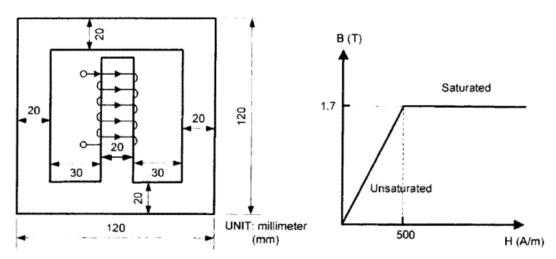
Q1. Fig. 1 shows the structure of an inductor. The unit of the dimensions is millimeter (mm). The B-H curve of the core is also shown, which is simplified from the real B-H curve with two asymptotes. The thickness of the core is **20 mm**. The length of the air gap is **1 mm**. The **100 turns** winding is mounted on the center leg. Neglect the fringing effect and winding resistance. If the excitation voltage (voltage across the winding) is **10 V** (AC rms, 60 Hz), determine the rms value of the excitation current.



Q2. Test results from a single phase, 20 kVA, 4160 V/208 V, 60 Hz transformer are as follows:

	Terminal voltage, $V_t$ (V)	Terminal Current, $I_t$ (A)	Input power, $P_{in}$ (W)
Open circuit test (LV side)	208	3.2	73
Short circuit test (HV side)	153	2.6	54

- a) Determine the parameters (Req , Xeq , Rc, and Xm ) of the transformer referred to the HV side.
- b) Draw the approximate equivalent circuit of the transformer referred to the HV side.

Q3. A shunt dc motor has the rated armature current of 40 A. The total resistance in the armature circuit is  $0.3 \Omega$  and the total resistance in the field circuit is  $100 \Omega$ . When the shunt motor is connected to a 180 V power supply, the terminal current is 4.8 A and the motor rotates at 1500 P rpm without any mechanical load. Assuming that the terminal voltage remains at 180V and the rotational loss is constant, answer the following questions:

- a) Calculate rotational loss P<sub>rot</sub>,
- b) Calculate speed and torque at the rated armature current, assuming no armature reaction,
- c) Calculate the efficiency at the rated armature current, assuming no armature reaction,

- d) Calculate the speed, torque at the rated armature current assuming a 6% flux reduction due to armature reaction.
- Q4. A **440 V**, **60 Hz**, Y-connected, 4-pole slip ring (wound rotor) induction motor has the following circuit parameters:  $R_1 = 0.6\Omega$ ,  $R_2' = 0.5\Omega$ ,  $X_1 = X_2' = 0.8\Omega$ ,  $X_m = 50\Omega$ , calculate the following:
  - a) The starting line current (stator current)  $I_1$ ,
  - b) Starting torque T<sub>st</sub>,
  - c) Speed of rotation n in rpm when the shaft developed torque is 160 Nm
  - d) Maximum developed torque,  $T_{\text{max}}$

Q1. If Be × 1.7T. Mc = 1.7/500 = 0.0034 A = Z0x20 = 400 mm<sup>2</sup>

$$R_g = \frac{l_g}{M_0 A} = \frac{1 \times 10^{-3}}{4\pi \times 10^{7} \times (0.02 \times 0.02)}$$

$$R_{c} = \frac{le}{u_{cA}} = 7.3529 \times 10^{6}$$

$$V = E = (0V = 4.44 f N \phi_{PK} \rightarrow \phi_{PK} = \frac{10}{4.44 \times 60 \times 100}$$
(no resistance) = 3.7538 × 10-4 Wb

$$Bpk = \frac{\phi_{PK}}{A} = 0.93847 < 1.77$$

$$NI_{PK} = \phi_{PK} \cdot R_{+} \Longrightarrow I = \frac{\phi_{PK} \cdot R_{+}}{N \cdot \sqrt{2}} = \frac{3.7538 \times (R_{1} / / R_{2} + R_{c} + R_{g})}{100 \times \sqrt{2}}$$

= 5.6709 A

$$R_{c,LV} = \frac{V_4^2}{P} = \frac{208^2}{73} = 592.66.2$$

$$I_{m} = \sqrt{I_{t}^{2} - I_{c}^{2}} = \sqrt{3.2^{2} - 0.35096^{2}} = \sqrt{10.1168} = 3.1807A$$

referred to the HV side:

$$\chi_m = a^2 \chi_{m,LV} = z_0^2 \times 65.39 = z_{6.16k\Omega}$$

$$\chi_{eq} = \sqrt{(V_{I_{+}})^{2} - (R_{eq})^{2}} = \sqrt{\frac{153}{2.6}^{2} - 7.9882^{2}} = \sqrt{3399.06} = 58.3.2$$

b)

$$I_f = V_f/R_f = 180/100 = 1.8A$$
,  $I_a = I_f - I_f = 4.8 - 1.8 = 3.A$   
 $P_{ele} = E_{a,NL}I_{a,NL} = (V_f - I_aR_a)I_a = (180 - 0.3 \times 3) \times 3 = 537.3W$   
 $P_{rot} = P_{ele} = 537.3W$ 

Ea, NL = 
$$V_4$$
 -  $IaRa = 180 - 0.3 \times 3 = 179.1 V$   
 $WNL = \frac{1500}{60} \times 2\pi = 157.08 \text{ rad/s}$   
 $Ka\phi = \frac{1}{60} \times 2\pi = 179.1/157.08 = 1.14 \text{ V. Sec/rad}$   
 $Ea_1FL = V_4$  -  $IaRa = 180 - 0.3 \times 40 = 168 \text{ V}$   
 $WFL = \frac{Ea_1FL}{Ka\phi} = \frac{168}{1.14} = \frac{147.368 \text{ rad/s}}{2\pi} \times 60 = \frac{147.386}{2\pi} \times 60 = \frac{1407.26 \text{ rpm}}{2\pi}$   
 $T = Ka\phi Ia = 1.14 \times 40 = 45.6 \text{ Nm}$ 

$$P_{in} = V_{4}(I_{f} + I_{a}) = 180 \times (40 + \frac{180}{100}) = 7524W$$
 $P_{ele} = E_{oi,FL}I_{a,FL} = 168 \times 40 = 6720W$ 
 $P_{out} = P_{ele} - P_{rot} = 6720 - 537.3 = 6182.7W$ 
 $h = P_{out}/P_{in} = 6182.7/7524 = 0.822$ 

d) n=1497.1 rpm T=42.864 Nm

$$K\alpha p_{FL} = 0.94 K\alpha p_{NL} = 0.94 \times 1.14 = 1.0716 V$$
 Sey rad  
 $E\alpha_{i}FL = V_{t} - I_{\alpha}R_{\alpha} = 180 - 0.3 \times 40 = 168 V$   
 $W_{FL} = \frac{E\alpha_{i}FL}{K\alpha p_{FL}} = \frac{168}{1.0716} = 156.775 \text{ rad/s}$   
 $n = \frac{W_{FL}}{2\pi} \times 60 = \frac{156.775}{2\pi} \times 60 = 1497.1 \text{ Npm}$   
 $T = K\alpha p_{FL} = 1.0716 \times 40 = 42.864 Nm$ 

Therenize the circuit at a-b  $V_{1} = V_{0} = \frac{j \times m}{R_{1} + j \times (X_{1} + \chi_{m})} V_{1} = \frac{j \times 0}{0.6 + j \times 0.8} V_{1} = \frac{j \times 0}{0.6 + j \times 0.8} V_{1} = 0.984 \angle 0.7^{\circ} V_{1}$   $V_{1} = 254.04V \implies V_{2} = \frac{j \times m}{R_{1} + j \times 1} V_{1} = \frac{j \times m}{R_{1} + j \times 1} V_{2} = \frac{j \times m}{R_$ 

a) 
$$Z_{+}$$
 at any speed or slip is  $Z_{+} = Z_{+}h + jX_{z}' + \frac{R_{z}'}{S} = 0.581 + j0.744 + j0.8 + \frac{0.5}{S}$ 

When starting,  $N_{r} = 0. \Rightarrow S = \frac{N_{s} - N_{r}}{N_{s}} = \frac{N_{s} - 0}{N_{s}} = 1$ 

i.  $Z_{T} = 0.581 + j0.744 + j0.8 + \frac{0.5}{1} = 1.081 + j1.594 = 1.926 \angle 55.86^{\circ}(52)$ 
 $I_{z}' = \frac{V_{+}h}{Z_{T}} = \frac{249.98 \angle 0.7^{\circ}}{1.926 \angle 55.86^{\circ}} = 129.792 \angle -55.16^{\circ}(A)$ 

i.  $V_{+}h = I_{z}'(\frac{R_{z}'}{I} + jX_{z}') = 129.792 \angle -55.16^{\circ}(0.5 + j0.8)$ 
 $= 129.792 \angle -55.16^{\circ}(0.9434257.995^{\circ})$ 
 $= 129.792 \angle -55.16^{\circ}(0.9434257.995^{\circ})$ 

Plow go back to I to equivalent circuit to calcute Im and  $I_{1}$ 
 $I_{m} = \frac{V_{+}h}{J_{m}} = \frac{122.45 \angle 2.84^{\circ}}{50 \angle 90^{\circ}} = 2.449 \angle -87.16^{\circ}(A)$ 
 $I_{1} = I_{z}' + I_{m} = 129.792 \angle -55.16^{\circ} + 2.449 \angle -87.16^{\circ}$ 
 $= 131.89 | \angle -55.73^{\circ}(A)$ 

b)  $T = 3 \frac{(I_{z}')^{2} R_{z}'}{W_{s}}$ , at starting,  $S = 1$ 
 $N_{S} = \frac{120f}{P} = \frac{120(60)}{A} = 1800 rpm$   $W_{S} = \frac{1800}{60}.2\pi = 188.5 rad/sec$ 

Tst = 3. (129.792) (0.5) 188.5 = 134.053 Nm

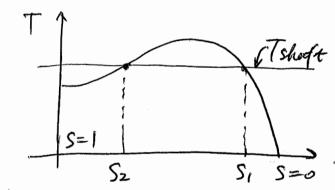
(b)

c) Torque at any slip 
$$T = \frac{3}{\omega_s} (I_z)^2 \frac{R_z^2}{S}$$

$$|I_{2}'| = \frac{|V_{4h}|^{2}}{\sqrt{(R_{4h} + \frac{R_{2}'}{s})^{2} + (X_{4h} + X_{2}')^{2}}} \Rightarrow |I_{2}'|^{2} = \frac{(249.98)^{2}}{(0.581 + \frac{0.5}{3})^{2} + (1.594)^{2}}$$

$$T = 160 = \frac{3}{188.5} \cdot \frac{(249.98)^2}{(0.581 + \frac{0.5}{3})^2 + (1.594)^2} \cdot (\frac{0.5}{5})$$

$$160 = \frac{497.268.5}{2.8795^2 + 0.5315 + 0.25} \Rightarrow 2.8795^2 - 2.5775 + 0.25 = 0$$



Sz operates in unstable region, only S, is acceptable

d) at Tmax. 
$$\frac{R_2'}{S_m} = \sqrt{R_{th}^2 + (X_{th} + X_2')^2}$$

$$\Rightarrow Sm = \frac{R_z^1}{\sqrt{R_{th}^2 + (\chi_{th}^2 + \chi_z^2)^2}}$$

$$= \frac{0.5}{\sqrt{(0.581)^2 + (0.794 + 0.8)^2}} = 0.295$$

Calculate 
$$I_2'$$
 using Thevenin circuit

$$I_2' = \frac{V_1}{(Rth + \frac{R_2'}{Sm}) + j(Xth + X_2')} = \frac{249.98 \times 0.7^{\circ}}{(0.581 + \frac{0.5}{D.295}) + j(0.744 + 0.8)}$$

$$= 89.953 \times 34.31^{\circ}(A)$$

$$= 89.953 \times 34.31^{\circ}(A)$$

$$= (89.953)^{\circ}(\frac{0.5}{0.295}) = 218.2 \times N.m$$