

Physical World 1D Final Report

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I. OBJECTIVES

To incorporate the following design considerations in designing a cooling system for a thermoelectric cooler, in order to cool an aluminium block to 7 Degree Celsius in 5 minutes:

- 1) Ensure effective cooling at the hot side of the Peltier chip, reducing delta T to increase the efficiency of the Peltier chip, with the use of forced air convection by fan.
- 2) Insulate the cool side of the Peltier chip and attached aluminium block to reduce heat gain from surrounding.

Our design includes a wind tunnel that directs the cold air from a fan attached to it towards the heat sink placed above the hot side of the Peltier chip. The heat sink is used to draw heat away from the hot side of the Peltier, together with the cold air directed by the wind tunnel. Additionally, the wind tunnel minimizes the change in air density, decreasing cross-sectional area and resulting in an increase in velocity. With that, cooling of the hot side of Peltier would increase, increasing the efficiency of the Peltier to cool the aluminium blocks within 5 minutes

II. MODELLING THE SYSTEM WITH PYTHON

Due to the complicated nature of the thermal system, a Python program was written to perform numerical analysis (Runge-Kutta Method) on the refrigerator to better predict the performance of the proposed design. (See attached Python file) It takes into account:

- 1) Heat capacity of the refrigerator's components, and hence varying temperatures of the hot and cold sides
- 2) Conduction of heat through the refrigerator's components
- 3) Conductive heat loss from the heat sink
- 4) Current I through the TEC as a function of T_c and T_h

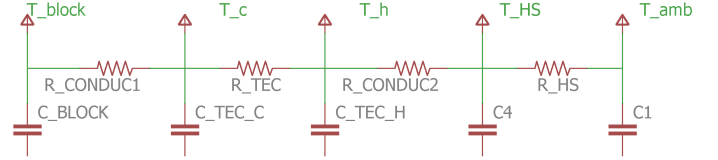


Fig. 1: Thermal Circuit Diagram of Refrigerator

Based on the thermal circuit diagram above, it can be seen that there are components in the system that have significant heat capacities. Furthermore, since there is a maximum voltage allowable, we cannot model the system as having a constant current. The current I therefore is modelled as a function of T_h and T_c , the other parameters being constant. Hence, the following equations were used to model the system.

- 1) $V = S_e(T_h - T_c) + IR \Rightarrow I = \frac{V - S_e(T_h - T_c)}{R}$
- 2) $\dot{Q} = S_e I T_c - \frac{I^2 R}{2} - \lambda(T_h - T_c)$
- 3) $\dot{Q} = mc\dot{T}$

Simulations were ran for $0s \leq t \leq t_f$, with a discrete time step of $\frac{t_f}{100000}$, where $t_f = 300s$. with a time It was found that it was possible to reach $7^\circ C$ within $78s$. The minimum temperature achieved after $300s$ is $3.20^\circ C$. The maximum temperature reached by the hot side is $35.29^\circ C$. Below is a summary of the simulation parameters.

Parameter	Value
Ambient Temp	$298.15K$
Heat Sink Mass	$0.045kg$
Heat Sink Surface Area	$0.072m^2$
Air Velocity	$0.4ms^{-2}$
Foam Insulation Thickness	$4mm$
Foam Thermal Conductivity	$0.045Wm^{-1}K^{-1}$
Mass of Aluminium Block	$0.0294kg$
TEC Resistance	2.3Ω
TEC Seebeck Coefficient	$0.042VK^{-1}$
TEC Thermal Conductance	$0.52WK^{-1}$
TEC Applied Voltage	$5.0V$

TABLE I: Simulation Parameters

Below is a graph of the cooling curve of the aluminium block for $0s \leq t \leq 300s$ illustrating the predicted performance of our system. It is observed that the initial cooling rate is large due to the non-zero capacity of the hot side; it takes some time for the hot side to heat up and for heat to conduct through the TEC back to the cold side.

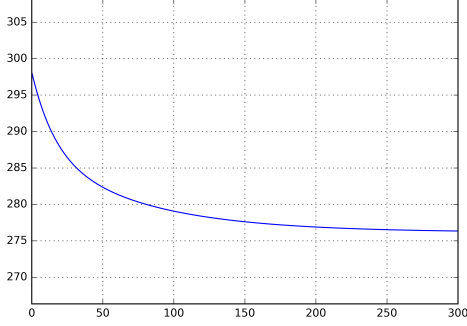


Fig. 2: Cooling curve: T_c/K against Time/s

Below is a graph of the heating curve of the aluminium block for $0s \leq t \leq 300s$ illustrating that the temperature does not reach absolute maximum ratings of the TEC as specified in the datasheet. There is a maximum temperature reached, showing that initially, $\dot{Q}_h = \dot{Q}_c + \dot{W}$ is large, but once the cold side has cooled sufficiently and reached the minimum temperature, then $\dot{Q}_c = 0$, thus T_h asymptotically reaches a steady state value of approximately $33^\circ C$.

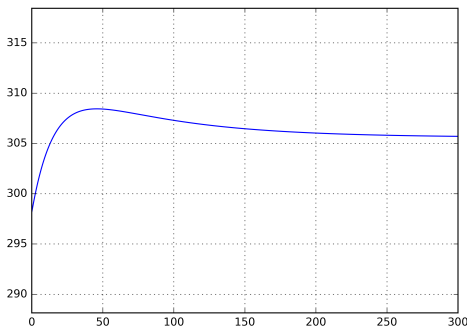


Fig. 3: Heating curve: T_h/K against Time/s

III. DESIGN OF REFRIGERATOR

Based on the simulation that we carried out in Python, we designed a refrigerator according

to or surpassing the parameters as specified in the simulation. A large aluminium heat sink with an approximate area of $720cm^2$ was chosen.

A wind tunnel design was also chosen to increase the air mass flow rate over the aluminium heat sink. Our designed wind tunnel has an inlet area of $0.0144m^2$ and an outlet area of $0.002m^2$.

According to manufacturer specifications, the fan exit velocity is $2.5m/s$ when operated at $12V$. Assuming the fan is operating at 20% power at $5V$, our inlet velocity would thus be $0.5m/s$. Mass Flow Rate, $\dot{m} = \rho AV = (1.184)(0.0144)(0.5) = 0.008525kg/s$, assuming density of air at $25^\circ C$, $c = 1.184kg \cdot m^{-3}$, and no change to temperature inside wind tunnel (laminar flow).

$$\therefore V_{out} = \frac{\dot{m}}{\rho \cdot A_{out}} = \frac{0.008525}{(1.184)(0.002)} = 3.6m/s$$

Based on our research (see references), the heat transfer coefficient of moving air h can be estimated empirically by the equation:

$$\begin{aligned} h &= 10.45 - V_{air} + 10\sqrt{V_{air}} \\ \therefore \dot{Q}_{Convection} &= -hA(T_H - T_{Ambient}) \\ &= (25.824)(0.072)(32 - 25) = 13.02W \end{aligned}$$

IV. SCHEMATICS OF THE REFRIGERATOR DESIGN

The diagram below shows the wind tunnel design chosen to increase mass flow rate of air over the heat sink.

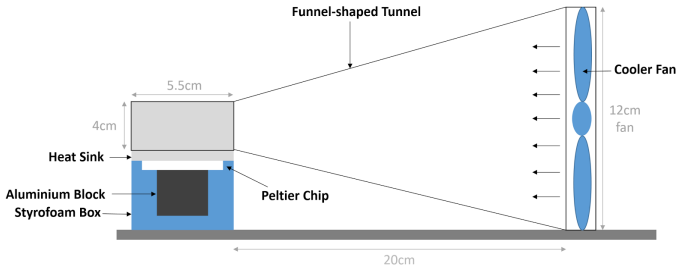


Fig. 4: Heating curve: T_h/K against Time/s

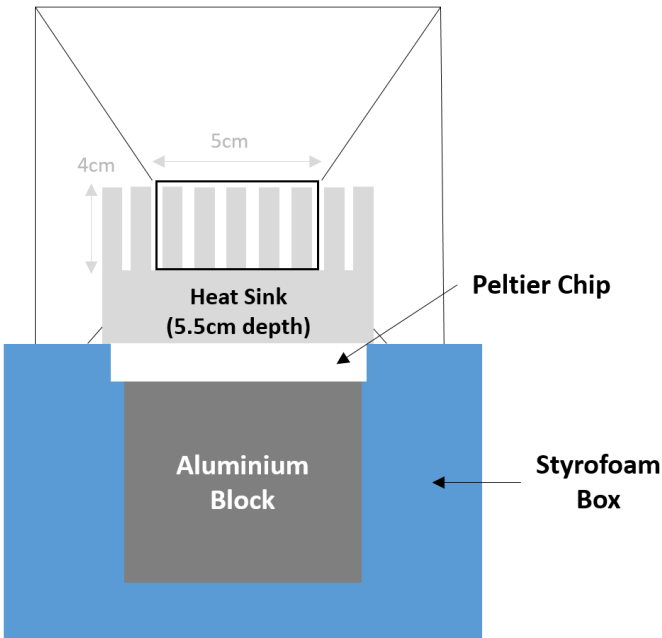


Fig. 5: Cross-section View of Nozzle and Heat Sink Fins

V. EXPERIMENTAL RESULTS

The graph below shows the graph of our experimental setup operating at 5V supply to the TEC. The final temperature attained at $t = 245s$ is $3.6^\circ C$.

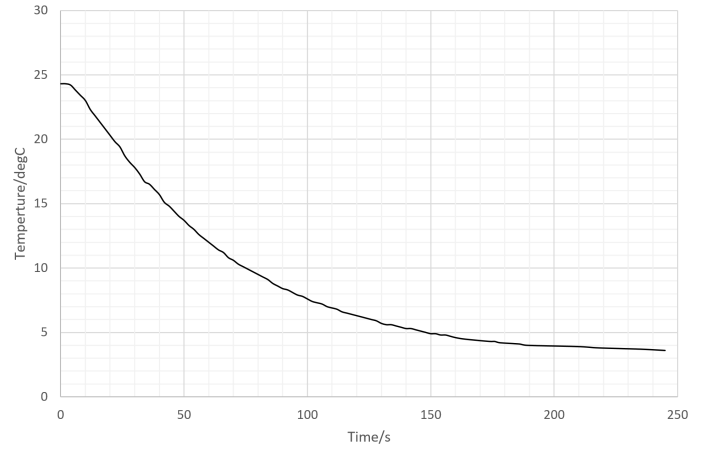


Fig. 6: Actual Cooling Curve: $T_c/^\circ C$ against Time/s

Based on the graph, the initial cooling rate is approximately $-0.21428 K s^{-1}$ which corresponds to $\dot{Q}_c = 0.0294 kg \cdot 900 J kg^{-1} K^{-1} \cdot 0.21428 K s^{-1} = 5.67 W$. This gives an initial Coefficient of performance $\frac{5.00V \cdot 2.04A}{5.67} = 1.79$

VI. RESULTS AND DISCUSSION

Based on our simulated estimate, the numerical analysis of the refrigerator shows significant correlation with our the empirical data, as the actual minimum temperature reached by our experiment is $3.6^\circ C$, while the simulation predicts the final temperature to be $3.6^\circ C$.

However, the actual setup reached $7^\circ C$ only at 108 seconds, whereas the simulation predicts the setup to reach $7^\circ C$ in 78 seconds. This may perhaps be due to the incorrect predicted parameters of the TEC's electrical resistance, thermal conductance and Seebeck coefficient.

VII. YOUTUBE LINK OF THE VIDEO

<https://youtu.be/wcEqXpmNJk4>

VIII. REFERENCES

http://www.engineeringtoolbox.com/convective-heat-transfer-d_430.html