

Solutions to Sec 3.2 Pre-lab Questions

The mark of each question is 1

1. **A-3** Based on the steady-state error result of a step response from Equation ,what *type* of system is the SRV02 when performing speed control (Type 0, 1, or 2) and why?

Answer 3.2.1

Outcome Solution

A-3 This is a *Type 0* system because the steady-state error is a constant given a step reference.

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2. **A-2** The nominal SRV02 model parameters, K and τ , found in SRV02 Modeling Laboratory (Section 1) should be about 1.53 (rad/s-V) and 0.0254 sec, respectively. Calculate the PI control gains needed to satisfy the time-domain response requirements.

Answer 3.2.2

Outcome Solution

A-2 Using the nominal SRV02 model parameters

$$K = 1.53 \text{ rad/(V.s)} \quad (\text{Ans.3.2.1})$$

and

$$\tau = 0.0254 \text{ s} \quad (\text{Ans.3.2.2})$$

along with the damping ratio given in Equation 3.1.20 with Equation 3.1.25 generates the proportional control gain

$$k_p = 1.34 \text{ V/(rad/s)} \quad (\text{Ans.3.2.3})$$

The integral control gain is obtained by substituting the model parameters given above with the minimum natural frequency specification given in 3.1.21 into Equation 3.1.26

$$k_i = 124.9 \text{ V/rad} \quad (\text{Ans.3.2.4})$$

Thus, if these gains are used, the speed response of the load gear on an SRV02 with a disc load will satisfy the specifications listed in Section 3.1.1.1.

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3. **A-2** Find the frequency response magnitude, $|P_i(\omega)|$, of the transfer function $P_i(s)$ given in Equation 3.1.27.

Answer 3.2.3

Outcome Solution

A-2 The frequency response of $P_i(s)$ is found by substituting $s = j\omega$ in 3.1.27.

$$P_i(j\omega) = \frac{K}{(\tau j\omega + 1) j\omega} \quad (\text{Ans.3.2.5})$$

Taking the magnitude of this expression gives the frequency response gain

$$|P_i(\omega)| = \frac{K}{\omega \sqrt{\tau^2 \omega^2 + 1}} \quad (\text{Ans.3.2.6})$$

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4. **A-2** Calculate the DC gain of $P_i(s)$ given in Equation 3.1.27. **Hint:** The DC gain is the gain when the frequency is zero, i.e. $\omega = 0 \text{ rad/s}$. However, because of its integrator, $P_i(s)$ has a singularity at zero frequency. Therefore, the DC gain is not technically defined for this system. Instead, approximate the DC gain by using $\omega = 1 \text{ rad/s}$. Make sure the DC gain estimate is evaluated numerically in dB using the nominal model parameters, $K = 1.53$ and $\tau = 0.0254$, (or use what you found for K and τ in Section 1).

Answer 3.2.4

Outcome Solution

A-2 Substituting $\omega = 1 \text{ rad/s}$ gives the approximate DC gain of

$$|P_i(1)| = \frac{K}{\sqrt{\tau^2 + 1}} \quad (\text{Ans.3.2.7})$$

Substituting the nominal SRV02 model parameters in the above expression results in the DC gain estimate of

$$|P_i(1)| = 1.53 \quad (\text{Ans.3.2.8})$$

or

$$|P_i(1)|_{dB} = 3.70 \text{ dB} \quad (\text{Ans.3.2.9})$$

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5. **A-1, A-2** The gain crossover frequency, ω_g , is the frequency at which the gain of the system is 1 or 0 dB. Express the crossover frequency symbolically in terms of the SRV02 model parameters K and τ . Then, evaluate the expression using the nominal SRV02 model parameters $K = 1.53$ and $\tau = 0.0254$, (or use what you found for K and τ in Section 1).

Answer 3.2.5

Outcome Solution

A-1 The crossover frequency is found by setting $|P_i(\omega_g)| = 1$ in equation Ans.3.2.6 and solving for ω_g

A-2

$$\omega_g = \frac{\sqrt{2} \sqrt{\frac{-1 + \sqrt{1 + 4\tau^2 K^2}}{\tau^2}}}{2} \quad (\text{Ans.3.2.10})$$

When evaluated with the nominal SRV02 parameters, the frequency where the gain is 0 dB is

$$\omega_g = 1.524 \text{ rad/s} \quad (\text{Ans.3.2.11})$$

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