Extending the regime of linear response with synthetic forcings

Renato Spacek

(CERMICS, École des Ponts & MATHERIALS Team, Inria Paris)

In collaboration with Gabriel Stoltz

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Outline

- General setting
 - Nonequilibrium dynamics
 - Analytical framework
- Linear response of nonequilibrium dynamics
 - Linear response theory
 - Transport coefficients
- Optimizing the perturbation
 - Notion of synthetic forcings
 - Examples
- Numerical illustrations

General setting

Notation

- ullet The measure μ has associated density ψ
- \mathcal{A}^{\dagger} denotes the L^2 -adjoint of the operator \mathcal{A} , i.e.

$$\int (\mathcal{A}\varphi)\phi = \int \varphi(\mathcal{A}^{\dagger}\phi), \quad \forall \varphi, \phi \in C_0^{\infty}$$

• \mathcal{A}^* denotes the $L^2(\psi)$ -adjoint of the operator \mathcal{A} , i.e.

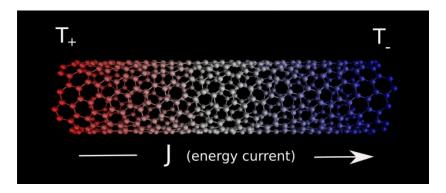
$$\int (\mathcal{A}\varphi)\phi\,\psi = \int \varphi(\mathcal{A}^*\phi)\,\psi, \quad \forall \varphi, \phi \in C_0^\infty$$

Physical context and motivation

Transport coefficients are quantitative estimates.

Example (thermal conductivity): Fourier's law

$$J = -\kappa \nabla T$$



Long computational times to estimate κ ; can take up to weeks/months.

Nonequilibrium framework

Example: State-space $\mathcal{X} = \mathbb{T}^d$, periodic C^{∞} potential V

Overdamped Langevin dynamics

$$dq_t = (-\nabla V(q_t) + \frac{\eta F(q_t)}{\beta}) dt + \sqrt{\frac{2}{\beta}} dW_t$$

Generator $\mathcal{L}_{\eta} = \mathcal{L}_0 + \eta \widetilde{\mathcal{L}}_{\mathsf{phys}}$, with

$$\mathcal{L}_0 = -\nabla V^T \nabla + \beta^{-1} \Delta, \qquad \widetilde{\mathcal{L}}_{\text{phys}} = F^T \nabla$$

Invariant probability measure ψ_n solves the Fokker–Planck

$$\mathcal{L}_{\eta}^{\dagger}\psi_{\eta} = 0, \qquad \psi_0(q) = \frac{1}{Z}e^{-\beta V(q)}$$

The perturbation $\eta F(q)$ induces a response $\mathbb{E}_{\eta}(R)$ for some observable R(q). For small η , the response is linear in η .

Assumptions

Uniqueness of the invariant probability measure, trajectorial ergodicity.

$$\frac{1}{t} \int_0^t R(q^\eta_s) \, ds \xrightarrow[t \to +\infty]{\text{a.s.}} \mathbb{E}_\eta(R) := \int_{\mathcal{X}} R \, \psi_\eta$$

- 2 Lyapunov estimates
- 3 Stability of regular functions by inverse operators
- Stability of regular functions by the perturbation operator

Regular: smooth functions that (and whose derivatives) grow at most polynomially

Expansion of the invariant measure

Although unique, ψ_{η} has closed form unknown

Perturbative regime: Write ψ_{η} as $f_{\eta}\psi_{0}$. In powers of η ,

$$f_{\eta} = \mathbf{1} + \eta \mathfrak{f}_{1} + \eta^{2} \mathfrak{f}_{2} + \cdots$$
$$\psi_{\eta} = \psi_{0} + \eta \overline{\psi}_{1} + \eta^{2} \overline{\psi}_{2} + \cdots$$

Formal asymptotics on the Fokker–Planck $(\mathcal{L}_0 + \eta \widetilde{\mathcal{L}}_{\mathsf{phys}})^\dagger \psi_\eta = 0$ leads to

$$-\mathcal{L}_0^*\mathfrak{f}_1=\widetilde{\mathcal{L}}_{\mathrm{phys}}^*\mathbf{1}, \qquad \mathfrak{f}_{n+1}=\left(-\mathcal{L}_0^*\right)^{-1}\widetilde{\mathcal{L}}_{\mathrm{phys}}^*\mathfrak{f}_n$$

Remark: Converging infinite expansion requires some regularity results on $\widetilde{\mathcal{L}}_{\text{phys}}$ and \mathcal{L}_0 .

¹T. Lelièvre and G. Stoltz, Acta Numerica **25**, (2016)

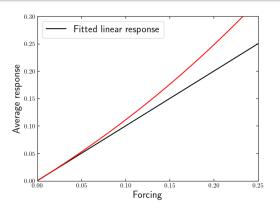
Linear response of nonequilibrium

stochastic dynamics

Linear response (1)

Linear response is used to compute transport coefficients. It is defined as

$$\rho_1 = \lim_{\eta \to 0} \frac{\mathbb{E}_{\eta}(R) - \mathbb{E}_{0}(R)}{\eta} = \lim_{\eta \to 0} \frac{\mathbb{E}_{\eta}(R)}{\eta}$$



Example: For constant F and $R(q) = F^T \nabla V$, ρ_1 represents the mobility.

Linear response (2)

Since $\psi_{\eta}=f_{\eta}\psi_{0}$, write the linear response as

$$\rho_1 = \lim_{\eta \to 0} \frac{1}{\eta} \int_{\mathcal{X}} R \, \psi_\eta = \lim_{\eta \to 0} \frac{1}{\eta} \int_{\mathcal{X}} R f_\eta \, \psi_0 = \int_{\mathcal{X}} R \mathfrak{f}_1 \, \psi_0$$

More generally, the n-th order response is given by

$$\rho_n = \int_{\mathcal{X}} R\mathfrak{f}_n \, \psi_0$$

Full response can be written as a polynomial in η

$$r(\eta) = \mathbb{E}_{\eta}(R) = \eta \rho_1 + \eta^2 \rho_2 + \eta^2 \rho_3 + \cdots$$

Linear response (3)

Estimator of linear response

$$\widehat{\rho}_{\eta,t} = \frac{1}{\eta t} \int_0^t R(q_s) \, ds \xrightarrow[t \to +\infty]{\text{a.s.}} \frac{1}{\eta} \int_{\mathcal{X}} R f_\eta \, \psi_0 = \rho_1 + O(\eta)$$

Main issue: Statistical error with asymptotic variance $O(\eta^{-2})$

Idea: Reduce variance by increasing η , but at which values of η does the nonlinear response develop?

Goal: Want to stay in the linear regime for η as large as possible.

Optimizing the perturbation

Synthetic forcings

Optimizing the perturbation

Idea: Introduce perturbation with generator $\widehat{\mathcal{L}}_{\text{extra}}$, where

$$\widetilde{\mathcal{L}}_{\mathsf{extra}}^* \mathbf{1} = 0$$

Resulting dynamics has generator

$$\mathcal{L}_{\eta} = \mathcal{L}_0 + \eta (\widetilde{\mathcal{L}}_{\mathsf{phys}} + \alpha \widetilde{\mathcal{L}}_{\mathsf{extra}})$$

The resulting perturbation is called a **synthetic forcing** 2 .

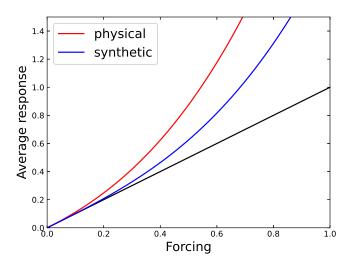
With the addition of the extra forcing, f_1 remains unchanged

$$\begin{split} \mathfrak{f}_1 &= -\mathcal{L}_0^{-1} (\widetilde{\mathcal{L}}_{\mathsf{phys}} + \alpha \widetilde{\mathcal{L}}_{\mathsf{extra}})^* \mathbf{1} \\ &= -\mathcal{L}_0^{-1} \widetilde{\mathcal{L}}_{\mathsf{phys}}^* \mathbf{1} \end{split}$$

²Evans. Morriss. (2008)

Formulation of synthetic forcing

In theory, we can find some $\widetilde{\mathcal{L}}_{\text{extra}}$ that extends the linear regime



Classes of synthetic forcings

- First-order differential operators $\widetilde{\mathcal{L}}_{\mathsf{extra}} = G^T \nabla_x$, with $\operatorname{div}(G\psi_0) = 0$.
- ② Second-order differential operators of the form $\widetilde{\mathcal{L}}_{\text{extra}} = -\partial_{x_i}^* \partial_{x_i}$. In this case, the operator is self-adjoint, i.e. $\widetilde{\mathcal{L}}_{\text{extra}} = \widetilde{\mathcal{L}}_{\text{extra}}^*$.
- $\begin{array}{l} \textbf{ § First-order differential operators with nontrivial zero order parts, such as} \\ \widetilde{\mathcal{L}}_{\text{extra}} = \partial_{x_i}^* = \partial_{x_i} U \partial_{x_i} \text{ for } \psi_0(x) = e^{-U(x)}. \end{array}$

Examples of synthetic forcings (overdamped Langevin)

Example 1: Divergence-free vector field

$$\begin{cases} \widetilde{\mathcal{L}}_{\text{extra}} = G(q)^T \nabla, & \text{such that} \quad \operatorname{div}(Ge^{-\beta V}) = 0 \\ dq_t = -\nabla V(q_t) \, dt + \eta F(q_t) \, dt + \eta \alpha G(q_t) \, dt + \sigma \, dW \end{cases}$$

Example 2: Modified fluctuation-dissipation

$$\begin{cases} \widetilde{\mathcal{L}}_{\text{extra}} = -\beta^{-1} \nabla^* \nabla = -\nabla V^T \nabla + \beta^{-1} \Delta \\ dq_t = -(1+\alpha\eta) \nabla V(q_t) \, dt + \eta F(q_t) \, dt + \sqrt{\frac{2(1+\alpha\eta)}{\beta}} dW \end{cases}$$

Example 3: Feynman-Kac forcing

$$\begin{cases} \widetilde{\mathcal{L}}_{\text{extra}} = \xi(q)^T \nabla^* = -\xi^T \nabla + \xi^T \nabla V \\ dq_t = -\nabla V(q_t) \, dt + \eta F(q_t) \, dt - \eta \alpha \xi(q_t) \, dt + \sigma dW \\ \omega_t \propto \exp\left(\alpha \eta \int_0^t \xi^T V(q_s) \, ds\right) \end{cases}$$

Examples of synthetic forcings (Langevin dynamics)

Example 1: Divergence-free vector field $\widetilde{\mathcal{L}}_{\text{extra}} = G_1^T \nabla_q + G_2^T \nabla_p$

$$\begin{cases} dq_t = M^{-1}p_t dt + \alpha \eta G_1(q_t, p_t) dt, \\ dp_t = -\nabla V(q_t) dt + \eta (F(q_t) + \alpha G_2(q_t, p_t)) dt - \gamma M^{-1}p_t dt + \sqrt{\frac{2\gamma}{\beta}} dW_t. \end{cases}$$

Example 2: Modified fluctuation-dissipation $\widetilde{\mathcal{L}}_{\text{extra}} = -\beta^{-1} \nabla_q^* \nabla_q - \beta^{-1} \nabla_p^* \nabla_p$

$$\begin{cases} dq_t = M^{-1}p_t dt - \alpha \eta \nabla V(q_t) dt + \sqrt{\frac{2\alpha\eta}{\beta}} dB_t, \\ dp_t = (-\nabla V(q_t) dt + \eta F(q_t)) dt - (\gamma + \frac{\alpha\eta}{\beta}) M^{-1}p_t dt + \sqrt{\frac{2(\gamma + \frac{\alpha\eta}{\beta})}{\beta}} dW_t. \end{cases}$$

Example 3: Feynman–Kac forcing $\widetilde{\mathcal{L}}_{\text{extra}} = \xi_1(p)^T \nabla_q^* + \xi_2(q)^T \nabla_p^*$

$$\begin{cases} dq_t = M^{-1} p_t \, dt - \alpha \eta \xi_1(p_t) \, dt, \\ dp_t = -\nabla V(q_t) \, dt + \eta (F(q_t) - \alpha \xi_2(q_t)) \, dt - \gamma M^{-1} p_t \, dt + \sqrt{\frac{2\gamma}{\beta}} \, dW_t, \end{cases}$$

Choosing magnitude of perturbation (1)

Recall: Response as a polynomial in η

$$r_{\alpha}(\eta) = \mathbb{E}_{\eta,\alpha}(R) = \eta \rho_1 + \eta^2 \rho_2(\alpha) + \eta^2 \rho_3(\alpha) + \cdots$$

Goal: Choose α s.t. the second-order response is killed.

With $\widetilde{\mathcal{L}}_{\mathsf{extra}}$, \mathfrak{f}_2 is given by

$$\mathfrak{f}_2 = \mathcal{L}_0^{-1} (\widetilde{\mathcal{L}}_{\mathsf{phys}} + \alpha \widetilde{\mathcal{L}}_{\mathsf{extra}})^* \mathcal{L}_0^{-1} \widetilde{\mathcal{L}}_{\mathsf{phys}}^* \mathbf{1}$$

Recall: Second-order response $\rho_2 = \int R\mathfrak{f}_2\,\psi_0$, so solve $\rho_2(\alpha^\star) = 0$

$$\rho_2 = \int_{\mathcal{X}} R\mathfrak{f}_{2,\mathsf{phys}} + \alpha \int_{\mathcal{X}} R\mathfrak{f}_{2,\mathsf{extra}} \implies \boxed{\alpha^* = \frac{\int R\mathfrak{f}_{2,\mathsf{phys}}\psi_0}{\int R\mathfrak{f}_{2,\mathsf{extra}}\psi_0}}$$

Choosing magnitude of perturbation (2)

Consider the relative error δ in the response relative to the linear response:

$$\delta_{\alpha}(\eta) = \left| \frac{r_{\alpha}(\eta) - \rho_{1}\eta}{\rho_{1}\eta} \right|.$$

Given some deviation ε , pick α such that

$$\alpha_{\star}(\varepsilon) = \operatorname*{arg\,max}_{\alpha \in \mathbb{R}} \eta_{\alpha}(\varepsilon), \qquad \eta_{\alpha}(\varepsilon) = \operatorname*{arg\,min}_{\eta \in \mathbb{R}} \left\{ |\eta| \colon \delta_{\alpha}(\eta) \geq \varepsilon \right\}.$$

In other words, stay within some neighborhood of the linear response for as long as possible.

Numerical illustration

Choosing the observable

Setting: Overdamped Langevin dynamics in 1D, potential $V(q) = \cos(2\pi q)$. We consider the observable

$$R(q) = (a\cos(2\pi q) + b\sin(2\pi q)) e^{\beta V(q)}$$

where $a, b \in \mathbb{R}$.

• b is chosen such that $\rho_1 = 1$, i.e.,

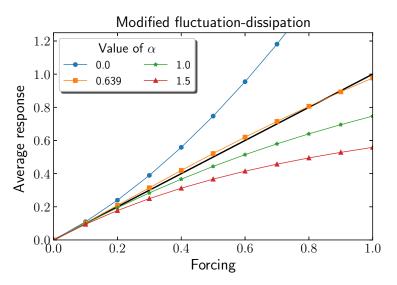
$$b = \left(Z^{-1} \int_{\mathcal{X}} \sin(2\pi q) \mathfrak{f}_1(q) dq\right)^{-1}, \quad Z = \int_{\mathcal{X}} e^{-\beta V(q)} dq$$

• Similarly, a can be chosen such that ρ_2 is arbitrarily large.

For nonsymmetric potentials, the above still gives $\rho_1, \rho_2 \sim O(1)$.

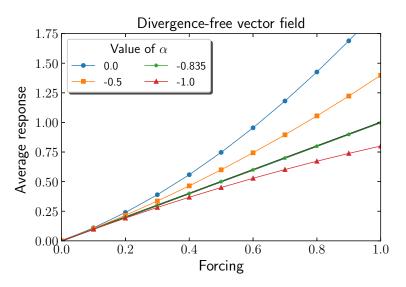
Numerical illustration: modified FD

$$\alpha^{\star} = 1.0, \qquad \alpha_{\star}(\varepsilon = 0.05) = 0.639$$



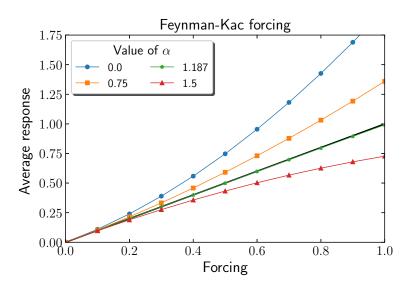
Numerical illustration: div-free vector field

$$\alpha^{\star} = -0.835$$

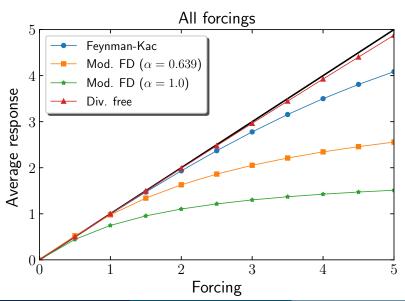


Numerical illustration: Feynman–Kac forcing

$$\alpha^{\star} = 1.187$$



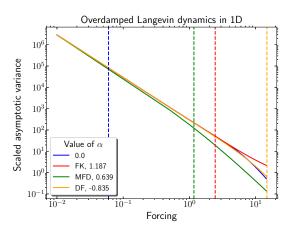
Numerical illustration: all forcings



Numerical illustration: variance reduction (1)

Asymptotic variance $\sigma_{R,\eta}^2$ same order as $\sigma_{R,0}^2$, up to small bias $O(\eta)$:

$$\frac{\sigma_{R,\eta}^2}{\eta^2} = \frac{\sigma_{R,0}^2}{\eta^2} + O\left(\frac{1}{\eta}\right)$$



Numerical illustration: variance reduction (2)

Define the gain as

$$gain = \left(\frac{\sigma_{R,\eta_0(\varepsilon)}^2}{\eta_0(\varepsilon)^2}\right) \left(\frac{\sigma_{R,\eta_\alpha(\varepsilon)}^2}{\eta_\alpha(\varepsilon)^2}\right)^{-1}.$$

Dynamics	Extra forcing				
	none	MFD	FK	DF (e^V)	DF ($A\nabla V$)
Ovd. 1D	1	6.56×10^{2}	1.58×10^3	1.28×10^5	-
Ovd. 2D	1	7.65×10^2	3.23×10^4	3.33×10^3	4.03×10^{0}
Lang. 1D	1	2.18×10^3	1.29×10^3	1.42×10^3	-

Future work and extensions

- Promising method: Can reduce variance by several orders of magnitude
- Potential applications: Lennard

 –Jones fluids (shear viscosity), systems of atom chains (thermal transport)
- Extension to actual MD systems: Transport coefficients are intensive quantities, i.e. not dependent on system size
 - \implies Notion of *preescreening*: two small simulations with $\alpha_1 \neq \alpha_2$, from which optimal α can be extrapolated