# GIZMO Implementation Details

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### 1 GIZMO: variables and basic equations

#### 1.1 Variables

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6 standard variables : \vec{x}, \vec{v}
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5 conserved variables  $(C): m, \vec{p}, E$ 

5 primitive variables  $(X): \rho, \vec{w}, P$ 

It could be that  $\vec{w} = \vec{v}$ , but this is not generally true for all methods...

6 matrix elements + the volume (can be computed from m and  $\rho$  if this is accurate enough)

15 gradients (3 for every primitive variable)

In total: 37 quantities per particle (without the volume), 34 if the velocity is equal to the fluid velocity

### 1.2 Equations by Neighbour Loops

#### 1.2.1 Loop 1: volumes (=densities) + matrix elements

Volumes are given by (combination of eqns. (7) and (27) from Hopkins):

$$V_{i} = \frac{1}{\sum_{j} W(|\vec{x_{i}} - \vec{x_{j}}|, h_{i})}$$
(1)

The 6 elements of the (symmetric) matrix  $E_i$  by (eqn. (14) in Hopkins without the normalization, because  $E_i$  is only used in combination with  $\psi_i$  (eqn. (12)), which contains the same normalization and cancels it out again):

$$E_i^{\alpha\beta} = \sum_{j} (\vec{x_j} - \vec{x_i})^{\alpha} (\vec{x_j} - \vec{x_i})^{\beta} W(|\vec{x_i} - \vec{x_j}|, h_i)$$
 (2)

The kernel functions in SWIFT do not include the normalization factor  $\frac{1}{h_i^3}$ , so this is added after the loop in the ghost.

#### 1.2.2 Ghost 1: primitive variables + matrix inversion

Use the volume to convert conserved variables to primitive variables (eqn. (5), (7) and (9) in the AREPO paper):

$$\rho = \frac{m}{V} \tag{3}$$

$$\vec{v} = \frac{\vec{p}}{m} \tag{4}$$

$$P = \frac{\gamma - 1}{V} \left( E - \frac{1}{2} \frac{|\vec{p}|^2}{m} \right) \tag{5}$$

Invert the matrix and call the inverse matrix  $B_i$  (eqn. (13) in Hopkins).

#### 1.2.3 Loop 2: gradients

Calculate gradients for the primitive variables (eqn. (12) in Hopkins with eqn. (6) inserted and the normalization constant eliminated):

$$\left(\vec{\nabla}X_i\right)^{\alpha} = \sum_{j} (X_j - X_i) \sum_{\beta} B_i^{\alpha\beta} (\vec{x_j} - \vec{x_i})^{\beta} W(|\vec{x_i} - \vec{x_j}|, h_i)$$
 (6)

If you want to use a slope limiter of some sorts, then this would also be the time to collect the necessary data.

#### 1.2.4 Ghost 2: nothing?

Perform the slope limiting if wanted.

#### 1.2.5 Loop 3: hydro

For every neighbour j, calculate an interface area (combination of eqn. (12) in Hopkins and the definition of  $\vec{A}_{ij}$ , given in between eqns. (18) and (19))

$$\left( \vec{A}_{ij} \right)^{\alpha} = V_i \sum_{\beta} B_i^{\alpha\beta} (\vec{x}_j - \vec{x}_i)^{\beta} W(|\vec{x}_i - \vec{x}_j|, h_i) + V_j \sum_{\beta} B_j^{\alpha\beta} (\vec{x}_j - \vec{x}_i)^{\beta} W(|\vec{x}_i - \vec{x}_j|, h_j)$$
 (7)

Calculate a position for the interface (eqn. (20) in Hopkins):

$$\vec{x_{ij}} = \vec{x_i} + \frac{h_i}{h_i + h_j} (\vec{x_j} - \vec{x_i})$$
 (8)

and a velocity (eqn. (21) in Hopkins):

$$\vec{v_{ij}} = \vec{v_i} + (\vec{v_j} - \vec{v_i}) \left[ \frac{(\vec{x_{ij}} - \vec{x_i}) \cdot (\vec{x_j} - \vec{x_i})}{|\vec{x_i} - \vec{x_j}|^2} \right]$$
(9)

Use the velocity to boost the primitive variables  $X_k$  (k = i, j) to the rest frame of the interface ( $X'_k$ ). This comes down to applying a correction to the fluid velocities.

Use the gradients to interpolate the primitive variables from positions  $\vec{x_i}$  and  $\vec{x_j}$  to  $\vec{x_{ij}}$  and predict them forward in time by half a time step to obtain second order accuracy

in time (eqn. (A3) in Hopkins):

$$X_k'' = X_k' + \left(\vec{\nabla}X\right)_k \cdot (\vec{x_{ij}} - \vec{x_k}) + \frac{\Delta t}{2} \frac{\partial X_k'}{\partial t}.$$
 (10)

The time derivatives are given by (eqn. (A4) in Hopkins)

$$\frac{\partial X_k'}{\partial t} = -\begin{pmatrix} \vec{w'} & \rho' & 0\\ 0 & \vec{w'} & 1/\rho'\\ 0 & \gamma P' & \vec{w'} \end{pmatrix} \vec{\nabla} X_k, \tag{11}$$

or, for example:

$$\frac{\rho_k^{n+1/2} - \rho_k^n}{\Delta t/2} = -(\vec{w_k} - \vec{v_{ij}}^n) \cdot \vec{\nabla} \rho_k^n - \rho_k^n \vec{\nabla} \cdot \vec{w_k}^n$$
 (12)

We then feed the  $X_k''$  to a 1D Riemann solver, that gives us a vector of fluxes  $\vec{F}_{ij}''$ , which we deboost to a static frame of reference  $(\vec{F}_{ij})$ . To account for the arbitrary orientation of the interface, we also feed the normal vector to the interface to the Riemann solver. The Riemann solver internally uses the fluid velocity along the interface normal to solve an effective 1D Riemann problem. The velocity solution along the interface normal is also internally added to the velocities (see GIZMO source code). Mathematically, this is the same as first rotating the velocities to a frame aligned with the interface and then rotating the solution back to the original frame (e.g. AREPO paper), but it is computationally cheaper and causes less round off error in the solution.

Given the solution vector  $X_{\text{half}}$  returned by the Riemann problem, the fluxes are given by (eqns. (1)-(3) in Hopkins)

$$\vec{F}_{\rho} = \rho_{\text{half}} \left( \vec{w}_{\text{half}} - \vec{v}_{ij} \right) \tag{13}$$

$$\vec{F}_{w_k} = \rho_{\text{half}} w_{k,\text{half}} \left( \vec{w}_{\text{half}} - \vec{v}_{ij} \right) + P_{\text{half}} \vec{n}_k \tag{14}$$

$$\vec{F}_P = \rho_{\text{half}} e_{\text{half}} \left( \vec{w}_{\text{half}} - \vec{v}_{ij} \right) + P_{\text{half}} \vec{w}_{\text{half}}, \tag{15}$$

with  $\vec{n}_k$  the unit vector along the coordinate axes (k = x, y, z) and  $e = \frac{P_{\text{half}}}{(\gamma - 1)\rho_{\text{half}}} + \frac{1}{2}\vec{w}_{\text{half}}^2$ .

Finally, we use the fluxes to update the conserved variables (eqn. (23) in Hopkins):

$$\Delta C_k = -\Delta t \sum_j \vec{F}_{ij} \cdot \vec{A}_{ij}. \tag{16}$$

# Equations

$$\psi_i(\mathbf{x}) = \frac{1}{\omega(\mathbf{x})} W(\mathbf{x} - \mathbf{x}_i, h(\mathbf{x}))$$
(17)

$$\omega(\mathbf{x}) = \sum_{j} W(\mathbf{x} - \mathbf{x}_{j}, h(\mathbf{x}))$$
(18)

where  $h(\mathbf{x})$  is some "kernel size" and  $\omega(\mathbf{x})$  is used to normalise the volume partition at any point  $\mathbf{x}$ .

It can be shown that (assuming the kernel  $W(\mathbf{x})$  is normalized such that  $\int_V W(\mathbf{x}) dV =$ 1):

$$V_i = \int_V \psi_i(\mathbf{x}) dV = \frac{1}{\omega(\mathbf{x}_i)}$$
 (19)

$$V = \sum_{i} V_i \tag{20}$$

$$V = \sum_{i} V_{i}$$

$$\int_{V} f(\mathbf{x}) dV = \sum_{i} f(\mathbf{x}_{i}) V_{i} + \mathcal{O}(\Delta x^{2})$$
(20)

Following Hopkins 2015, we arrive at the equation

$$\frac{\mathrm{d}}{\mathrm{d}t}(V_i \mathbf{U}_{k,i}) + \sum_j \mathbf{F}_{k,ij} \cdot \mathbf{A}_{ij} = 0$$
(22)

with

$$\mathbf{A}_{ij}^{\alpha} = V_i \tilde{\boldsymbol{\psi}}_j^{\alpha}(\mathbf{x}_i) - V_j \tilde{\boldsymbol{\psi}}_i^{\alpha}(\mathbf{x}_j)$$
 (23)

for every component k of the Euler equations and every gradient component  $\alpha$ 

The  $\tilde{\psi}(\mathbf{x})$  come from the  $\mathcal{O}(h^2)$  accurate discrete gradient expression from Lanson and Vila 2008:

$$\frac{\partial}{\partial x_{\alpha}} f(\mathbf{x}) \Big|_{\mathbf{x}_{i}} = \sum_{j} \left( f(\mathbf{x}_{j}) - f(\mathbf{x}_{i}) \right) \tilde{\boldsymbol{\psi}}_{j}^{\alpha}(\mathbf{x}_{i}) \tag{24}$$

$$\tilde{\boldsymbol{\psi}}_{j}^{\alpha}(\mathbf{x}_{i}) = \sum_{\beta=1}^{\beta=\nu} \mathbf{B}_{i}^{\alpha\beta}(\mathbf{x}_{j} - \mathbf{x}_{i})^{\beta} \psi_{j}(\mathbf{x}_{i})$$
(25)

$$\mathbf{B}_i = \mathbf{E_i}^{-1} \tag{26}$$

$$\mathbf{E}_{i}^{\alpha\beta} = \sum_{j} (\mathbf{x}_{j} - \mathbf{x}_{i})^{\alpha} (\mathbf{x}_{j} - \mathbf{x}_{i})^{\beta} \psi_{j}(\mathbf{x}_{i})$$

$$(27)$$

where  $\alpha$  and  $\beta$  again represent the coordinate components for  $\nu$  dimensions.

## 3 Explicit Computations

#### 3.1 Normalization

To compute the normalisations 18, we need to sum over all neighbouring particles and sum the kernels correctly. To evaluate the kernels, we use the kernel\_deval(xij, wij, wij\_dx) function in SWIFT.

If a kernel is defined as

$$W_i(\mathbf{x}) = W(\mathbf{x} - \mathbf{x}_i, h(\mathbf{x})) = \frac{1}{h(\mathbf{x})^{\nu}} w\left(\frac{|\mathbf{x} - \mathbf{x}_i|}{h(\mathbf{x})}\right)$$

then kernel\_deval computes

$$\begin{split} \text{wij} &= w(\text{xij}) \\ \text{and} \quad \text{wij\_dx} &= \frac{\partial w(r)}{\partial r} \big|_{r=\text{xij}} \\ \text{with} \quad \text{xij} &= \frac{|\mathbf{x}_i - \mathbf{x}_j|}{h(\mathbf{x}_i)} \end{split}$$

So for a specific particle position i, we need to compute

$$\begin{split} \omega(\mathbf{x}_i) &= \sum_j W(\mathbf{x}_i - \mathbf{x}_j, h(\mathbf{x}_i)) \\ &= \sum_j \frac{1}{h(\mathbf{x}_i)^{\nu}} w\left(\frac{|\mathbf{x}_i - \mathbf{x}_j|}{h(\mathbf{x}_i)}\right) \\ &= \sum_j \frac{1}{h_i^{\nu}} \text{wij} \end{split}$$

with  $h_i = h(\mathbf{x}_i)$ .

## 3.2 Analytical gradients of $\psi(x)$

For the Ivanova et al. 2013 expression of the effective surfaces  $\mathbf{A}_{ij}$ , we need analytical gradients in Cartesian coordinates of  $\psi_i(\mathbf{x}_j)$ .

From eq. 17 we have that

$$\psi_j(\mathbf{x}_i) = \frac{W(\mathbf{x}_i - \mathbf{x}_j, h(\mathbf{x}_i))}{\omega(\mathbf{x}_i)}$$

Let  $r_{ij} \equiv |\mathbf{x}_i - \mathbf{x}_j|$  and  $q_{ij} \equiv \frac{r_{ij}}{h_i}$ . Then

$$\frac{\partial}{\partial x}\psi_{j}(\mathbf{x}_{i}) = \frac{\partial}{\partial x} \frac{W(\mathbf{x}_{i} - \mathbf{x}_{j}, h(\mathbf{x}_{i}))}{\omega(\mathbf{x}_{i})} = \frac{\partial}{\partial x} \frac{W(r_{ij}, h_{i})}{\omega(\mathbf{x}_{i})}$$

$$= \frac{\frac{\partial W}{\partial x}(r_{ij}, h_{i}) \ \omega(\mathbf{x}_{i}) - W(r_{ij}, h_{i}) \frac{\partial \omega}{\partial x}(\mathbf{x}_{i})}{\omega(\mathbf{x}_{i})^{2}}$$

$$= \frac{1}{\omega(\mathbf{x}_{i})} \frac{\partial W}{\partial x}(r_{ij}, h_{i}) - \frac{1}{\omega(\mathbf{x}_{i})^{2}} W(r_{ij}, h_{i}) \frac{\partial}{\partial x} \sum_{k} W(r_{ik}, h_{i})$$

$$= \frac{1}{\omega(\mathbf{x}_{i})} \frac{\partial W}{\partial x}(r_{ij}, h_{i}) - \frac{1}{\omega(\mathbf{x}_{i})^{2}} W(r_{ij}, h_{i}) \sum_{k} \frac{\partial W}{\partial x}(r_{ik}, h_{i})$$
(28)

If a kernel<sup>1</sup> is defined as

<sup>&</sup>lt;sup>1</sup> Helpful way to think of the indices:  $W_j(\mathbf{x}_i) = W(|\mathbf{x}_j - \mathbf{x}_i|, h_i)$  is the kernel value of particle i at position  $\mathbf{x}_i$  evaluated at the position  $\mathbf{x}_j$ . Personally I would've used the indices the other way around

$$W_j(\mathbf{x}_i) = W(\mathbf{x}_i - \mathbf{x}_j, h_i) = \frac{1}{h_i^{\nu}} w\left(\frac{|\mathbf{x}_i - \mathbf{x}_j|}{h_i}\right) = \frac{1}{h_i^{\nu}} w(q_{ij})$$

and we assume that the smoothing length  $h_i$  is treated as constant at this point, then the gradient of the kernel is given by

$$\frac{\partial}{\partial x} W_j(\mathbf{x}_i) = \frac{\partial}{\partial x} \left( \frac{1}{h_i^{\nu}} w(q_{ij}) \right) 
= \frac{1}{h_i^{\nu}} \frac{\partial w(q_{ij})}{\partial q_{ij}} \frac{\partial q_{ij}(r_{ij})}{\partial r_{ij}} \frac{\partial r_{ij}}{\partial x}$$
(29)

We now use

$$\frac{\partial q_{ij}(r_{ij})}{\partial r_{ij}} = \frac{\partial}{\partial r_{ij}} \frac{r_{ij}}{h_i} = \frac{1}{h_i} 
\frac{\partial r_{ij}}{\partial x} = \frac{\partial}{\partial x} \sqrt{(\mathbf{x}_i - \mathbf{x}_j)^2} = \frac{1}{2} \frac{1}{\sqrt{(\mathbf{x}_i - \mathbf{x}_j)^2}} \cdot 2(\mathbf{x}_i - \mathbf{x}_j) 
= \frac{\mathbf{x}_i - \mathbf{x}_j}{r_{ij}}$$
(31)

To be perfectly clear, we should in fact write

$$r_j(\mathbf{x}) \equiv |\mathbf{x} - \mathbf{x}_j|$$

which again leads to

$$\frac{\partial r_{ij}}{\partial x} = \frac{\partial r_j(\mathbf{x}_i)}{\partial x} = \frac{\partial r_j(\mathbf{x})}{\partial x} \Big|_{\mathbf{x} = \mathbf{x}_i}$$

$$= \frac{\partial}{\partial x} \sqrt{(\mathbf{x} - \mathbf{x}_j)^2} \Big|_{\mathbf{x} = \mathbf{x}_i} = \frac{1}{2} \frac{1}{\sqrt{(\mathbf{x} - \mathbf{x}_j)^2}} \cdot 2(\mathbf{x} - \mathbf{x}_j) \Big|_{\mathbf{x} = \mathbf{x}_i}$$

$$= \frac{\mathbf{x} - \mathbf{x}_j}{r_j(\mathbf{x})} \Big|_{\mathbf{x} = \mathbf{x}_i} = \frac{\mathbf{x}_i - \mathbf{x}_j}{r_{ij}}$$

for simplified thinking, but I'm going to stick to this notation because Hopkins also uses it.

Inserting expressions 30 and 31 in 29, we obtain

$$\frac{\partial}{\partial x}W_j(\mathbf{x}_i) = \frac{1}{h_i^{\nu+1}} \frac{\partial w(q_{ij})}{\partial q_{ij}} \frac{\mathbf{x}_i - \mathbf{x}_j}{r_{ij}}$$
(32)

 $\frac{\partial w(q_{ij})}{\partial q_{ij}}$  is given by wij\_dx of kernel\_deval.

Finally, inserting 32 in 28 we get

$$\frac{\partial}{\partial x}\psi_j(\mathbf{x}_i) = \frac{1}{\omega(\mathbf{x}_i)} \frac{1}{h_i^{\nu+1}} \text{wij\_dx} \frac{\mathbf{x}_i - \mathbf{x}_j}{r_{ij}} - \frac{1}{\omega(\mathbf{x}_i)^2} W(r_{ij}, h_i) \sum_k \frac{1}{h_i^{\nu+1}} \text{wik\_dx} \frac{\mathbf{x}_i - \mathbf{x}_k}{r_{ik}} \quad (33)$$

The definition of  $r_{ij}$  requires a bit more discussion. Since kernels used in hydrodynamics (at least in those methods currently implemented in SWIFT) are usually taken to be spherically symmetric, we might as well have defined

$$r'_{ij} = |\mathbf{x}_j - \mathbf{x}_i|$$

which would leave the evaluation of the kernels invariant  $[r'_{ij} = r_{ij}]$ , but the gradients would have the opposite direction:

$$\frac{\partial r'_{ij}}{\partial x} = \frac{\mathbf{x}_j - \mathbf{x}_i}{r'_{ij}} = -\frac{\mathbf{x}_i - \mathbf{x}_j}{r_{ij}} = -\frac{\partial r_{ij}}{\partial x}$$

So which definition should we take?

Consider a one-dimensional case where we choose two particles i and j such that  $x_j > x_i$  and  $q_{ij} = |x_j - x_i|/h_i < H$ , where H is the compact support radius of the kernel of choice. Because we're considering a one-dimensional case with  $x_j > x_i$ , we can now perform a simple translation such that particle i is at the origin, i.e.  $x'_i = 0$  and  $x'_j = x_j - x_i = |x_j - x_i| = r_{ij}$ . In this scenario, the gradient in Cartesian coordinates and in spherical coordinates must be the same:

$$\frac{\partial}{\partial x'}W(|x_i'-x'|,h_i)\Big|_{x'=x_j'} = \frac{\partial}{\partial r_{ij}}W(r_{ij},h_i)$$

$$\Rightarrow \frac{1}{h_i^{\nu}} \frac{\partial w(q_{ij}')}{\partial q_{ij}'} \frac{\partial q_{ij}'(r_{ij}')}{\partial r_{ij}'} \frac{\partial r_i'(x')}{\partial x'} \Big|_{x'=x_j'} = \frac{1}{h_i^{\nu}} \frac{\partial w(q_{ij})}{\partial q_{ij}} \frac{\partial q_{ij}(r_{ij})}{\partial r_{ij}}$$
(34)

We have the trivial case where

$$r'_{ij} = |x'_i - x'_j| = |x_i - x_j| = r_{ij}$$

$$q'_{ij} = r'_{ij}/h_i = q_{ij}$$

$$\Rightarrow \frac{\partial w(q'_{ij})}{\partial q'_{ij}} = \frac{\partial w(q_{ij})}{\partial q_{ij}}, \quad \frac{\partial q'_{ij}(r'_{ij})}{\partial r'_{ij}} = \frac{\partial q_{ij}(r_{ij})}{\partial r_{ij}}$$

giving us the condition from 34:

$$\frac{\partial r_i'(x')}{\partial x'}\Big|_{x'=x_j'} = 1 = \frac{\partial r_i(x)}{\partial x}$$
(35)

this is satisfied for

$$r_j(\mathbf{x}) = |\mathbf{x} - \mathbf{x}_j|$$
  
 $\Rightarrow r_{ij} = |\mathbf{x}_i - \mathbf{x}_j|, \text{ not } r_{ij} = |\mathbf{x}_j - \mathbf{x}_i|$ 

### References

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