

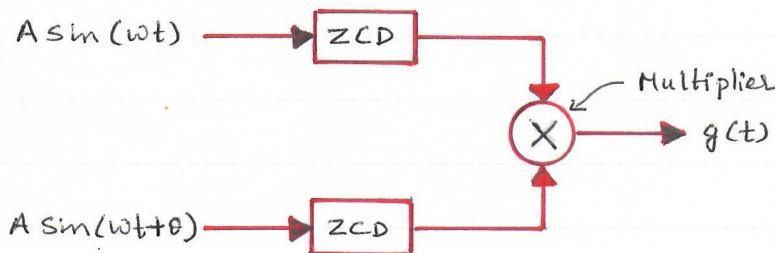
Solutions to Tutorial Sheet - 2

IEC103

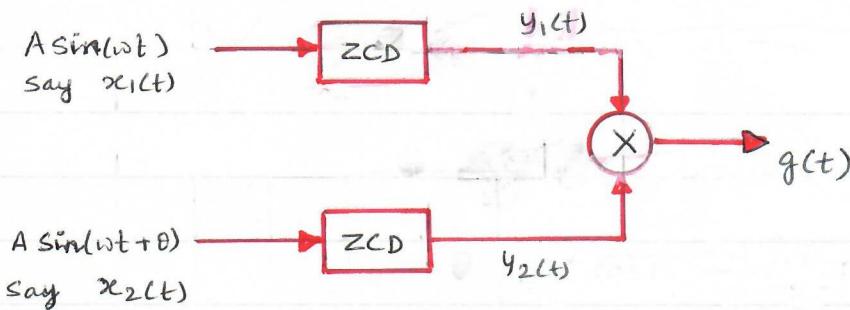
(Q1) A device called zero crossing detector (ZCD) has the following property.

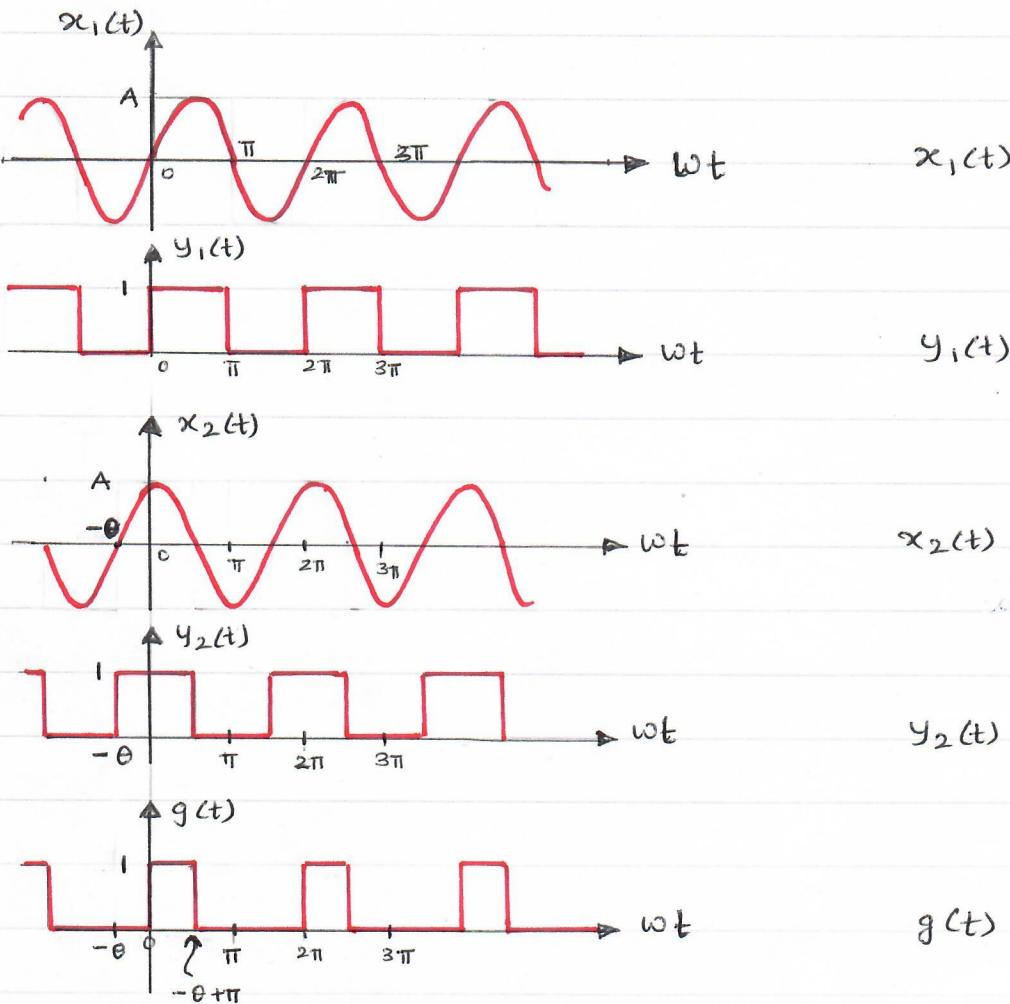
$$\text{output Amplitude} = \begin{cases} 1, & \text{for input amplitude} > 0 \\ 0, & \text{for input amplitude} < 0 \end{cases}$$

The waveforms  $A \sin(\omega t)$  and  $B \sin(\omega t + \theta)$  are passed through a system shown below : Find the amplitude and RMS value of  $g(t)$



Sol.





Amplitude of  $g(t) = 1$

RMS value of  $g(t)$

$$g_{\text{RMS}}^2 = \frac{1}{2\pi} \int_{-\pi}^{\pi} (g(t))^2 d\omega t$$

$$= \frac{1}{2\pi} \int_0^{\pi - \theta} (1)^2 d\theta'$$

$$= \frac{1}{2\pi} (\pi - \theta)$$

$$g_{\text{RMS}} = \sqrt{\frac{(\pi - \theta)}{2\pi}}$$

Q2 In the circuit shown in Fig. Q2,  $R_1 = 1.5 \text{ k}\Omega$ ;  $R_2 = 2.0 \text{ k}\Omega$ , and  $C = 0.5 \mu\text{F}$ .

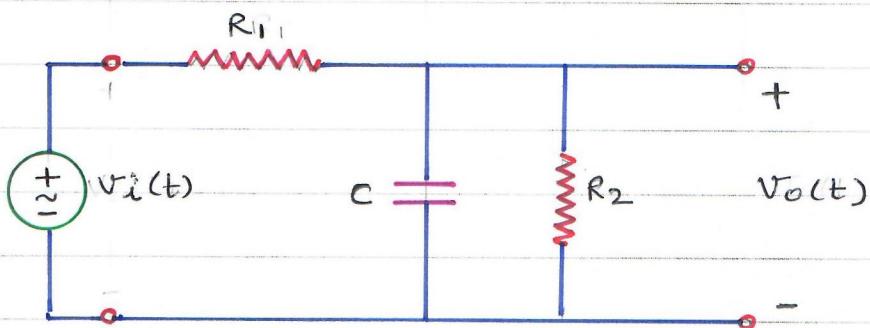


Fig. Q2

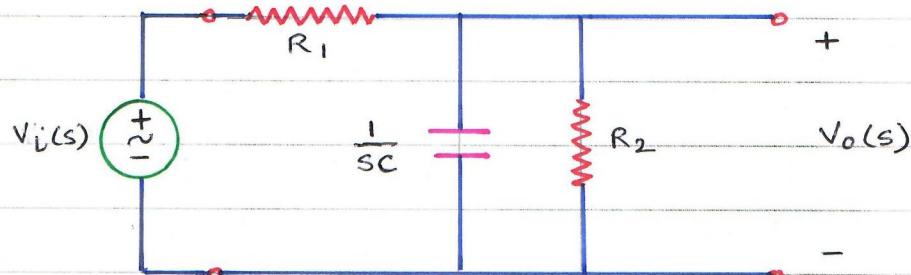
Determine

- The voltage transfer function  $H_V(\omega) = \frac{V_o(\omega)}{V_i(\omega)}$
- How the voltage transfer function  $H_V(\omega)$  behaves at extremely high and low frequencies.
- Show that the transfer function can be manipulated into the form  $H_V(\omega) = \frac{H_0}{1 + jf(\omega)}$

Find  $H_0$  and  $f(\omega)$ .

- Find the frequency at which  $f(\omega) = 1$  and the value of  $H_V(\omega)$  in decibels.

Sol. a) converting the circuit to frequency domain



$$\text{where } s = j\omega$$

$$V_o(s) = \frac{\frac{1}{sc} || R_2}{R_1 + \frac{1}{sc} || R_2} \times V_i(s)$$

$$\begin{aligned}
&= \frac{\frac{R_2}{sc}}{\frac{R_2 + \frac{1}{sc}}{R_1 + \frac{R_2/sc}{R_2 + 1/sc}} \times V_i(s)} \\
&= \frac{R_2}{1 + SR_2C} \times V_i(s) \\
&= \frac{R_2}{R_1 + \frac{R_2}{1 + SR_2C}} \times V_i(s) \\
&= \frac{R_2}{R_1(1 + SR_2C) + R_2} \times V_i(s) \\
&= \frac{R_2}{R_1 + R_2 + SR_1R_2C} \times V_i(s)
\end{aligned}$$

$$\Rightarrow \frac{V_o(s)}{V_i(s)} = H_V(s) = \frac{R_2}{(R_1 + R_2) + SR_1R_2C}$$

$$\Rightarrow H_V(\omega) = \frac{R_2}{(R_1 + R_2) + j\omega R_1 R_2 C}$$

b)  $H_V(\omega) = \frac{R_2}{(R_1 + R_2) + j\omega R_1 R_2 C}$

when  $\omega \ll 1$  i.e.,  $\omega \rightarrow 0$   $H_V(\omega) \approx \frac{R_2}{R_1 + R_2} = \frac{2K}{1.5K + 2K} = \frac{2}{3.5} = \frac{20}{35} = \frac{4}{7}$

when  $\omega \gg 1$  i.e.,  $H_V(\omega) \approx \frac{R_2}{j\omega R_1 R_2 C} = \frac{2}{j\omega \times 1.5 \times 10^3 \times 2 \times 10^3 \times 0.5 \times 10^{-6}}$

as  $\omega \rightarrow \infty = \frac{2}{j\omega \times 10^{-5}} \approx 0$

since  $\omega$  is very large

$$c) H_V(\omega) = \frac{R_2}{(R_1+R_2) + j\omega R_1 R_2 C}$$

$$= \frac{\frac{R_2}{(R_1+R_2)}}{1 + \frac{j\omega R_1 R_2 C}{(R_1+R_2)}} = \frac{H_0}{1 + j f(\omega)}$$

where  $H_0 = \frac{R_1}{R_1+R_2}$  is the gain at zero frequency

$$f(\omega) = \frac{\omega R_1 R_2 C}{(R_1+R_2)}$$

$$d) f(\omega) = \frac{\omega R_1 R_2 C}{(R_1+R_2)} = 1$$

$$\Rightarrow \omega = \frac{(R_1+R_2)}{R_1 R_2 C} = \frac{(1.5+2) \times 10^3}{1.5 \times 10^3 \times 2 \times 10^3 \times 0.5 \times 10^{-6}}$$

$$= \frac{3.5 \times 10^3}{1.5} \text{ rad/sec}$$

$$= 2.33 \text{ K rad/sec}$$

$$H_V(\omega) = \frac{H_0}{1 + j f(\omega)}$$

$$H_V(2.33 \text{ K rad/sec}) = \frac{4/7}{1 + j}$$

$$H_0 = 4/7 = 0.57 = 20 \log_{10}(0.57) \text{ dB}$$

$$= -4.86 \text{ dB}$$

(Q3) One application of narrowband filters is seen in rejecting interference due to AC line power. Any undesired 50 Hz signal originating in the AC line power can cause serious interference in sensitive instruments. In medical instruments such as the electrocardiograph, 50 Hz notch filters are often provided to reduce the effect of this interference on cardiac measurements. Fig. Q3 depicts a circuit in which the effect of 50 Hz noise is represented by way of 50Hz sinusoidal generator connected in series with a signal source ( $V_s$ ), representing the desired signal. In this example we design a 50Hz narrowband (or notch) filter to remove the unwanted 50Hz noise.

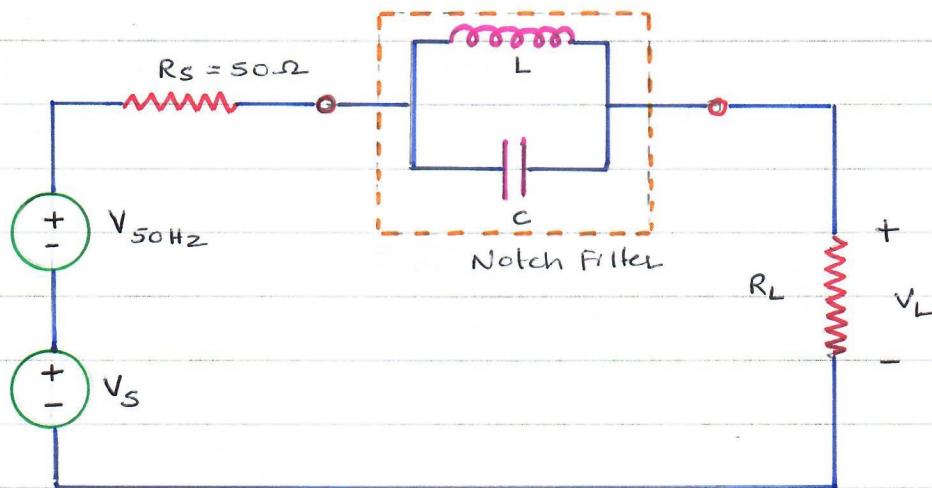


Fig. Q3 50Hz Notch Filter

Find the appropriate value of  $L$  and  $C$  for the notch filter.

Sol.

Sol.

$$\text{Impedance of the notch filter} = j\omega L \parallel \frac{1}{j\omega C}$$

$$= \frac{j\omega L \times \frac{1}{j\omega C}}{j\omega L + \frac{1}{j\omega C}}$$

$$= \frac{j\omega L}{1 - \omega^2 LC}$$

Note that when  $\omega^2 LC = 1$ , the impedance of the circuit is infinite! The frequency  $\omega_0 = \frac{1}{\sqrt{LC}}$  is the <sup>resonant</sup> frequency of the LC circuit. If the resonant frequency were selected to be equal to 50Hz, the series circuit would show an infinite impedance to 50Hz currents, and would therefore block the interference signal, while passing most of the other frequency components. We thus select values of L and C that results in  $\omega_0 = 2\pi \times 50$ .

$$\text{Let } L = 100 \text{ mH, then } C = \frac{1}{\omega_0^2 L} = 101 \mu\text{F}$$

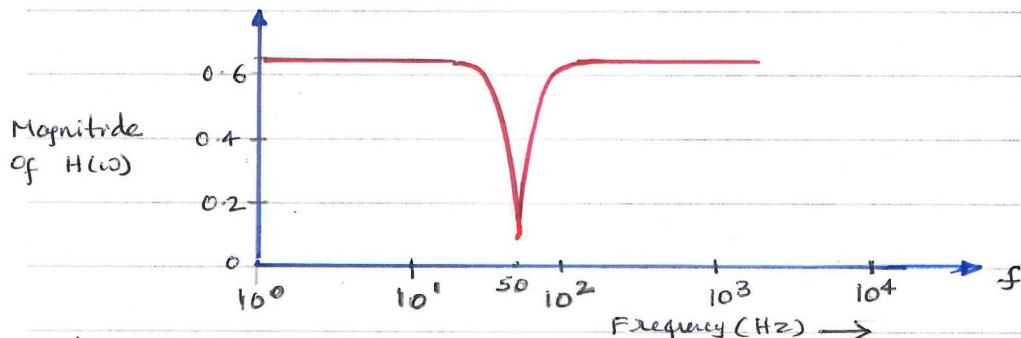
The frequency response of the complete circuit is given below

$$\begin{aligned} H(\omega) &= \frac{V_o(\omega)}{V_i(\omega)} = \frac{R_L}{R_S + Z_{\text{notch}} + R_L} \\ &= \frac{R_L}{R_S + \frac{j\omega L}{1 - \omega^2 LC} + R_L} \\ &= \frac{R_L}{R_S + R_L + j\omega L / (1 - \omega^2 LC)} \end{aligned}$$

$$|H(\omega)| = \frac{R_L (1 - \omega^2 LC)}{\left[ (R_S + R_L)^2 (1 - \omega^2 LC)^2 + (\omega L)^2 \right]^{1/2}}$$

$$\angle H(\omega) = -\tan^{-1} \left( \frac{\omega L}{(R_S + R_L)(1 - \omega^2 LC)} \right)$$

Magnitude response (qualitative) as given below.

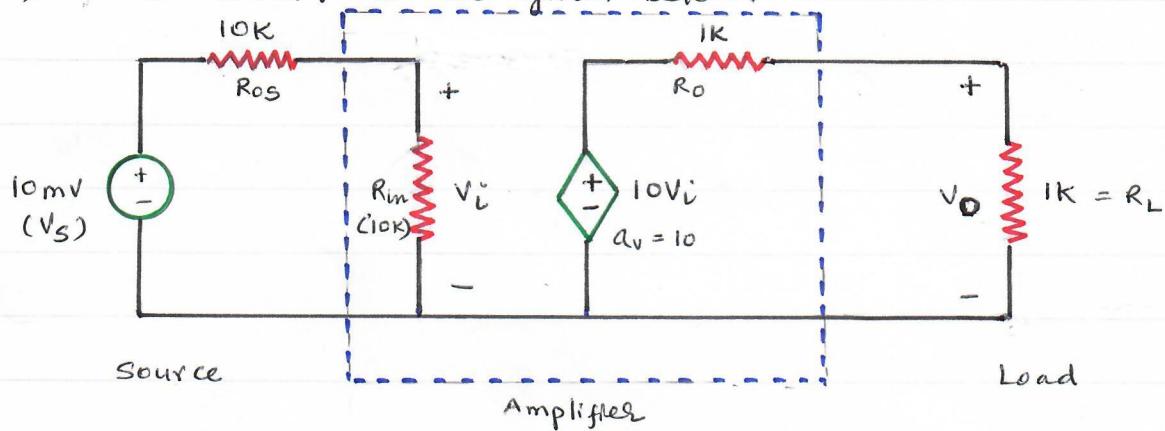


Q4) A source with output resistance of  $10\text{K}$  puts out a signal of  $10\text{mV}$  amplitude. It is intended to amplify the signal to feed into a load of  $1\text{K}$ . An amplifier is available with open-loop voltage gain of  $10$  and output resistance  $1\text{K}$  and input resistance of  $10\text{K}$ .

- What would be the output amplitude if the available amplifier is used.
- If  $N$  such amplifiers are connected in cascade and used between source and load, what is the signal amplitude at the output?

Sol.

- The circuit is as given below.



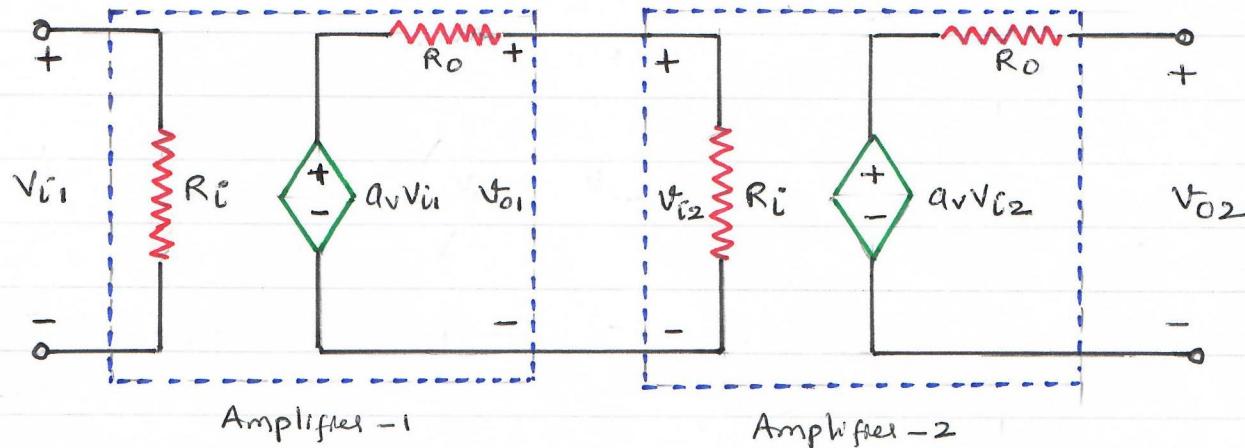
$$V_i = V_S \times \frac{R_{IN}}{R_{IN} + R_{OS}} = 10\text{mV} \times \frac{10\text{K}}{10\text{K} + 10\text{K}} = \frac{10\text{mV}}{2} = 5\text{mV}$$

$$I_L = \frac{10V_i}{R_O + R_L} = \frac{10 \times 5 \times 10^{-3}}{1\text{K} + 1\text{K}} = \frac{10 \times 5 \times 10^{-3}}{2 \times 10^3} \\ = 25 \times 10^{-6} \text{ A} \\ = 25 \text{ mA}$$

$$V_O = I_L R_L = 25 \times 10^{-6} \times 10^3 = 25 \times 10^{-3} = 25\text{mV}$$

$$\therefore V_O = 25\text{mV}$$

(iii) If 2-amplifiers are connected in cascade, the overall voltage gain can be found out as given below.



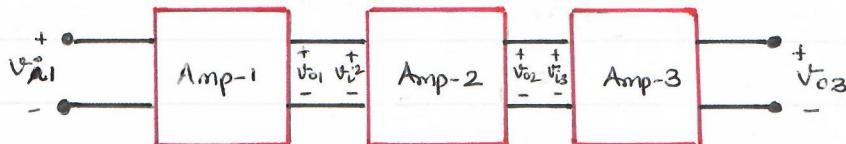
Since the amplifiers are connected in cascade, the output of amplifier-1 is input<sup>voltage</sup> to the amplifier-2 i.e.,  $V_{O1} = V_{i2}$

$$V_{O1} = \left( \frac{av V_{i1}}{R_o + R_i} \right) \times R_i = V_{i2}$$

$$V_{O2} = av V_{i2} = av \times \left( \frac{av V_{i1}}{R_o + R_i} \right) \times R_i$$

$$\therefore \text{overall gain} = \frac{V_{O2}}{V_{i1}} = \frac{av^2}{\left( \frac{R_o + R_i}{R_i} \right)} V_{i1}$$

If 3-such amplifiers are connected in cascade



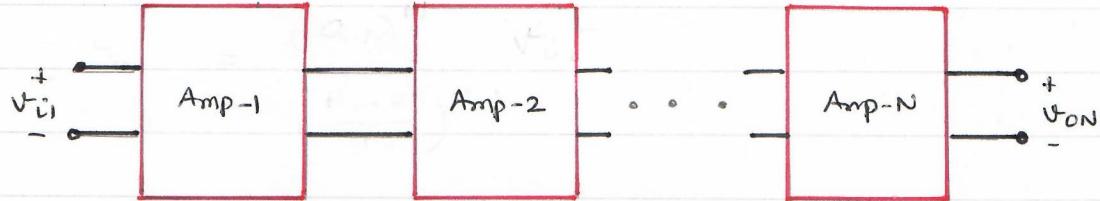
$V_{O2}$  will be the output voltage of 2nd amplifier and is input to the 3rd amplifier

$$V_{O1} = \frac{av \cdot R_i \cdot V_{i1}}{(R_o + R_i)} = V_{i2}$$

$$V_{O2} = \frac{av V_{i2} \times R_i}{(R_o + R_i)} = \frac{av}{(R_o + R_i)} \times R_i \times \frac{av R_i}{(R_o + R_i)} V_{i1} = \frac{av^2}{\left( \frac{R_o + R_i}{R_i} \right)^2} V_{i1}$$

$$V_{O3} = av V_{O2} = \frac{av^3}{\left( \frac{R_o + R_i}{R_i} \right)^2} V_{i1}$$

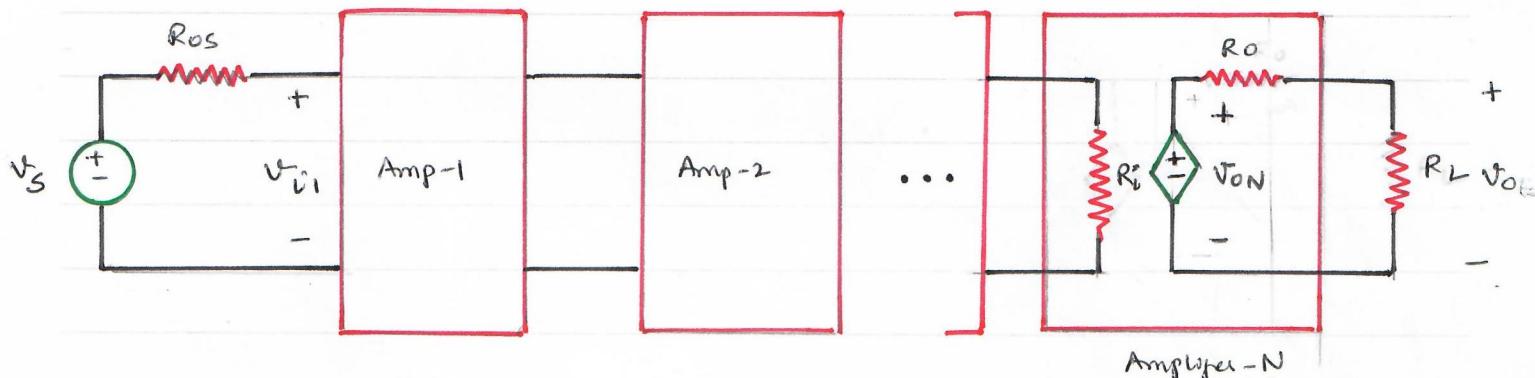
If  $N$  such amplifiers are connected in cascade



$N$  such amplifiers are connected in cascade

$$V_{ON} = \frac{(\alpha v)^N}{\left(\frac{R_i + R_o}{R_i}\right)^{N-1}} V_{ii}$$

Now if we connect the source with resistance  $R_{os}$  to i/p of amplifier-1 and connect load of resistance  $R_L$  to o/p of amplifier-N.



$$V_{ii} = V_s \times \frac{R_i}{(R_i + R_{os})}$$

$$V_{OL} = V_{ON} \times \frac{R_L}{(R_L + R_o)}$$

$$\text{where } V_{ON} = \frac{(\alpha v)^N}{\left(\frac{R_i + R_o}{R_i}\right)^{N-1}} V_{ii}$$

Substituting the values of  $V_s$ ,  $R_{os}$ ,  $R_i$ ,  $R_o$ , &  $R_L$ , the output voltage across the load can be calculated.

$$V_{ii} = V_s \times \frac{R_i}{R_i + R_{os}} = \frac{10 \times 10^{-3}}{10 + 10} \times \frac{10K}{10K + 10K} = 5 \times 10^{-3} = 5mV$$

$$\alpha v = 10; \quad \frac{R_i + R_o}{R_i} = \frac{10K + 1K}{10K} = \frac{11}{10}$$

$$\therefore V_{ON} = \frac{(10)^N}{\left(\frac{11}{10}\right)^{N-1}} V_{ii} = \frac{(10)^N}{\left(\frac{11}{10}\right)^{N-1}} \times 5 \times 10^{-3}$$

$$\therefore V_{OL} = V_{ON} \times \frac{R_L}{R_L + R_o} = \frac{V_{ON} \times 1K}{1K + 1K} = \frac{V_{ON}}{2} = \frac{(10)^N}{\left(\frac{11}{10}\right)^{N-1}} \times 2.5 \times 10^{-3} V$$

Q5 Derive the exact formula for the overall gain of an inverting op-amp circuit ( $V_o/V_s$ ) shown in Fig. Q5.

a) If  $R_1 = 1\text{ k}\Omega$ ,  $R_f = 10\text{ k}\Omega$ ,  $R_i = 100\text{ k}\Omega$ ,  $R_o = 100\Omega$ , and open-loop gain  $A_{OL} = 10^5$ , evaluate the gain of this inverting amplifier.

b) Compare the result in part a) with ideal op-amp approximation

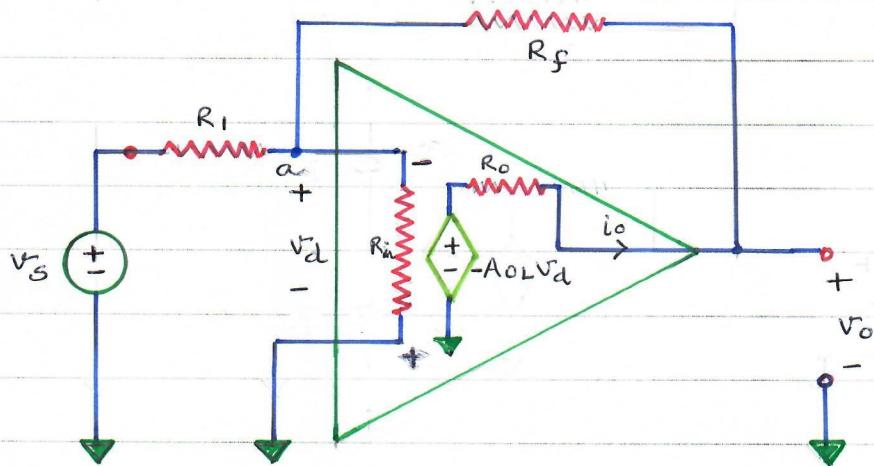


Fig. Q5

$$\text{Sol. } V_o = -A_{OL}V_d - i_o R_o \quad \text{where } i_o = (V_o - V_d)/R_f$$

Applying KCL at node 'a'

$$\frac{V_d - V_s}{R_1} + \frac{V_d}{R_i} + \frac{V_d - V_o}{R_f} = 0$$

$$\Rightarrow V_d \left( \frac{1}{R_1} + \frac{1}{R_i} + \frac{1}{R_f} \right) - \frac{V_o}{R_f} = \frac{V_s}{R_1} \dots \textcircled{A}$$

$$V_o = -A_{OL}V_d - i_o R_o$$

$$= -A_{OL}V_d - R_o \left( \frac{V_o - V_d}{R_f} \right)$$

$$\Rightarrow V_o \left( 1 + \frac{R_o}{R_f} \right) = \left( -A_{OL} + \frac{R_o}{R_f} \right) V_d$$

$$\Rightarrow V_d = \frac{(R_f + R_o) V_o}{(R_o - R_f A_{OL})} \dots \textcircled{B}$$

Substituting the expression for  $V_d$  from (B) in eq. (A), we have

$$V_d \left( \frac{1}{R_1} + \frac{1}{R_i} + \frac{1}{R_f} \right) - \frac{V_o}{R_f} = \frac{V_s}{R_1}$$

$$\Rightarrow \frac{(R_f + R_o)}{(R_o - A_{OL}R_f)} \left( \frac{1}{R_1} + \frac{1}{R_i} + \frac{1}{R_f} \right) - \frac{V_o}{R_f} = \frac{V_s}{R_1}$$

$$\Rightarrow \left[ \frac{(R_f + R_o)}{(R_o - A_{OL}R_f)} \left( \frac{1}{R_1} + \frac{1}{R_i} + \frac{1}{R_f} \right) - \frac{1}{R_f} \right] V_o = \frac{V_s}{R_1}$$

$$\Rightarrow \frac{V_o}{V_s} = \frac{1}{R_1 \left[ \frac{(R_f + R_o)}{(R_o - A_{OL}R_f)} \left( \frac{1}{R_1} + \frac{1}{R_i} + \frac{1}{R_f} \right) - \frac{1}{R_f} \right]}$$

a)  $R_1 = 1\text{ k}\Omega; R_f = 10\text{ k}\Omega; R_i = 100\text{ k}\Omega; R_o = 100\Omega; A_{OL} = 10^5$

$$\frac{V_o}{V_s} = \frac{1}{10^3 \left[ \frac{(10 \times 10^3 + 100)}{100 - 10^5 \times 10 \times 10^3} \left( \frac{1}{10^3} + \frac{1}{100 \times 10^3} + \frac{1}{10 \times 10^3} \right) - \frac{1}{10 \times 10^3} \right]}$$

$$= \frac{1}{10^3 \left[ \frac{10100}{-10^9} \times \frac{1}{10^3} \left( 1 + \frac{1}{100} + \frac{1}{10} \right) - \frac{1}{10^4} \right]}$$

$$\approx \frac{-10^4}{10^3} = -10$$

The exact value of  $V_o/V_s = -9.99888$

b) For an ideal op-amp  $R_i = \infty; R_o = 0; A_{OL} = 0$

$$\frac{V_o}{V_s} = -\frac{R_f}{R_1} = -\frac{10 \times 10^3}{10^3} = -10$$

$$\therefore \text{error} = \frac{-9.99888 - (-10)}{-9.99888} = -0.0112\%$$