

Sigma-Point Kalman Filter based Integrated Navigation Systems (Overview)

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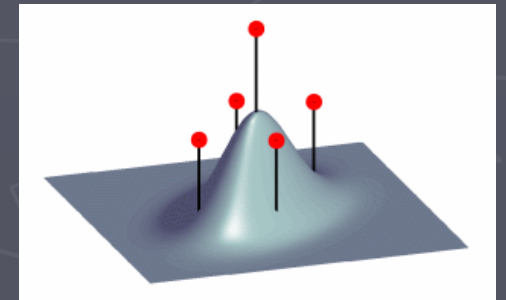


SPKF Integrated Navigation

- ▶ Integration of IMU, GPS, and additional sensors (e.g., altimeter) to provide accurate vehicle state estimation.
 - States (position, attitude, velocity, etc.) used for feedback control, fault detection, tracking, trajectory planning, etc.
- ▶ Core to all current Integrated Navigation systems is the Extended Kalman Filter (EKF).
- ▶ New Sigma-Point Kalman Filter (SPKF) is theoretically superior to the EKF
- ▶ Software Solution
- ▶ Provides significant performance/cost benefits.
- ▶ Applicable to Manned or Unmanned vehicles.
- ▶ Patent Pending

Sigma Point Kalman Filtering

- ▶ New approach to nonlinear recursive Bayesian Inference.
- ▶ Consistently outperform the Extended Kalman Filter (EKF).
- ▶ Same order computational complexity as the EKF.
- ▶ Accurate to at least the 2nd order (3rd for Gaussian inputs).
- ▶ Efficient “sampling” approach using only functional evaluations (no analytic derivatives).
- ▶ *See separate presentation or references for details.*



SPKF Integrated Navigation Solution

► Kinematic System Model

- 16 state 6DOF model of vehicle dynamics used for state estimation
 - 3D position and velocity (inertial frame : North, East, Down)
 - 4D attitude (body frame : quaternion representation)
 - IMU gyro rate and linear acceleration biases (6D)
- IMU used to capture and summarize forces and moments operating on vehicle
 - "Vehicle Independent"
- Accounts for coordinate transformation between body and inertial frames.
- Accounts for sensor coupling due to geometry (e.g., GPS offset from center of gravity)

► Sensor updates

- GPS - Measures lagged position and velocity in inertial frame
- Altimeter - Barometric measurement of absolute altitude
- Nonlinear function of the system state.
- Used for discrete measurement update (prediction correction)

► Efficient SPKF implementation

- Provides accurate state estimates accounting for nonlinearities, asynchronous, and lagged measurement update.

Details: Kinematic Model

- State :

$$\mathbf{x} = [\mathbf{p} \ \mathbf{v} \ \mathbf{e} \ \mathbf{b}_\omega \ \mathbf{b}_a]^T = [x_N \ x_E \ x_D \ v_N \ v_E \ v_D \ e_0 \ e_1 \ e_2 \ e_3 \ b_p \ b_q \ b_r \ b_{ax} \ b_{ay} \ b_{az}]^T$$

- IMU data first corrected using estimated biases:

$$\bar{\boldsymbol{\omega}} = \boldsymbol{\omega} - \mathbf{b}_\omega = [\bar{p} \ \bar{q} \ \bar{r}]^T = [p \ q \ r]^T - [b_p \ b_q \ b_r]^T$$

$$\bar{\mathbf{a}} = \mathbf{a} - \mathbf{b}_a = [\bar{a}_x \ \bar{a}_y \ \bar{a}_z]^T = [a_x \ a_y \ a_z]^T - [b_{ax} \ b_{ay} \ b_{az}]^T$$

- Time-update of state at IMU rate using nonlinear "kinematic" function

$$\dot{\mathbf{x}} = \mathbf{f}(\mathbf{x}_k, \bar{\boldsymbol{\omega}}_k, \bar{\mathbf{a}}_k) \left\{ \begin{array}{l} \dot{\mathbf{p}} = \mathbf{v} \\ \dot{\mathbf{v}} = \mathbf{T}^{b \rightarrow i} \left(\bar{\mathbf{a}} - \dot{\bar{\boldsymbol{\omega}}} \times \mathbf{r}_{IMU} - \bar{\boldsymbol{\omega}} \times (\bar{\boldsymbol{\omega}} \times \mathbf{r}_{IMU}) \right) + [0 \ 0 \ g]^T \\ \dot{\mathbf{e}} = -\frac{1}{2} \tilde{\boldsymbol{\Omega}} + l \left(1 - \|\mathbf{e}\|^2 \right) \mathbf{e} \\ \dot{\mathbf{b}}_\omega = 0 \\ \dot{\mathbf{b}}_a = 0 \end{array} \right.$$

IMU offset from CG

Lagrange multiplier

Details: Kinematic Model

- Body-to-inertial frame transformation (DCM) matrix:

$$\mathbf{T}^{b \rightarrow i} = \left(\mathbf{T}^{i \rightarrow 2} \right)^T = \frac{1}{2} \begin{bmatrix} 1 - 2(e_2^2 + e_3^2) & 2(e_1 e_2 + e_0 e_3) & 2(e_1 e_3 + e_0 e_2) \\ 2(e_1 e_2 + e_0 e_3) & 1 - 2(e_1^2 + e_3^2) & 2(e_2 e_3 + e_0 e_1) \\ 2(e_1 e_3 + e_0 e_2) & 2(e_2 e_3 + e_0 e_1) & 1 - 2(e_1^2 + e_2^2) \end{bmatrix}$$

- Quaternion update matrix:

$$\tilde{\mathbf{\Omega}} = \begin{bmatrix} 0 & \bar{p} & \bar{q} & \bar{r} \\ -\bar{p} & 0 & -\bar{r} & \bar{q} \\ -\bar{q} & \bar{r} & 0 & -\bar{p} \\ -\bar{r} & -\bar{q} & \bar{p} & 0 \end{bmatrix}$$

- Euler solution:

$$\mathbf{p}_{k+1} = \mathbf{p}_{k+1} + \dot{\mathbf{p}}_k \cdot dt$$

$$\mathbf{v}_{k+1} = \mathbf{v}_{k+1} + \dot{\mathbf{v}}_k \cdot dt$$

$$\mathbf{e}_{k+1} = \exp\left(-\frac{1}{2} \tilde{\mathbf{\Omega}} \cdot dt\right) \mathbf{e}_k = \left[\mathbf{I} \left(\cos(s) + l \cdot \left(1 - \|\mathbf{e}\|^2 \right) \cdot dt \right) - \frac{1}{2} \tilde{\mathbf{\Omega}} \cdot dt \cdot \frac{\sin(s)}{s} \right] \mathbf{e}_k$$

$$s = \frac{1}{2} \sqrt{(\bar{p}_k \cdot dt)^2 + (\bar{q}_k \cdot dt)^2 + (\bar{r}_k \cdot dt)^2}$$

Details: Kinematic Model

- ▶ Kinematic process model comments
 - IMU data first corrected using estimated biases.
 - Time-update of state at IMU rate using nonlinear “kinematic” function
 - ▶ Accounts for sensor coupling due to geometry (e.g., GPS offset from center of gravity)
 - ▶ Quaternion updated with exact nonlinear solution
 - ▶ Accounts for coordinate transformation between body and inertial frames.
- ▶ Sensor observations (GPS, Altimeter)
 - Nonlinear function of the system state.
 - Nonlinear effect modeled: sensor latency, quantization.
 - Used for discrete measurement update (prediction correction)

Details: Observation Model - GPS

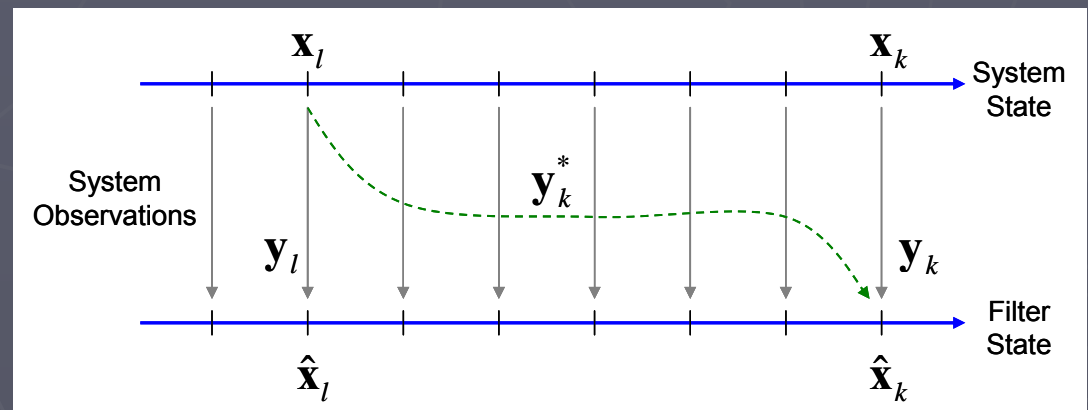
- Measure lagged position and velocity in inertial frame

$$\mathbf{p}_k^* = \mathbf{p}_l + \mathbf{T}_l^{b \rightarrow i} \cdot \mathbf{r}_{GPS} + \mathbf{n}_{p_l}$$

$$\mathbf{v}_k^* = \mathbf{v}_l + \mathbf{T}_l^{b \rightarrow i} \cdot \bar{\boldsymbol{\omega}}_l \times \mathbf{r}_{GPS} + \mathbf{n}_{v_l}$$

$$l = k - N_{lat}$$

$$N_{lat} = \{ \text{GPS latency} \} / dt$$



- Practical issues that were addressed:
 - antenna not at CG
 - measurement latency \rightarrow current reading corresponds with vehicle state in the past. Complicates measurement updates.
 - SPKF formulation allows for an elegant way to deal with latencies.

Details: Observation Model - Altimeter

- Barometric measurement of absolute altitude.

$$z_k^{ALT} = -(1/\gamma) \log \left(\rho_{quant} \text{floor} \left((\rho_0 \exp(\gamma z_k) + n_k^{ALT}) / \rho_{quant} \right) / \rho_0 \right)$$

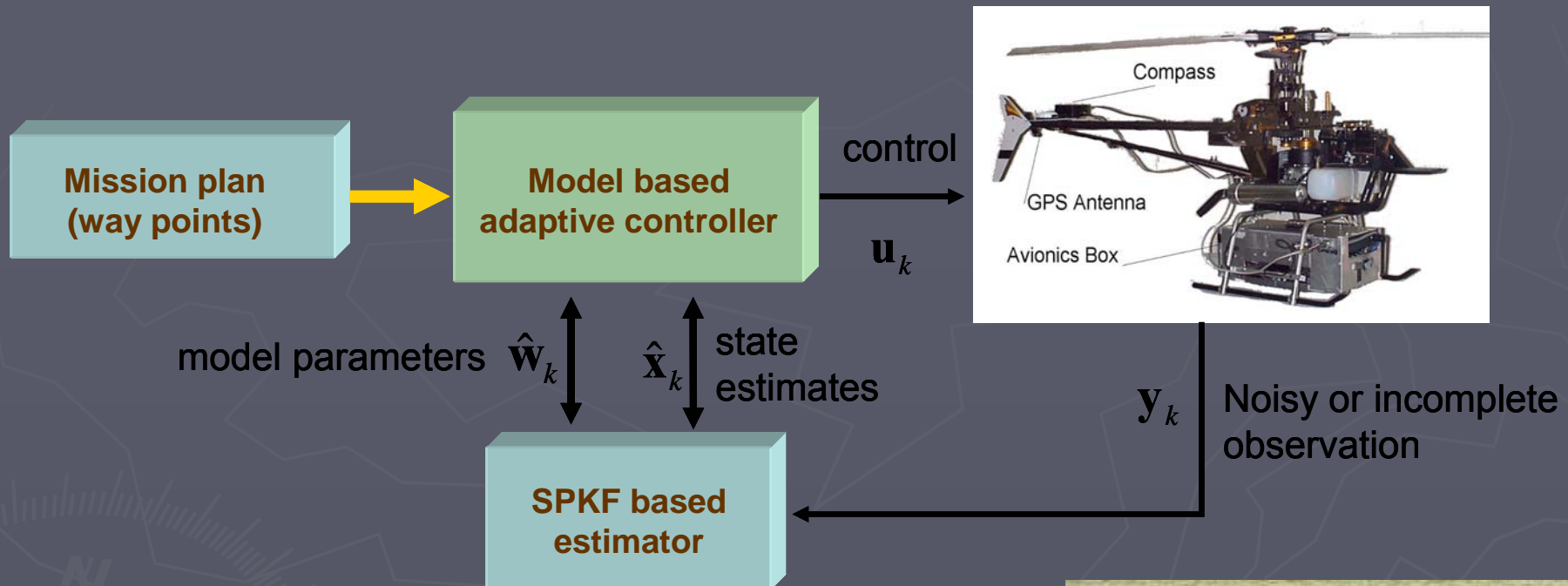
γ : atmospheric pressure decay rate

ρ_0 : sea level pressure ρ_{quant} : quantization pressure

- Issues:

- Nonlinear due to quantization effects : makes SPKF use attractive
- Low resolution
- Inaccurate close to ground due to rotor-downwash
- Can be affected by atmospheric conditions
- Ideally combined with other relative altitude sensors such as sonar, radar or lidar.

Test Platform: X-Cell-90 Helicopter



► Complete avionics suite

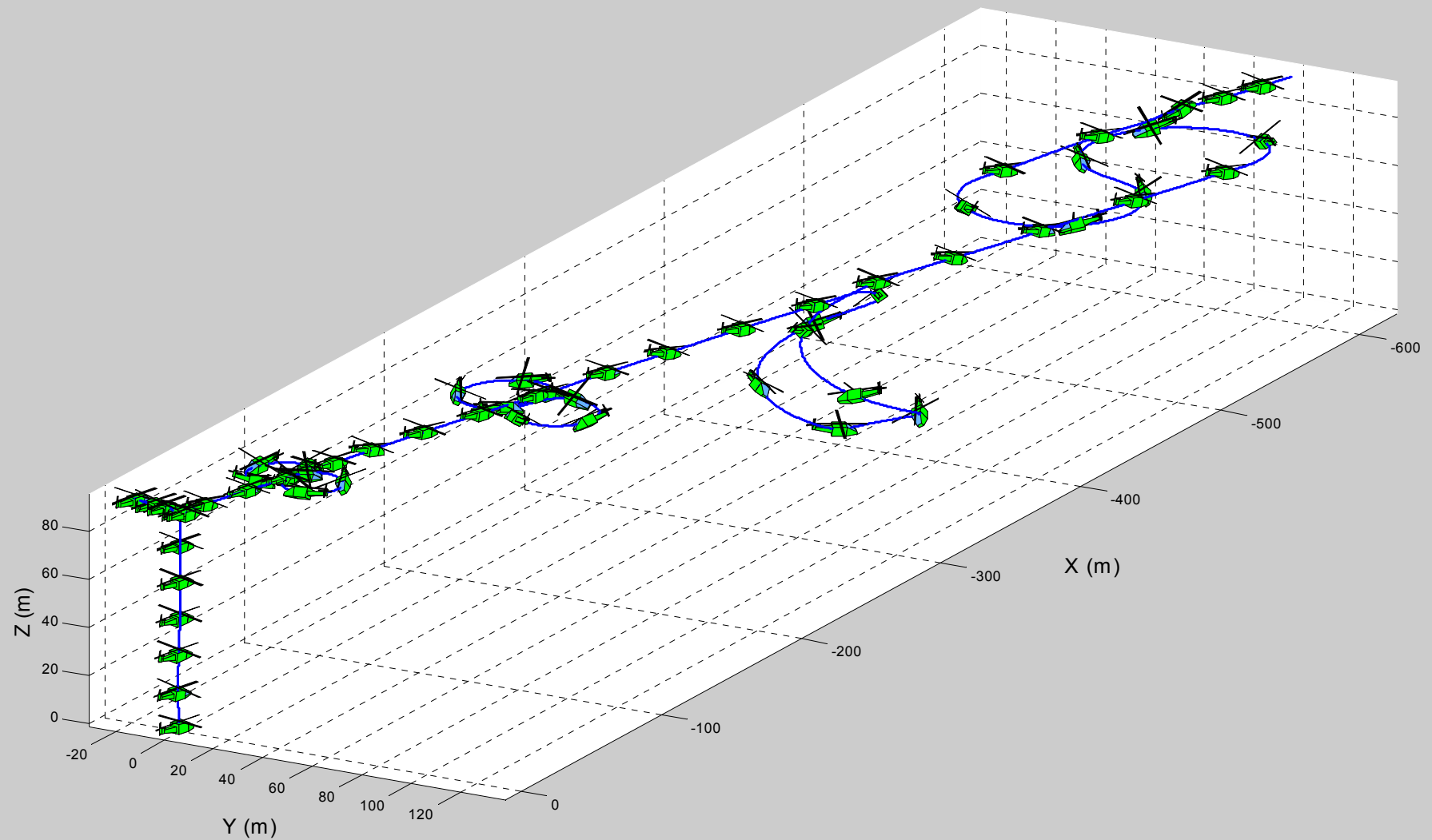
- Flight computer (300MHz DSP400), IMU, GPS, Barometric altimeter, Three-Axis Magnetic compass, Wireless Ethernet link, Flash memory, Custom servo board, R/C transmitter, Hardware-in-the loop system for testing.

► MIT-Draper X-Cell-90 Dynamic Model

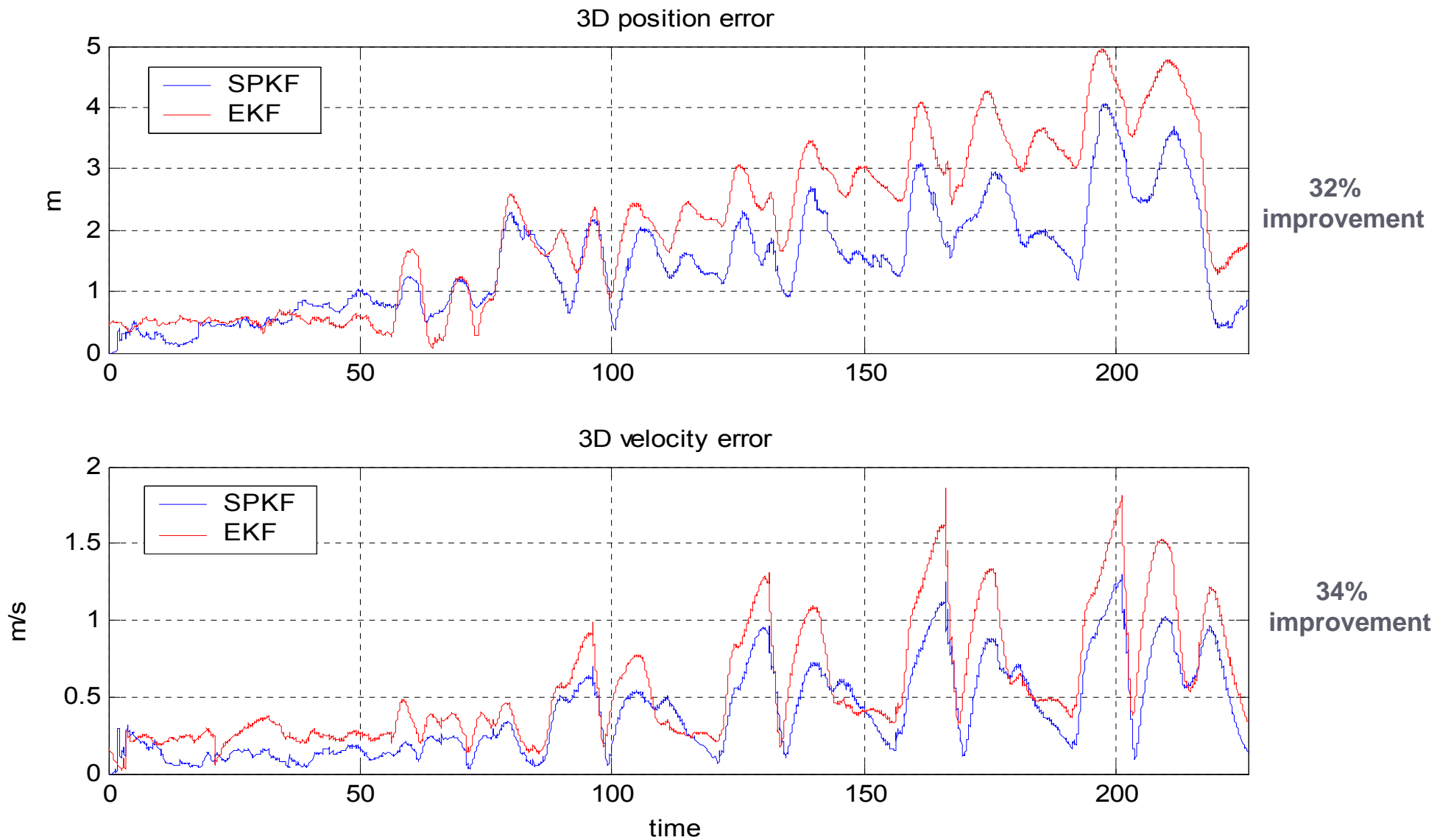
- High fidelity quaternion based nonlinear model
- 26 states and ~70 parameters (rotor forces, torque, and thrust, flapping dynamics, horizontal stabilizer and vertical tail forces and moments, fuselage drag, and actuator states)



State Estimation Experiment: Test Trajectory

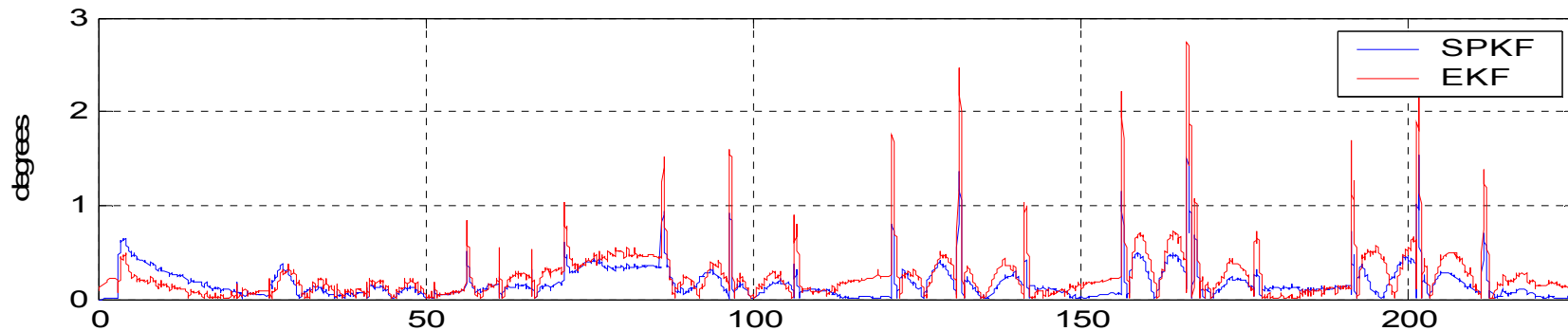


State Estimation Experimental Results (Position & Velocity)



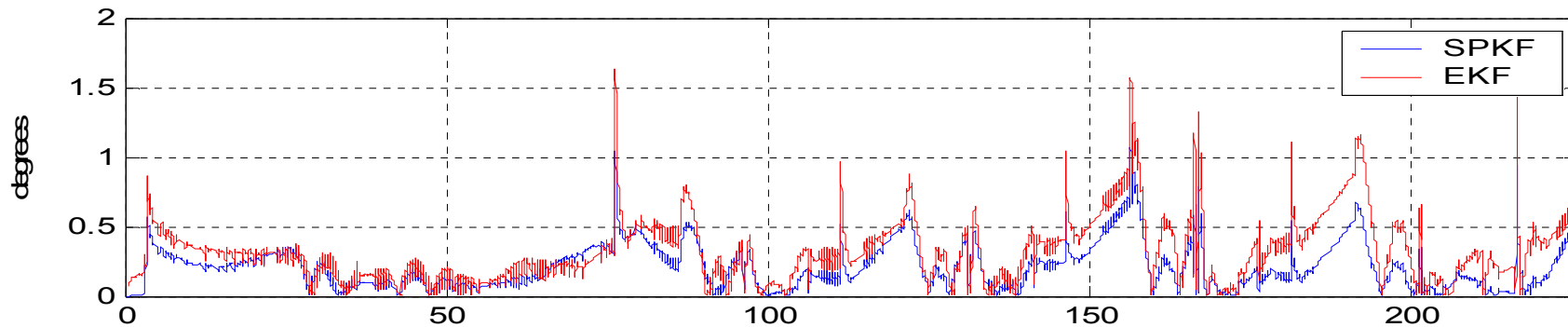
State Estimation Experimental Results (Euler Angles)

Absolute Pitch Angle Error



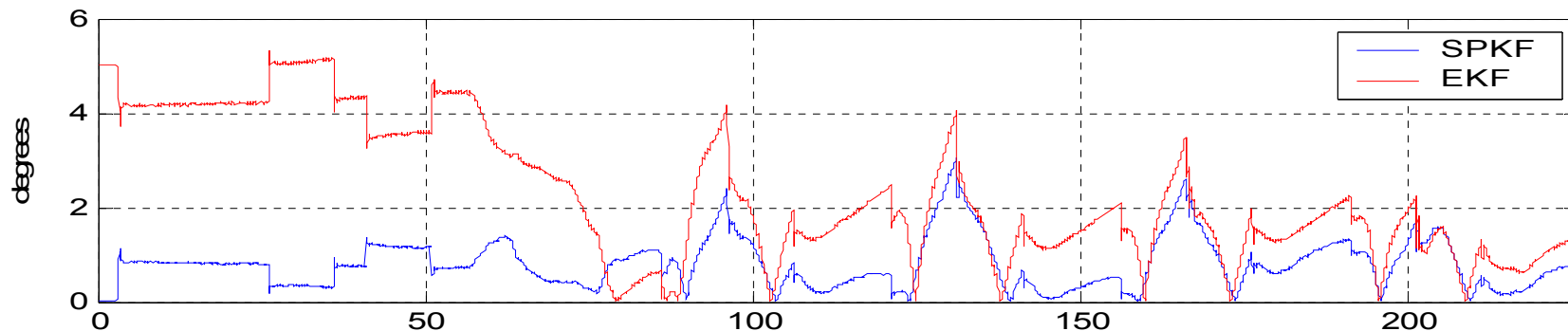
**34%
improvement**

Absolute Roll Angle Error



**32%
improvement**

Absolute Yaw Angle Errors



**65%
improvement**

time

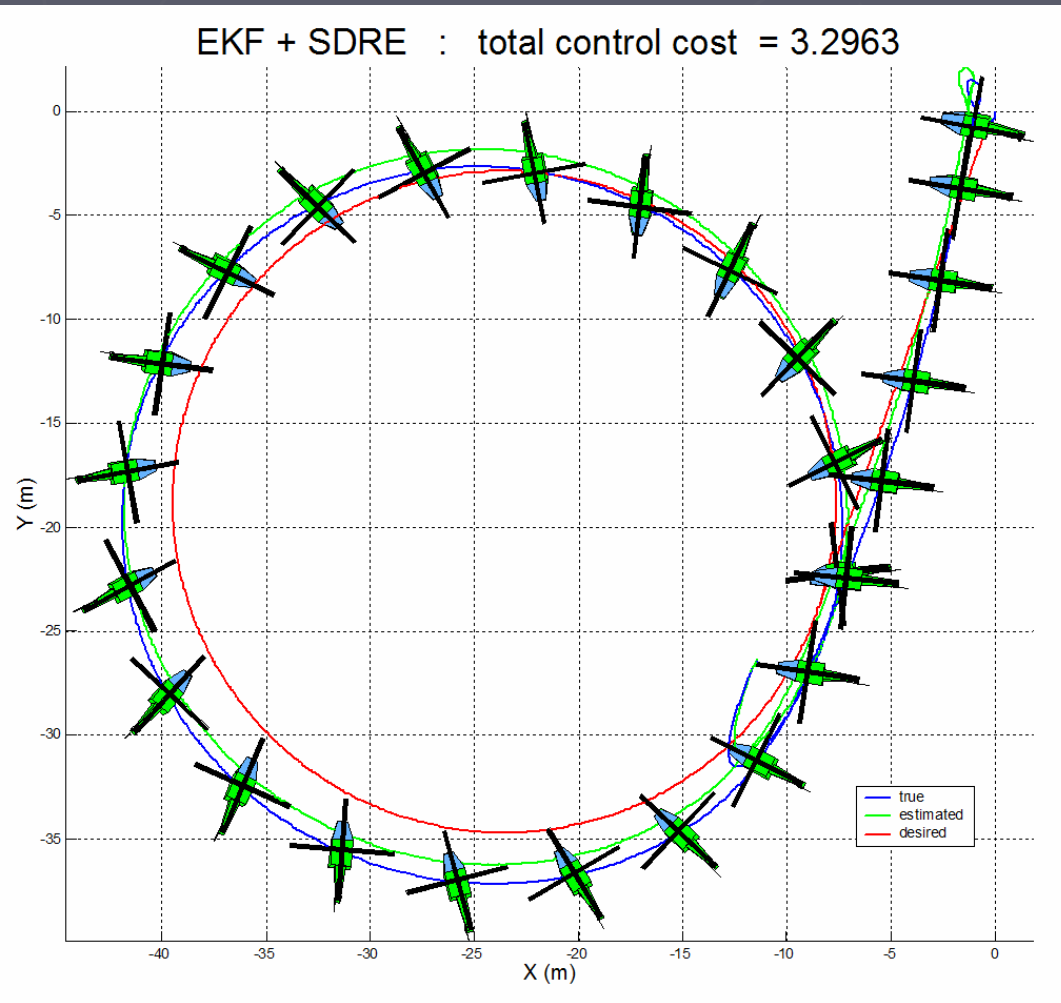
Performance Summary

► EKF vs. SPKF with and without GPS Latency Compensation

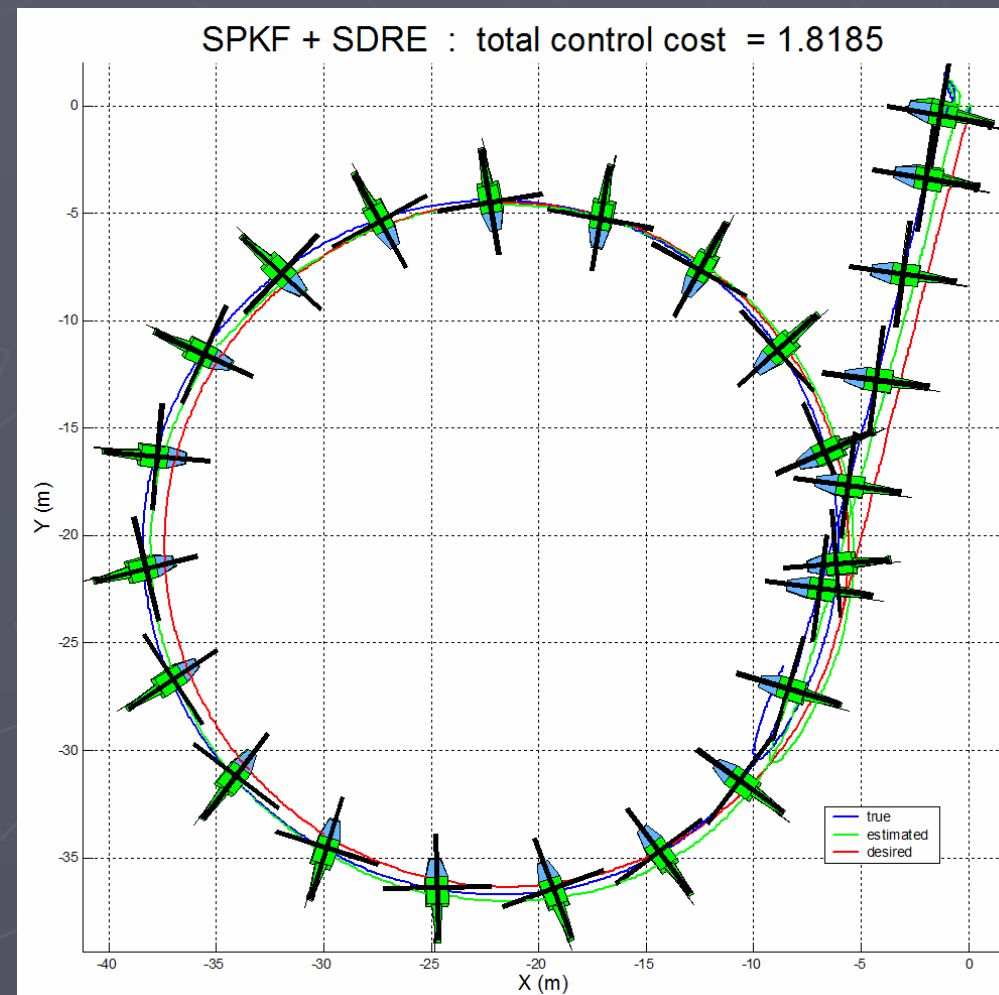
Algorithm	Average RMS Error				
	position (m)	velocity (m/s)	Euler angles (degrees)		
			roll	pitch	yaw
EKF	2.1	0.57	0.25	0.32	2.29
SPKF - without LC	1.9 (10%)	0.52 (9%)	0.20 (20%)	0.26 (19%)	1.03 (55%)
SPKF - with LC	1.4 (32%)	0.38 (34%)	0.17 (32%)	0.21 (34%)	0.80 (65%)

Closed Loop State Estimation & Control

- Use of SPKF estimator reduces control cost by 45%

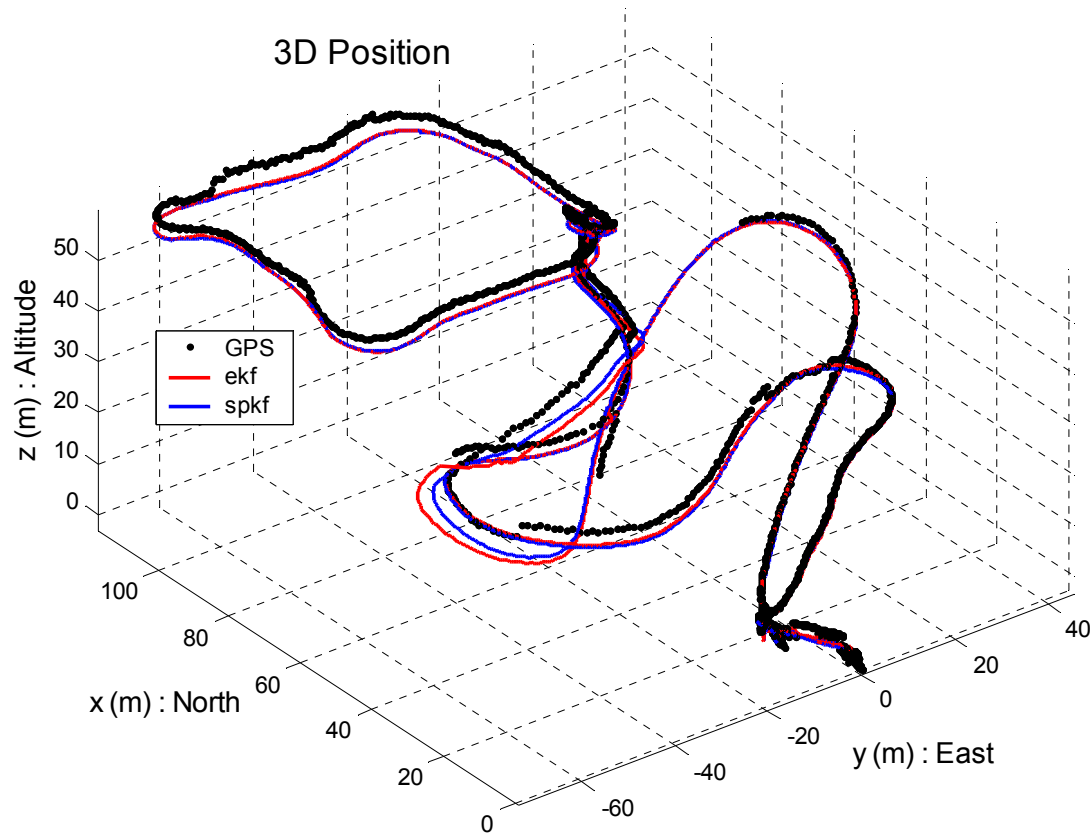


EKF
Control cost : 3.30

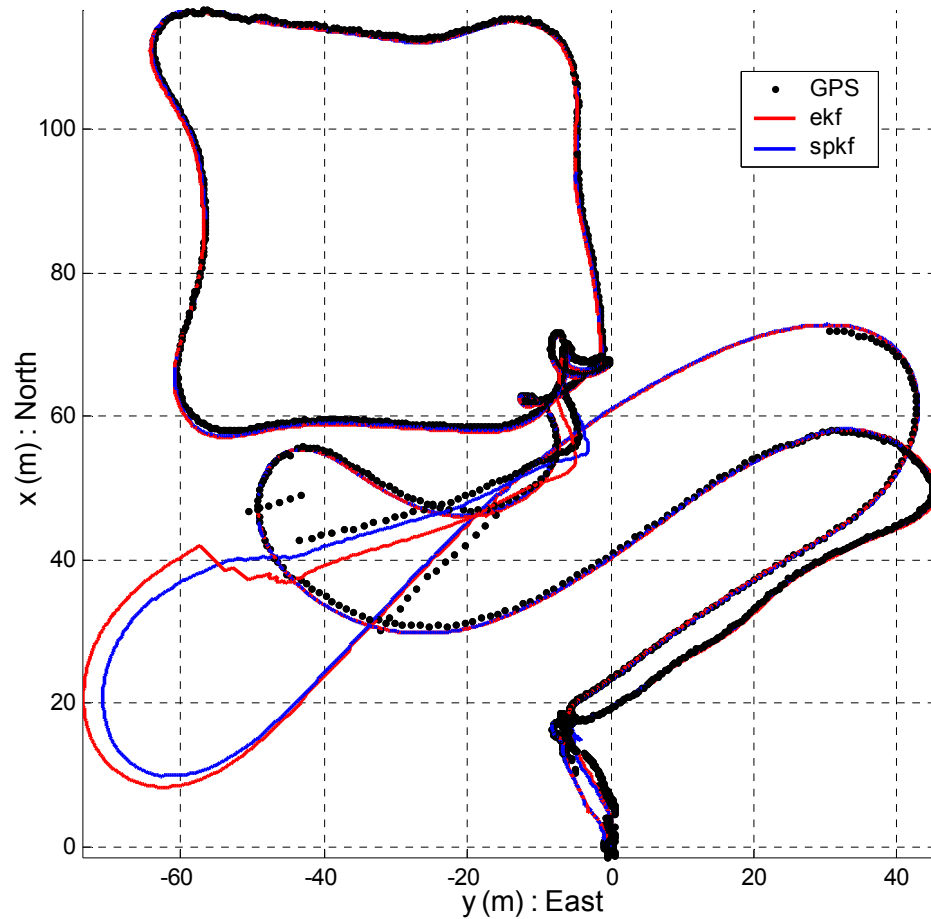


SPKF
Control cost : 1.82

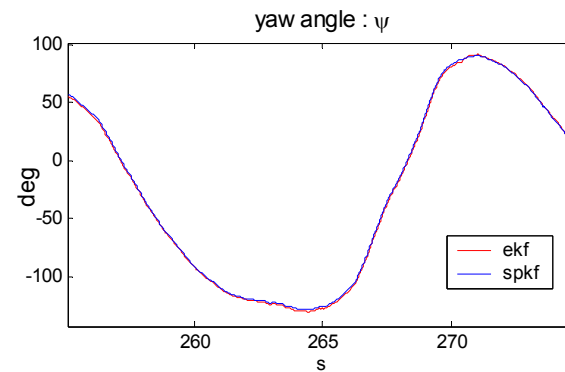
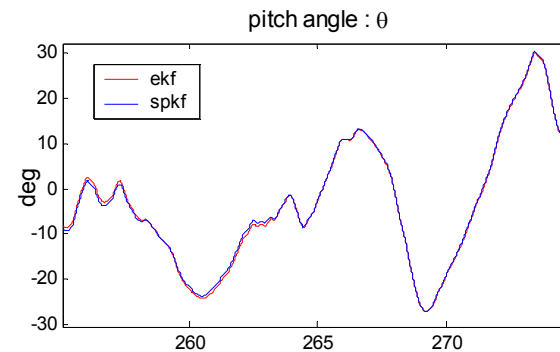
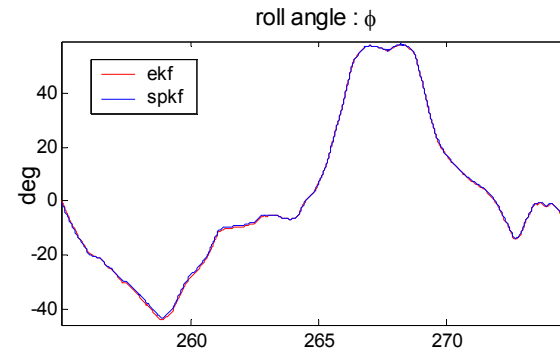
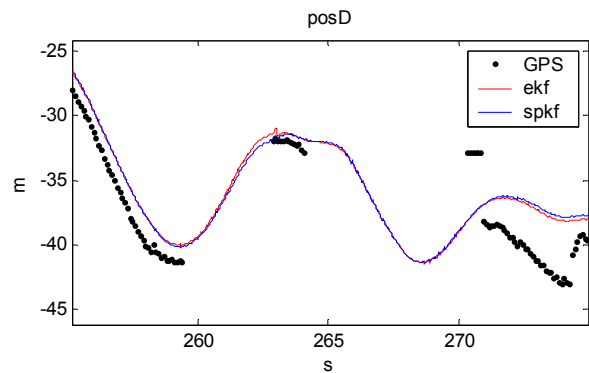
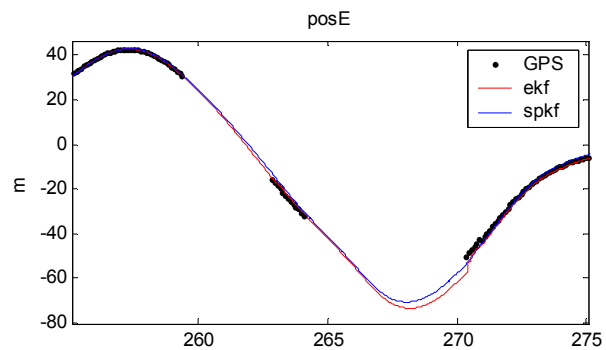
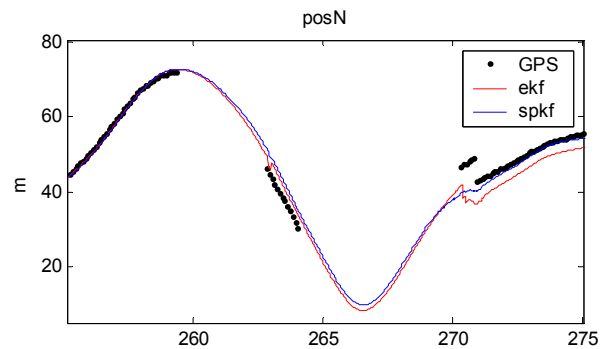
Results on Actual Flight Data



Results on Actual Flight Data



Results on Actual Flight Data

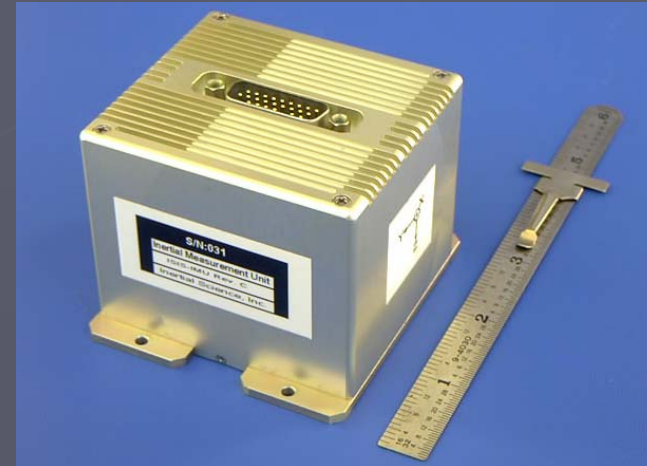


SPKF Cost Savings



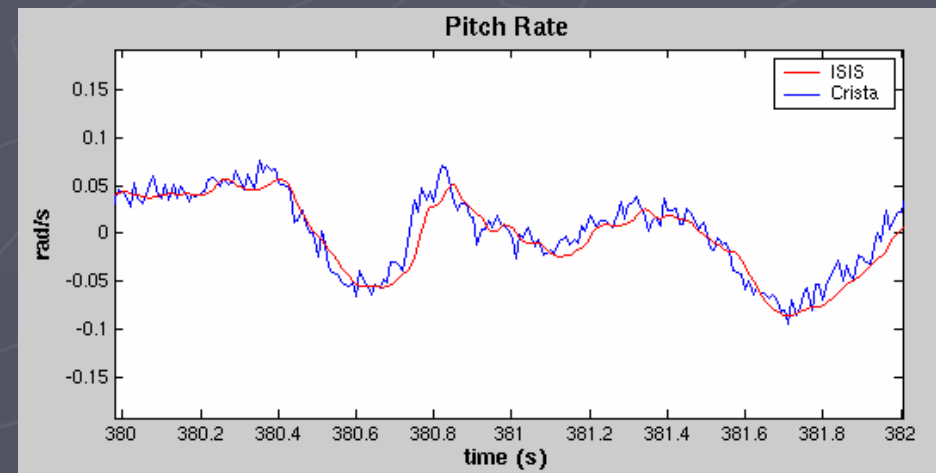
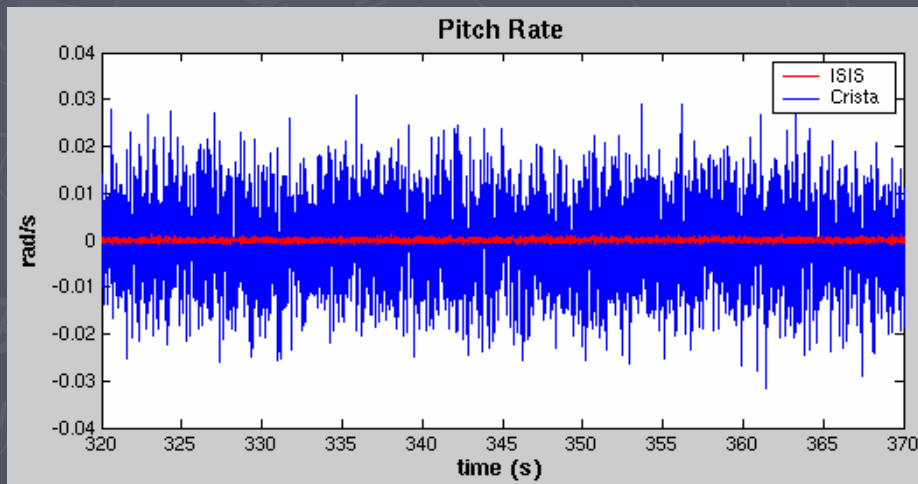
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Cloud Cap Crista IMU
.35" x 1.50" x 0.80, 19 grams
< \$2k

Inertial Sciences ISIS-IMU
3.30" x 2.5 " x 1.83 , 250 grams
> \$10k

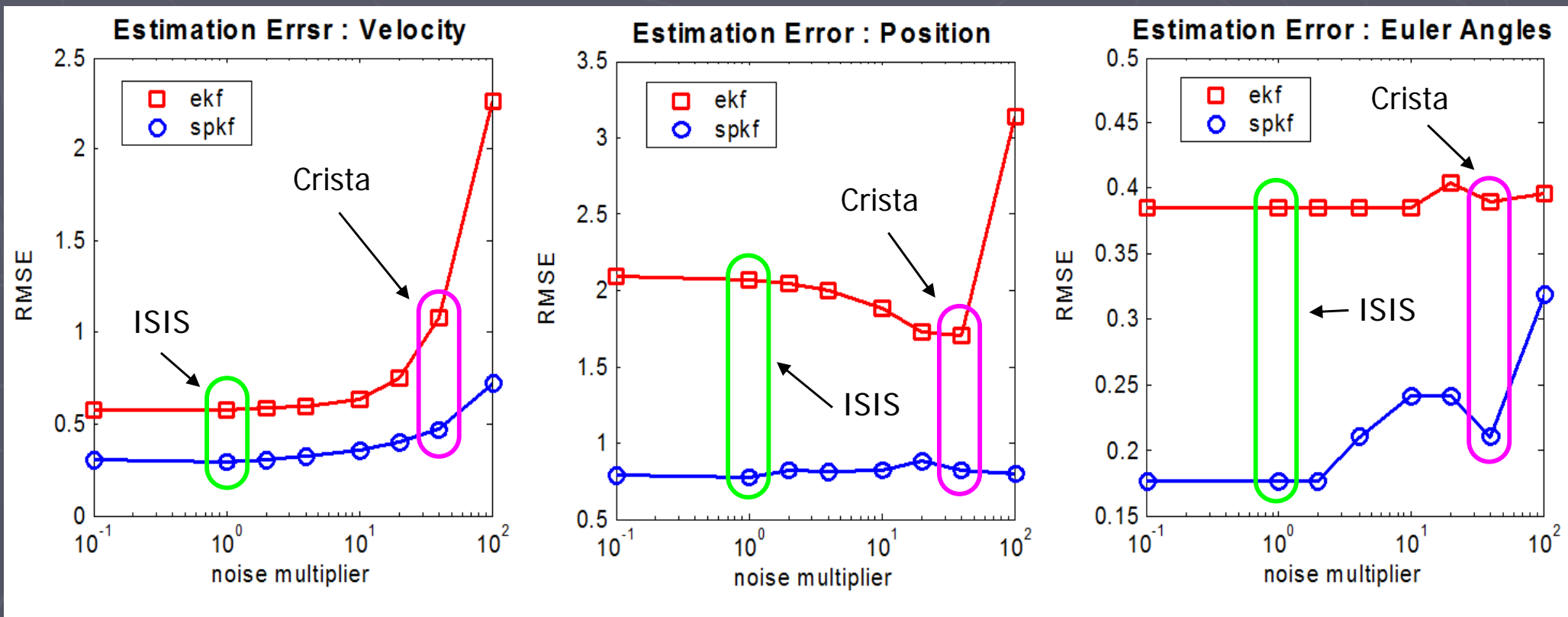


Noise floor std: (gyros=30x, accel=10x)

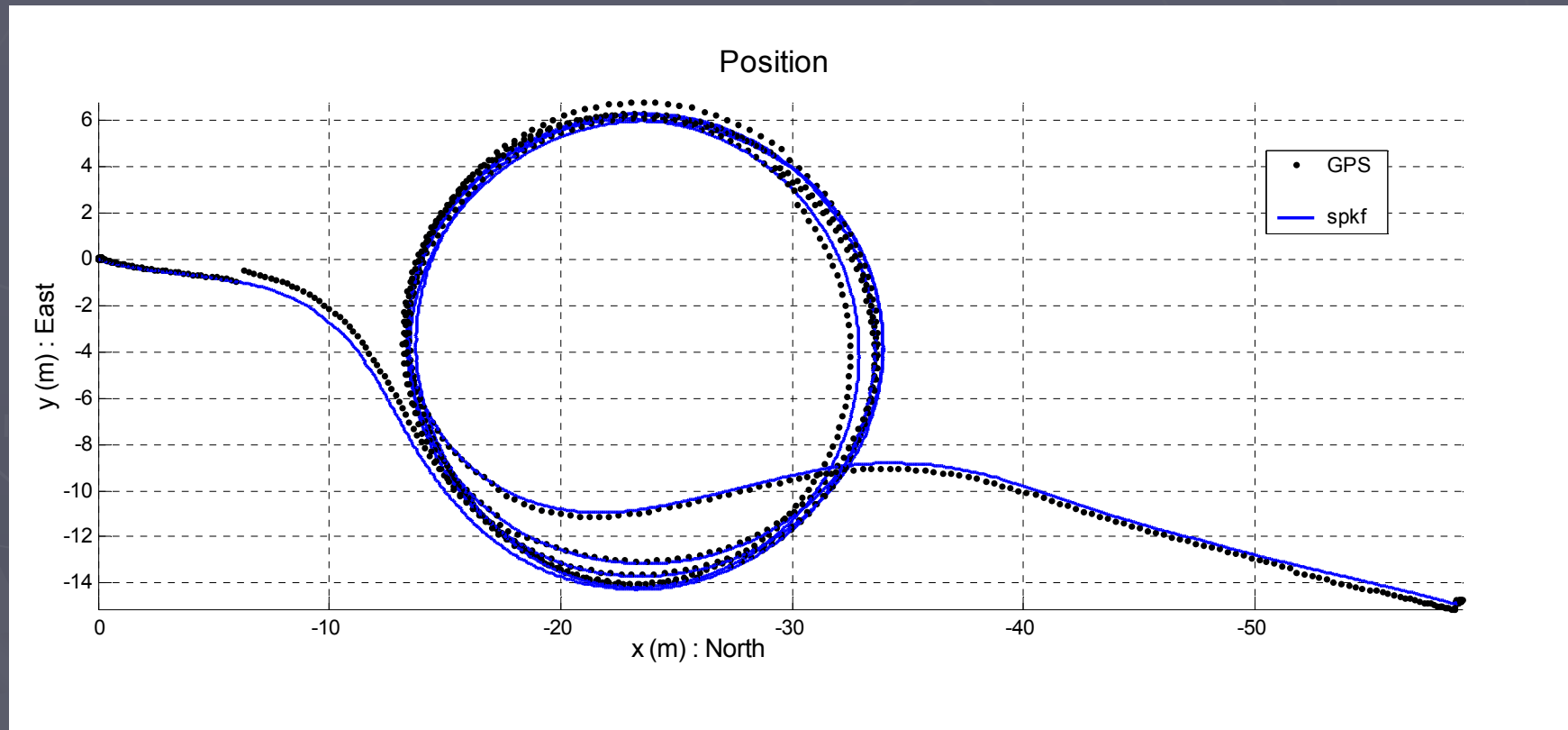
Signal Dynamics

ISIS vs. Crista IMU: Estimation Performance

- Simulation Results (worst case : 40x difference in noise level std.)

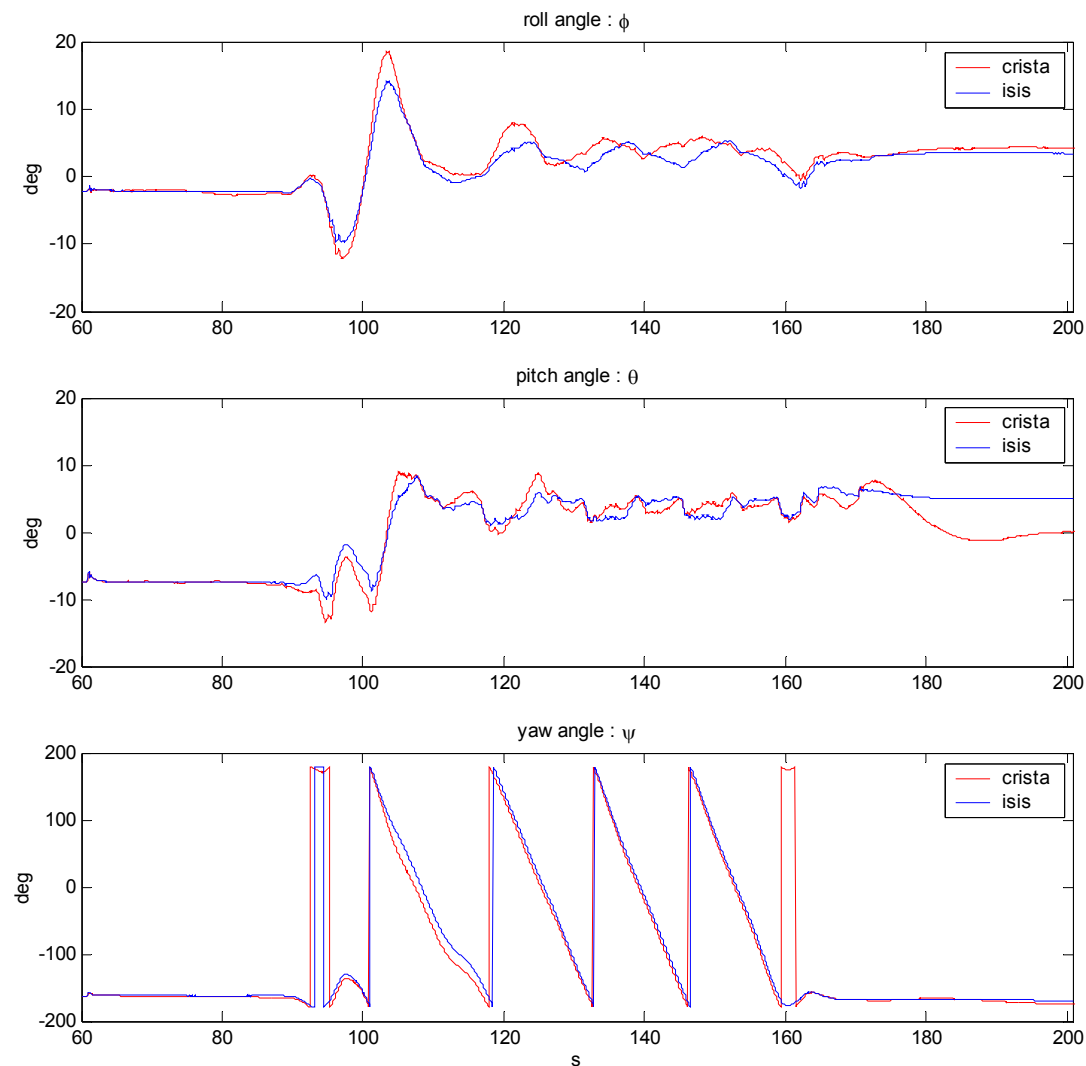


ISIS vs. Crista – Real Data Experiments



2-d position (driving in a car)

ISIS vs. Crista – Real Data Experiments



Attitude estimates

Summary

- ▶ Improved integrated navigation solution.
- ▶ Superior performance over traditional EKF based systems
 - More accurately accounts for nonlinearities.
 - Exact modeling of asynchronous and lagged sensor updates.
 - Computational load is equivalent to EKF.
- ▶ Vehicle Independent: Easily ported to other UAVs, UGVs, UUVs, etc.
- ▶ Cost Savings: Can use less expensive/less accurate sensors.

Extensions/Enhancements

- ▶ Equation Error Formulation
- ▶ IMU Noise Modeling
- ▶ Adaptive noise covariance estimation
- ▶ System initialization and calibration
- ▶ Other Sensors:
 - Compass, sonar, radar, laser, lidar, video, etc.
- ▶ Tightly-coupled GPS integration
 - Integrate individual satellite signals using SPKF.
- ▶ Distributed and Multiple IMU/GPS integration

Extras



SPKF Based Latency Compensation

- Combine current prediction of state with lagged innovation

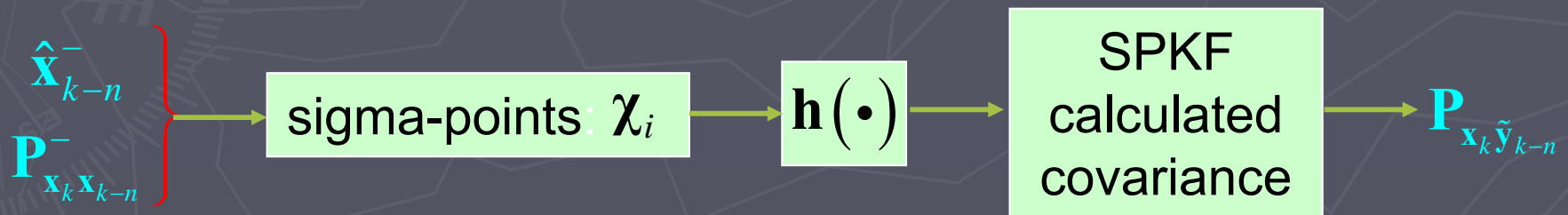
$$\hat{\mathbf{x}}_k = \hat{\mathbf{x}}_k^- + \mathbf{\kappa}_k \tilde{\mathbf{y}}_{k-n} \quad \mathbf{\kappa}_k = \mathbf{P}_{\mathbf{x}_k \tilde{\mathbf{y}}_{k-n}} \left(\mathbf{P}_{\tilde{\mathbf{y}}_{k-n}} \right)^{-1} \quad n = N_{lat}$$

- Key insight: Maintain lagged state and covariance:

$$\hat{\mathbf{x}}_{k-n}^-$$

$$\mathbf{P}_{\mathbf{x}_k \mathbf{x}_{k-n}}^- = E \left[\left(\mathbf{x}_k - \hat{\mathbf{x}}_k^- \right) \left(\mathbf{x}_{k-n} - \hat{\mathbf{x}}_{k-n}^- \right)^T \right]$$

- *Sigma-point approach* implicitly calculates: $\mathbf{P}_{\mathbf{x}_k \tilde{\mathbf{y}}_{k-n}}$



SPKF Based Latency Compensation

- Augment state and redefine process & observation model

$$\mathbf{x}_k^a = \begin{bmatrix} \mathbf{x}_k \\ \mathbf{x}_l \end{bmatrix} \quad \mathbf{x}_{k+1}^a = \begin{bmatrix} \mathbf{f}(\mathbf{x}_k) \\ \mathbf{x}_l \end{bmatrix} \quad \mathbf{y}_k = \tilde{\mathbf{h}}(\mathbf{x}_k^a) = \begin{cases} \mathbf{h}_1(\mathbf{x}_k) & k \neq l + N_{lat} \\ \mathbf{h}_2(\mathbf{x}_l) & k \neq l + N_{lat} \end{cases}$$

- When lagged sensor measurement arrives at $k = l + N_{lat}$

- Result of time-update:

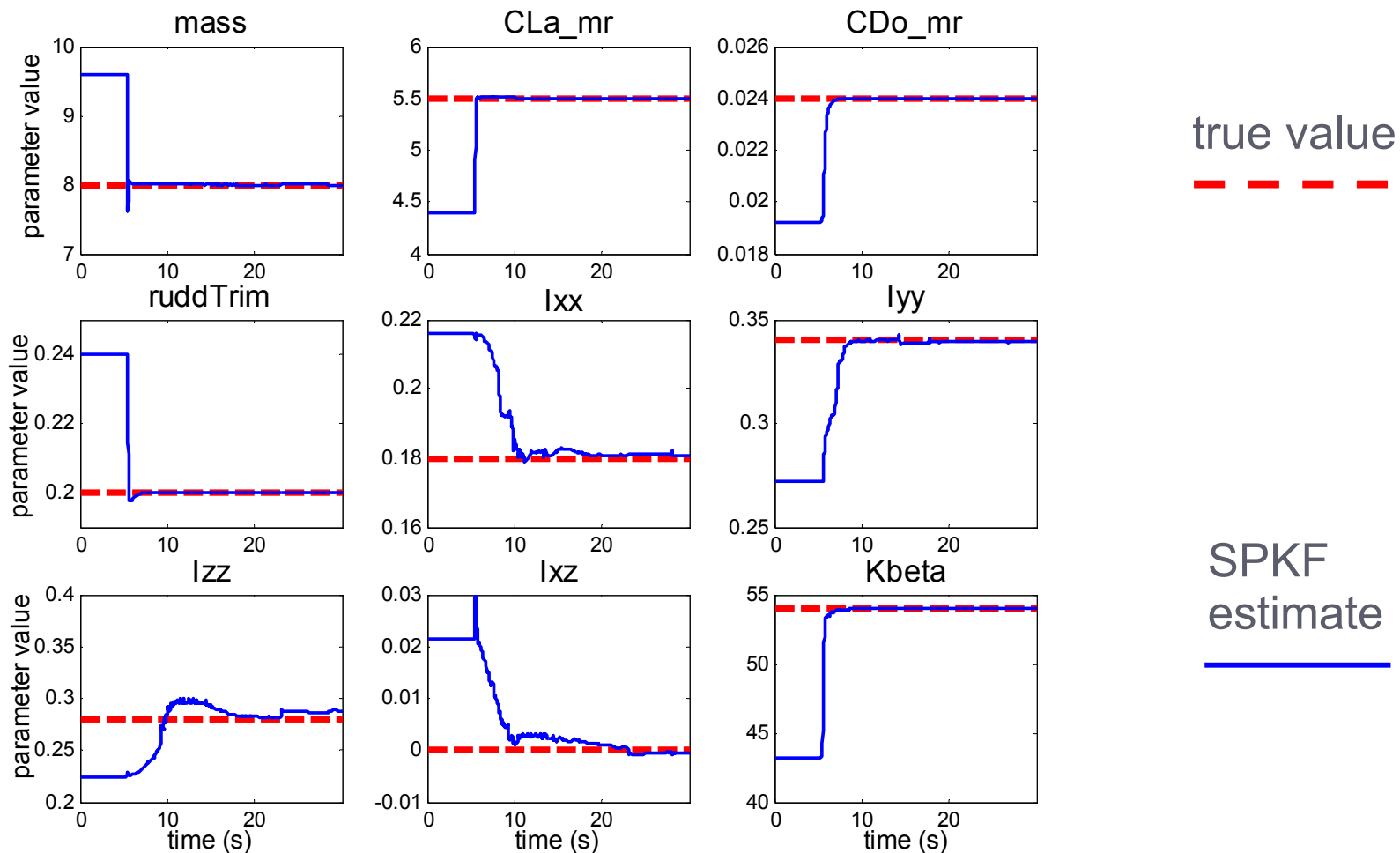
$$\hat{\mathbf{x}}_k^{a-} = \begin{bmatrix} \hat{\mathbf{x}}_k^- \\ \hat{\mathbf{x}}_l^* \end{bmatrix} \quad \mathbf{P}_{\mathbf{x}_k^a}^- = \begin{bmatrix} \mathbf{P}_{\mathbf{x}_k \mathbf{x}_k}^- & \mathbf{P}_{\mathbf{x}_k \mathbf{x}_l}^- \\ \mathbf{P}_{\mathbf{x}_l \mathbf{x}_k}^- & \mathbf{P}_{\mathbf{x}_l \mathbf{x}_l}^- \end{bmatrix} \quad l = k - N_{lat}$$

- Measurement update (Kalman gain):

$$\mathbf{P}_{\mathbf{x}_k^a \tilde{\mathbf{y}}_l} = \begin{bmatrix} \mathbf{P}_{\mathbf{x}_k \tilde{\mathbf{y}}_l} \\ \mathbf{P}_{\mathbf{x}_l \tilde{\mathbf{y}}_l} \end{bmatrix} \quad \boldsymbol{\kappa}_k = \mathbf{P}_{\mathbf{x}_k^a \tilde{\mathbf{y}}_l} \left(\mathbf{P}_{\tilde{\mathbf{y}}_l} \right)^{-1} = \begin{bmatrix} \mathbf{P}_{\mathbf{x}_k \tilde{\mathbf{y}}_l} \mathbf{P}_{\tilde{\mathbf{y}}_l}^{-1} \\ \mathbf{P}_{\mathbf{x}_l \tilde{\mathbf{y}}_l} \mathbf{P}_{\tilde{\mathbf{y}}_l}^{-1} \end{bmatrix}$$

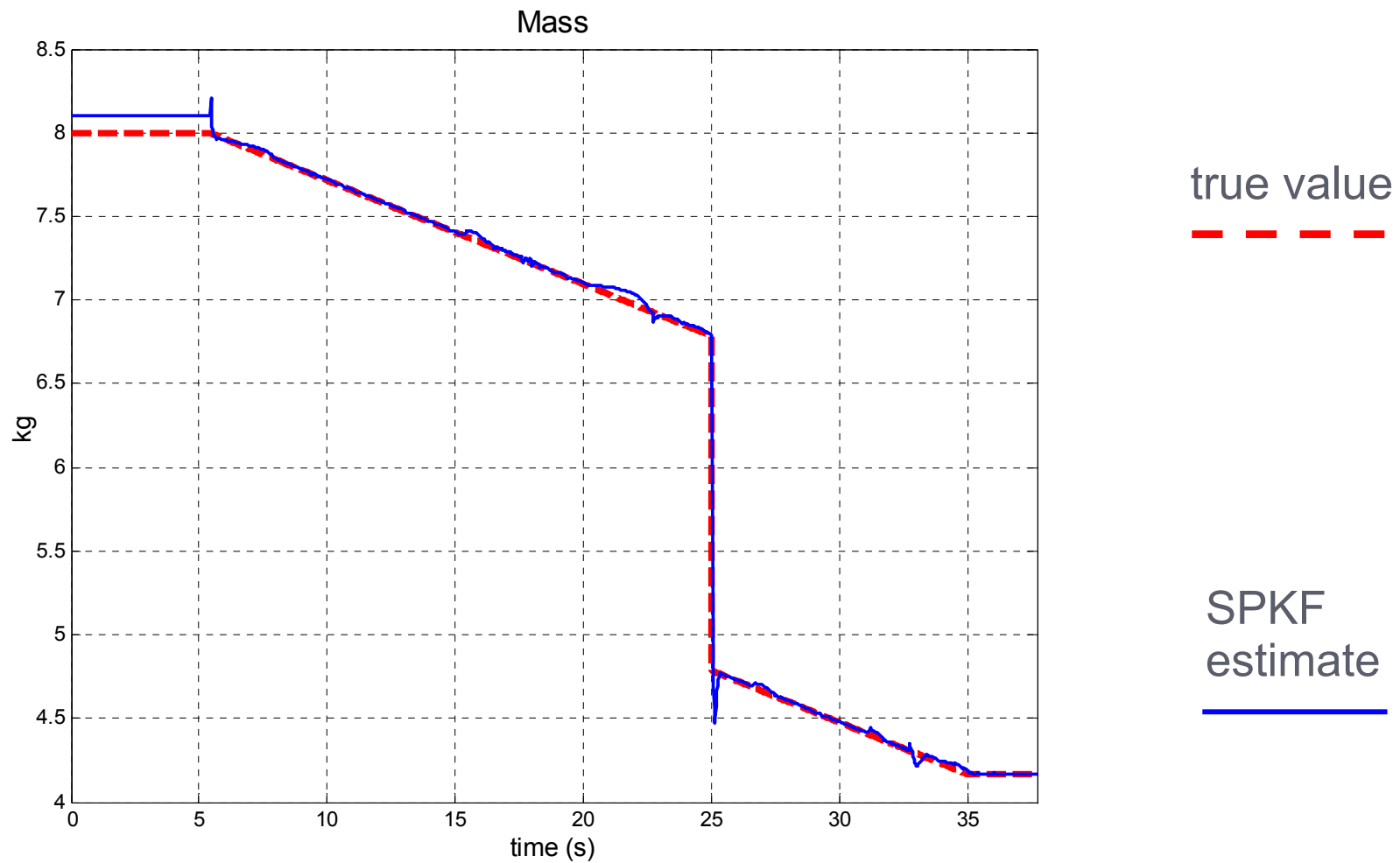
Experimental Results

► Parameter Estimation



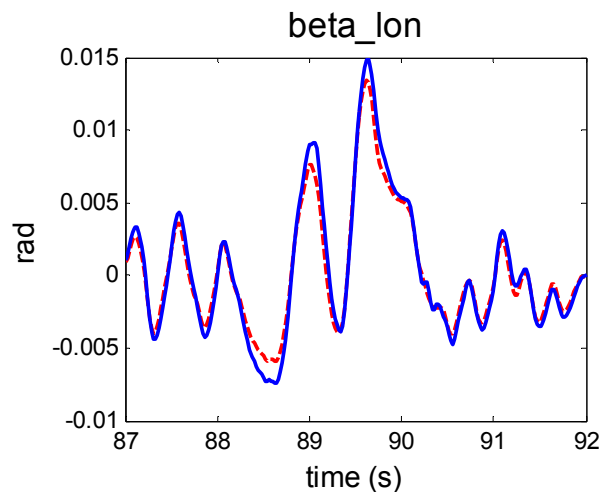
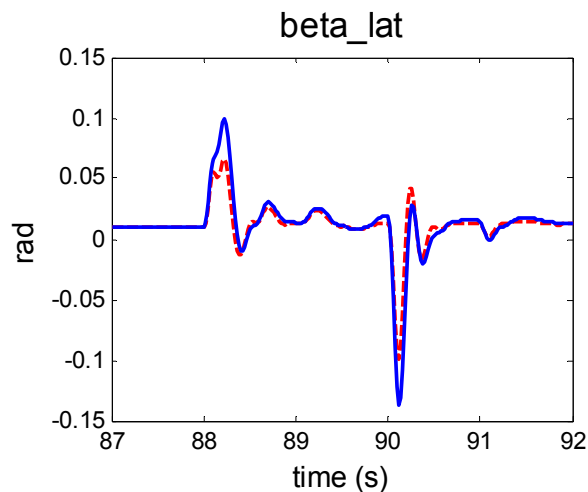
Experimental Results

► Parameter Estimation



Experimental Results

► Dual Estimation: Auxiliary States & Parameters

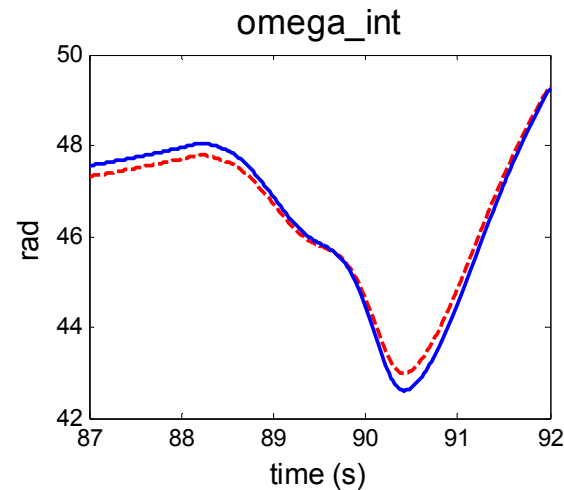
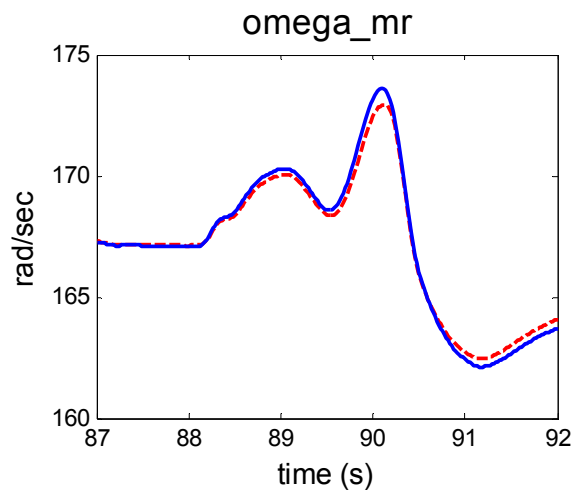


Flapping angles

true value

SPKF
estimate

—



Engine RPM
states

Experimental Results

► Dual Estimation: Dynamic Mass Tracking

