

The background of the slide features a photograph of several white wind turbines with three blades each, set against a clear blue sky with a few wispy clouds. The turbines are positioned in a staggered pattern across the frame.

IMPLEMENTATION OF PRESSURE BASED SOLVER FOR SU2

3rd SU2 Developers Meet | Akshay.K.R, Huseyin Ozdemir, Edwin van der Weide

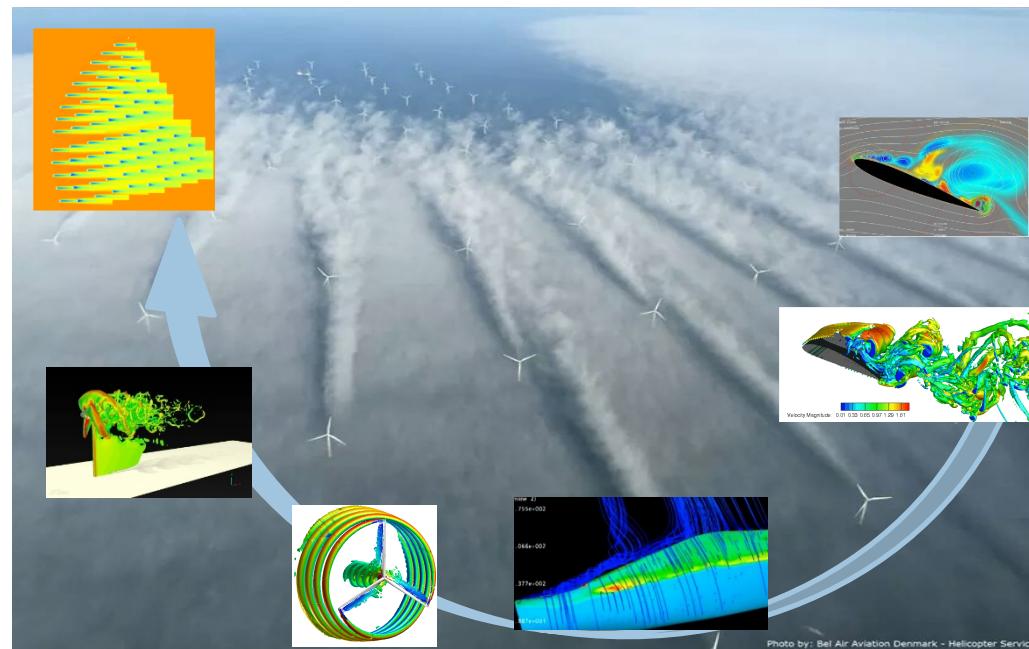


Content

- › ECN part of TNO
- › SU2 applications at ECN
- › Incompressible flow solver
- › Pressure-based solver
- › Research plan
- › SU2 in past and current projects

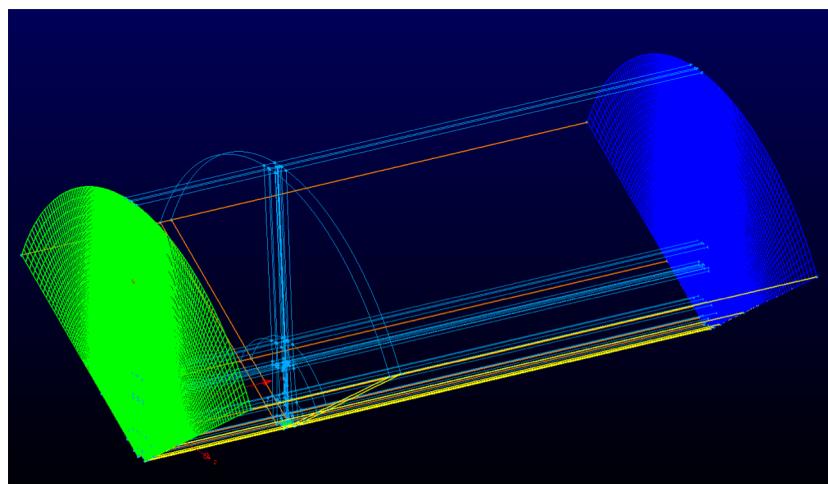
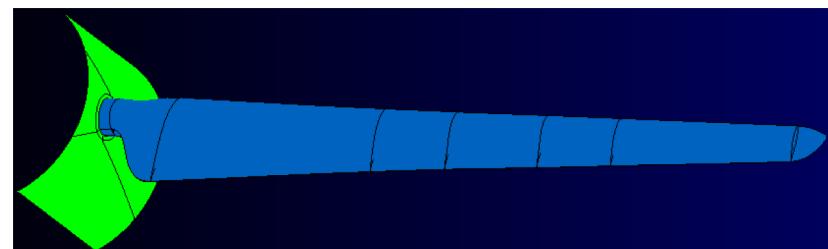
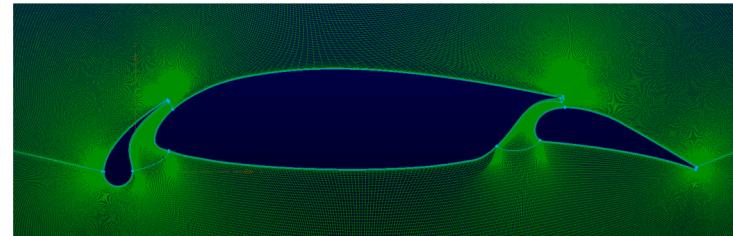
ECN part of TNO

- › ECN - Energy Research Center of the Netherlands merged with TNO as of April 2018.
- › Research on many topics of **renewable energy technologies**
 - › Wind energy, Solar energy, Biomass, etc.
- › Wind energy unit mainly focused on **low-fidelity tools** that are tailor made for wind energy applications (about 50 researchers on various topics)
- › **SU2** is our first serious attempt to include **CFD** in our research/design tool chain



SU2 Applications at ECN

- › Airfoil analysis:
 - › Thick airfoils (30%-40% thickness)
 - › Blade sections with add-ons like VGs
- › Wind turbine rotor simulations
 - › Rotating and periodic simulations
 - › Load computations
- › Wind farm simulations (planned)
 - › Actuator disk models



Incompressible Flow Solver

- › Wind energy applications have typical $\text{Ma} \sim 0$ and $\text{Re} \sim 10^6$.
- › Artificial compressibility method not suitable in this regime – ***very high mesh requirements*** and accuracy issues.
- › Need an ***accurate incompressible solver*** for wind energy applications.
- › Segregated ***pressure-based*** solver – SIMPLE family of algorithms.

Pressure Based Solver: Governing Equations

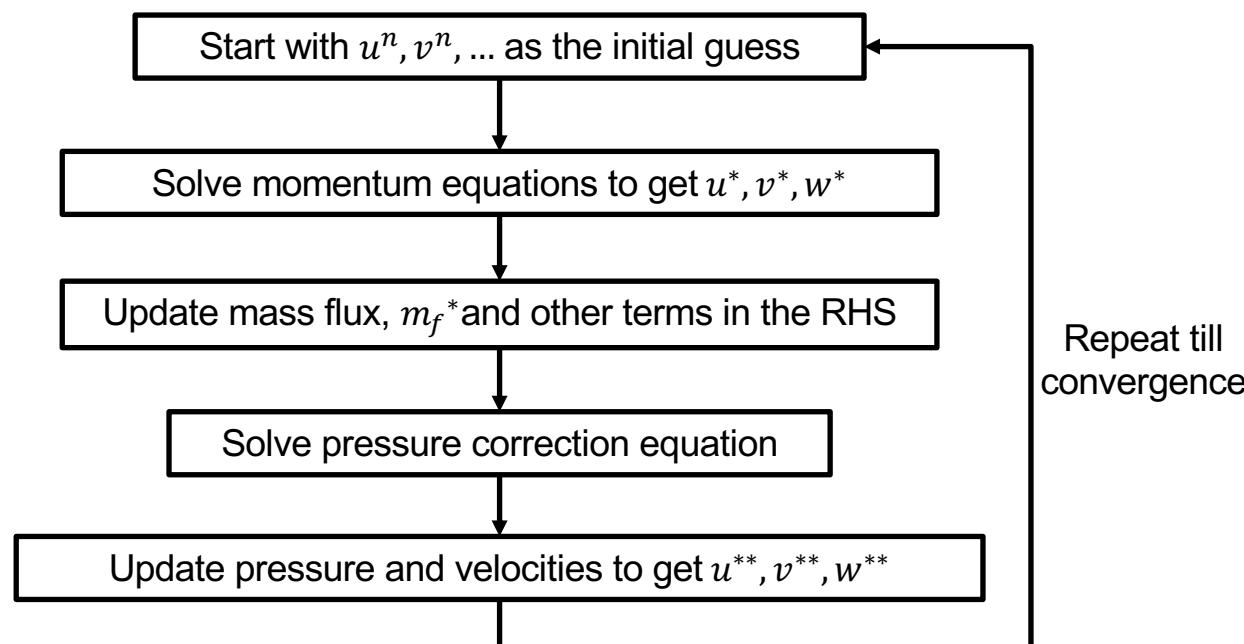
Momentum Equation:

$$\partial_t U + \nabla \cdot (\vec{F^c} - \vec{F^v}) - Q = -\nabla P$$

Pressure correction equation:

$$\nabla \cdot \nabla k P' = \sum_f \dot{m}^* + RHS$$

SIMPLE



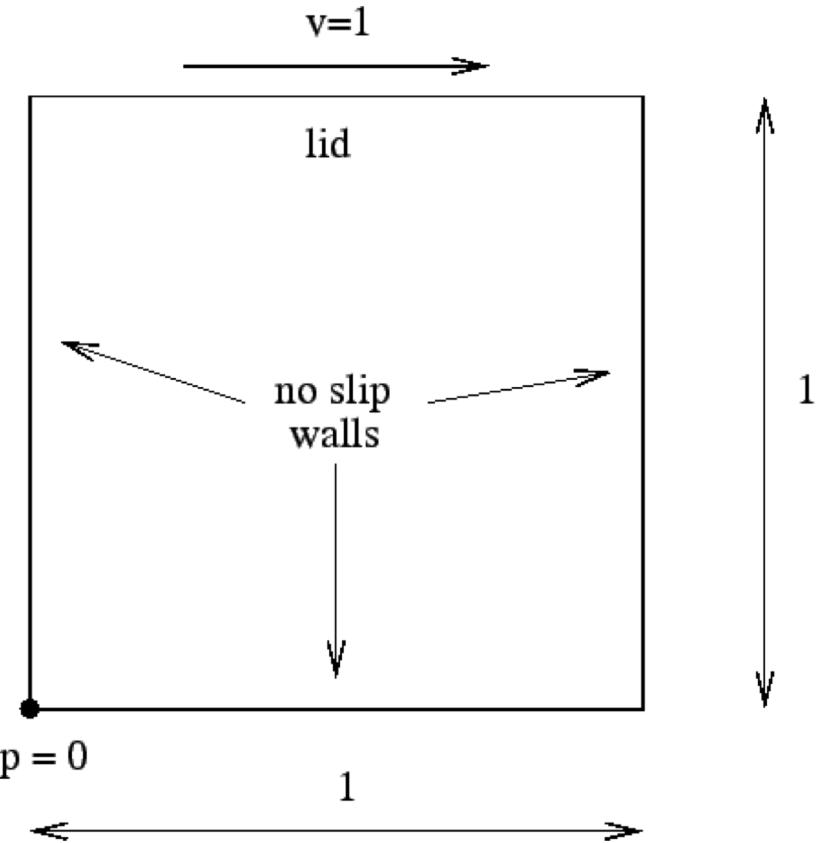
Research Plan

- › Research code
 - › Develop **research code** to test and analyze different features of the code
 - › Implement an **artificial compressibility** version and a **pressure-based** version
- › SU2
 - › A finite volume discretization for the **Poisson problem** in SU2
 - › **Euler solver** with the convective terms and **N-S solver** with the viscous terms following the code structure of SU2

Results: Research Code

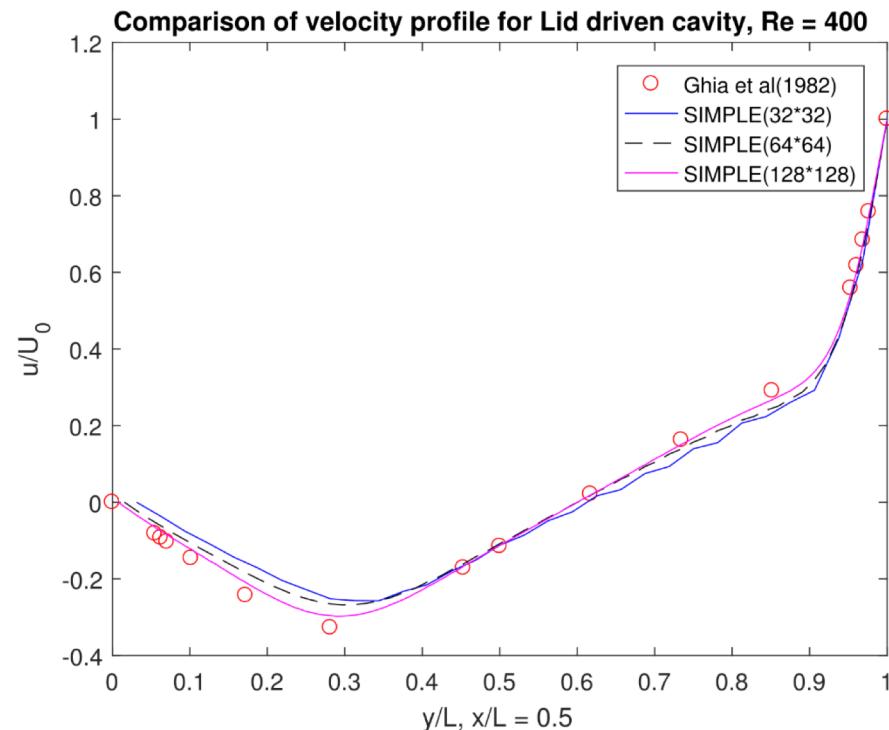
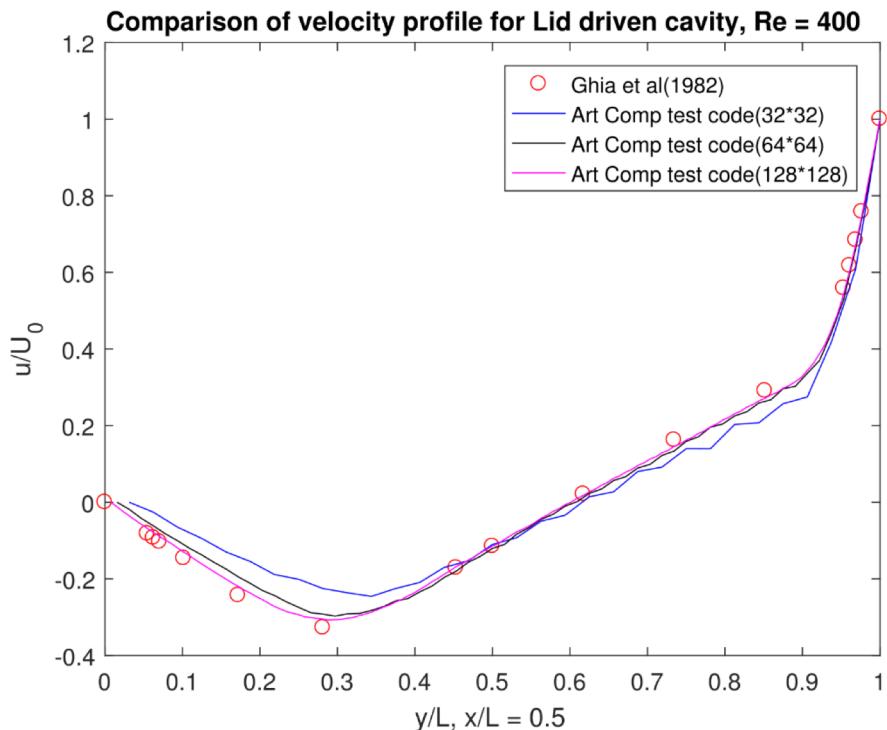
Lid driven cavity problem

- › $Re = 400$
- › Vertex based FVM
- › Uniform, cartesian grid
- › Spatial discretization:
 - › 1st order upwind
 - › Central
- › Time discretization:
 - › Implicit Euler
 - › Explicit Euler
- › Linear solver:
 - › Tri-Diagonal Matrix Algorithm (with ADI)
 - › Gauss-Seidel
 - › Plan to add MG



Results: Research Code

Lid driven cavity problem

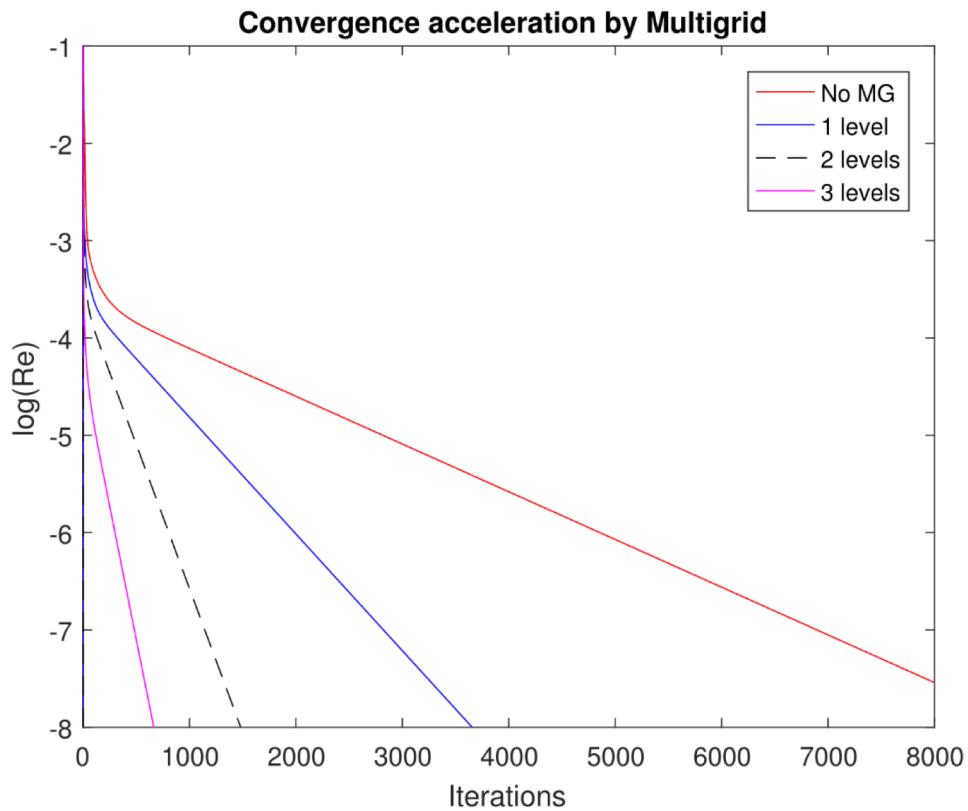


Centreline velocity

Results: SU2

Poisson Solver FVM

- › Implement a FV discretization of Poisson equation.
- › Solve an analytical test case to check solution.
- › Needs to solved multiple times within every iteration.
- › Enable multigrid to obtain a fast solution from the Poisson solver
- › Algebraic multigrid might be necessary for unsteady problems to obtain acceptable computational times.



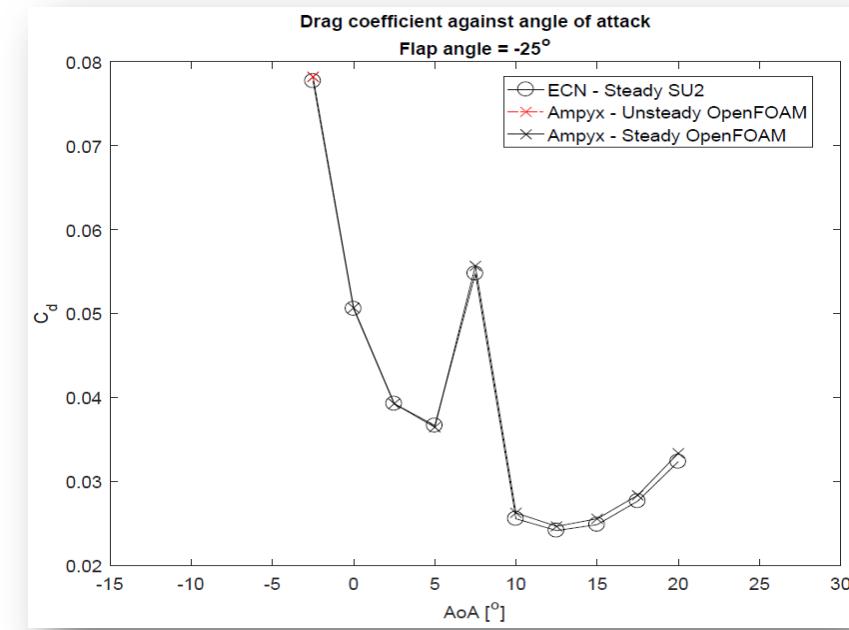
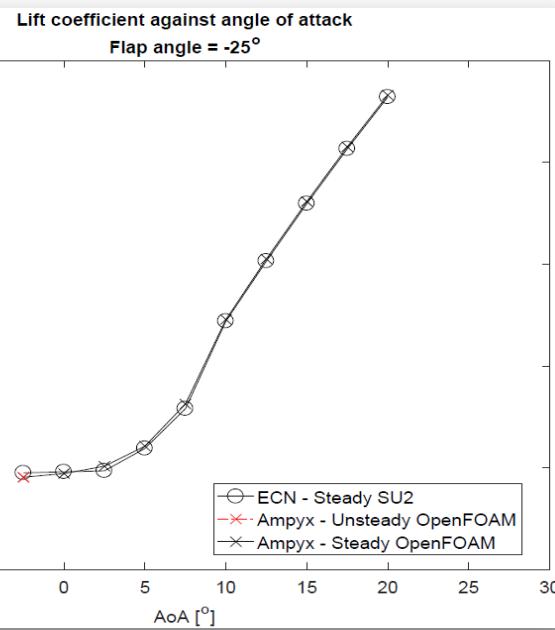
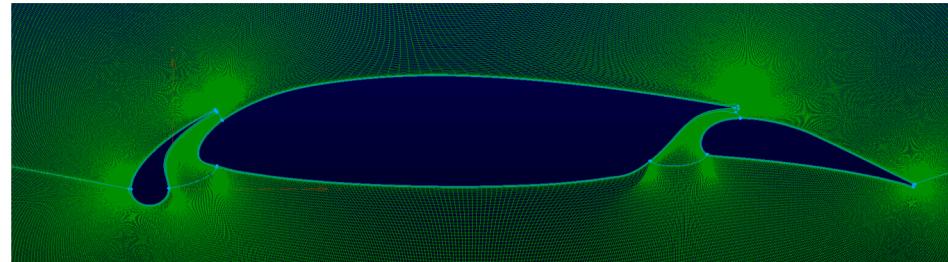
Current Status of Research

SU2 Euler/NS solver

- › Implementing the solver, numerical, variable and other associated routines for a pressure based system.
- › Coupled the flow solver with the Poisson solver.
- › Experimenting with different spatial discretization methods for the pressure-based solver.
 - › Plan to implement first and second order upwind and central schemes initially.
 - › Testing in the research code
- › Extend the multigrid to not only Poisson but also to flow solver.
- › Works only on single node so far.
- › Add ALE, periodic options.

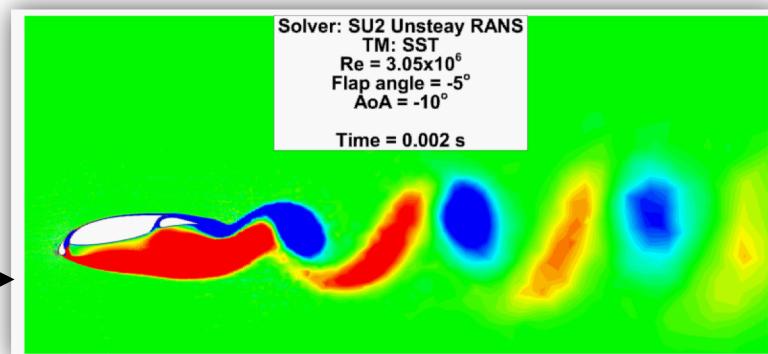
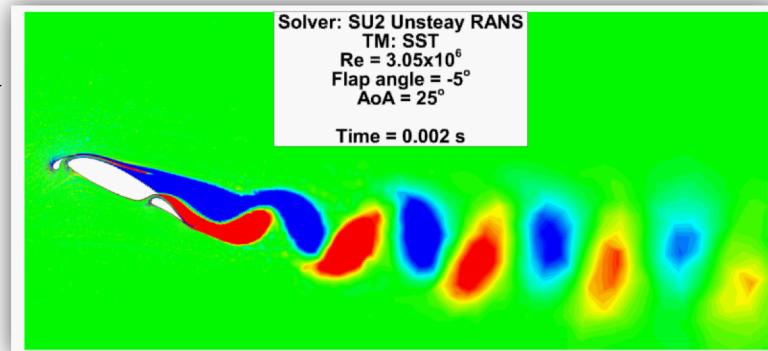
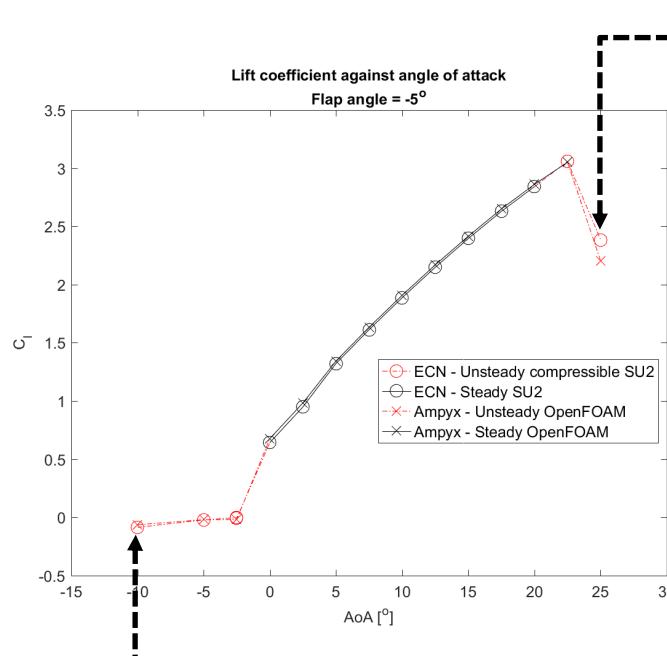
SU2 in Current Projects at ECN

Airfoil with add-ons



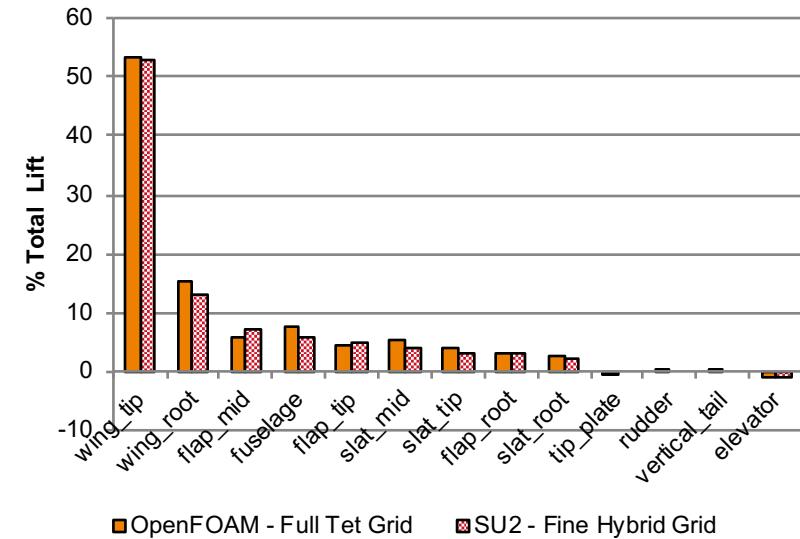
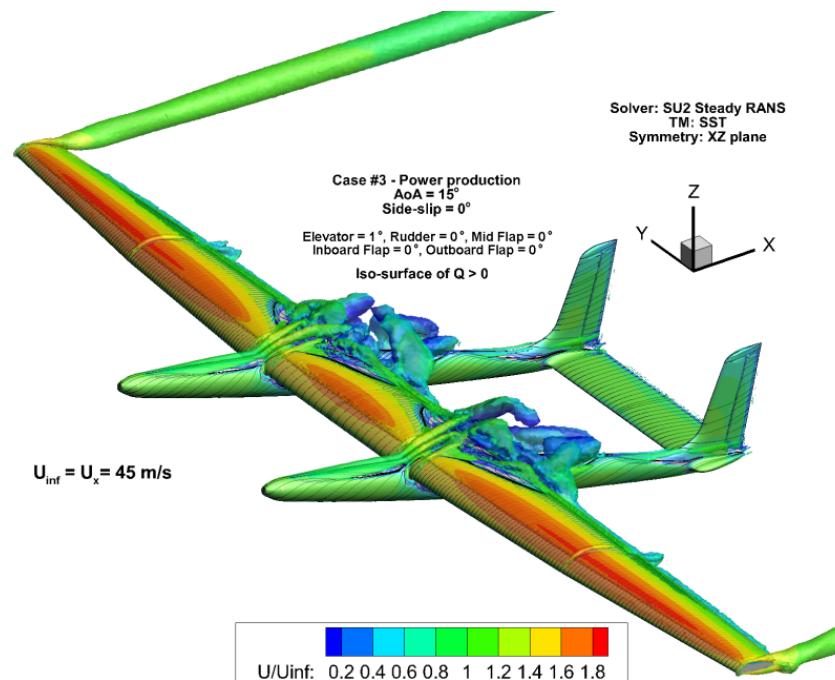
Aero polar for flap angle = -5deg

Airfoil with add-ons



Load Computation

Power plane – Novel concepts for wind power generation.

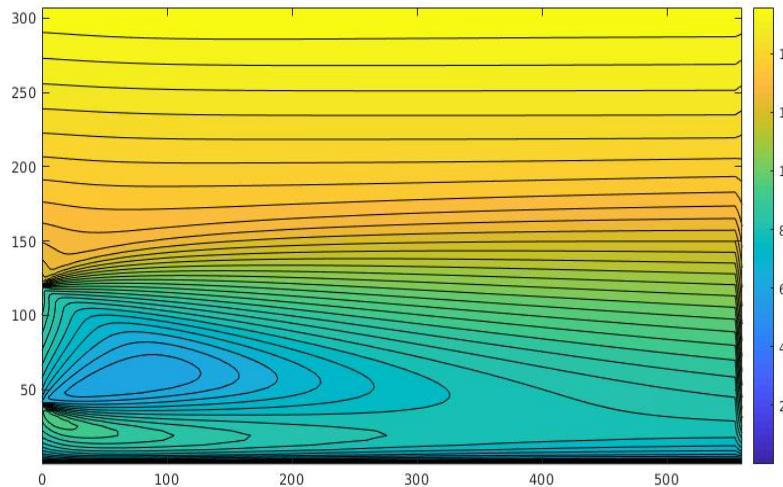


Comparison between OpenFOAM and SU2

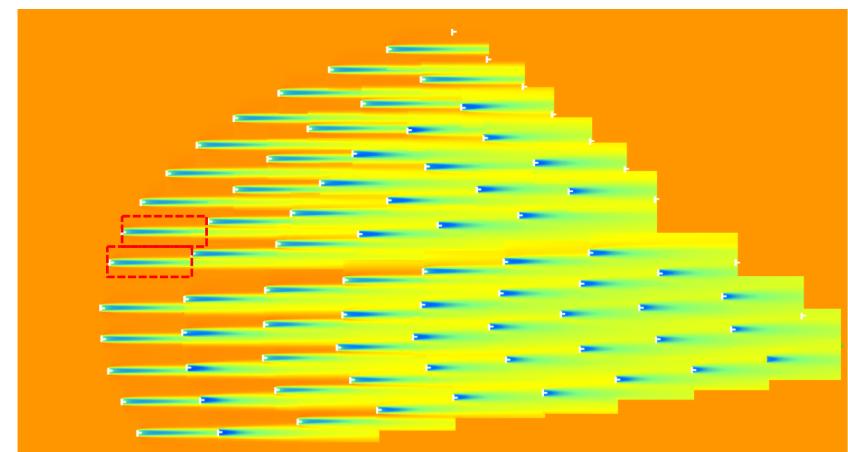
An alternative to traditional wind turbine designs.

Wind farm modelling

- › Use actuator disk to approximate the turbine.
- › Compute power output and optimize wind farm layouts.
- › Currently use parabolized N-S solver, plan to use SU2.



Wake behind a turbine



Wind farm layout



THANK YOU FOR YOUR ATTENTION

TNO.NL/ECNPARTOFTNO



ECN

TNO

innovation
for life

FarmFlow simulation time

- › A typical case consists of
 - $10 \times 10 = 100$ wind turbines
 - 25 wind speed levels
 - 72 wind directions
 - 1 turbulence intensity level
- › In total
 - $(10 \times 9) \times 25 \times 72 \times 1 = 162000$ cases to simulate
 - $162000 \times 3 \text{ seconds} / 3600$

~ 135 hours

FarmFlow simulation time for a single case

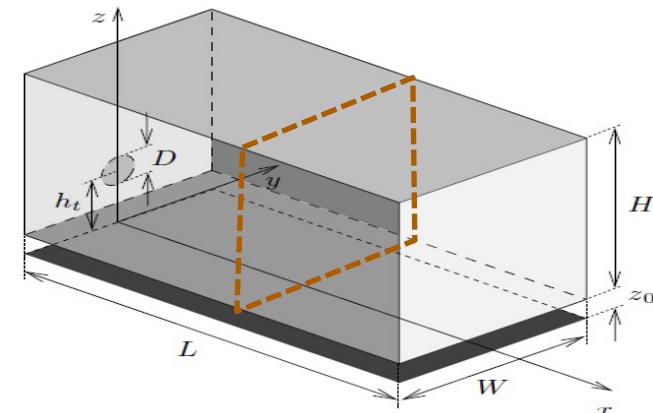
› Simulation time (CPU time) for a single:

- Wind turbine (single wake)
- Wind speed
- Wind direction
- Turbulence intensity level

› On a:

- Intel® Xeon® CPU E5620 @2.40 GHz
- 8 GB ram
- Windows 64 bit operating system

› **~ 3.0 seconds**



ABL stability model

Stable conditions:

$$u = \frac{u_{*0}}{\kappa} \left[\ln\left(\frac{z}{z_0}\right) - \psi_m(z/L) \left(1 - \frac{z}{2z_i}\right) + \frac{z}{L_{MBL}} - \frac{z}{z_i} \left(\frac{z}{2L_{MBL}}\right) \right]$$

Unstable conditions:

$$u = \frac{u_{*0}}{\kappa} \left[\ln\left(\frac{z}{z_0}\right) - \psi_m(z/L) + \frac{z}{L_{MBL}} - \frac{z}{z_i} \left(\frac{z}{2L_{MBL}}\right) \right]$$

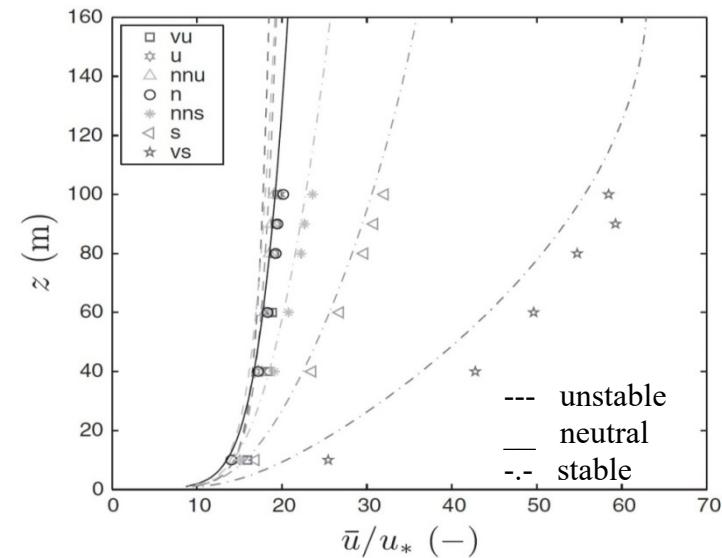
Neutral conditions:

$$u = \frac{u_{*0}}{\kappa} \left[\ln\left(\frac{z}{z_0}\right) + \frac{z}{L_{MBL}} - \frac{z}{z_i} \left(\frac{z}{2L_{MBL}}\right) \right]$$

Empirical fit for scaling parameter, L_{MBL} :

$$\frac{u_{*0}}{fL_{MBL}} = \left(-2 \ln\left(\frac{u_{*0}}{fz_0}\right) + 55 \right) e^{\left(-\frac{(u_{*0}/fL)^2}{400}\right)}$$

Gryning et.al. "On the extension of the wind profile over homogeneous terrain beyond the surface boundary layer," Boundary-Layer Meteorology, Vol. 124, No. 2, 2007, pp. 251–268.



	Unstable	Neutral	Stable
L	-128 m	321 m	41 m
z_i	117 m	205 m	49 m
L_{MBL}	283 m	866 m	69 m

$$z_i = c \frac{u_{*0}}{|f|}$$