

Digital Signal Processing

## Chapter V. Digital filtering

## Response of LTI systems to harmonic signals

- ▶ We consider an LTI system with  $h[n]$
- ▶ Input signal = complex harmonic (exponential) signal  $x[n] = Ae^{j\omega_0 n}$
- ▶ Output signal = convolution

$$\begin{aligned}y[n] &= \sum_{k=-\infty}^{\infty} h[k]x[n-k] \\&= \sum_{k=-\infty}^{\infty} h[k]e^{-j\omega_0 k} Ae^{j\omega_0 n} \\&= H(\omega_0) \cdot x[n]\end{aligned}$$

- ▶  $H(\omega_0)$  = Fourier transform of  $h[n]$  evaluated for  $\omega = \omega_0$

# Response of LTI systems to harmonic signals

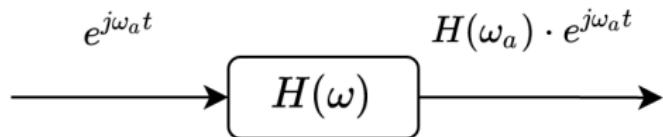


Figure 1: Output = a constant  $\times$  Input

- ▶  $H(\omega)$  = Fourier transform of  $h[n]$  evaluated for  $\omega$  = **transfer function**

# Eigen-function

- ▶ Complex exponential signals are **eigen-functions** (funcții proprii) of LTI systems:
  - ▶ output signal = input signal  $\times$  a (complex) constant
- ▶  $H(\omega_0)$  is a constant that multiplies the input signal
  - ▶ Amplitude of input gets multiplied by  $|H(\omega_0)|$
  - ▶ Phase of input signal is added with  $\angle H(\omega_0)$
- ▶ Why are sin/cos/exp functions important?
  - ▶ If input signal = sum of complex exponentials (like cosines + sines),
  - ▶ then output = same sum of complex exponentials, each scaled with some coefficients

## Response to cosine and sine

- ▶ Cosine / sine = sum of two exponentials, via Euler

$$\cos(\omega n) = \frac{e^{j\omega n} + e^{-j\omega n}}{2}$$

$$\sin(\omega n) = \cos(\omega n - \frac{\pi}{2})$$

- ▶ System is linear and real =>
  - ▶ amplitude is multiplied by  $|H(\omega_0)|$
  - ▶ phase increases by  $\angle H(\omega_0)$
- ▶ See proof at blackboard

# Frequency response

- ▶ Naming:
  - ▶  $H(\omega)$  = **frequency response** of the system
  - ▶  $|H(\omega)|$  = **amplitude response** (or magnitude response)
  - ▶  $\angle H(\omega)$  = **phase response**
- ▶ Magnitude response is non-negative:  $|H(\omega)| \geq 0$
- ▶ Phase response is an angle:  $\angle H(\omega) \in (-\pi, \pi]$ 
  - ▶ Phase response may have jumps of  $2\pi$  (wrapped phase)
  - ▶ Stitching the pieces in a continuous function = phase *unwrapping*
  - ▶ Unwrapped phase: continuous function, may go outside interval  $(-\pi, \pi]$
  - ▶ Example: at blackboard

- ▶ Warning:  $\cos(\omega n)$  does not start at  $n = 0$
- ▶ The above harmonic signals start at  $n = -\infty$ .
- ▶ What's wrong if the signal starts at some time  $n$ ?

## Permanent and transient response

- ▶ What if the signal starts at some time  $n$ ?
- ▶ Total response = transient response + permanent response
  - ▶ transient response goes towards 0 as  $n$  increases
  - ▶ permanent response = what remains
- ▶ So the above relations are valid only in **permanent regime**
  - ▶ i.e. after the transient regime has passed
  - ▶ i.e. after the transient response has practically vanished
  - ▶ i.e. when the signal started very long ago (from  $n = -\infty$ )
  - ▶ i.e. when only the permanent response remains in the output signal
- ▶ Example at blackboard

## Permanent response of LTI systems to periodic inputs

- ▶ Consider an input  $x[n]$  which is periodic with period N
- ▶ Then it can be represented as a Fourier series with coefficients  $c_k$ :

$$x[n] = \frac{1}{N} \sum_{k=0}^{N-1} c_k e^{j2\pi kn/N}$$

- ▶ Since the system is linear, each component  $k$  gets multiplied with  $H\left(\frac{2\pi}{N}k\right)$
- ▶ So the total output is:

$$y[n] = \frac{1}{N} \sum_{k=0}^{N-1} c_k H\left(\frac{2\pi}{N}k\right) e^{j2\pi kn/N}$$

- ▶ The output is still periodic, same period, same frequencies

## Response of LTI systems to non-periodic signals

- ▶ Consider a general input  $x[n]$  (not periodic)
- ▶ The output = input convolution with impulse response

$$y[n] = x[n] * h[n]$$

$$Y(\omega) = X(\omega) \cdot H(\omega)$$

- ▶ Output spectrum = Input spectrum  $\times$  Transfer function

## Response of LTI systems to non-periodic signals

- ▶ The transfer function  $H(\omega)$  “shapes” the spectrum

$$Y(\omega) = X(\omega) \cdot H(\omega)$$

- ▶ In polar form:

- ▶ modulus is multiplied

$$|Y(\omega)| = |X(\omega)| \cdot |H(\omega)|$$

- ▶ phases is added:

$$\angle Y(\omega) = \angle X(\omega) + \angle H(\omega)$$

## Response of LTI systems to non-periodic signals

- ▶ The system **attenuates/amplifies** the input frequencies and **changes their phases**
- ▶  $H(\omega)$  = the **transfer function**
- ▶  $H(z)$  = the **system function**
- ▶  $H(\omega) = H(z = e^{j\omega})$  if unit circle is in CR

## Power spectral density

- ▶  $S_{zz}(\omega) = |Y(\omega)|^2 = |H(\omega)|^2 \cdot S_{xx}(\Omega)$
- ▶ The poles and zeros of  $S(\omega)$  come in pairs  $(z, 1/z)$  and  $p, 1/p$

- ▶ LTI systems are also known as **filters** because their transfer function shapes (“filters”) the frequencies of the input signals
- ▶ The transfer function can be found from  $H(z)$  and  $z = e^{j\omega}$
- ▶ Alternatively, the transfer function can be found by the **geometrical method** based on the locations of poles and zeros

## Ideal filters

- ▶ Draw at whiteboard the ideal transfer function of a:
  - ▶ low-pass filter
  - ▶ high-pass filter
  - ▶ band-pass filter
  - ▶ band-stop filter
  - ▶ all-pass filter (*changes the phase*)

- ▶ The **order** of a filter = maximum degree in numerator or denominator of  $H(z)$ 
  - ▶ i.e. largest power of  $z$  or  $z^{-1}$
- ▶ Any filter can be implemented, in general, with this number of unit delay blocks ( $z^{-1}$ )
- ▶ Higher order -> better filter transfer function
  - ▶ closer to ideal filter
  - ▶ more complex to implement
  - ▶ more delays (bad)
- ▶ Lower order
  - ▶ worse transfer function (not close to ideal)
  - ▶ simpler, cheaper
  - ▶ faster response

## Filter design by pole and zero placements

- ▶ Based on geometric method
- ▶ The gain coefficient must be found by separate condition
  - ▶ i.e. specify the desired magnitude response at one frequency
- ▶ Examples at blackboard

## Filter distortions

- ▶ When a filter is non-ideal:
  - ▶ non-constant amplitude → amplitude distortions
  - ▶ non-linear phase → phase distortions
- ▶ Phase distortions may be tolerated by certain applications
  - ▶ e.g. human auditory system is largely insensitive to phase distortions of sounds

## Effect of system's phase

- ▶ What is the effect of system's phase response  $\angle H(\omega)$ ?
- ▶ Extra phase = delay
  - ▶ different frequencies are delayed differently
  - ▶ phase
- ▶ **Linear-phase** filter: delays all frequencies with the same amount of time
  - ▶ i.e. the whole signal is delayed, but otherwise not distorted
  - ▶ otherwise, we get distortions

## Linear-phase filters

- ▶ For a sinusoidal signal, extra phase of  $2\pi =$  delay of a period  $N = \frac{1}{f}$
- ▶ To ensure same delay for all frequencies (in time), the phase  $\angle H(\omega)$  must be proportional to the frequency
  - ▶ draw at blackboard
  - ▶ hence the name **linear**

## Linear-phase filters

- ▶ Example: consider the following filter with **linear phase** function:

$$H(\omega) = C \cdot e^{-j\omega n_0}$$

- ▶ The output signal is

$$Y(\omega) = X(\omega) \cdot C \cdot e^{-j\omega n_0}$$

$$y[n] = C \cdot x[n - n_0]$$

- ▶ Linear phase means **just a delaying** of the input signal

- ▶ Fourier property:  $x[n - n_0] <--> X(\omega)e^{-j\omega n_0}$

## Group delay

- ▶ Group delay = The time delay experienced by a component of frequency  $\omega$  when passing through the filter

- ▶ as opposed to “phase delay” = the phase added by the filter

- ▶ **Group delay** of the filter:

$$\tau_g(\omega) = \frac{d\Theta(\omega)}{d\omega}$$

- ▶ Linear phase = constant group delay = all frequencies delayed the same = whole signal delayed

## Linear-phase FIR filters

What type of filters can have linear phase?

- ▶ IIR filters cannot have linear phase (no proof provided)
- ▶ Only FIR filters can have linear phase, and only if they satisfy some symmetry conditions

## Symmetry conditions for linear-phase FIR

- ▶ Let filter have an impulse response of length  $M$  (order is  $M - 1$ )
- ▶ The filter coefficients are  $h[0], \dots, h[M - 1]$
- ▶ Linear-phase is guaranteed in two cases

- ▶ **Positive symmetry**

$$h[n] = h[M - 1 - n]$$

- ▶ **Negative symmetry (anti-symmetry)**

$$h[n] = -h[M - 1 - n]$$

- ▶ The delay = the delay of the middle point of the symmetry

## Cases of linear-phase FIR

- ▶ Proofs at blackboard
  - 1. Positive symmetry,  $M = \text{odd}$
  - 2. Positive symmetry,  $M = \text{even}$
  - 3. Negative symmetry,  $M = \text{odd}$
  - 4. Negative symmetry,  $M = \text{even}$
- ▶ Check constraints for  $H(0)$  and  $H(\pi)$
- ▶ For what types of filters is each case appropriate?

## Proof example

Linear-phase proof for a FIR system with positive symmetry,  $M = \text{odd}$

- ▶ Only for an example, it is simpler (general case at blackboard)
- ▶ Suppose we have a FIR filter with  $M = 5$  coefficients:

$$h[n] = \{4, 3, 2, 3, 4\}$$

$$H(z) = 4 + 3z^{-1} + 2z^{-2} + 3z^{-3} + 4z^{-4}$$

- ▶ having positive symmetry (first = last, second = second to last, etc)
- ▶ and length  $M = \text{odd}$ , i.e. one coefficient is alone in the middle

## Proof example

- ▶ Let's compute  $H(\omega)$ :

$$\begin{aligned} H(\omega) &= \sum_n h[n] e^{-j\omega n} \\ &= 4e^0 + 3e^{-j\omega} + 2e^{-j2\omega} + 3e^{-j3\omega} + 4e^{-j4\omega} \\ &= e^{-j2\omega}(4e^{j2\omega} + 3e^{j\omega} + 2 + 3e^{-j1\omega} + 4e^{-j2\omega}) \\ &= e^{-j2\omega}(4e^{j2\omega} + 4e^{-j2\omega} + 3e^{j\omega} + 3e^{-j1\omega} + 2) \\ &= e^{-j2\omega}(4 \cdot 2 \cos(2\omega) + 3 \cdot 2 \cos(\omega) + 2) \\ &= \underbrace{e^{j\angle H(\omega)}}_{e^{j \cdot \text{phase}}} \underbrace{|H(\omega)|}_{\text{real}} \end{aligned}$$

- ▶ The phase is  $\angle(H(\omega)) = -2\omega$ , a **linear** function
- ▶ The phase of the filter is linear

## Proof explained

Key points in this proof:

- ▶ we pull a common factor, so that the first and last terms have the same exponents, but with opposite signs
- ▶ we group first with last term, second with second-to-last:
  - ▶ they have same coefficient in front, because of positive symmetry
  - ▶  $e^{jx} + e^{-jx} = 2 \cos(x) = \text{real}$
- ▶ everything remaining in the right-side parenthesis is a real-valued

Since  $H(\omega) = |H(\omega)|e^{j\angle H(\omega)}$ , we identify the two terms:

- ▶  $|H(\omega)|$  must be the real part in the right-side
- ▶  $\angle H(\omega)$  must be the term  $-2\omega$ , which is a linear function of  $\omega$  (up to some changes in sign of the real part)

Generalizations:

- ▶ the filter length can be anything, as long as it has symmetry
- ▶ if  $M$  is even, there is no single term remaining in the middle, but the proof stays the same
- ▶ if we have **negative** symmetry, the terms have opposite signs, and we use:

$$e^{jx} - e^{-jx} = 2j \sin(x) = 2 \sin(x) \cdot e^{j\frac{\pi}{2}}$$

## Zero-phase FIR filters

- ▶ Can we avoid delay altogether?
- ▶ **Zero-phase** filter = a particular type of linear-phase filter with zero delay
- ▶ For a zero-phase filter, the phase response  $\angle H(\omega) = 0$ 
  - ▶ (Group) delay = derivative of  $\angle H(\omega)$
  - ▶ delay 0  $\Leftrightarrow$  flat  $\angle H(\omega) \Leftrightarrow \angle H(\omega) = 0$
- ▶ Delay is 0  $\Leftrightarrow$  symmetry with respect to  $h[0]$ 
  - ▶ the system cannot be causal

## Zero-phase FIR filters

- ▶ Zero-phase filters must be non-causal
  - ▶ left side of  $h[n]$  symmetrical to right side of  $h[n]$
- ▶ For causal, we need to delay  $h[n]$  to be wholly on the right side => delay

## Example

- Linear-phase filter (low-pass):

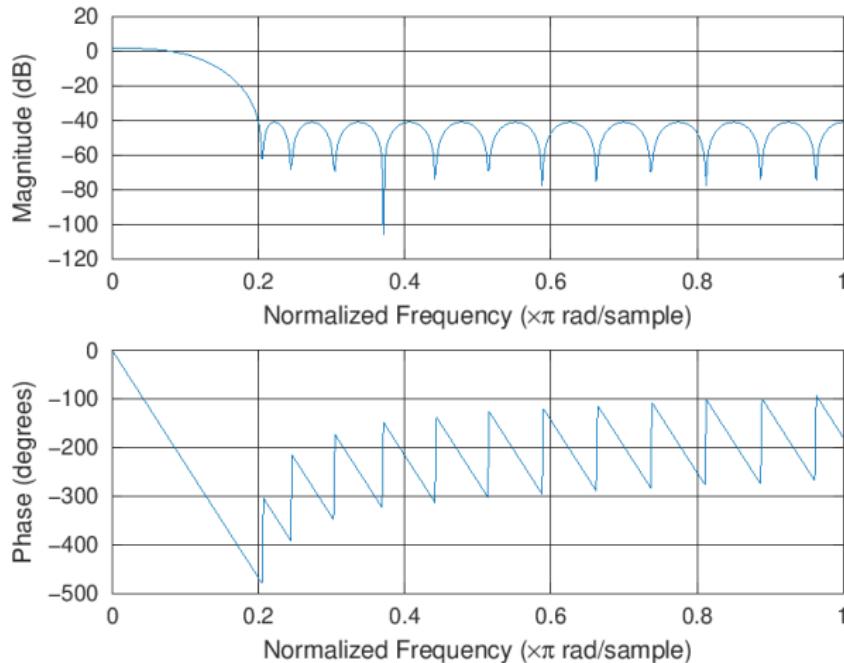


Figure 2: Transfer function of linear-phase filter

## Example

- ▶ The impulse response (positive symmetry):

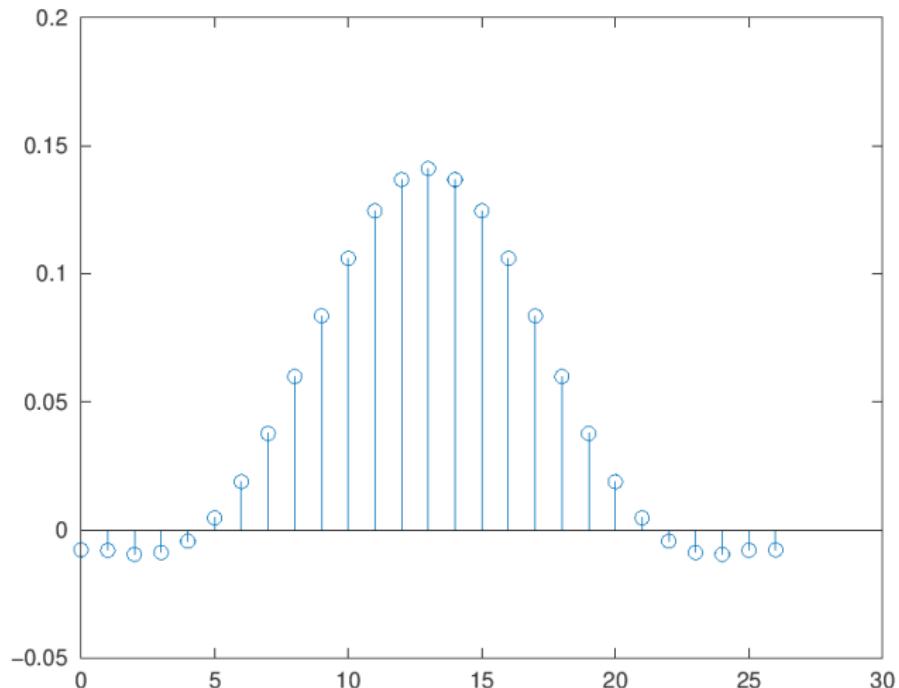


Figure 3: Impulse response of linear-phase filter

## Example

- ▶ ECG signal: original and filtered. Filtering introduces **delay**

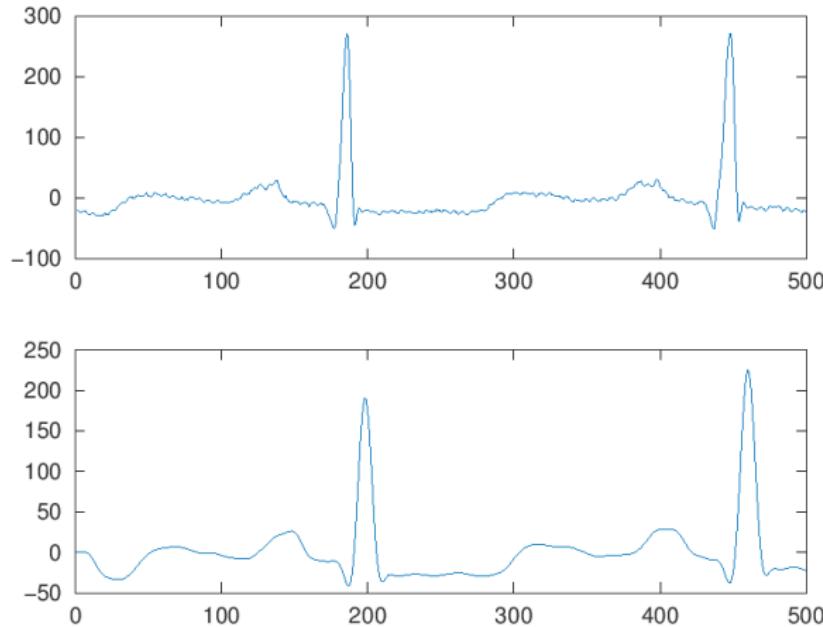


Figure 4: Delay introduced by filtering

## Example

- ▶ Solution: zero-phase filter (positive symmetry, and centered in 0):
- ▶ But filter is **not causal** anymore

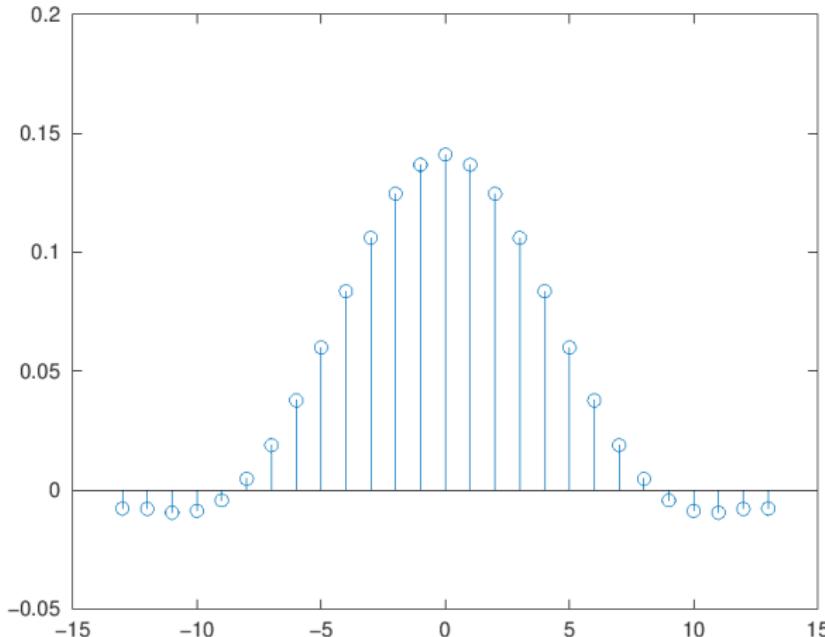


Figure 5: Impulse response of zero-phase filter

## Example

- ▶ Filtering with zero-phase filter introduces **no delay**

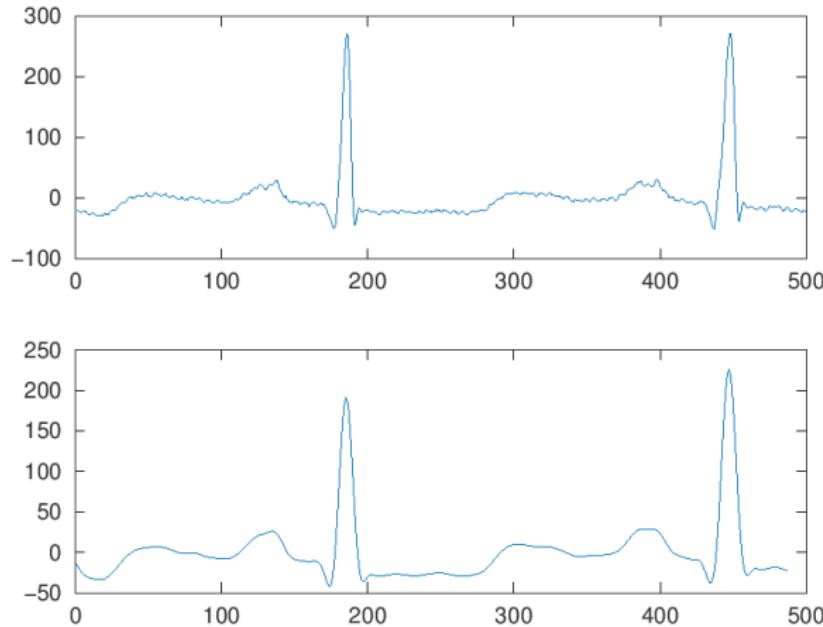


Figure 6: Zero-phase filter introduces no delay

- ▶ **Digital resonators** = very selective band pass filters
  - ▶ poles very close to unit circle
  - ▶ may have zeros in 0 or at 1/-1
- ▶ **Notch filters**
  - ▶ have zeros exactly on unit circle
  - ▶ will completely reject certain frequencies
  - ▶ has additional poles to make the rejection band very narrow
- ▶ **Comb filters**
  - ▶ = periodic notch filters

- ▶ **Oscillator** = a system which produces an output signal even in absence of input
- ▶ Has a pair of complex conjugate poles **exactly on unit circle**
- ▶ Example at blackboard

- ▶ Sometimes is necessary to **undo** a filtering
  - ▶ e.g. undo attenuation of a signal passed through a channel
- ▶ Inverse filter: has inverse system function:

$$H_I(z) = \frac{1}{H(z)}$$

- ▶ Problem: if  $H(z)$  has zeros outside unit circle,  $H_I(z)$  has poles outside unit circle  $\rightarrow$  unstable
- ▶ Examples at blackboard