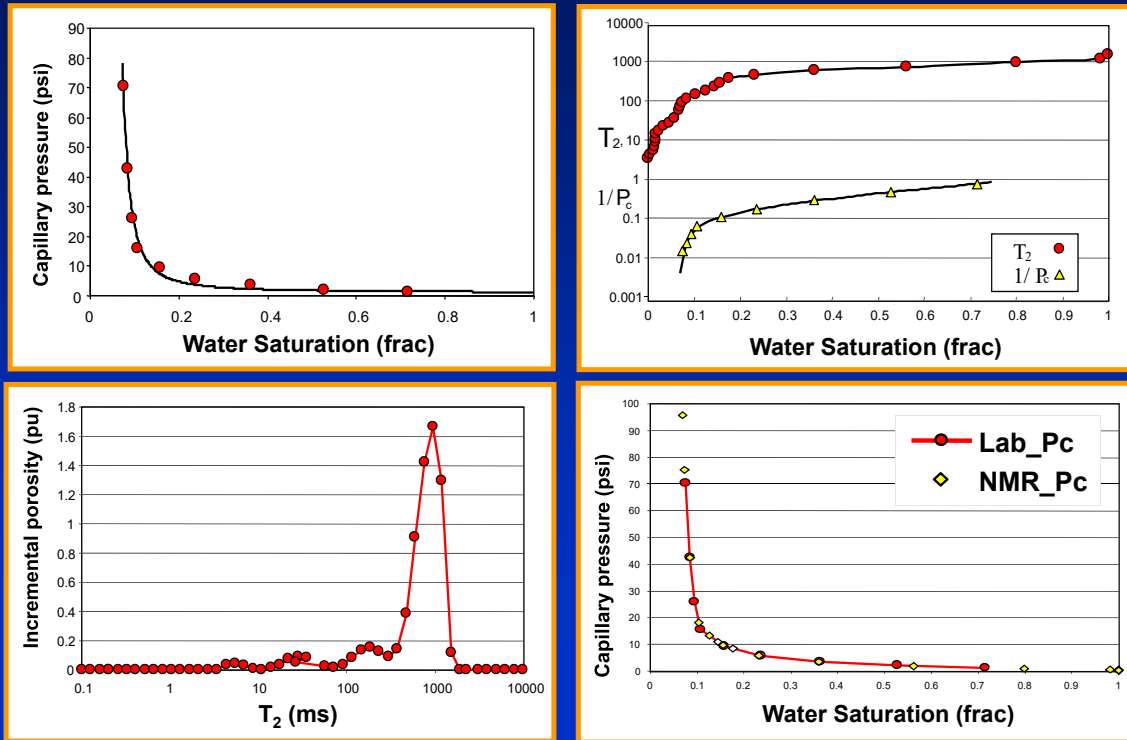
$$C = \frac{\rho_2}{2\sigma \cos(\theta)} \frac{r_{pt}}{r_b} F_s$$

$$\left(\frac{1}{P_c} \right) = C T_2$$

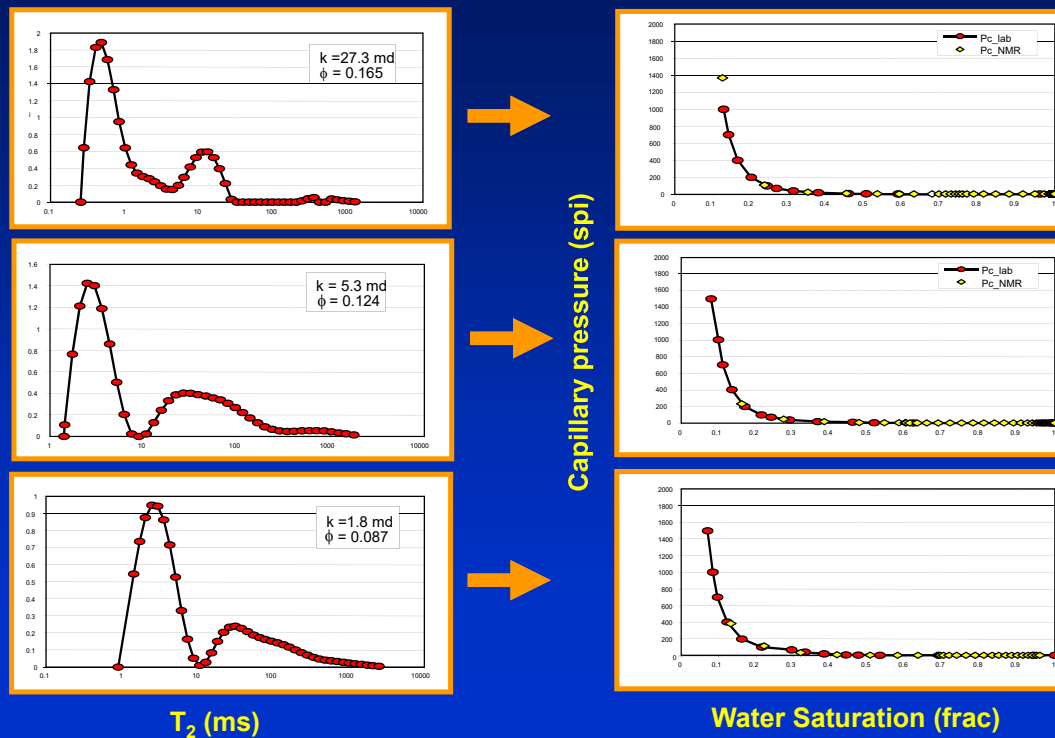
$$\text{Log} \left(\frac{1}{P_c} \right) = \text{Log}(C) + \text{Log}(T_2)$$

$$\text{Log}(C) = \text{Log} \left(\frac{1}{P_c} \right) - \text{Log}(T_2)$$

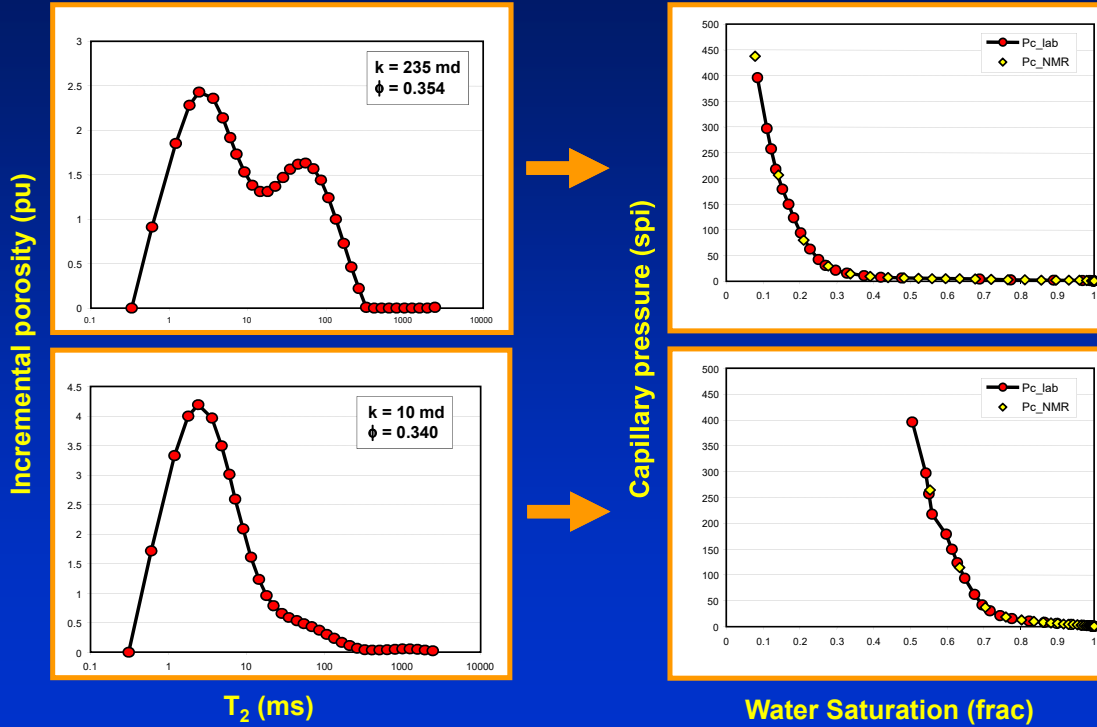
Pseudo-Pc curves from NMR T_2 Spectra



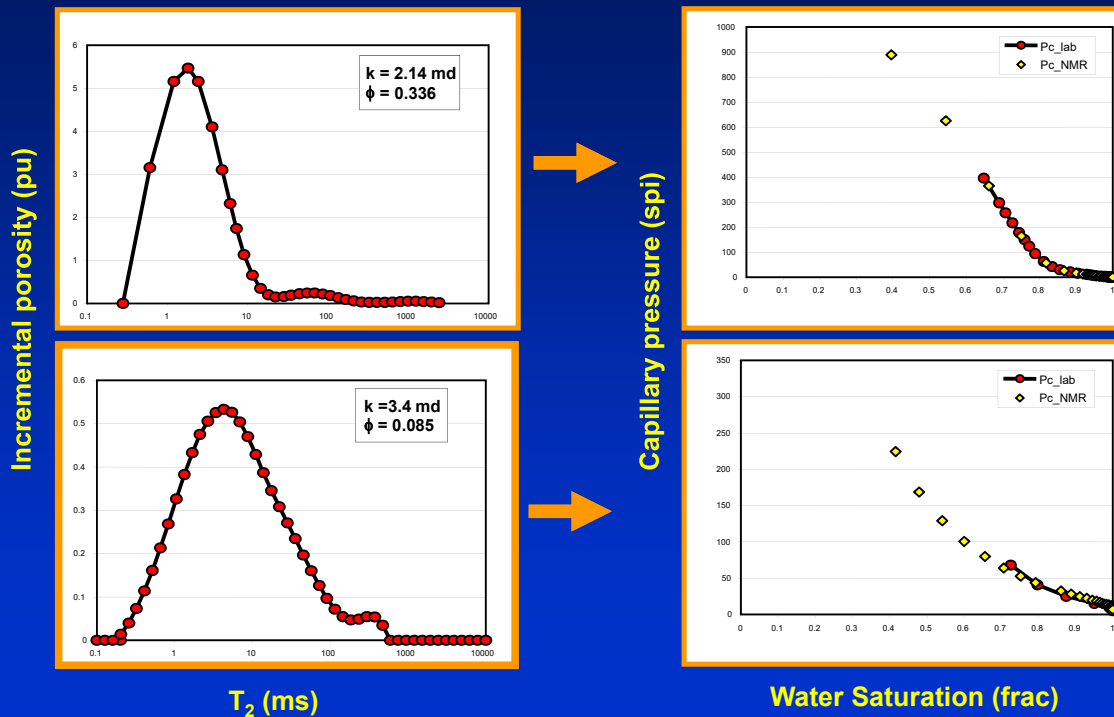
Pseudo-Pc curves from NMR T_2 Spectra



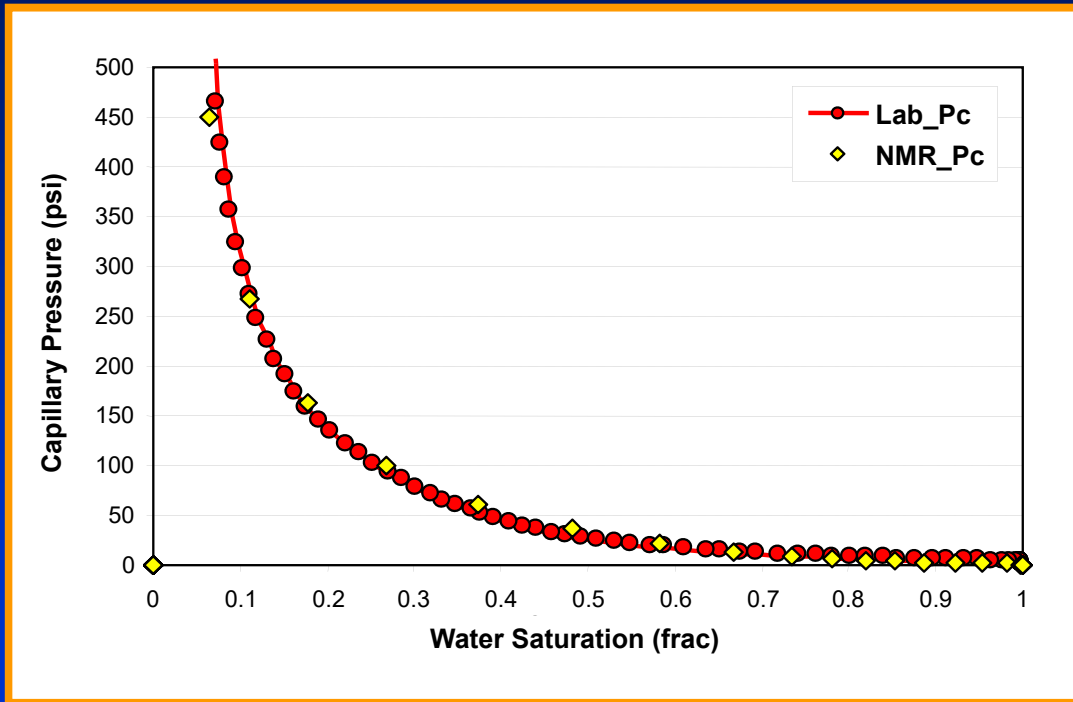
Pseudo-Pc curves from NMR T_2 Spectra



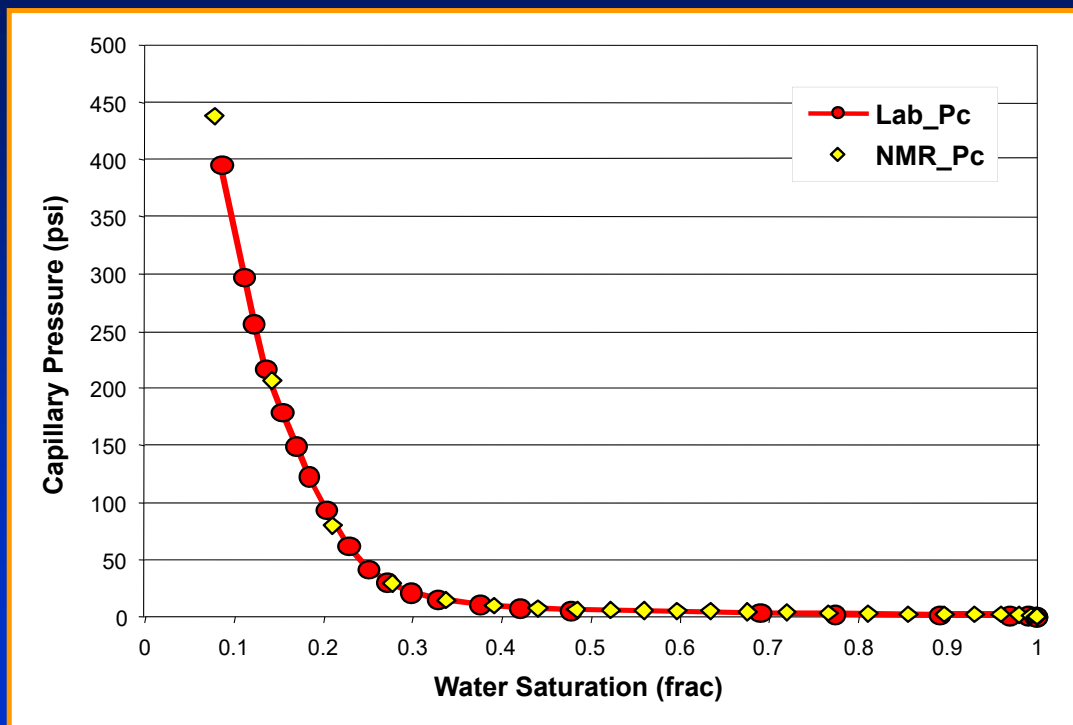
Pseudo-Pc curves from NMR T_2 Spectra



Pseudo-Pc curves from NMR T_2 Spectra

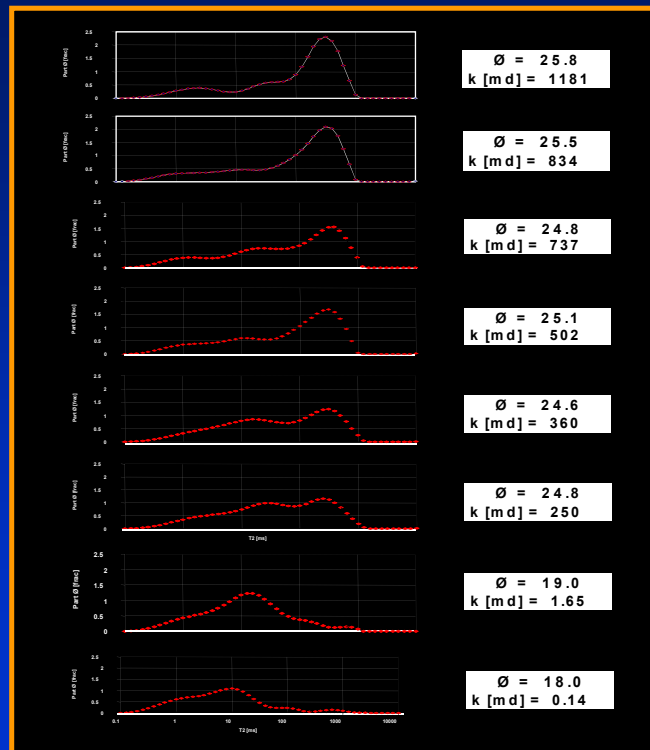


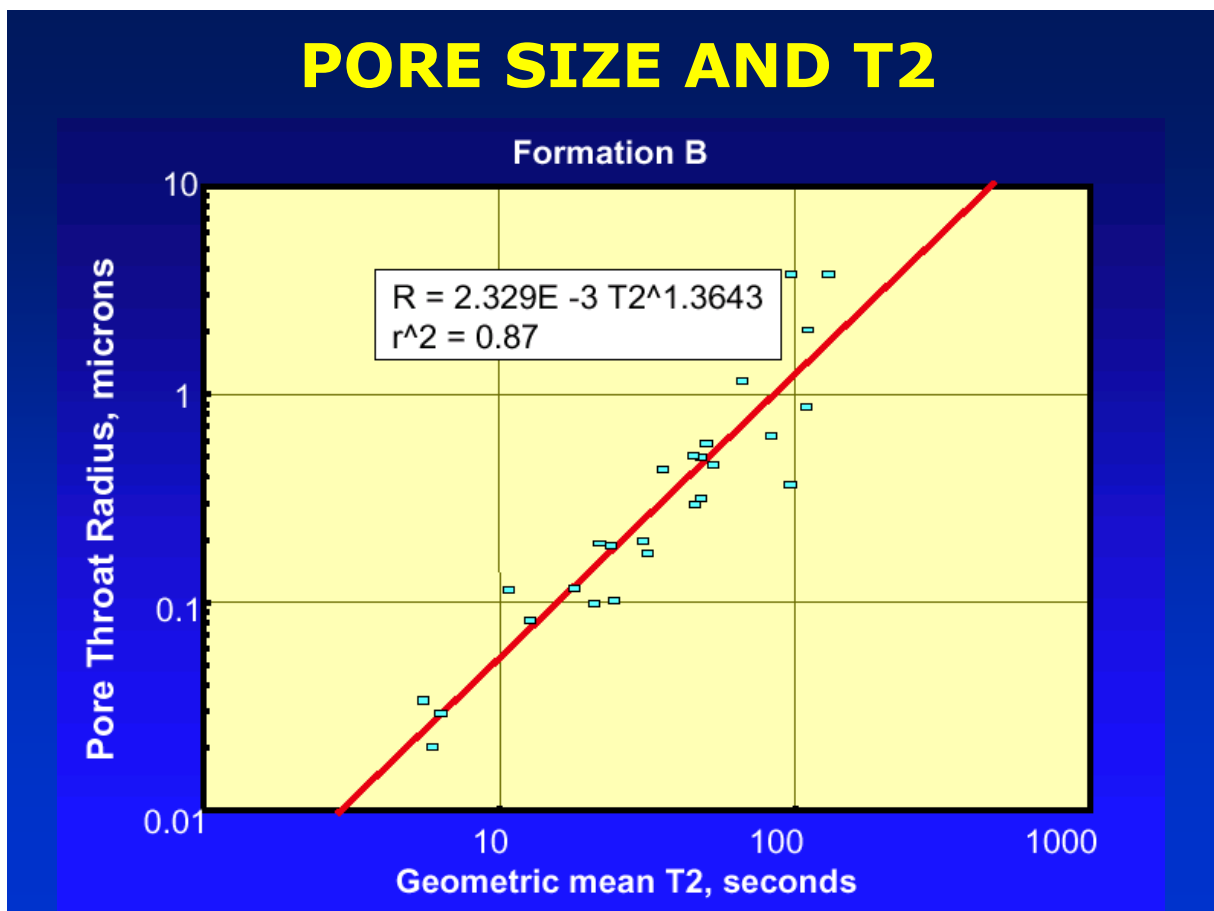
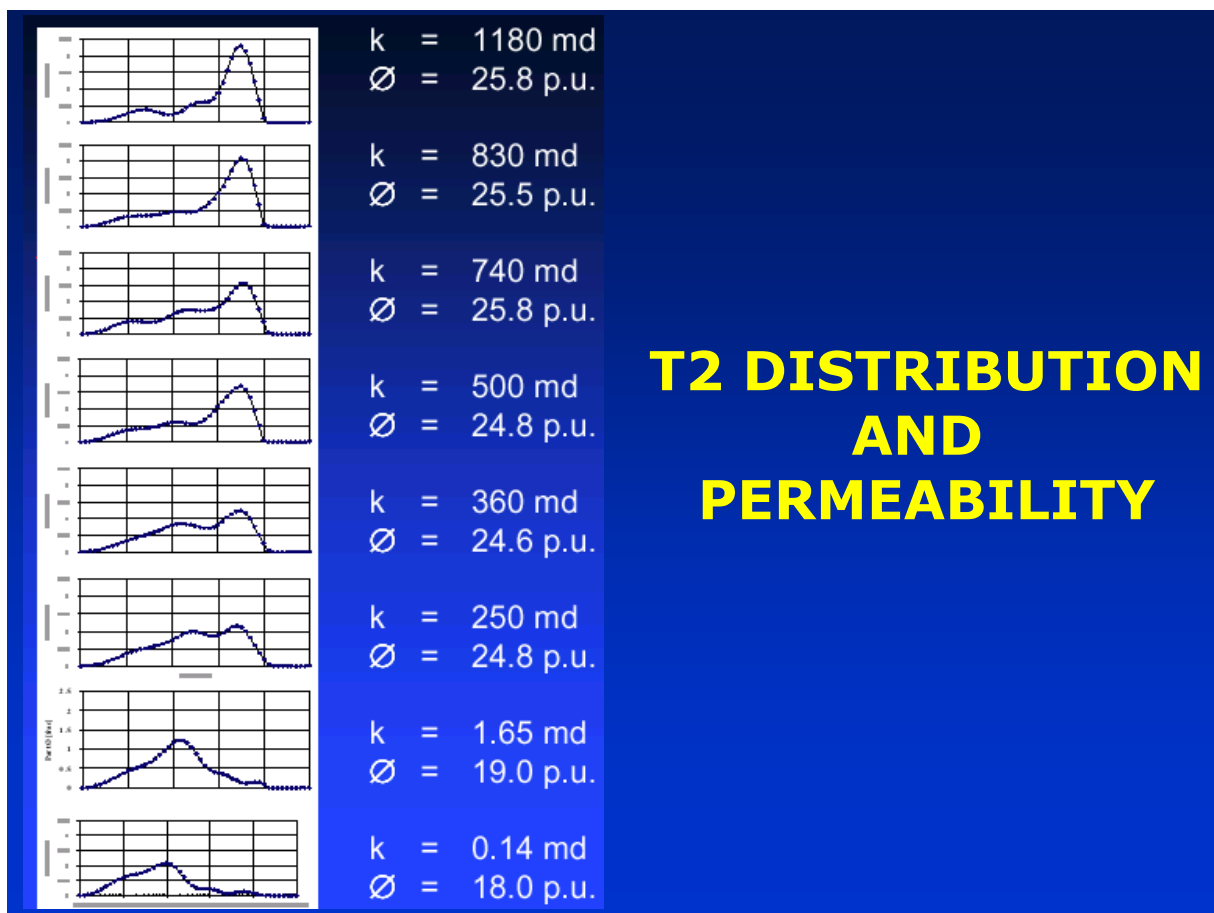
Pseudo-Pc curves from NMR T_2 Spectra



PERMEABILITY DATA AND NMR MEASUREMENTS

T₂ Distribution & Permeability



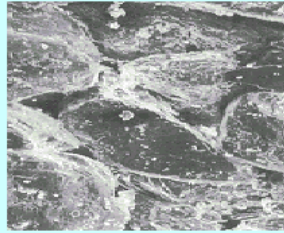


TWO PERMEABILITY MODELS

BVM/BVI concept

*looks on
pore surface*

$$k \propto \frac{1}{S_{por}^2} \propto \frac{1}{S_{w,irr}^2} \propto \left(\frac{BVM}{BVI} \right)^2$$



T₂ concept

*looks on
pore radius*

$$k \propto (\text{"average" pore radius})^2 \propto (\text{average } T_2)^2$$

- Best overall model, sensitive to accuracy of BVI
- high viscosity can increase BVI and lower k

- Sensitive to residual fluids in measurement volume
- work best in zones that have been completely flushed

BVM/BVI CONCEPT: Empirical Equations for k

Pore properties empirically expressed in irreducible water saturation terms (Timur 1968, Coates & Dumanoir 1974):

$$k = \left[100 \cdot \frac{\phi^{2.25}}{S_{w,irr}} \right]^2$$

--> permeability determination from NMR **measurements**:

$$k = \left[\frac{\phi}{C} \right]^4 \cdot \left[\frac{MBVM}{MBVI} \right]^2$$

MBVM - bulk volume moveable fluids

MBVI - bulk volume irreducible fluids

BOUND WATER MODELS

Timur 1966

$$k \propto \phi^{4.4} = \frac{1}{S_{wir}^2}$$

Coates Equation for Permeability

$$k, md = \left[\frac{\phi}{10} \right]^4 \left[\frac{BVM}{BVI} \right]^2 = \left[\frac{\phi}{10} \right]^4 \left[\frac{1 - S_{wir}}{S_{wir}} \right]^2$$

$$k, md = \left[\frac{\phi}{c} \right]^4 \left[\frac{BVM}{BVI} \right]^2 = \left[\frac{\phi}{c} \right]^4 \left[\frac{1 - S_{wir}}{S_{wir}} \right]^2$$

Benefits:

- Effective permeability = 0 for BVM = 0
- No hydrocarbon effects

Determination of the scaling factor c:

$$c = \left(\frac{1}{n} \sum_{i=1}^n \left[\frac{\phi^4}{k} \right] \left[\left(\frac{BVM}{BVI} \right)^2 \right]^{0.25} \right)^{-1}$$

Generalized Coates:

$$k = \left[\frac{\phi}{c} \right]^m \left[\frac{BVM}{BVI} \right]^n$$

Note - 3 parameters: c, m, n, and T₂ cutoff

T2 CONCEPT

T₂ relates to pore body radius

Permeability controlled by pore throats

Pore body radius and pore throat radius are proportional

We remember: $k \sim r_2$

Permeability can be approximated by T₂

$$k = C \langle \phi \rangle^4 \langle T_2 \rangle^2$$

where C is a variable

COMPARISON BETWEEN BOUND WATER AND AVERAGE T₂ MODEL

Bound Water Model

$$k = \left[\frac{\phi}{c} \right]^m \left[\frac{BVM}{BVI} \right]^n$$

- Best overall model
- Sensitive to accuracy of MBVI (T₂ cutoff determination)
- High viscosity crude can increase BVI and reduce k.

Average T₂ Model

$$k = C \langle \phi \rangle^4 \langle T_2 \rangle^2$$

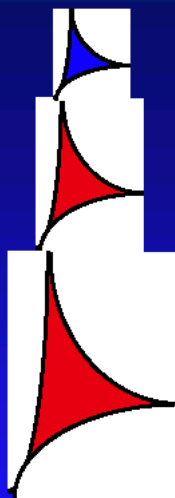
where C is a variable

- Sensitive to residual fluids in measurement volume
- These models work best in zones that have been completely flushed.

TWO VIEWS OF BVI

Small

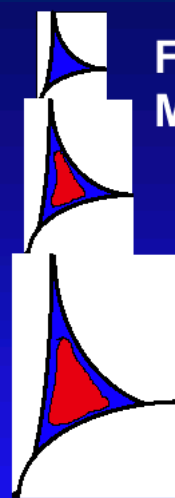
Large Pores



Bimodal Model

Bimodal - Fixed T₂

- Small Pores Contain Irreducible Fluid
- Large Pores Contain Moveable Fluid



Film Model

Film (Spectral) Model

- Small Pores Contain Irreducible Fluid
- Large Pores Contain Both Irreducible (Film) and Moveable Fluids
- Water Films Appear Like Small Pores

WHICH BVI MODEL TO USE?

■ Bimodal - Fixed T_2

- ❑ Hydrocarbon-bearing intervals
- ❑ Shaly sands
- ❑ Bimodal porosity systems

■ Film (Spectral) Model

- ❑ 100% water saturated homogenous sands
- ❑ Oil-based mud

■ Variable T_2 Cutoff

- ❑ Carbonates
- ❑ Mixed lithologies

NMR POROSITY/PERMEABILITY SUMMARY

■ Mineralogy Independent ϕ

- ❑ no interpretation constants required

■ Effective and Total ϕ and BVI and BVM

■ T_1 and T_2 depends on S/V and ρ

■ NMR echo decay is related to S/V

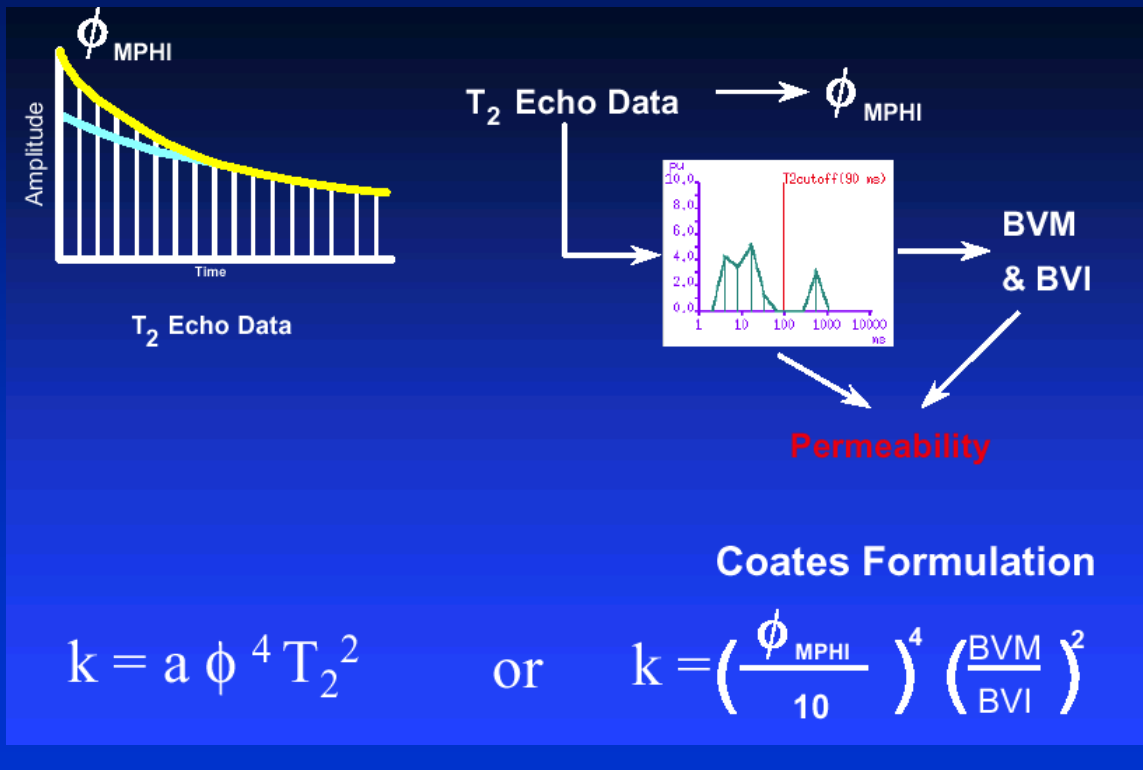
- ❑ pore-size distributions
- ❑ grain-size distribution

■ S/V related to k

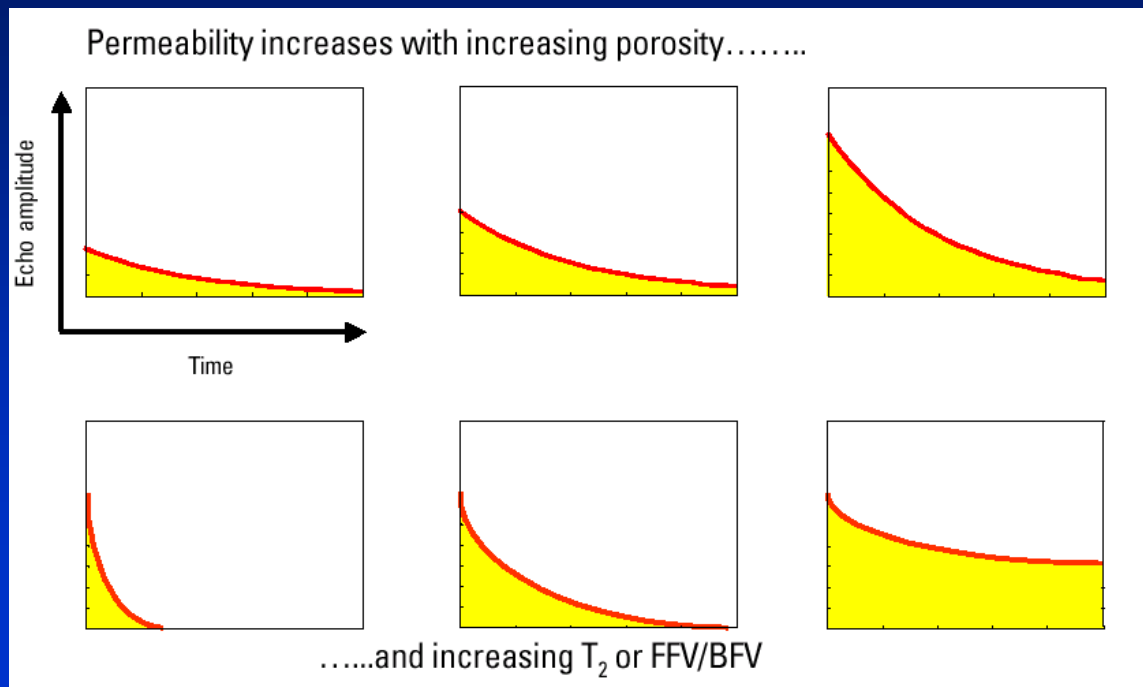
T_2 relates to pore body radius.

Permeability is controlled by pore throat radius !

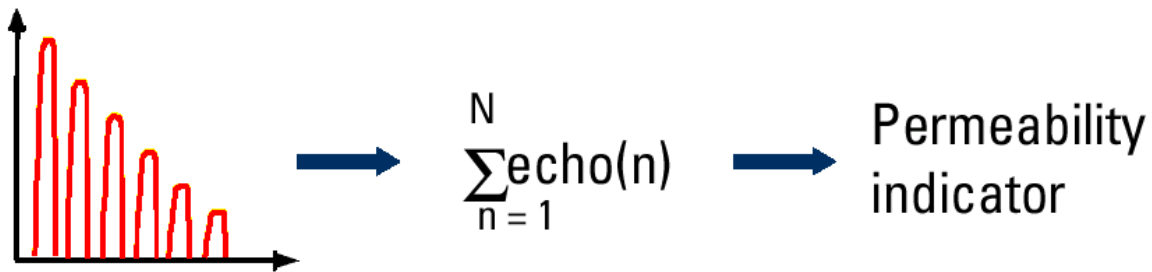
NMR POROSITY/PERMEABILITY SUMMARY



NMR POROSITY/PERMEABILITY SUMMARY



NMR POROSITY/PERMEABILITY SUMMARY



NMR Permeability Models

Kenyon Model:

$$k = C \cdot \left(\phi_{NMR} \right)^a \cdot \left(T_2 \text{ Geo. Mean} \right)^b$$

Coates-Timur Model :

$$k = \left(\frac{\phi_{NMR}}{C} \right)^a \cdot \left(\frac{BVM}{BVI} \right)^b$$

Where assumed default parameters are: $C=10$, $a=4$ & $b=2$

Note: These models will produce a permeability index unless explicitly calibrated to local reservoir data.

NMR Permeability Models

Kenyon Model:

$$k = C \cdot \left(\phi_{NMR} \right)^a \cdot \left(T_2 \text{ Geo. Mean} \right)^b$$

Where default parameters are: **C = 10**, **a = 4** & **b = 2**

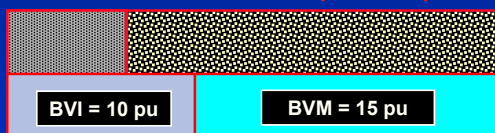
Kenyon Model - Ideal Conditions

(Wetting Phase Saturation = 100%)

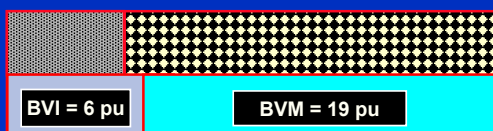


← $\phi_{NMR} = 25 \text{ pu}$ →

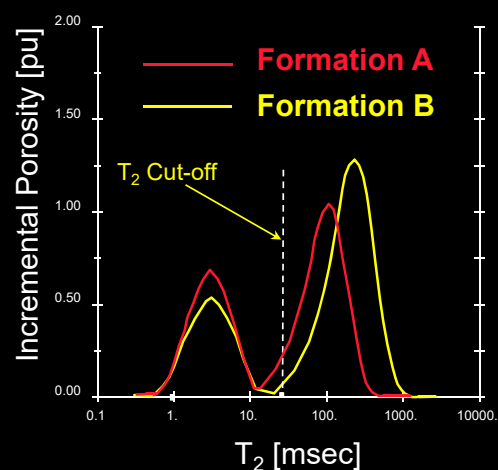
Formation A (Low-k)



Formation B (high-k)



T_2 Spectra @ $Sw = 1.0$



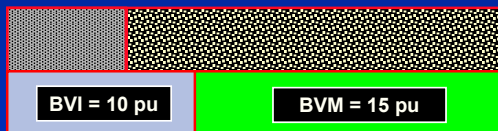
Kenyon Model - Loss of Sensitivity

(2-Phases with Wetting Phase Saturation @ Irreducible)

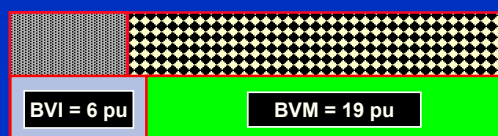


$\phi_{NMR} = 25 \text{ pu}$

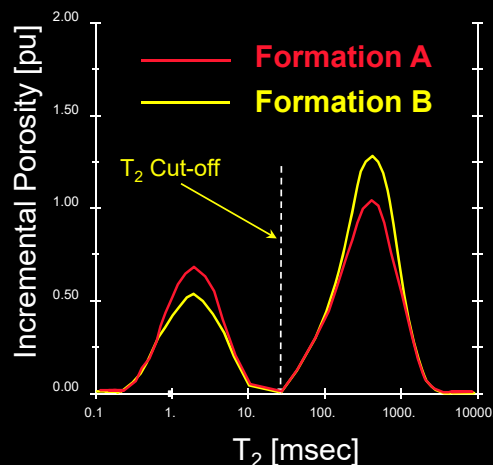
Formation A (Low-k)



Formation B (high-k)



T_2 Spectra @ $S_w = S_{wir}$



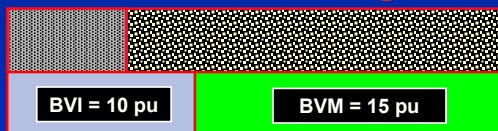
Kenyon Model Breaks Down

The correlation of T_2 to pores size (and permeability) becomes confounded by variations in fluid phases and saturation

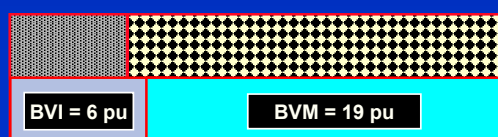


$\phi_{NMR} = 25 \text{ pu}$

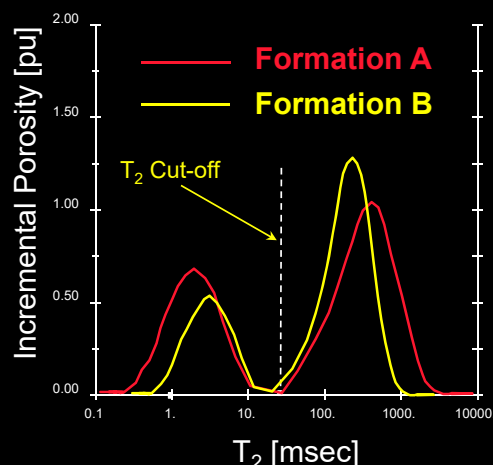
Formation A (Low-k) @ S_{wir}



Formation B (high-k) @ $S_w = 1.0$



T_2 Spectra @ $S_w = S_{wir}$



Limitations of Kenyon Permeability Model

- T2 spectra will only reflect pore size distribution when fully 100% saturated with wetting phase fluid.
- Application of the model is predicated on assumption that pore size (as reflected in the T2 distribution under above conditions) has an implicit relationship to pore throat diameter and pore connectivity.
- The model loses sensitivity when T2 spectra become dominated by non-wetting phase bulk relaxivities.
- A model calibrated in a hydrocarbon leg cannot be applied to a water legs (and visa versa).

Permeability from NMR

Generalized Coates-Timur Model:

$$k = \left(\frac{\phi}{c} \right)^a \cdot \left(\frac{1 - S_{wir}}{S_{wir}} \right)^b$$

This model is designed to compute the effective (non-wetting phase) permeability model based on the lower permeability boundary condition which is controlled by the ratio of non-wetting phase (1-S_{wir}) to wetting phase (S_{wir}) saturation .

Permeability from NMR

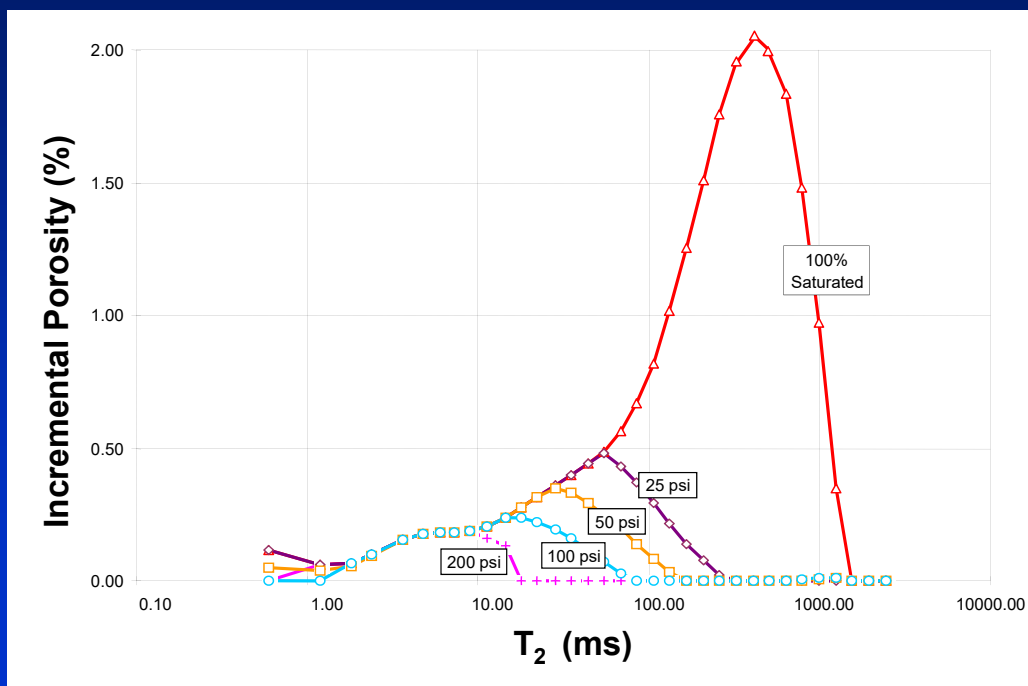
Coates-Timur Model (**NMR version**):

$$k = \left(\frac{\phi_{NMR}}{C} \right)^a \cdot \left(\frac{BVM}{BVI} \right)^b$$

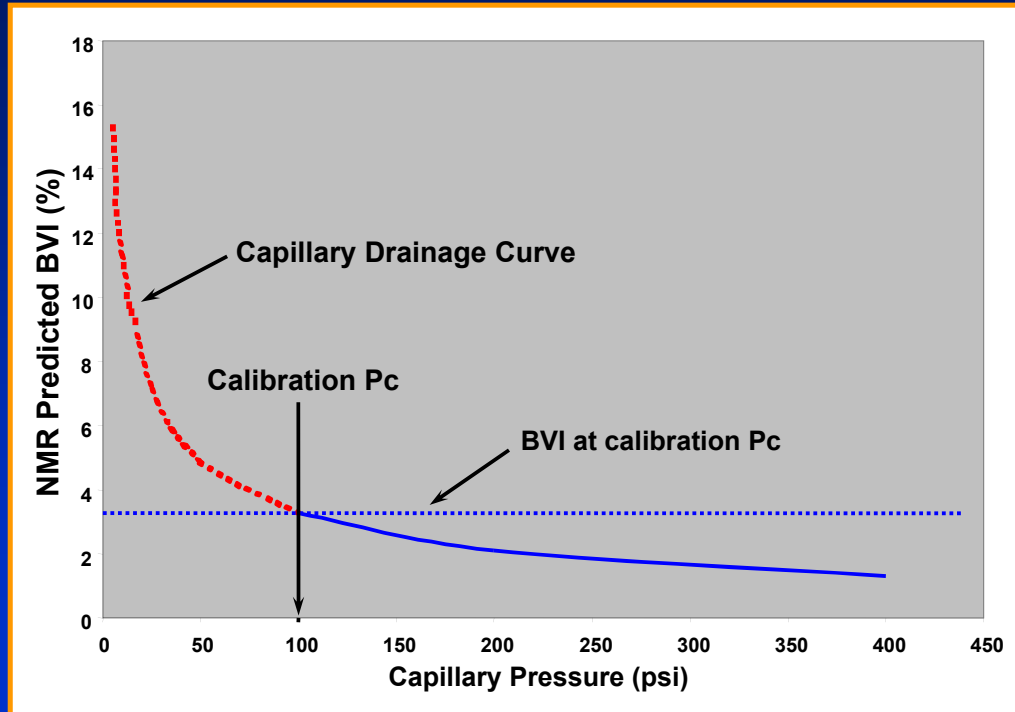
Where default parameters are: **C = 10**, **a = 4** & **b = 2**

BVI Dependence on Capillary Pressure/Height above FWL

T₂ Distributions at Partial Saturations



BVI Dependence on Capillary Pressure/Height above FWL

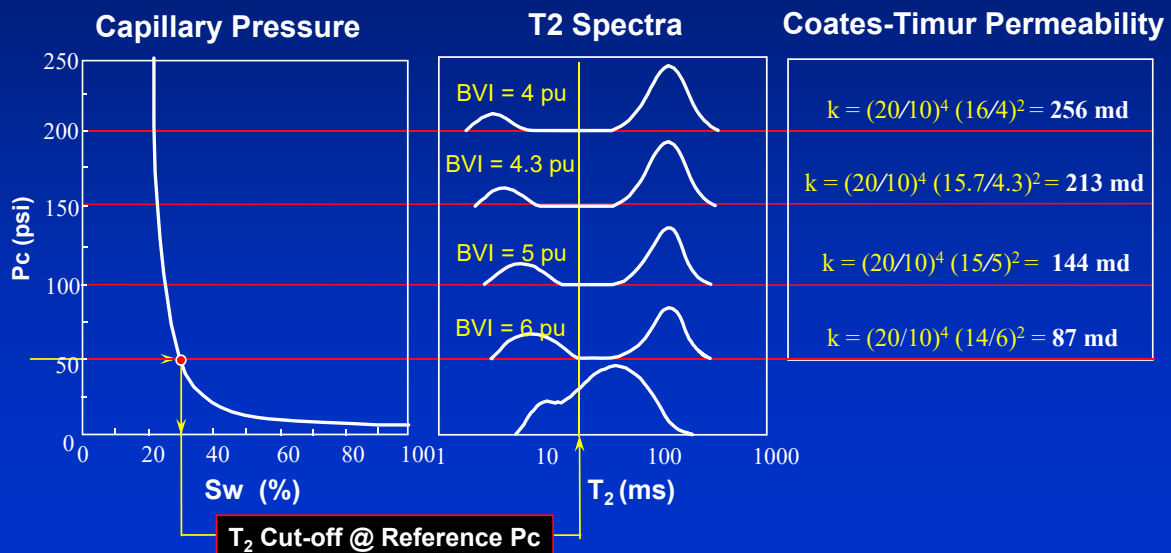


Coates-Timur Permeability vs. Column Height

$$\phi_{NMR} = 20 \text{ pu}$$

$$k_{\text{absolute}} = 256 \text{ md}$$

$$k = \left(\frac{\phi_{NMR}}{10} \right)^4 \cdot \left(\frac{\phi_{NMR} - BVI}{BVI} \right)^2$$



Limitations of Coates-Timur Permeability Model

- Application of the model is predicated on assumption that the porosity is all interconnected, and that pore throat diameter systematically increases proportional to an increase in the magnitude of the bulk free fluid volume (BVM).
- Computed permeability may systematically increase as a function of increasing height above free water level. This effect is most likely to occur for lower quality reservoirs with highly sloped capillary pressure curves, but should not be an issue for very high permeability reservoirs where capillary pressure curves are near-asymptotic.
- Model Losses sensitivity at very high permeabilities where irreducible water saturation is on the asymptote of the capillary pressure curve, and porosity doesn't increase relative to increased pore size and/or pore throat size.

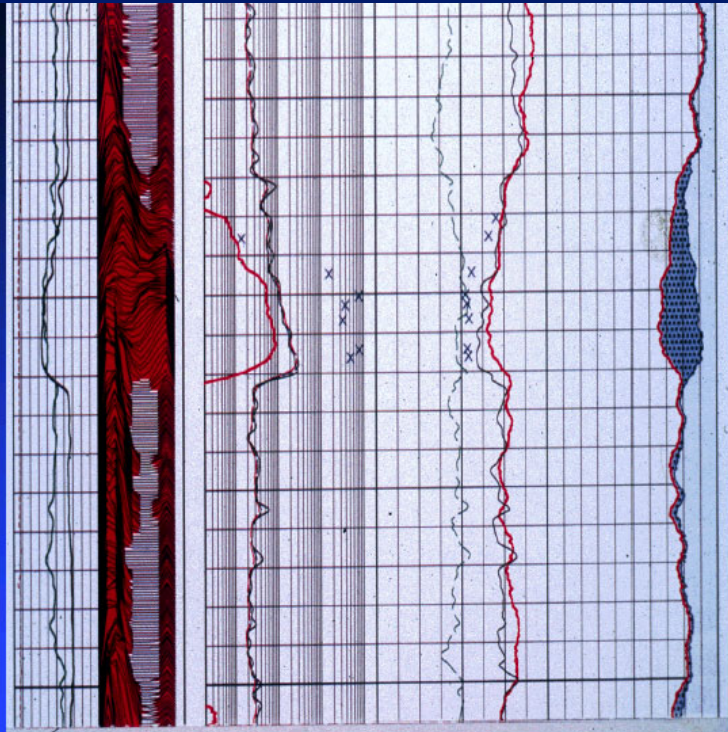
Calibration of Coates-Timur Permeability Model

- Local calibration of model fitting parameters (C , a & b) are necessary to account for variations in the complexity and connectivity of the pore system, which control the permeability and its correlation to the bulk pore volumetric elements of which model is strictly comprised.
- Multi-linear regression can be employed to solve for the the formation-specific fitting parameters (C , m & n) when reference permeability data from core or formation tests are available.
- Minimum error analysis can also be employed to solve for an optimum value of the porosity denominator C while holding parameters " a " and " b " constant at default values.

UNCALIBRATED PERMEABILITY

Coates' Constant

$$k = \left(\frac{\phi_{\text{MPHI}}}{C} \right)^4 \left(\frac{\text{BVM}}{\text{BVI}} \right)^2$$

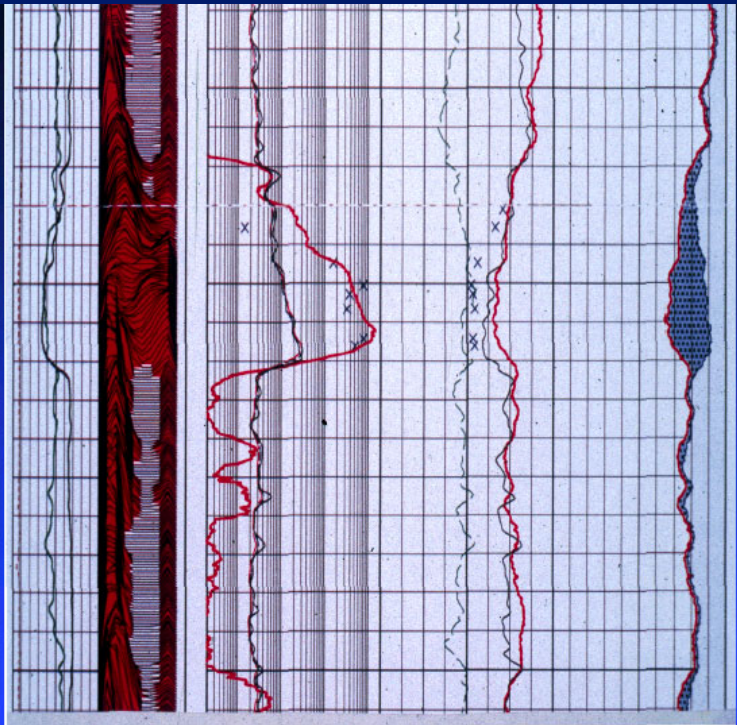


CALIBRATED PERMEABILITY

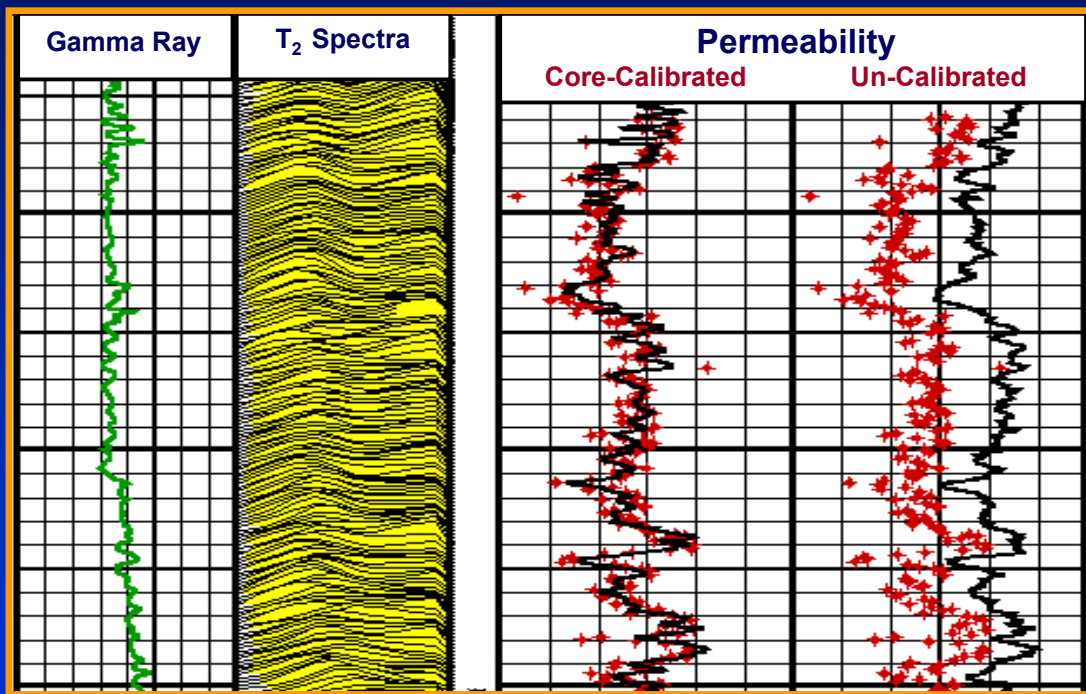
Calibrated
Permeability
Model

Coates' Constant

$$k = \left(\frac{\phi_{\text{MPHI}}}{4} \right)^4 \left(\frac{\text{BVM}}{\text{BVI}} \right)^2$$



MRIL Permeability Index versus Core-Calibrated MRIL Permeability



Permeability - Frames of Reference

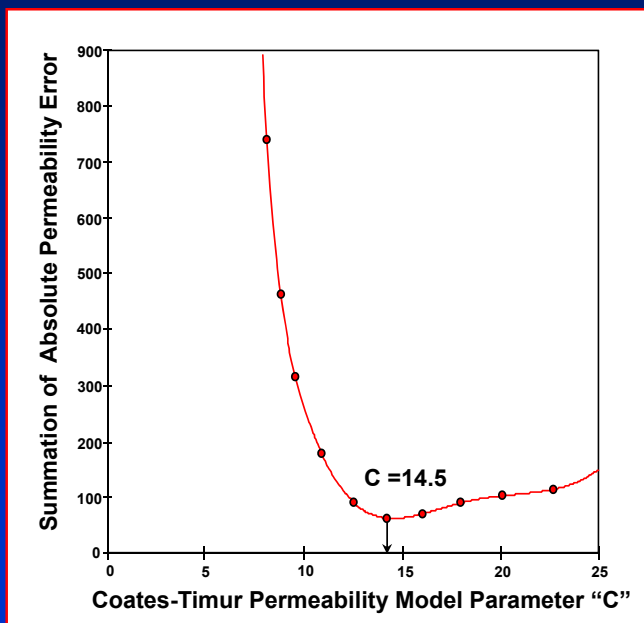
- $k_{\text{air}} > k_{\infty} \sim k_{\text{liquid}} > k_{\text{effective}}$
- $k_{\text{ambient stress}} > k_{\text{reservoir overburden stress}}$

Reference Permeability Sources

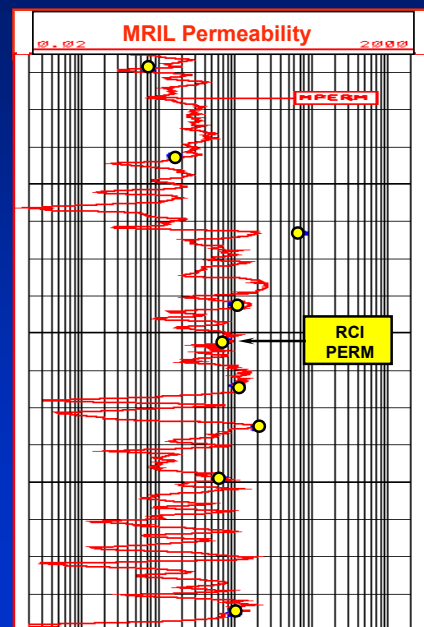
- ▣ **Conventional Cores**
 - Whole Core
 - Core Plugs
 - Probe Permeameters
 - Thin Section estimates
- ▣ **Rotary Sidewall Cores**
- ▣ **Well Production Tests**
- ▣ **Drillstem Tests**
- ▣ **Wireline Formation Testers**

NMR Permeability Calibration

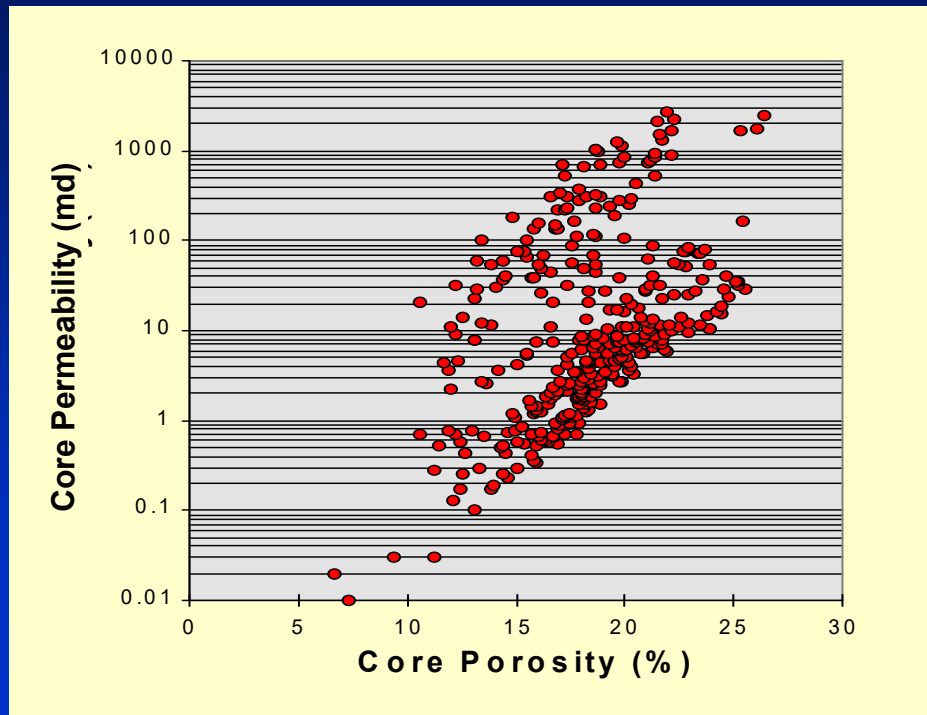
Coates-Timur Model Optimization Plot



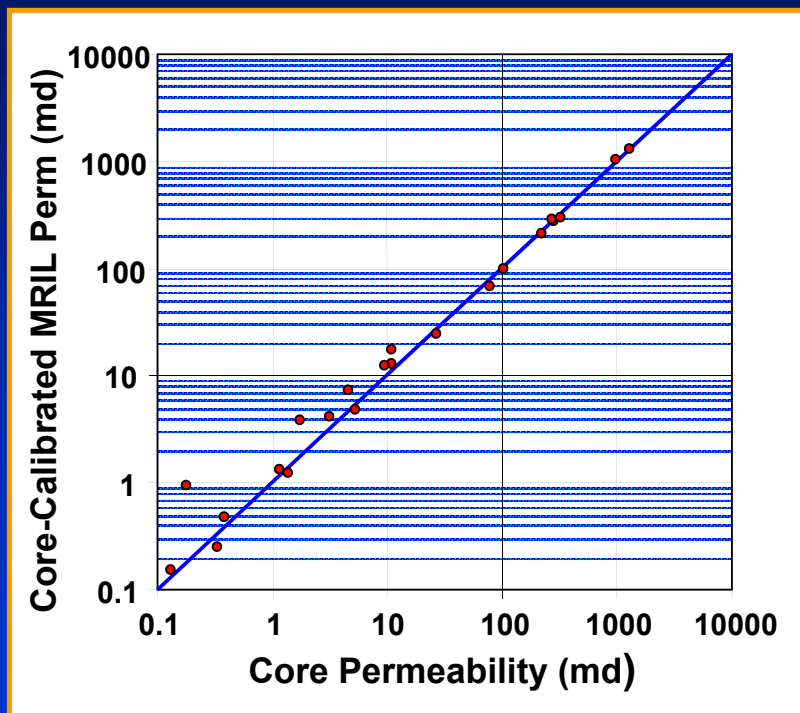
Core- Calibrated Results



CASE STUDY: Well A



Core-Calibrated MRIL Permeability Carbonate Example

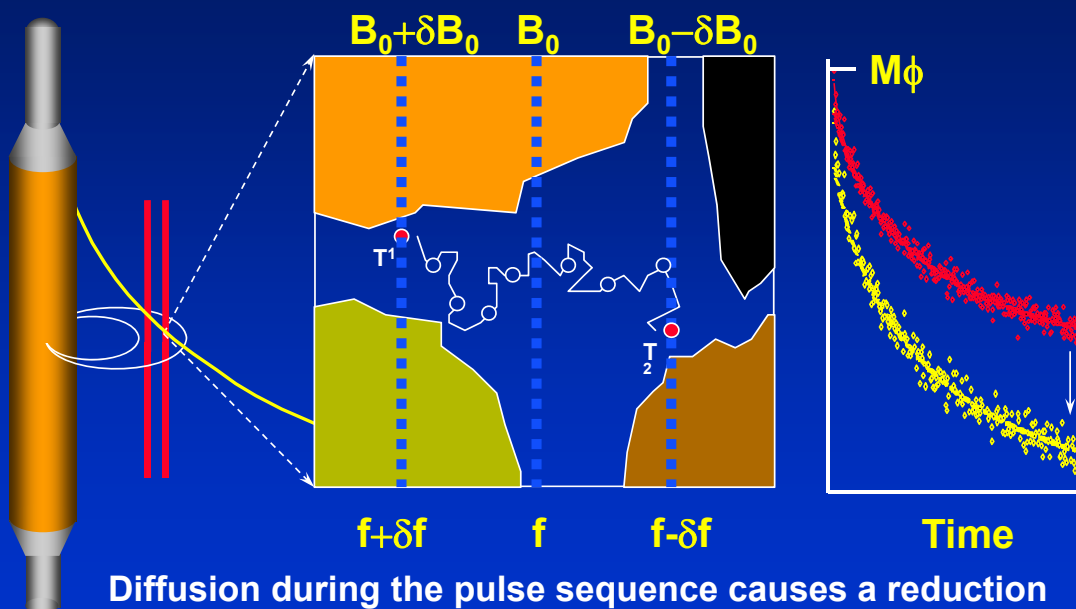


NMR

GRADIENT DIFFUSION

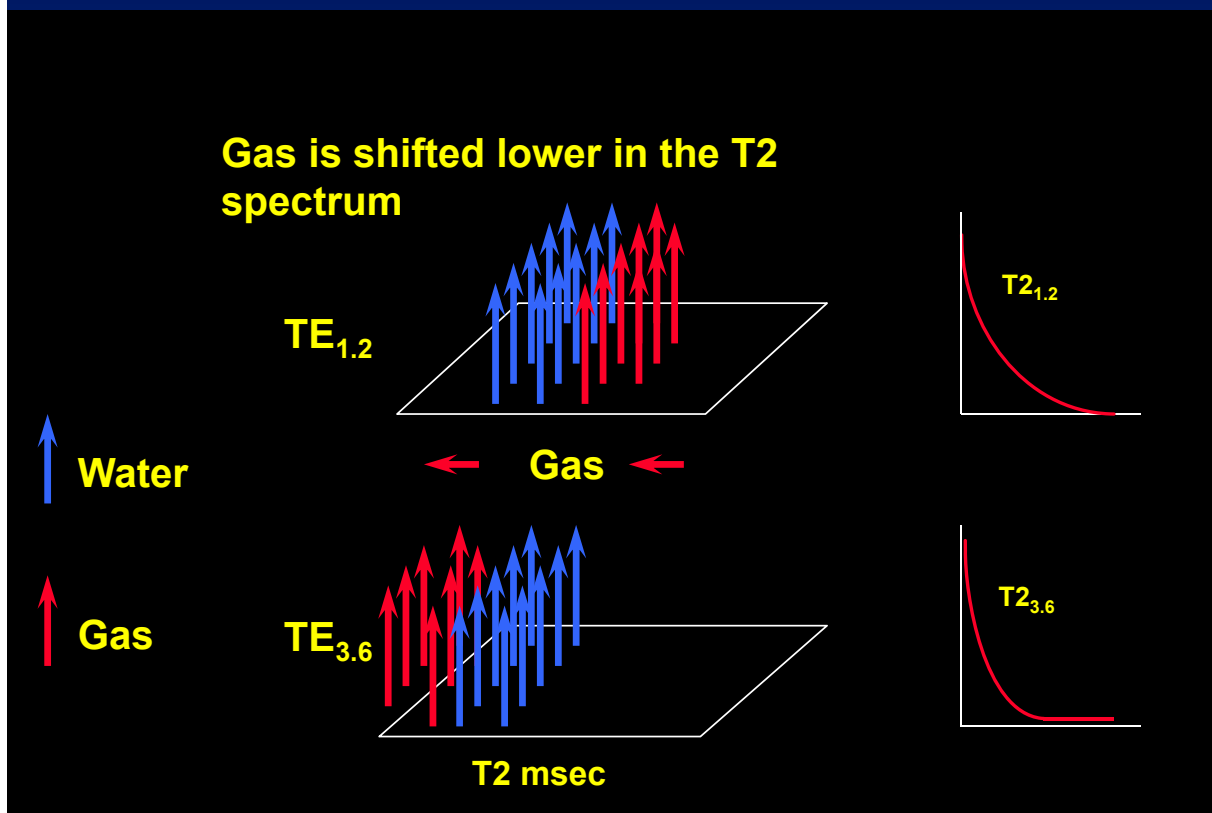
MEASUREMENTS

MRIL Gradient Field and Diffusion

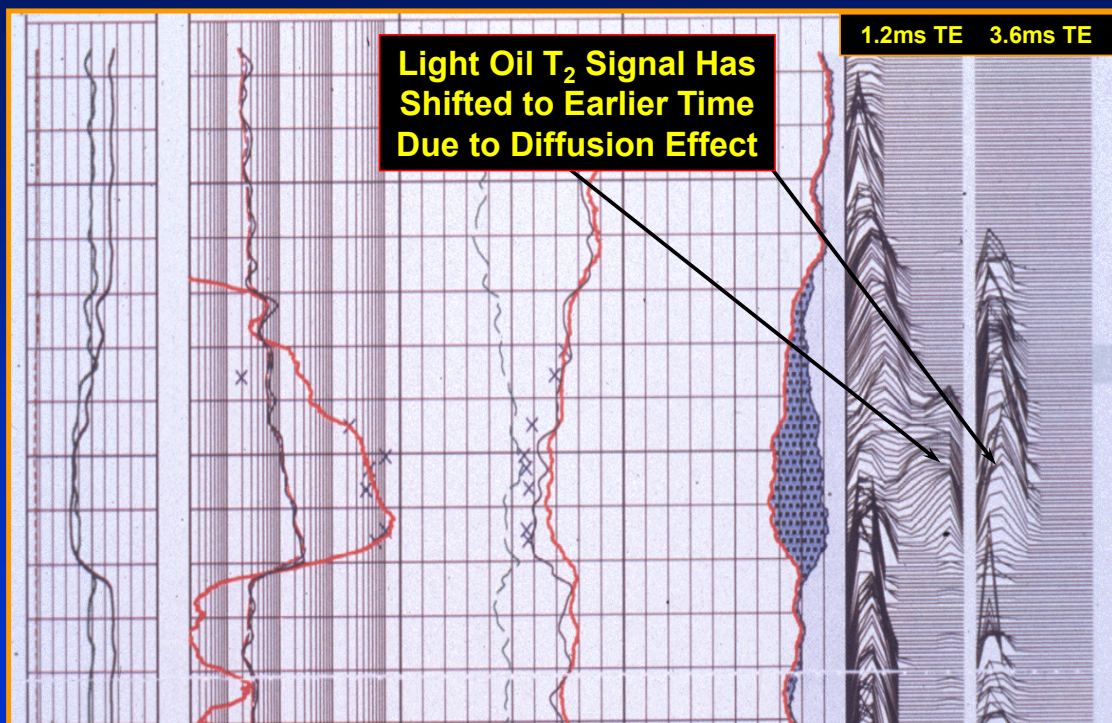


Diffusion during the pulse sequence causes a reduction in signal amplitude with time and decreases T_2 .

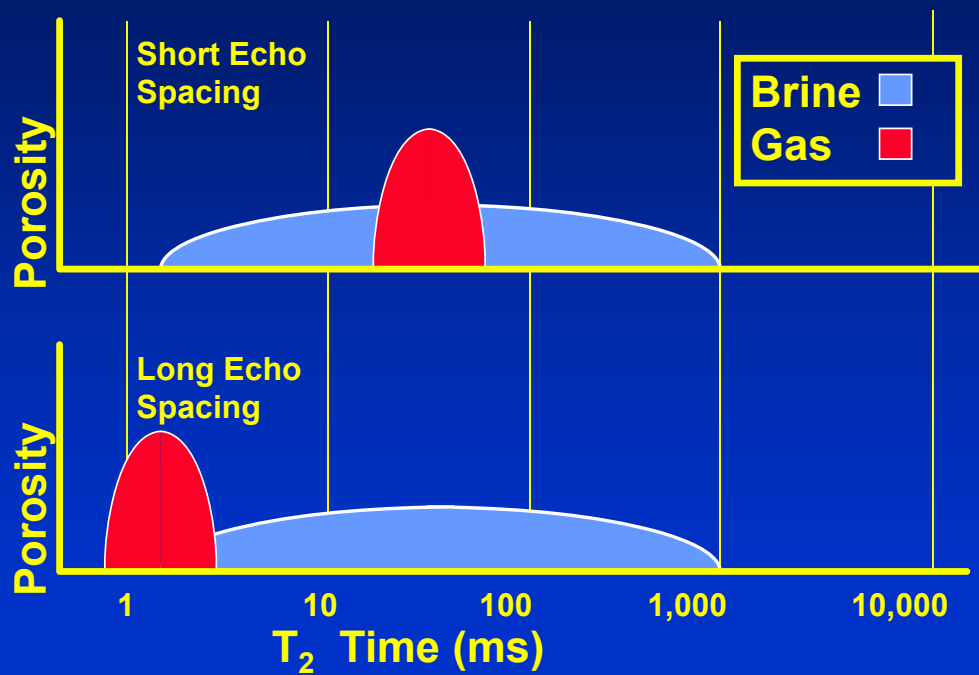
Shifted Spectrum - Gas Detection



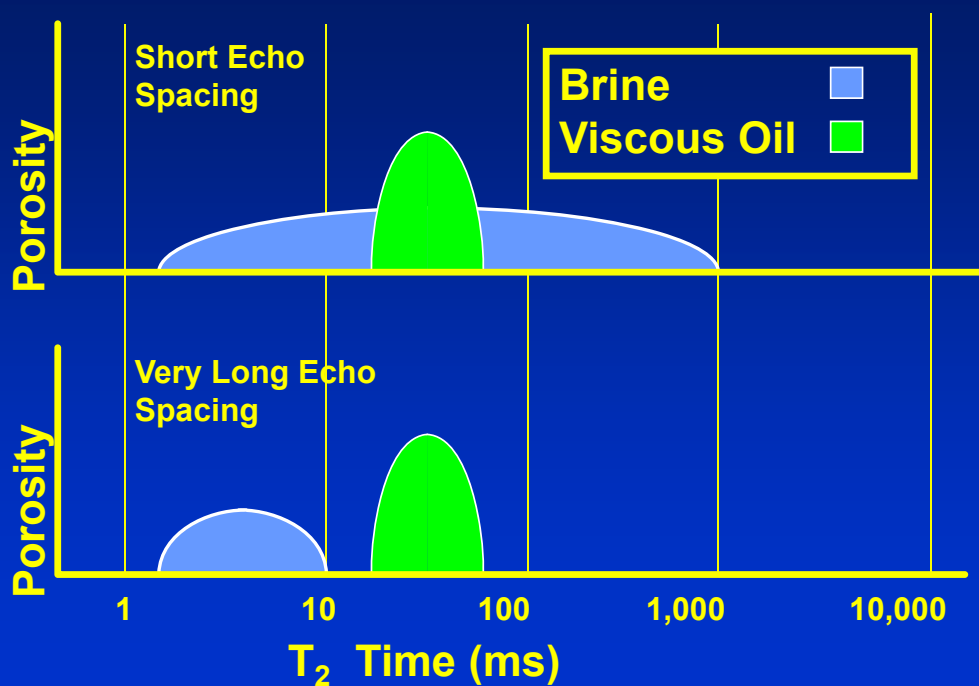
Delta TE Log



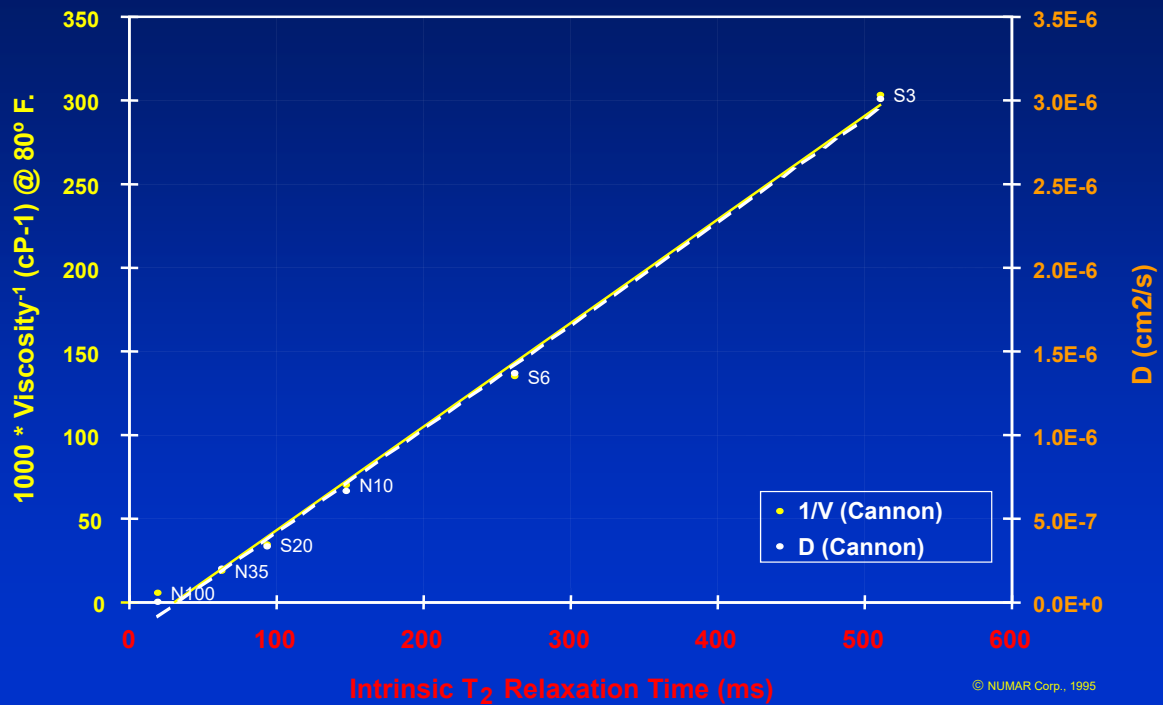
Shifted Spectrum - Gas Detection



Shifted Spectrum - Viscous Oil Detection

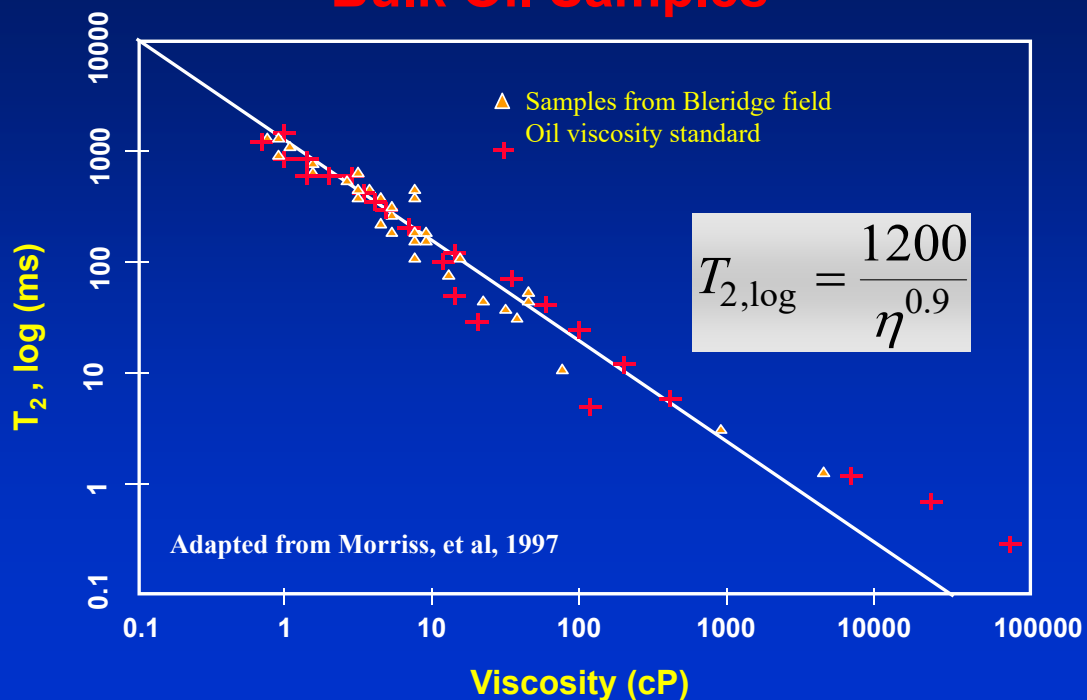


Viscosity, Diffusivity & Intrinsic T₂

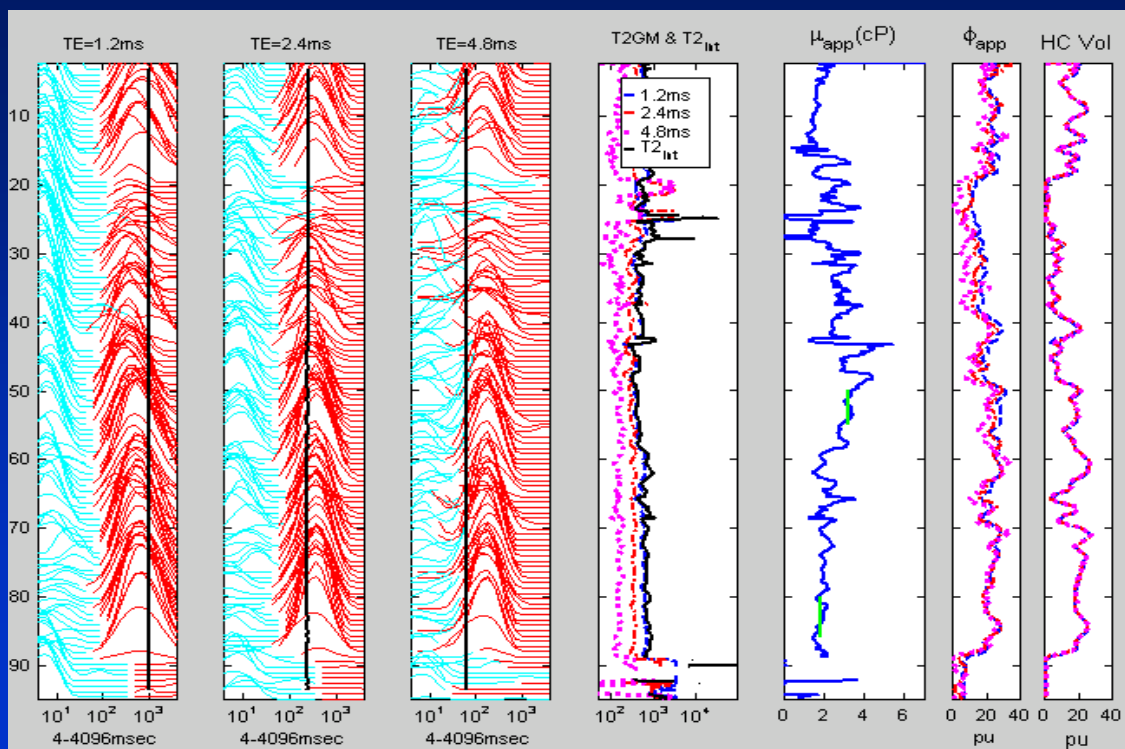


Intrinsic T₂ vs. Oil Viscosity

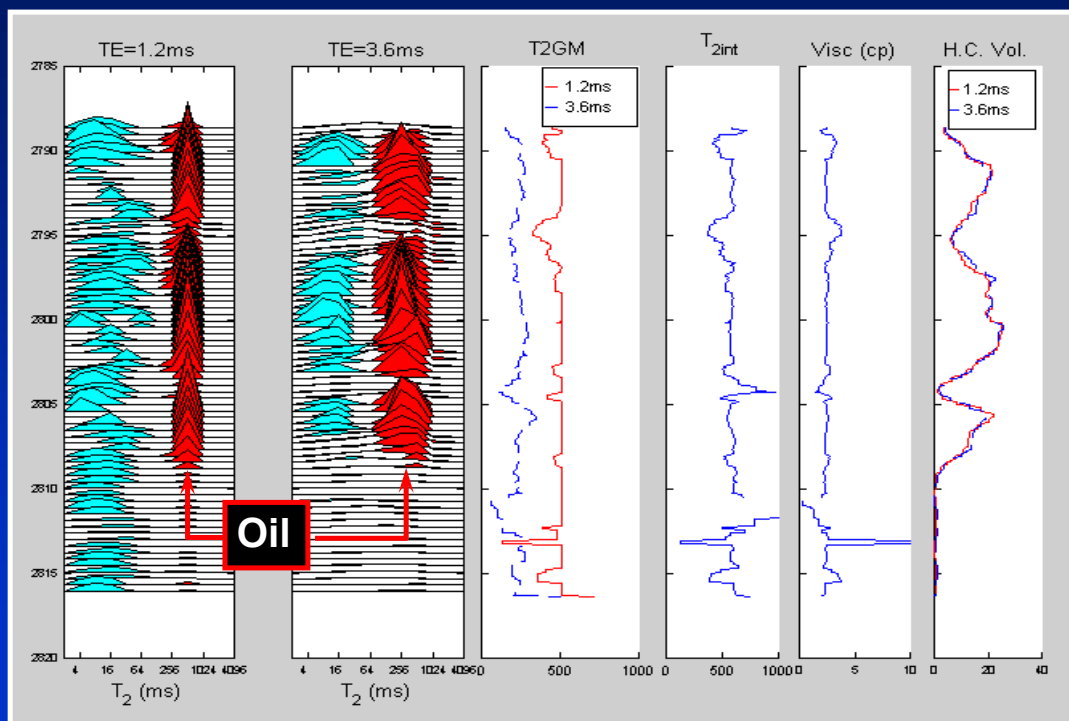
Bulk Oil Samples



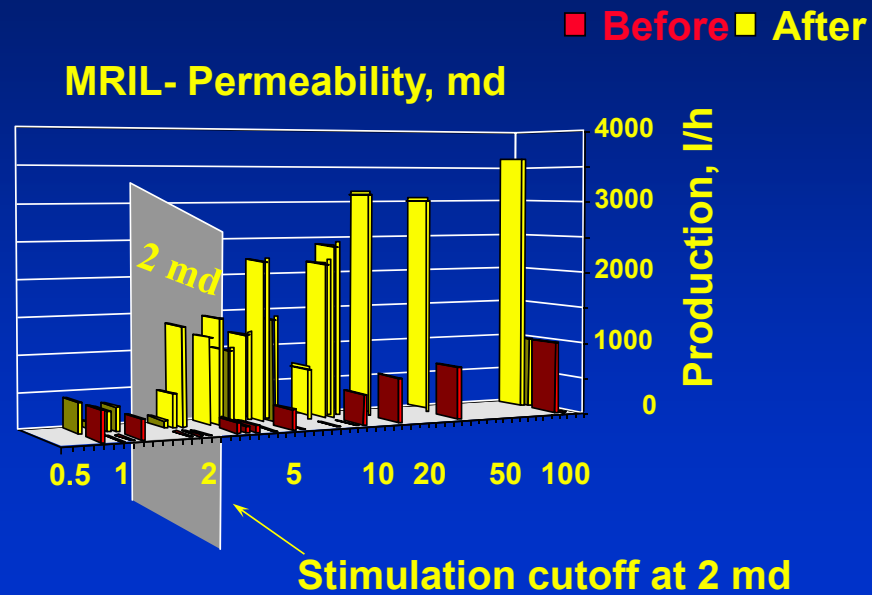
Multiple TE Analysis Deliverables



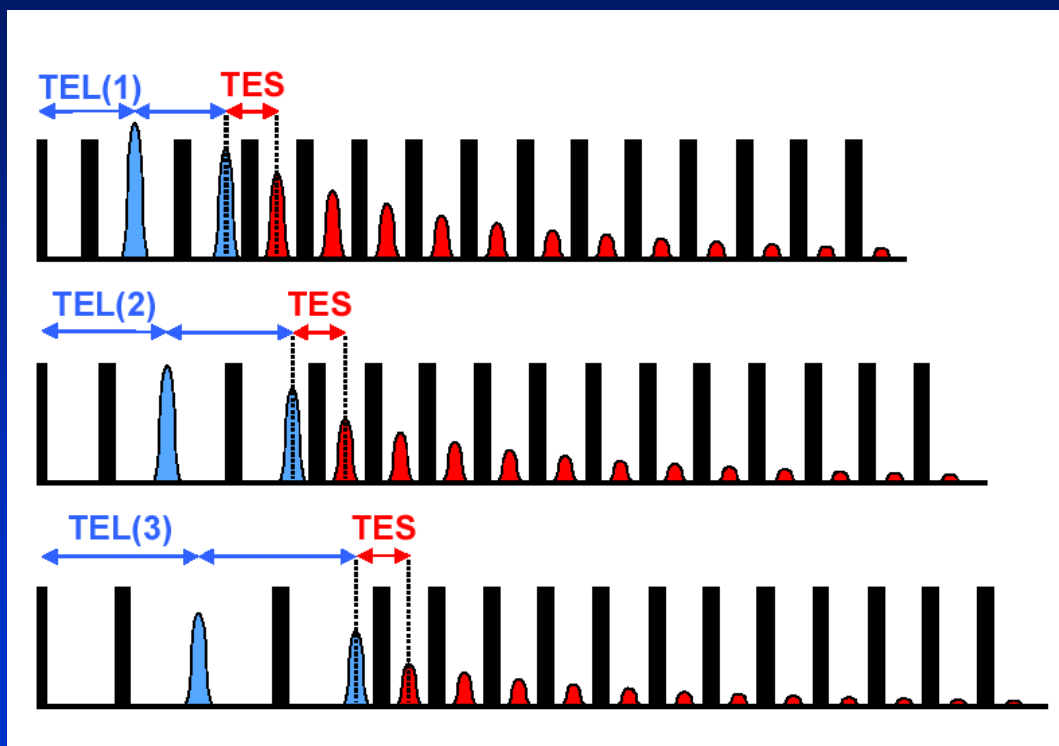
Oil Viscosity Analysis from DTE MRIL Data



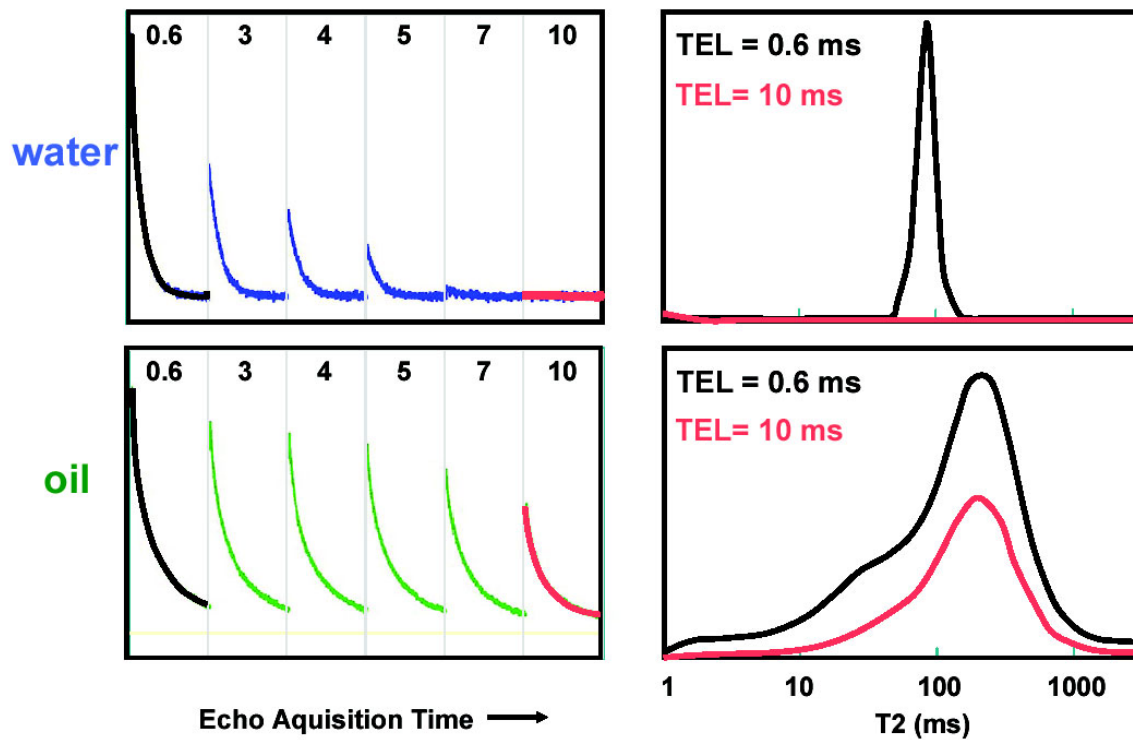
MRIL - Stimulation Success Story



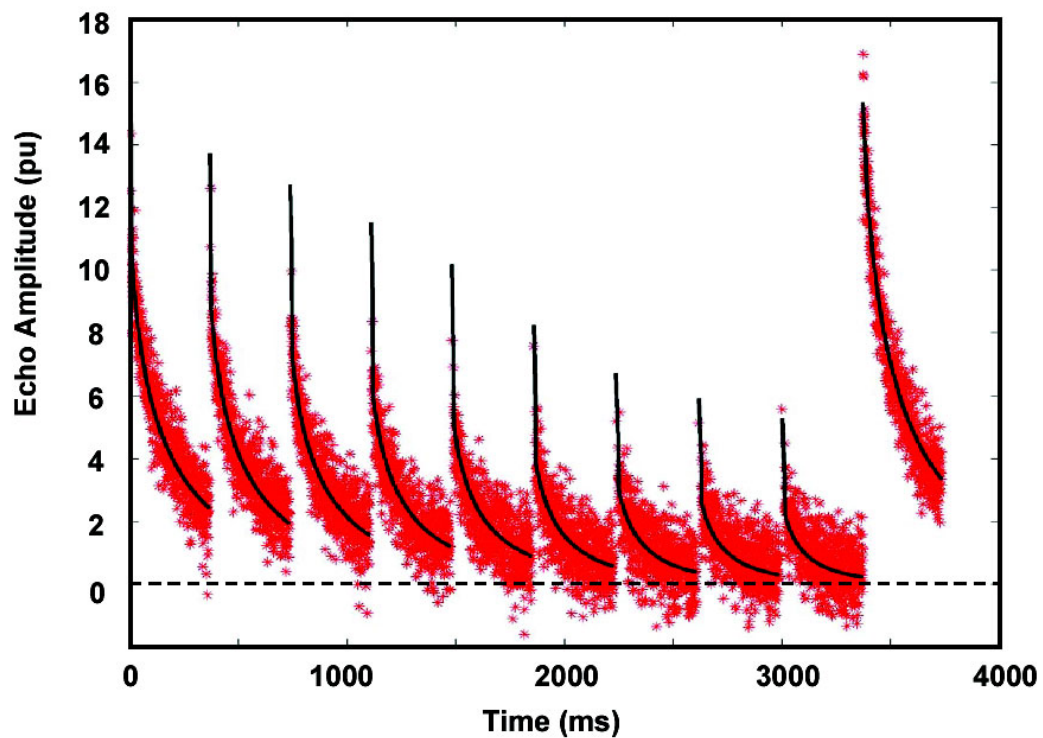
DIFFUSION EDITING PULSING SEQUENCE



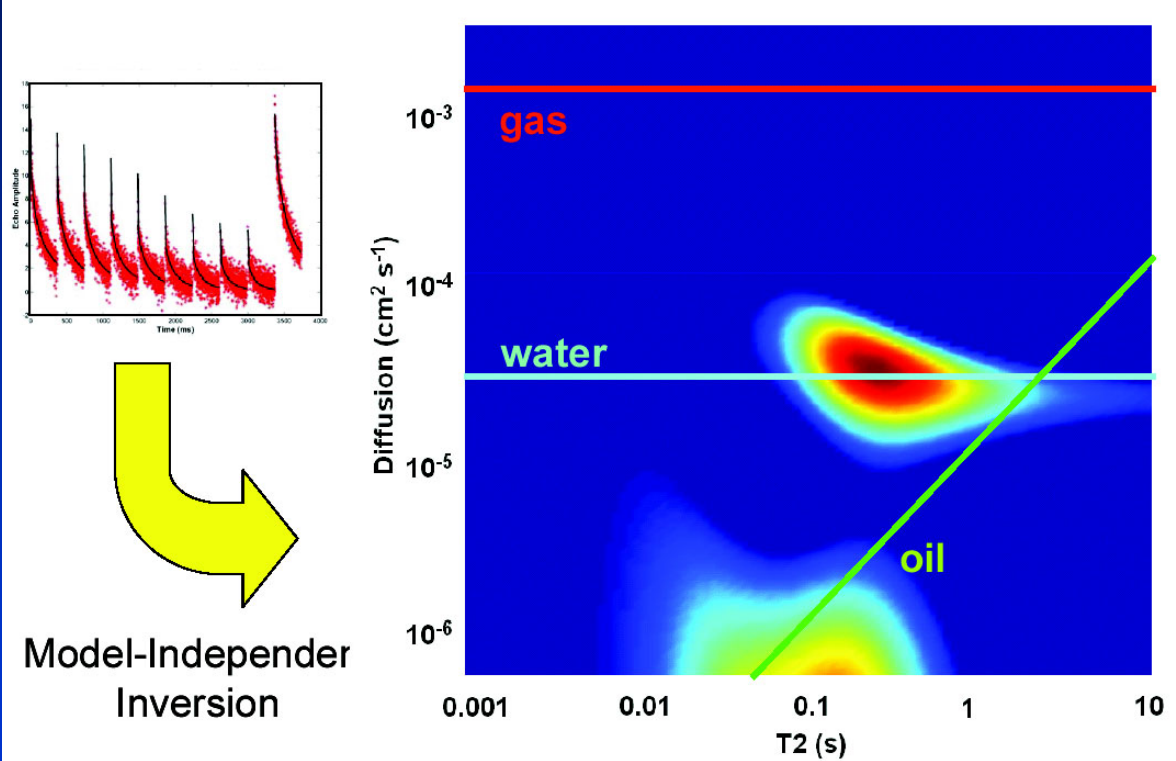
DIFFUSION EDITING MEASUREMENTS



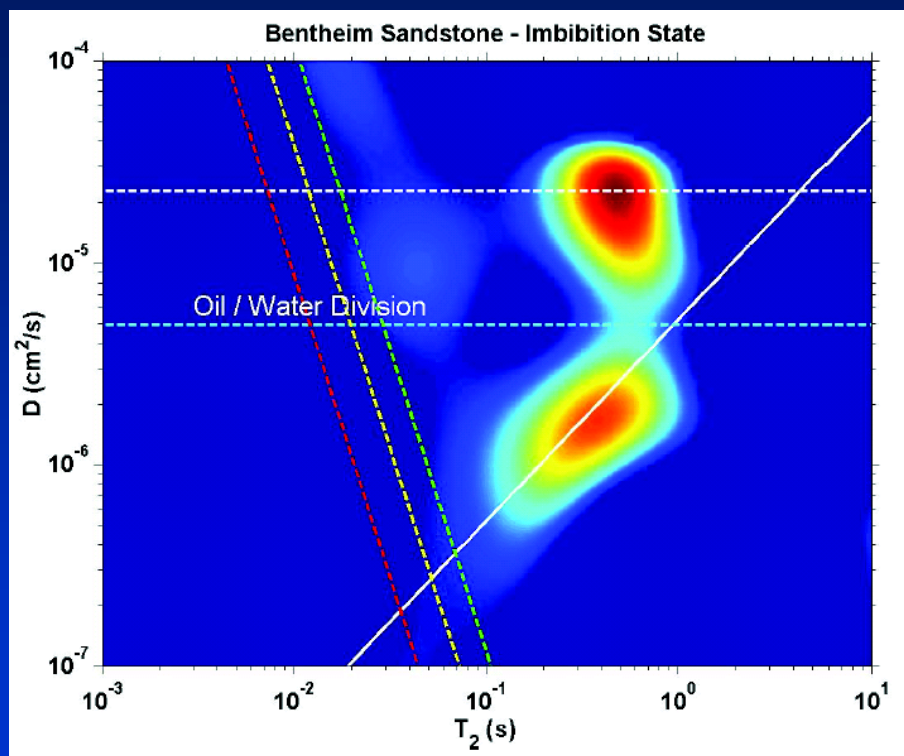
MRX DIFFUSION EDITING DATA



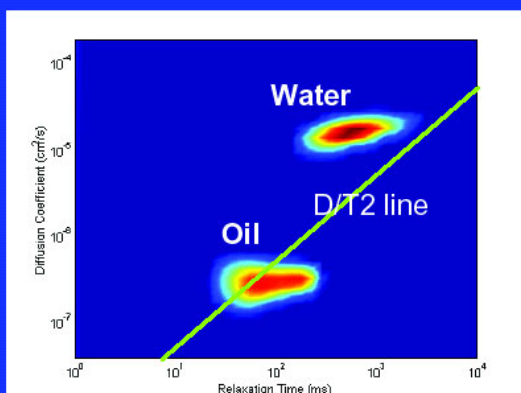
MODEL INDEPENDENT ANALYSIS



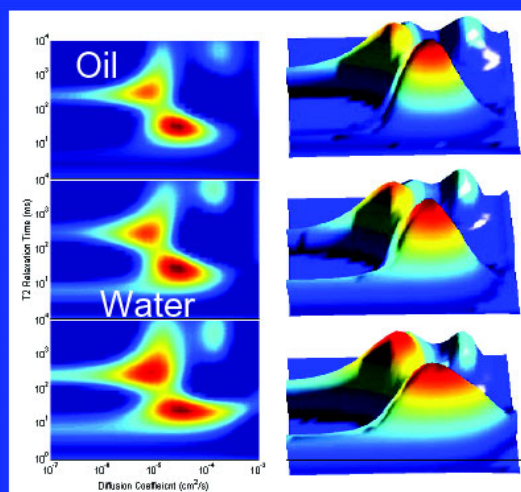
LABORATORY MEASUREMENTS (Hirasaki et al.)



LABORATORY MEASUREMENTS (ChevronTexaco)

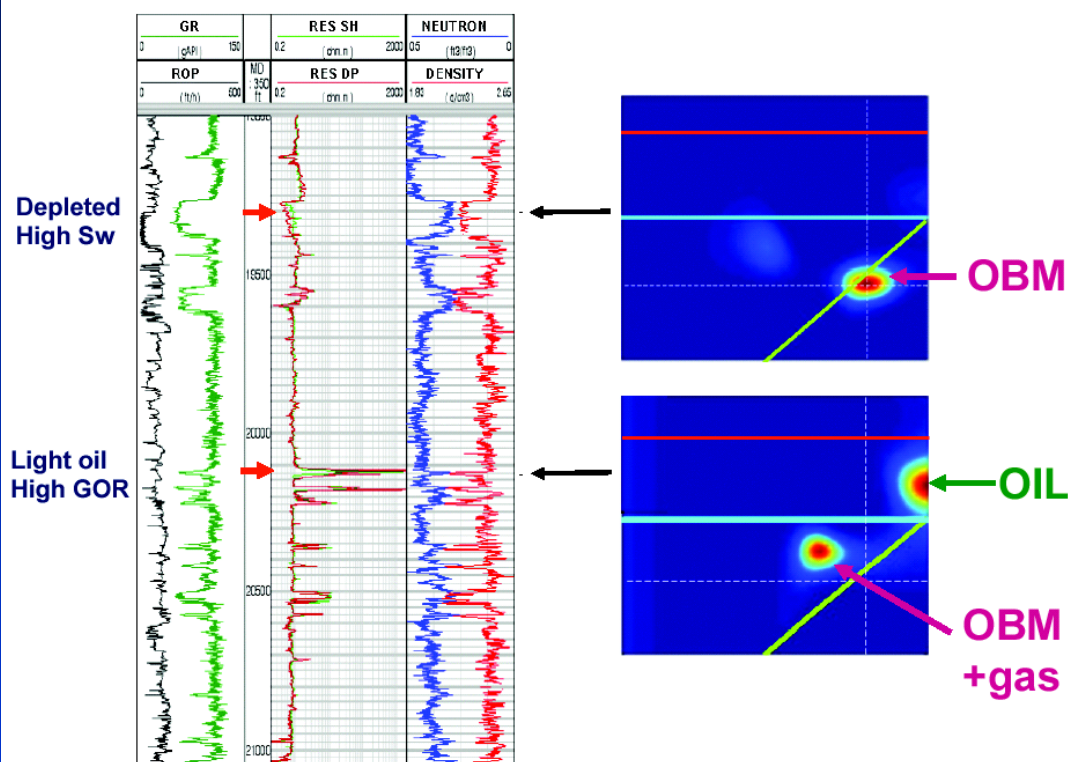


RD2D of Water-oil mixed glass beads measured at laboratory.

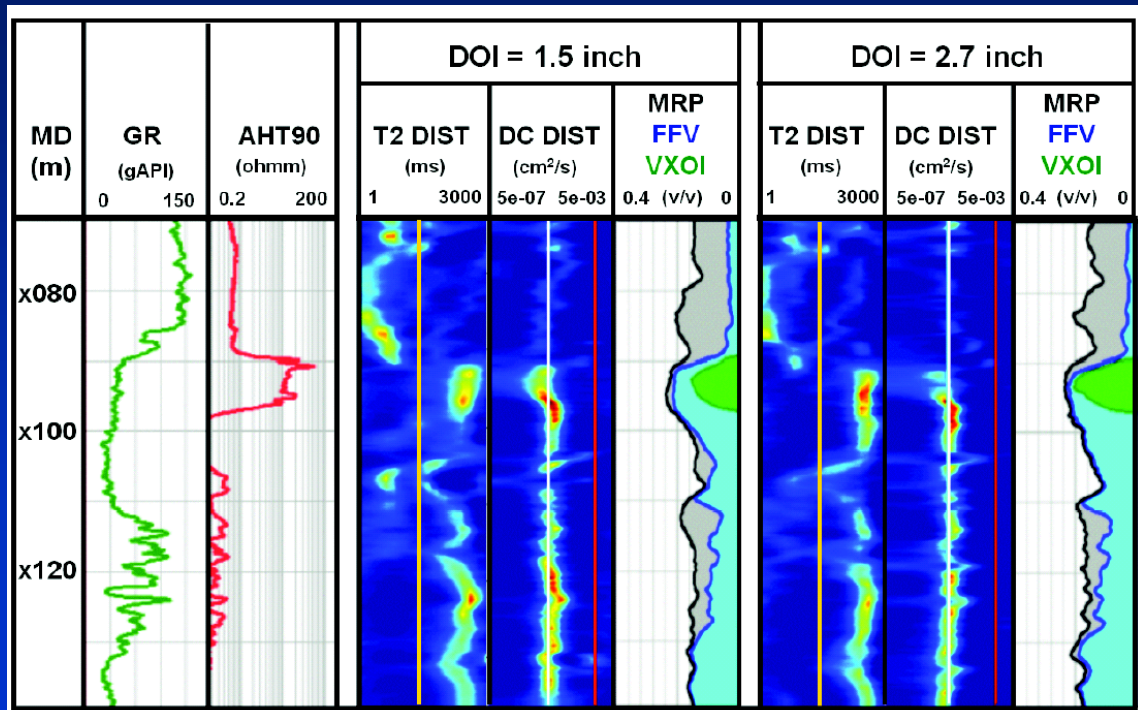


Field example shows resolved oil and water peaks in RD2D map.

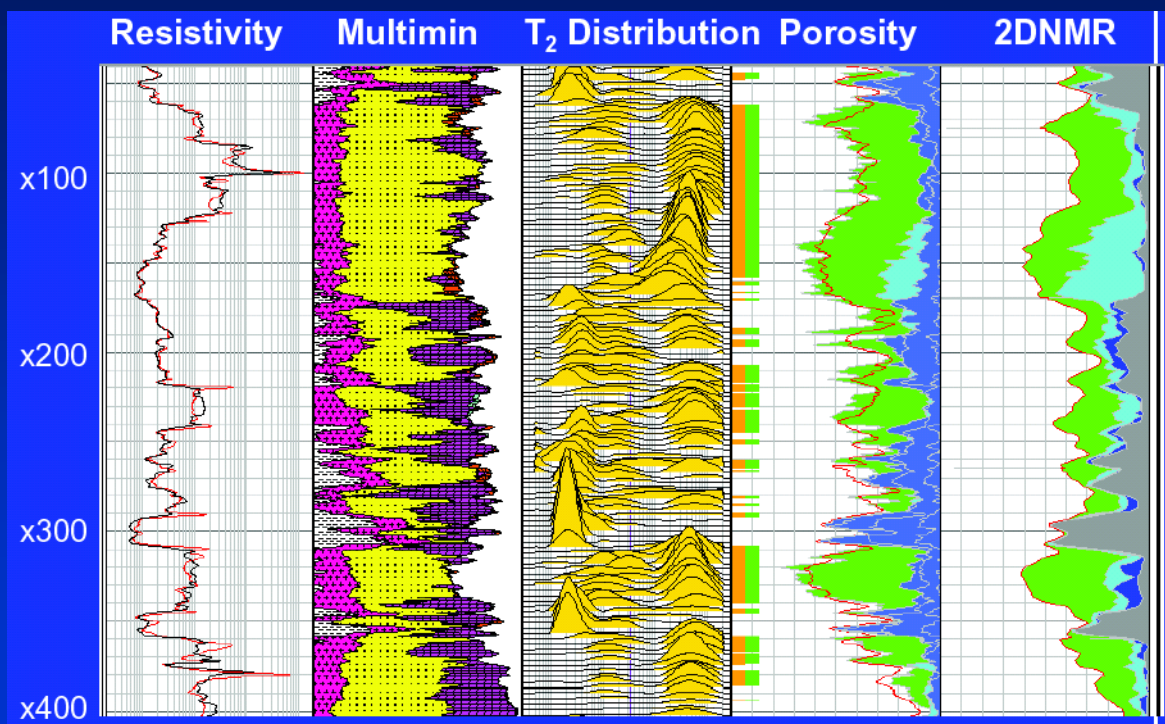
FLUID CHARACTERIZATION: Oil-Base Mud



EXAMPLE



EXAMPLE OF 2DNMR



Acknowledgements:

**Baker Atlas
Schlumberger
Halliburton**