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Non-Ideal Compressible-Fluid Dynamics in the SU2 Framework

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1st Annual SU2 Developers Meeting – September 5th – Delft NL

Outline

- What is NICFD?
- Applications
- Making SU2 a NICFD solver
- Where are we now?
- What's next



NICFD: what is that?

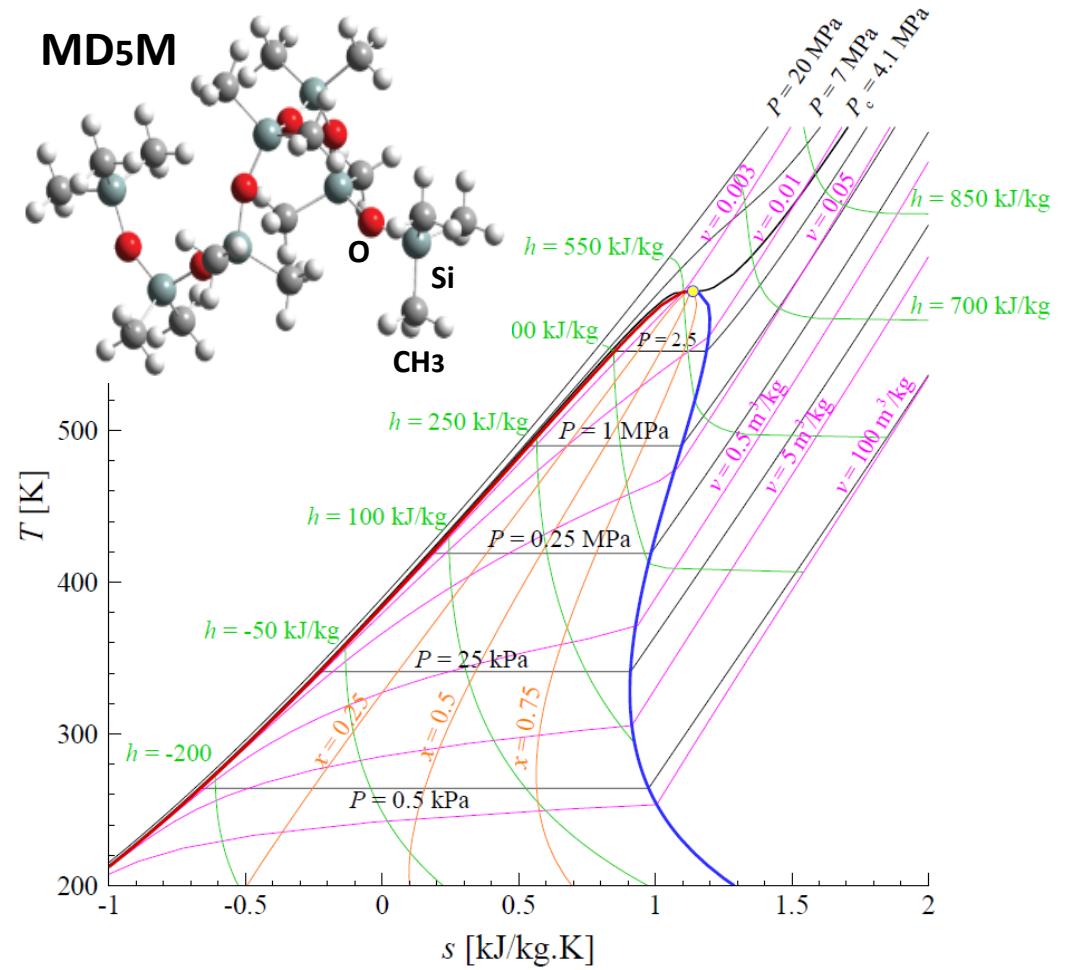


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Non-Ideal Compressible-Fluid Dynamics

NICFD: $PV \neq RT$

- Dense vapor flows
- High-compressibility
- Non-ideal speed-of-sound behavior
- Critical point effects
- Phase transition
- Super-critical flows



NICFD of molecularly complex fluids ($\Gamma < 1$)

Nozzle design for uniform outflow

Exit Mach = 2.25

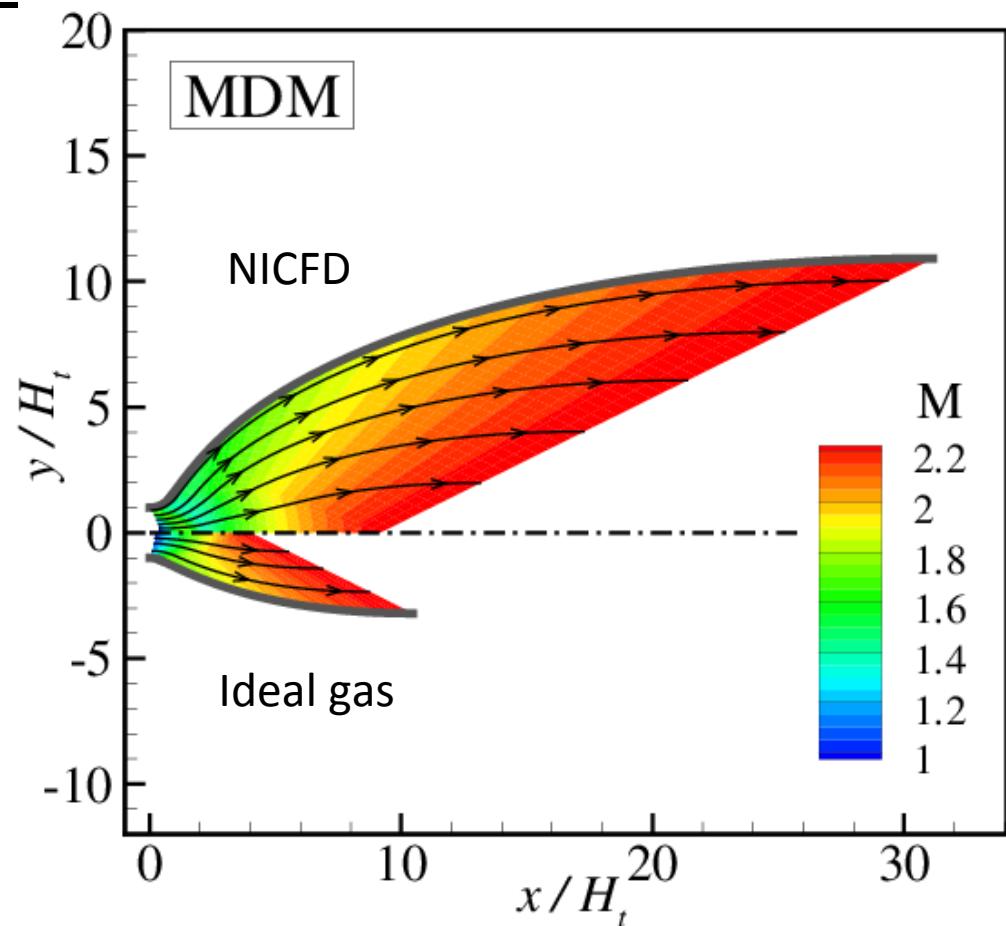
P0 = 25 bar, T0 = 310.3

Exp. Ratio b = 25

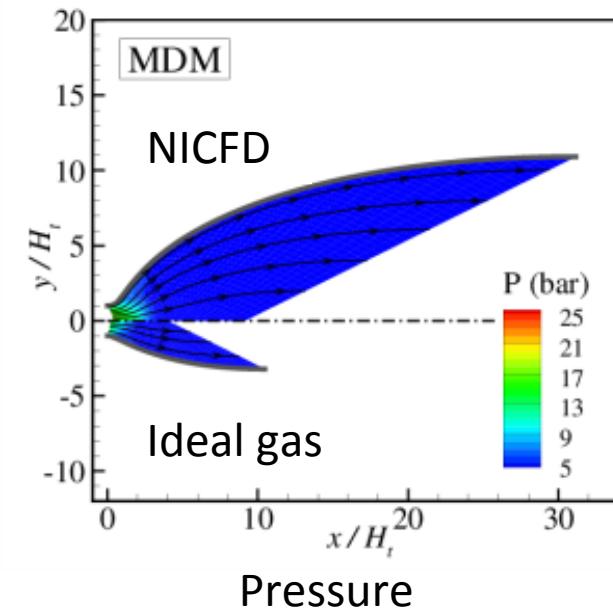
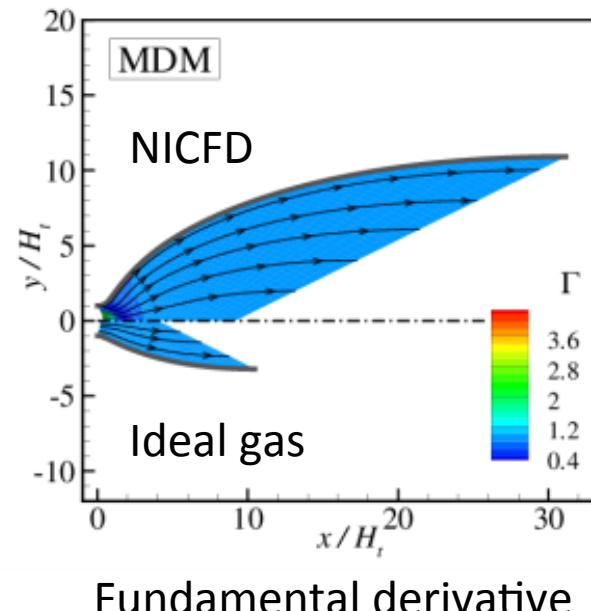
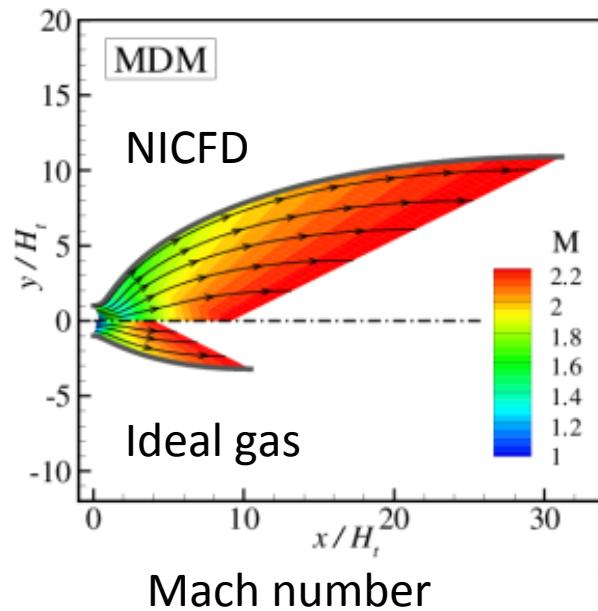
Fluid siloxane: MDM

Non-ideal vs ideal:

- nozzle length is x 3!
- exit section x 3!



NICFD of molecularly complex fluids ($\Gamma < 1$)

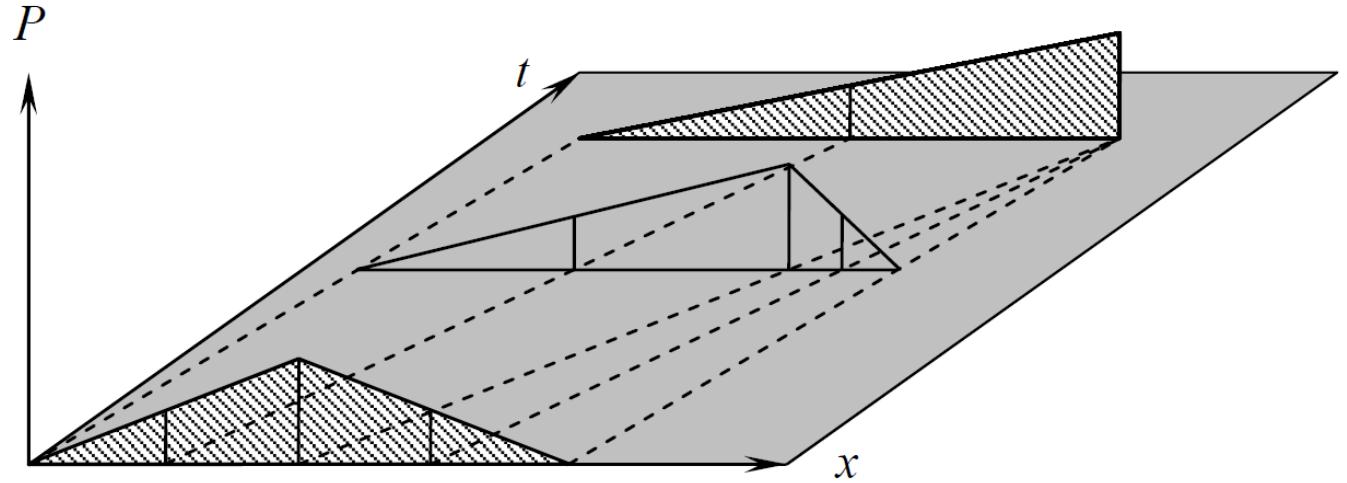


The Mach number variation along an isentropic expansion is NON-MONOTONE if $\Gamma < 1$!

Shock formation in a non-ideal fluid

Fundamental derivative of gasdynamics

$$\Gamma \equiv 1 - \frac{\nu}{c} \left(\frac{\partial c}{\partial \nu} \right)_s$$



$$\text{Speed of sound } c^2 \equiv -\nu^2 \left(\frac{\partial P}{\partial \nu} \right)_s$$

$$\text{Acoustic wave speed } w = u + c$$

$$dw = \left[\frac{\nu}{c} - \frac{\nu^2}{c^2} \left(\frac{\partial c}{\partial \nu} \right)_s \right] dP \Rightarrow dw = \frac{\nu}{c} \Gamma dP$$

Applications

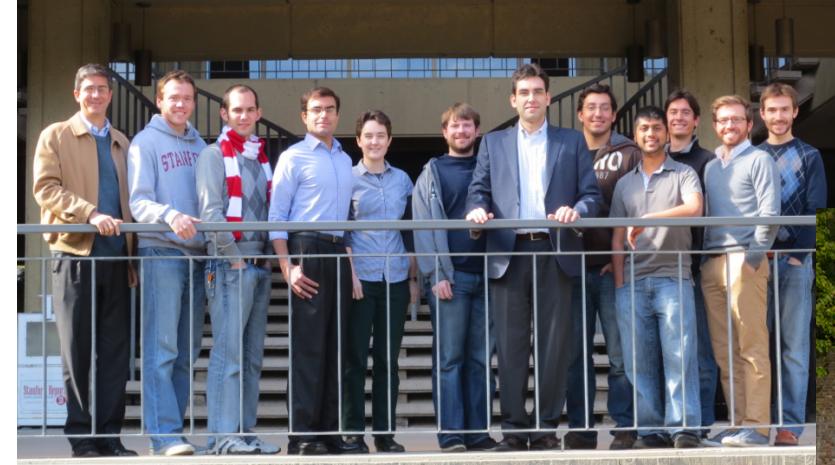
- Fundamentals of fluid mechanics
- ORC power systems
- scCO₂ power systems
- Trans-critical heat exchangers
- Oil and Gas compressors/expanders
- Super / transcritical injection (I.C.E., gas turbines)
- Cryogenic processes
- Rocket engines (turbopumps)
- Refrigeration / HVAC
- Chemical processes
- ...



Making SU2 a NICFD solver



Making SU2 a NICFD solver



Stanford University



First: get the
smart people!



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Rules of the game: governing equations

Euler equation for mono-component fluid at
chemical & thermodynamic equilibrium

$$\left\{ \begin{array}{l} \partial_t \rho + \nabla \cdot (\rho \mathbf{u}) = 0, \\ \partial_t (\rho \mathbf{u}) + \nabla \cdot (\rho \mathbf{u} \otimes \mathbf{u} + P) = 0, \\ \partial_t E^t + \nabla \cdot [(E^t + P) \mathbf{u}] = 0, \text{ with } E^t = \rho e + \frac{1}{2} \rho |\mathbf{u}|^2 \end{array} \right.$$

Thermodynamic closure is needed!

Perfect gas: $P = P(E, \rho) = (\gamma - 1) \rho e = (\gamma - 1) E$

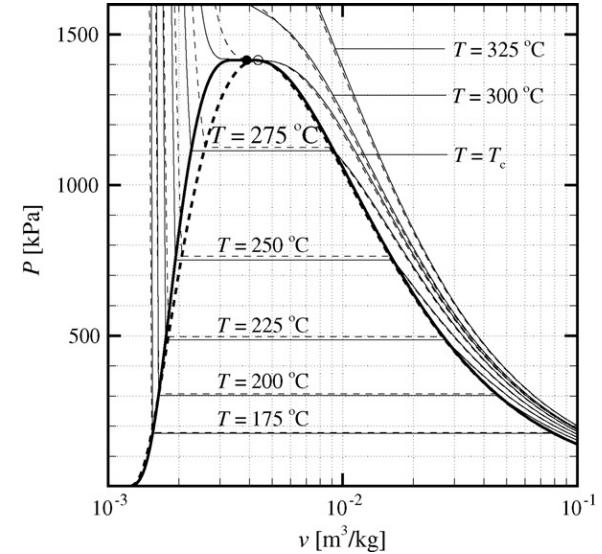


Thermodynamics models... PV ≠ RT!

$$\frac{\Psi(T, \rho)}{RT} = \psi^0(\tau, \delta) + \psi^r(\tau, \delta)$$

Span-Wagner 12-parameter EoS (2003)

$$\begin{aligned}\psi^0(\tau, \delta) &= \frac{h_0^0 \tau}{RT_c} - \frac{s_0^0}{R} - 1 + \ln \left(\frac{\tau_0 \delta}{\delta_0 \tau} \right) \\ &\quad - \frac{\tau}{R} \int_{\tau_0}^{\tau} \frac{C_P^0}{\tau^2} d\tau + \frac{1}{R} \int_{\tau_0}^{\tau} \frac{C_P^0}{\tau} d\tau \\ \psi^r(\tau, \delta) &= n_1 \delta \tau^{0.250} + n_2 \delta \tau^{1.125} + n_3 \delta \tau^{1.500} + n_4 \delta^2 \tau^{1.375} \\ &\quad + n_5 \delta^3 \tau^{0.250} + n_6 \delta^7 \tau^{0.875} + n_7 \delta^2 \tau^{0.625} e^{-\delta} \\ &\quad + n_8 \delta^5 \tau^{1.750} e^{-\delta} + n_9 \delta \tau^{3.625} e^{-\delta^2} + n_{10} \delta^4 \tau^{3.625} e^{-\delta^2} \\ &\quad + n_{11} \delta^3 \tau^{14.5} e^{-\delta^3} + n_{12} \delta^4 \tau^{12.0} e^{-\delta^3}\end{aligned}$$

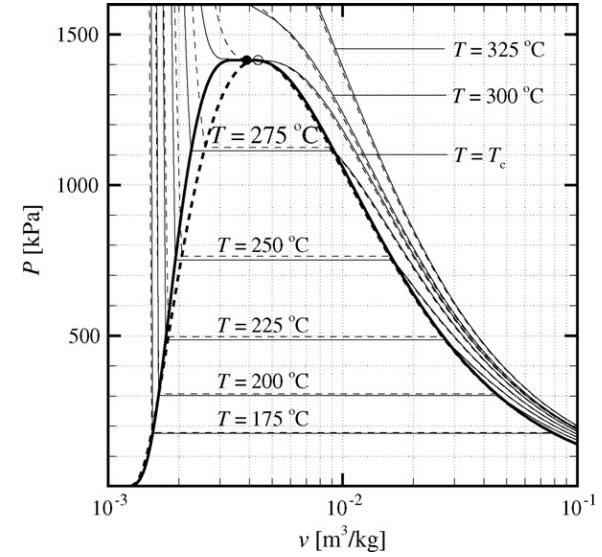


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$$P = P(E, \rho)$$



There may be trouble ahead...

Structure of the code changes deeply:

- Flux Jacobian is possibly NOT an homogeneous function of degree one w.r.t. conservative variables (Roe scheme?)
- More complex eigenstructure w.r.t. ideal gas.
- Thermodynamics:
 - Computationally expensive
 - Possibly numerically unstable
 - Non-unique solutions (VLE)
 - Look-Up Table must be consistent
 - $e \neq e(T)$, $h \neq h(T)$, $c \neq c(T)$
- Boundary conditions

...let's face the music and dance!



Where are we now?



Where are we now?

Thermodynamic modeling

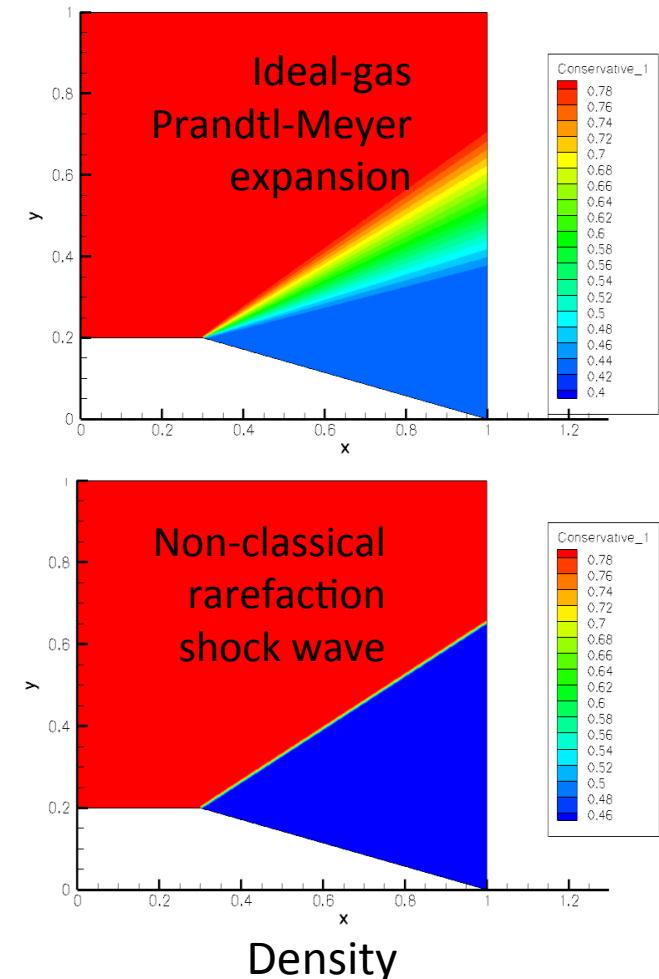
- Constant-specific-heat ideal gas
- van der Waals fluid
- Peng-Robinson Stryjek-Vera
- Coupling to FluidProp

Numerical schemes

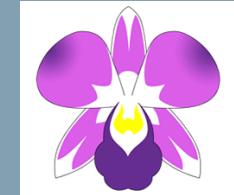
- Roe scheme
- HLLC scheme
- AUSM+

Boundary conditions

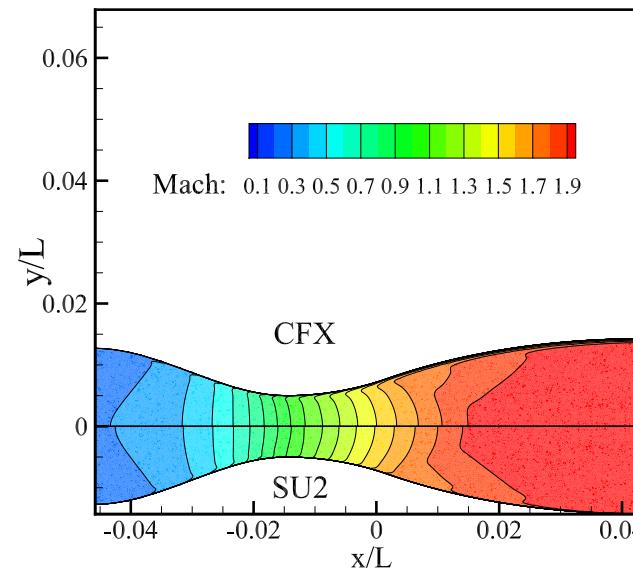
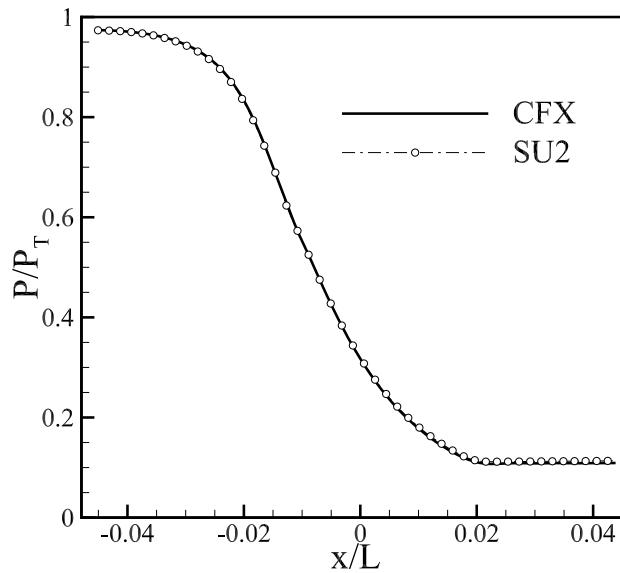
- Riemann boundary conditions
- Diverse input data: P , (ρ, u) , (h, s) , ...



ORCHID: ORC Hybrid Integrated Device @TUDelft



- Single regenerated BoP, closed loop configuration, dual TS operation (at one time)
- Continuous, steady-state, flexible in operation (multiple WF and op. conditions)



TROVA: Test-Rig for Organic Vapours @Politecnico di Milano

ERC NSHOCK Project

- Goal: first-time observation of Rarefaction Shock Waves in nozzle flows!
- Mixture thermodynamics & gasdynamics
- New measurement techniques for non-ideal compressible-fluid dynamics



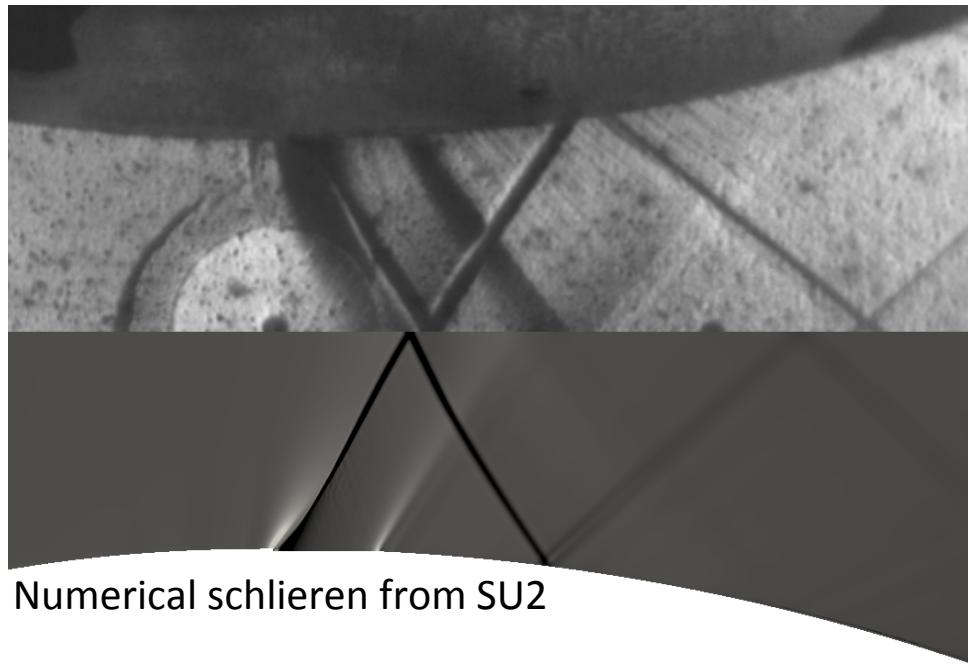
European Research Council
Established by the European Commission



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TROVA: Test-Rig for Organic Vapours @Politecnico di Milano

Schlieren visualisation of non-ideal nozzle flow
of siloxane fluid MDM

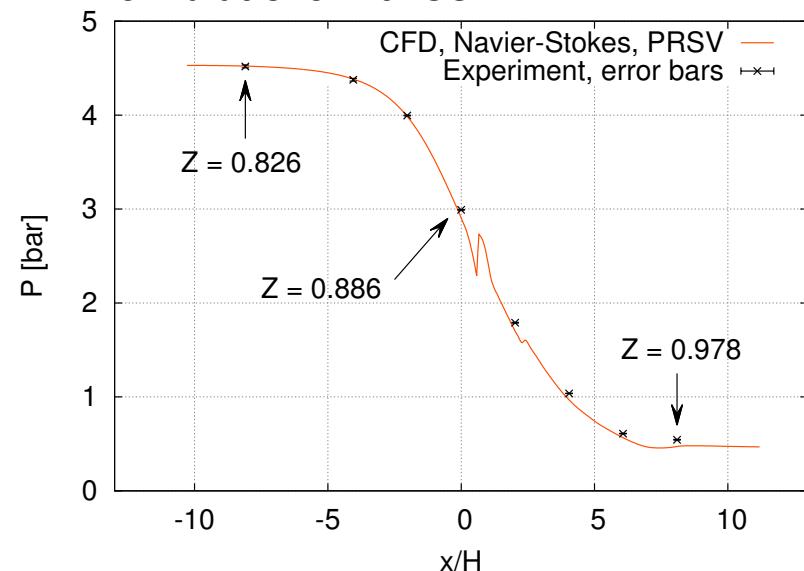


Test conditions $P^t = 4.68$ bar (meas.)
 $T^t = 246.9$ °C (meas.)
 $Z^t = 0.826$ (model)

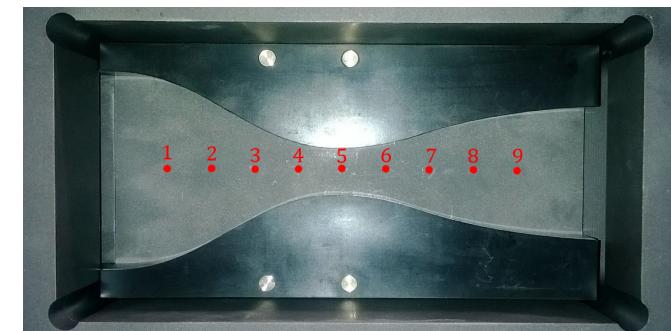


European Research Council
Established by the European Commission

Pressure measurements vs numerical
simulations with SU2



Compressibility
factor
 $Z = P/(RT\rho)$

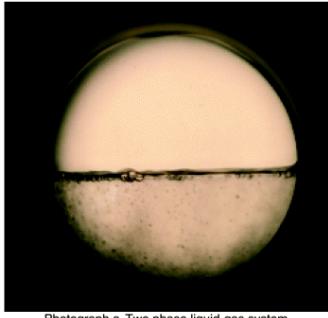


What's next?

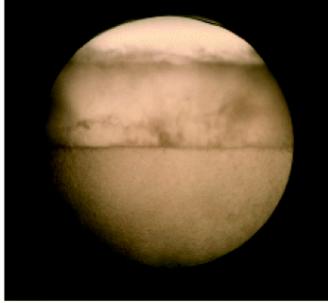


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What's next: modeling



Photograph a. Two phase liquid-gas system



Photograph b. Meniscus less well defined



Photograph c. Homogeneous supercritical fluid

Oaks et al. (2001)

- Viscosity/thermal conductivity
- Critical point flows
- Two-phase equilibrium flows
 - Cavitation/condensation
- Single and two-phase mixtures
- Non-equilibrium two-phase:
 - Particle nucleation
 - Super/sub-cooled TMD state
- Three-phase TMD:
 - In-flight ice formation
 - Deposition processes



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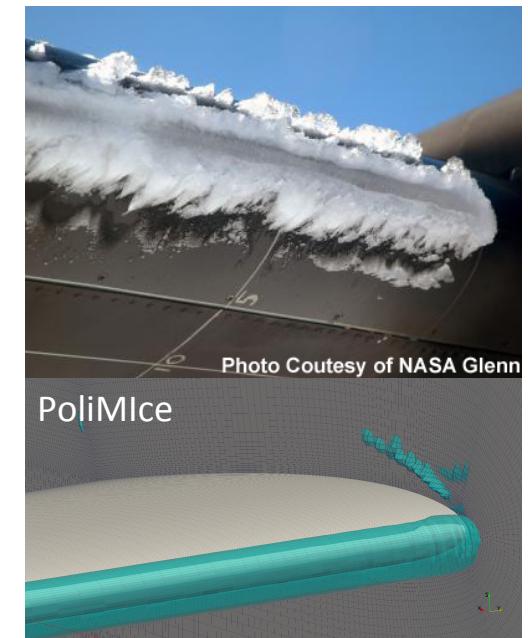
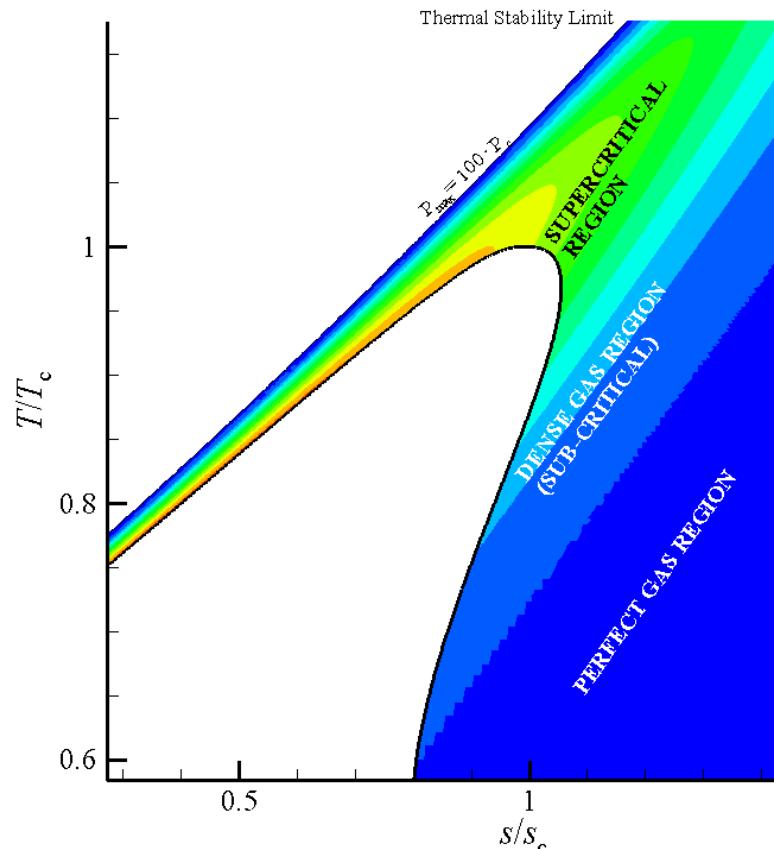


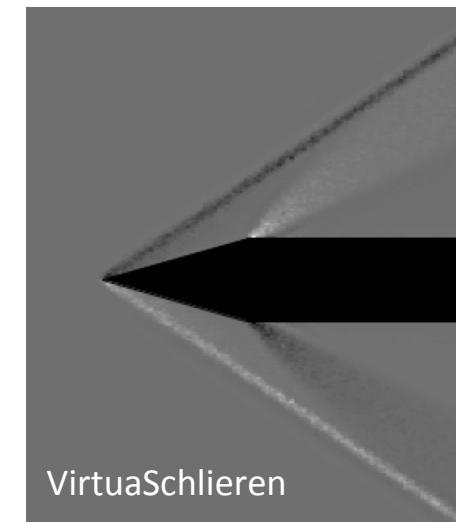
Photo Courtesy of NASA Glenn

PoliMice

What's next: algorithms



- Two-phase flow solver
- Robust schemes for CP flows
- Lagrangian particle tracking
- Multi-species solver
- Virtual Schlieren for non-ideal fluids
- Speed-up TMD
 - Look-Up Table
 - Inversion of $\psi(T, v)$
 - Hybrid LUT



Conclusions

- SU2 is now a fully capable NICFD solver for three-dimensional complex geometry
- It embeds state-of-the-art thermodynamic models for pure fluids and mixtures, which are relevant to diverse applications, ranging for ORC and scCO₂ power systems to refrigeration
- NICFD development within SU2 is supported by a strong team and funded via numerous projects on fundamental science (ERC, Marie-Curie, NWO) and strong industrial partnership
- Preliminary validation against experimental data from the TROVA test-rig confirms the accuracy of the NICFD tool set

Conclusions

Thank you for your attention!
Question?

CREA Lab @Polimi: crealab.polimi.it

Propulsion & Power Group @TUDelft: www.lr.tudelft.nl

Download SU2 from GitHub: <https://github.com/su2code/SU2>

