The Impact of Inter-Pin Spatial Self-Shielding on Pin-Wise Reaction Rates

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Abstract

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1. Introduction

Signficant progress has been made in recent years to develop deterministic neutron transport-based tools for full-core reactor analysis (Gunow et al., 2017; Ryu et al., 2015; Kochunas et al., 2013; Evans et al., 2010; Palmiotti et al., 2007). These efforts are motivated by the desire to obtain Monte Carlo-quality solutions with computationally efficient multi-group methods. The focal point for much of this work has been the implementation and analysis of parallel algorithms to make full-core analysis feasible on large computing machines. However, much work remains to develop methods for multi-group cross section (MGXS) generation that enable multi-group transport codes to achieve sufficient predictive accuracy to complement (or replace) analysis with continuous energy Monte Carlo methods.

A two-pronged approach is needed to generate MGXS which enable Monte Carlo-quality solutions with multi-group methods. First, the approximation errors inherent to multi-group transport methods must be rigorously isolated and quantified by benchmarking multi-group transport with continuous energy Monte Carlo methods on fully-detailed heterogeneous benchmarks. These approximation errors may take on more (or less) relevance than they did for validation of the coarse-mesh multi-group diffusion-based codes used today. Second, the quantifiable results from these analyses should inform the development of solutions that rectify biases observed between multi-group and continuous energy transport methods.

This paper specifically investigates approximation error due to the effects of spatial self-shielding in Pressurized Water Reactors (PWRs) on multi-group cross sections. The effects of neighboring pins, control rod guide tubes, burnable poisons, water reflectors and the core baffle are each of interest in the context of spatial self-shielding. In particular, this paper quantifies the difference in the approximation error between simulations in which the same MGXS are used for each unique fuel pin *composition* (*e.g.*, each fuel enrichment), and those in which unique MGXS are used in each *instance* of each fuel pin throughout a core geometry. The former approach does little to model spatial self-shielding effects beyond those accounted for by an infinite fuel pin lattice model, while the latter goes much further to resolve inter-pin spatial self-shielding effects, albeit at the expense of much larger MGXS libraries.

This work employs Monte Carlo (MC) neutron transport simulations to generate MGXS. Monte Carlo methods have increasingly been used to generate few group constants for coarse mesh diffusion, most notably by the Serpent MC code (Leppänen, 2013), and to a much lesser extent, for high-fidelity neutron transport methods (Redmond, 1997; Nelson, 2014; Cai, 2014; Boyd, 2016). The advantage of a MC-based approach is that all of the relevant physics are directly embedded into MGXS by weighting the continuous energy cross sections with a statistical proxy to the true neutron scalar flux. This paper replaces the traditional multi-step approach to MGXS generation with a single Monte Carlo eigenvalue calculation of the complete benchmark geometry to generate MGXS for each fuel pin instance. Furthermore, the same MC calculation is used to compute a reference solution to benchmark the approximate solution from a multi-group code and to quantify the significance of spatially self-shielded MGXS.

The content in this paper is organized as follows. The methodology used to generate MGXS is discussed in Sec. 2. The simulation tools for continuous energy Monte Carlo simulations with OpenMC, and deterministic multi-group calculations with OpenMOC, are discussed in Sec. 3. Two heterogeneous PWR benchmarks used are presented in Sec. 4 to evaluate the efficacy of the spatial self-shielding models in Sec. 5. The need for a new, flexible approach to spatial homogenization which appropriately captures spatial self-shielding effects with minimal computational expense is discussed in Sec. 6.

2. MGXS Generation

This paper uses Monte Carlo to generate MGXS for deterministic methods. The single-step framework used to generate MGXS from Monte Carlo is discussed in Sec. 2.1. The two pin-wise spatial homogeniation schemes used to quantify approximation error due to inter-pin spatial self-shielding model are introduced in Sec. 2.2.

2.1. A Single-Step Framework

In general, MGXS generation schemes use a multi-step approach to decouple the energy, angular and spatial dimensions of the transport equation. The multi-step approach typically applies high-fidelity models of the energy self-shielding

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physics to low-fidelity geometric models of unique core components. The multi-step approach uses a combination of models of varying complexity to optimize overall simulation speed with accuracy. However, this is often done at the expense of generality. For example, multi-step MGXS generation schemes do not typically model inter-assembly physics or the effect of reflectors and other core heterogeneities on the spatial distribution of the flux. Instead, geometric heuristics are often used to embed spatial self-shielding effects in MGXS for similarly shielded spatial zones (*e.g.*, fuel pins with similar neighboring pins). The approximations to the energy and spatial variation of the flux introduce approximation error in full-core calculations and limit the core design parameter space for which multi-level schemes may be applied.

This work abandons the multi-step approach in favor of a single-step framework. Furthermore, this work employs Monte Carlo methods to generate MGXS since it presents a natural approach to replace engineering prescriptions to approximate the flux with a stochastic approximation of the exact flux. However, MC-based MGXS generation methods to date have retained the multi-step geometric framework to tabulate MGXS for individual reactor components – such as infinite fuel pins and/or assemblies – for subsequent use in full-core multi-group calculations. Although the use of MC within a multi-step framework eliminates the need to approximate the flux in energy, it does not account for spatial self-shielding effects throughout a reactor core.

This work takes an additional step and uses MC eigenvalue simulations of the complete heterogeneous geometry to simultaneously account for all energy and spatial effects in a single step. The single-step framework may be impractical for MGXS generation for industrial applications since it is constrained by the slow convergence rate of Monte Carlo tallies. Nevertheless, it allows for the rigorous quantification of approximation error due to spatial self-shielding models used to generate MGXS, which is the focal point of this paper.

2.2. Pin-wise Spatial Self-Shielding Models

This paper employs two different spatial homogenization schemes to model spatial self-shielding effects in MGXS. Although all spatial zones may experience spatial self-shielding, this chapter only models the impact of spatial self-shielding on MGXS in fissile regions. The null and degenerate spatial homogenization schemes are introduced in Sec. 2.2.1 and Sec. 2.2.2, respectively. These schemes model spatial self-shielding for each fuel pin with increasing granularity and complexity.

2.2.1. Null Spatial Homogenization

The *null* spatial homogenization scheme uses a single Monte Carlo calculation of the complete heterogeneous geometry to generate MGXS for each material. The spatially self-shielded flux is used to collapse the cross sections in each material with a unique isotopic composition. The null scheme does not account for spatial self-shielding effects experienced by different fuel pins filled by the same fuel composition, and instead averages these effects across the entire geometry. A single MGXS is employed in each instance of a material zone, such as a fuel pin replicated many times throughout a benchmark geometry. The null scheme serves as the base case in this paper to illustrate the approximation error which results when inter-pin spatial self-shielding effects are neglected, even when the exact flux from Monte Carlo is used to collapse continuous energy cross sections.

2.2.2. Degenerate Spatial Homogenization

The *degenerate* spatial homogenization scheme accounts for spatial self-shielding effects experienced by each instance of each fuel pin throughout a heterogeneous geometry. Like the null scheme, a single MC calculation of the complete heterogeneous geometry is used to generate MGXS for all materials. Unlike the null scheme, the MGXS are tallied separately for each instance of fissile material zones. For example, if a heterogeneous benchmark includes N fuel pins, then N collections of MGXS are separately tabulated for each fuel pin instance. The degenerate scheme tallies different MGXS even if the isotopic compositions in the fuel pin instances are identical, since each instance may experience different spatial self-shielding effects and hence have different MGXS. The degenerate scheme demonstrates the reduction in approximation error between multi-group and continuous energy transport methods that can be achieved when inter-pin spatial self-shielding effects are sufficiently modeled in MGXS.

3. Simulation Tools

This work employed both continuous energy and multi-group neutron transport codes. The OpenMC Monte Carlo code (Romano and Forget, 2013) was generated multi-group cross sections and reference solutions as discussed in Sec. 3.1. The MGXS generated by OpenMC were used by the OpenMOC code (Boyd et al., 2014) for deterministic multi-group transport calculations as highlighted in Sec. 3.2.

3.1. Continuous Energy Calculations with OpenMC

The OpenMC continuous energy Monte Carlo (MC) code (Romano and Forget, 2013) was employed to generate multi-group cross sections, and reference eigenvalues and pin-wise fission and capture reaction rates. The `openmc.mgxs` Python module was used to tally multi-group cross sections in CASMO's seventy energy group structure (Rhodes et al., 2006) from a single eigenvalue calculation. The multi-group cross sections were calculated with OpenMC's distributed cell tally algorithm (Lax et al., 2014), which permits spatial tally zones across repeated cell instances. In particular, unique MGXS were computed for each fuel pin cell with distributed cell tallies (Lax et al., 2014) in the repeating lattice benchmarks described in Sec. 4. The OpenMC simulations were performed with 1000 batches with 10^6 particle histories per batch for each benchmark. Stationarity of the fission source was obtained with 100 inactive batches for each benchmark.

The OpenMC simulations used the "iso-in-lab" feature to enforce isotropic in lab scattering. The "iso-in-lab" feature

samples the outgoing neutron energy from the scattering laws prescribed by the continuous energy cross section library, but the outgoing neutron direction of motion is sampled from an isotropic in lab distribution. Although isotropic in lab scattering is a poor approximation for LWRs, it eliminated scattering source anisotropy as one possible cause of approximation error between OpenMC and OpenMOC. This simplification made it possible to isolate the approximation error resulting from the spatial self-shielding model used to generate MGXS.

3.2. Multi-Group Calculations with OpenMOC

The OpenMOC code (Boyd et al., 2014) was employed to use the MGXS generated by OpenMC for deterministic multi-group calculations. The OpenMOC code is a 2D method of characteristics code designed for fixed source and eigenvalue neutron transport calculations. OpenMOC approximates the scattering source as isotropic in the lab coordinate system, and discretizes the geometry into flat source regions (FSRs) which approximate the neutron source as constant across each spatial zone. The OpenMOC eigenvalue and energy-integrated, pin-wise reaction rates were compared with the reference solution computed by OpenMC.

Each OpenMOC simulation used a characteristic track laydown with 128 azimuthal angles and 0.05 cm spacing. All eigenvalue calculations were converged to 10^{-5} on the root mean square of the energy-integrated fission source in each FSR. The Coarse Mesh Finite Difference (CMFD) acceleration scheme was employed on a pin-wise spatial mesh to reduce the number of iterations required to converge the fine-mesh transport calculations. The 70-group MGXS used for MOC were collapsed to a 14-group structure for CMFD to significantly improve the speed of the CMFD eigenvalue calculations.

4. Test Cases and Reference Results

This paper modeled two test cases derived from the Benchmark for Evaluation And Validation of Reactor Simulations (BEAVRS) PWR model (Horelik et al., 2013). Each test case includes heterogeneous features – and corresponding spatial self-shielding effects – in order to understand their implications for accurate pin-wise MGXS generation. Although BEAVRS is an axially heterogeneous 3D core model, both benchmarks were fabricated in 2D due to the geometric constraints in OpenMOC. The impact of fuel enrichment, control rod guide tubes (CRGTs), burnable poisons (BPs), inter-assembly currents and water reflectors is considered. The geometric and material specifications for the two test cases are summarized in Sec. 4.1. The reference results computed with OpenMC are discussed in Sec. 4.2.

4.1. Benchmark Configurations

The two test cases were comprised of materials from the BEAVRS model, including 1.6% and 3.1% enriched UO_2 fuel, borated water[1], zircaloy, helium, air, borosilicate glass and stainless steel. The densities and isotopic compositions for each material are detailed in the BEAVRS specifications (Horelik et al., 2013). Each material was modeled with cross sections from the ENDF/B-VII.1 continuous energy cross section library (X-5 Monte Carlo Team, 2003) evaluated at 600K for hot zero power conditions.

The first benchmark was a single fuel assembly with an array of 264 fuel pins of 1.6% enriched UO_2 fuel with zircaloy cladding and a helium gap. The assembly included 24 CRGTs filled by borated water and surrounded by zircaloy cladding, and a central instrument tube filled with air surrounded by two zircaloy tubes separated by borated water. The intra-pin grid spacer and grid sleeve separating each assembly in the BEAVRS model were not included in the assembly benchmark. The assembly was modeled with reflective boundary conditions. The fuel assembly benchmark is illustrated for null and degenerate spatial homogenization in Fig. 2.

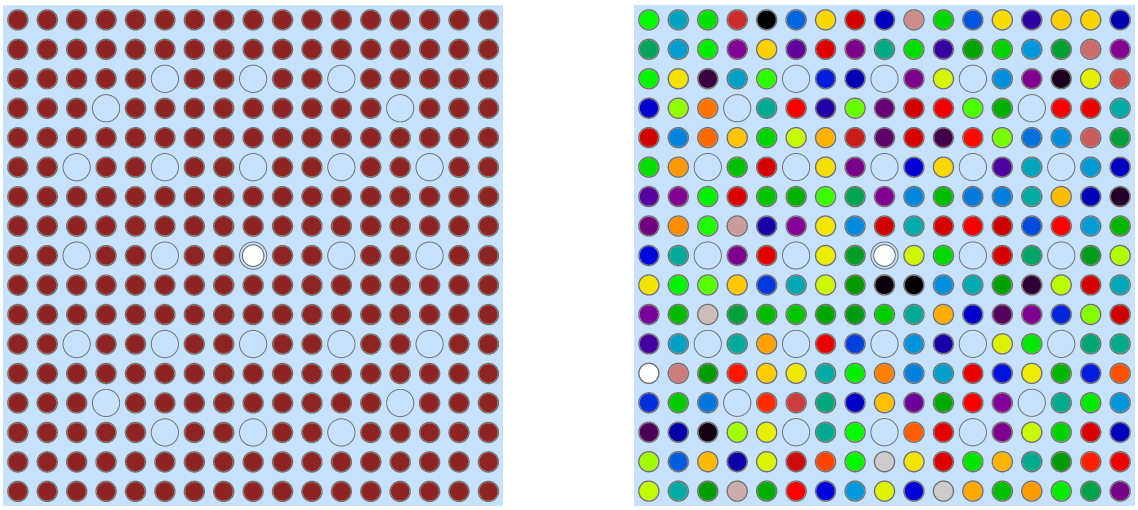
The second benchmark was constructed as a 2×2 colorset of two fuel assemblies extracted from the BEAVRS model. The top-left and bottom-right fuel assemblies in the colorset were of the same enrichment and configuration as the first benchmark configuration. The top-right and bottom-left fuel assemblies included 264 fuel pins of 3.1% enriched UO_2 fuel, 20 CRGTs and a central instrument tube. In addition, the two 3.1% enriched assemblies included four BPs consisting of eight layers of air, steel, borosilicate glass and zircaloy. The colorset was surrounded by a water reflector on the bottom and right that was of the same width as a fuel assembly. The colorset was modeled with reflective boundaries on the top and left and vacuum boundaries on the bottom and right. The colorset benchmark is illustrated for null and degenerate spatial homogenization in Fig. 2.

Flat source region spatial discretization meshes were applied to both benchmarks for the OpenMOC simulations as shown in Fig. 3. The UO_2 fuel was subdivided into five equal volume radial rings, while ten radial rings were employed in the water-filled CRGTs and instrument tubes. The borosilicate glass and borated water material zones filling the BPs were each discretized into five equal volume radial rings. Five equally spaced rings were used in the moderator zones surrounding each pin. Eight equal angle subdivisions were used in all pin cell material zones. The 13.85824 cm of water reflector nearest the fuel assemblies in the colorset benchmark was discretized in a 0.125984 cm × 0.125984 cm rectilinear mesh, equivalent to a 10×10 mesh in each pin. The 7.55904 cm of reflector furthest from the fuel assemblies was discretized in a 1.25984 cm × 1.25984 cm pin-wise mesh.

4.2. Verification Metrics

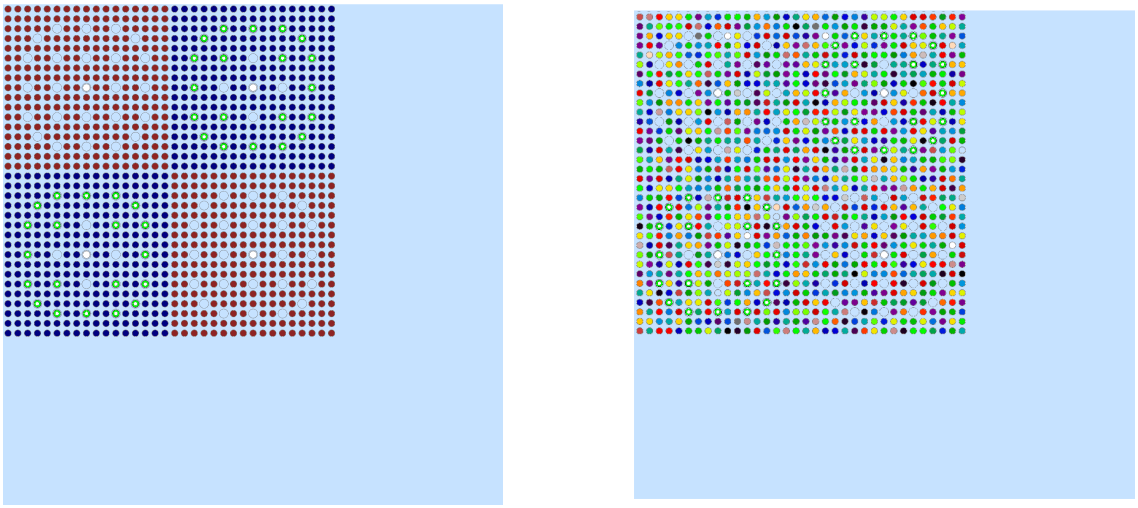
A series of OpenMC simulations were used to calculate reference eigenvalues, pin-wise fission rates, and pin-wise U-238 capture rates for both benchmarks. The reference solutions were computed with 100 inactive and 900 active batches of 10^7 particle histories per batch. The reference eigenvalues are listed in Tab. 1. The OpenMC "combined" eigenvalue estimator is reported along with the associated 1-sigma uncertainty of one pcm for both test cases.

[1]The water consisted of 975 parts per million (ppm) boron.



(a) (b)

Figure 1. OpenMOC materials for the assembly with null (a) and degenerate (b) homogenization.



(a) (b)

Figure 2. OpenMOC materials for the colorset with null (a) and degenerate (b) homogenization.

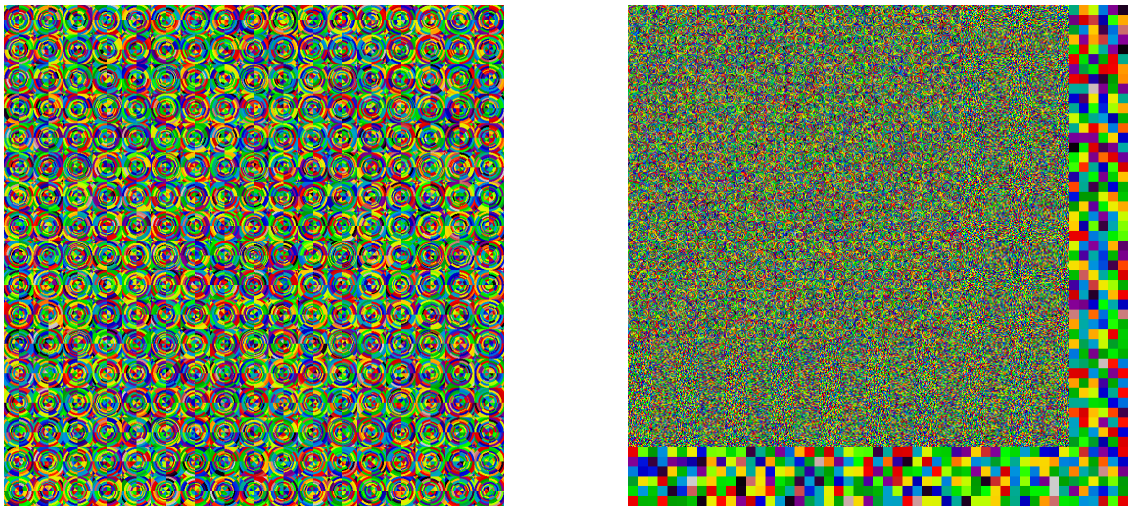
Table 1. Reference OpenMC eigenvalues for each benchmark.

Assembly	Colorset
0.99326 ± 0.00001	0.94574 ± 0.00001

The reference energy-integrated fission and U-238 capture rate spatial distributions were computed using rectilinear, pin-wise tally meshes in OpenMC and are shown in Fig. 4. The reaction rates were volume-integrated across each fuel pin. The fission rates include fission from only U-235 and U-238 for the fresh PWR UO_2 fuel. The reaction rates were normalized to the mean of all non-zero reaction rates in each benchmark. The reaction rates in the instrument tubes, CRGTs and BPs are all zero and are illustrated in white. The 1-sigma uncertainties are less than 0.08% in each pin for each benchmark.

As illustrated in the figures, the reaction rate rate distributions are strongly dependent on the spatially heterogeneous features in each benchmark. For example, the CRGTs provide additional moderation and increase the fision and U-238 capture rates in nearby fuel pins. The inclusion of BPs reduces the neutron population and therefore the reaction rates for the surrounding fuel pins. The presence of a reflector with a mixture of vacuum and reflective BCs induces a tilt in the reaction rates across the assemblies in the colorset.

Although spatial heterogeneities generally have similar effects on both fission and U-238 capture rates, there are a few important differences to note. The U-238 capture rates in the assemblies are more sensitive than the fission rates to the spatial self-shielding induced by moderation in CRGTs. In addition, the capture rates in the colorset are more smoothly varying at the inter-assembly and assembly-reflector inter-



(a) **(b)**

Figure 3. FSRs for the assembly (a) and colorset (b) benchmarks.

facea than the fission rates.

5. Results

Both benchmarks were modeled with OpenMOC using MGXS generated by OpenMC for the null and degenerate spatial homogenization schemes. The eigenvalues and pin-wise fission and U-238 capture rates computed by OpenMOC are compared to the reference OpenMC solutions in Sec. 5.1, Sec. 5.2 and Sec. 5.3, respectively.

5.1. Eigenvalues

The OpenMOC eigenvalues were compared to the reference OpenMC eigenvalues from Tab. 1. The eigenvalue bias $\Delta\rho$ was calculated by comparing the eigenvalue k_{eff}^{MOC} from OpenMOC to the reference eigenvalue k_{eff}^{MC} computed by OpenMC in units of pcm:

$$\Delta\rho = \left(k_{eff}^{MOC} - k_{eff}^{MC}\right) \times 10^5 \quad (1)$$

The bias is listed for both benchmarks and spatial homogenization schemes in Tab. 2. The slightly negative bias of a few hundred pcm is likely due to the flux separability approximation (Boyd et al., 2017), which permits use of the scalar rather than the angular neutron flux to collapse cross sections. The eigenvalues for the null and degenerate schemes are identical for the fuel assembly and are consistent to within 10 pcm for the colorset benchmark. As these results show, the choice of null or degenerate spatial homogenization schemes is inconsequential to the eigenvalue predictions. This is to be expected since the two methods uses the same MC flux to collapse the MGXS and preserve global reactivity.

5.2. Fission Rates

5.3. Capture Rates

-add figures of spatial distribution of errors

Table 2. OpenMOC eigenvalue bias $\Delta\rho$.

Benchmark	Null	Degenerate
Assembly	-161	-161
Colorset	-142	-132

Table 3. OpenMOC fission rate percent relative errors.

Benchmark	Metric	Null	Degenerate
Assembly	Max	0.380	0.315
	Mean	0.074	0.079
Colorset	Max	0.764	0.602
	Mean	0.178	0.138

Table 4. OpenMOC U-238 capture rate percent relative errors.

Benchmark	Metric	Null	Degenerate
Assembly	Max	-1.101	0.386
	Mean	0.479	0.086
Colorset	Max	-1.969	-0.783
	Mean	0.478	0.165

6. Conclusions

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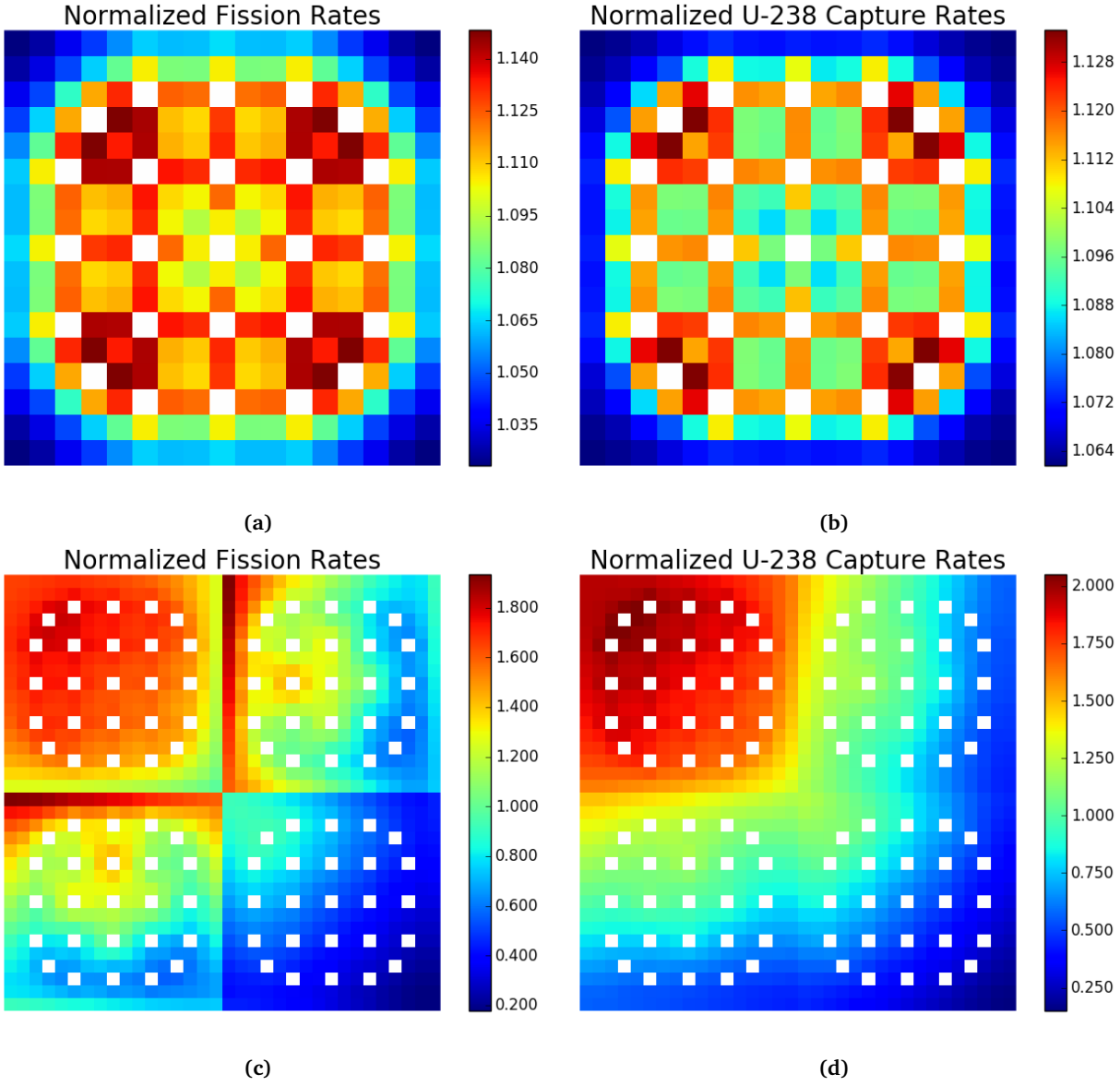

Figure 4. Reference OpenMC fission and U-238 capture rates for the assembly (a) – (b) and colorset (c) – (d) benchmarks.

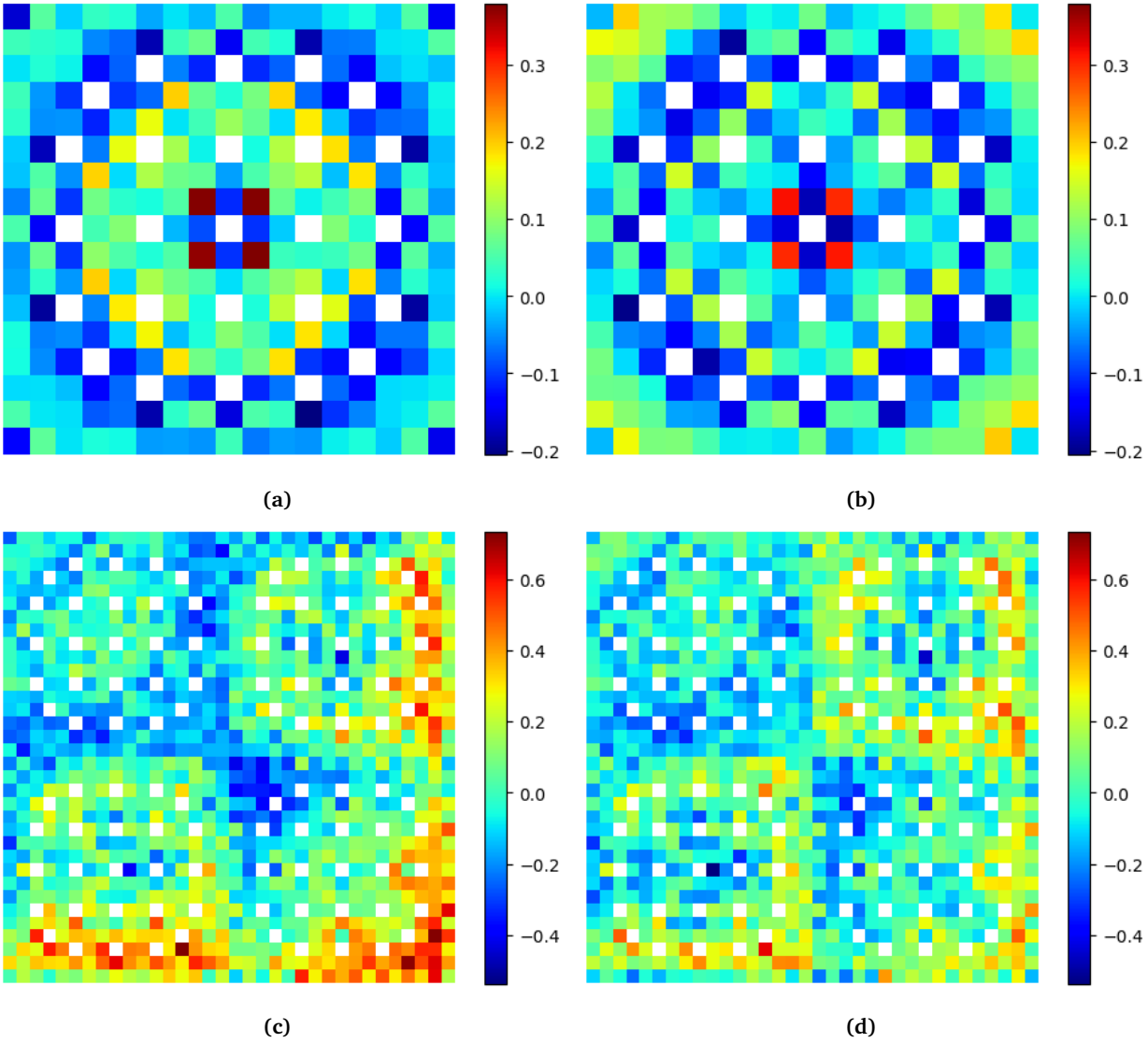

Figure 5. OpenMOC fission rate percent relative errors for the (a) assembly and (b) 2×2 colorset models.

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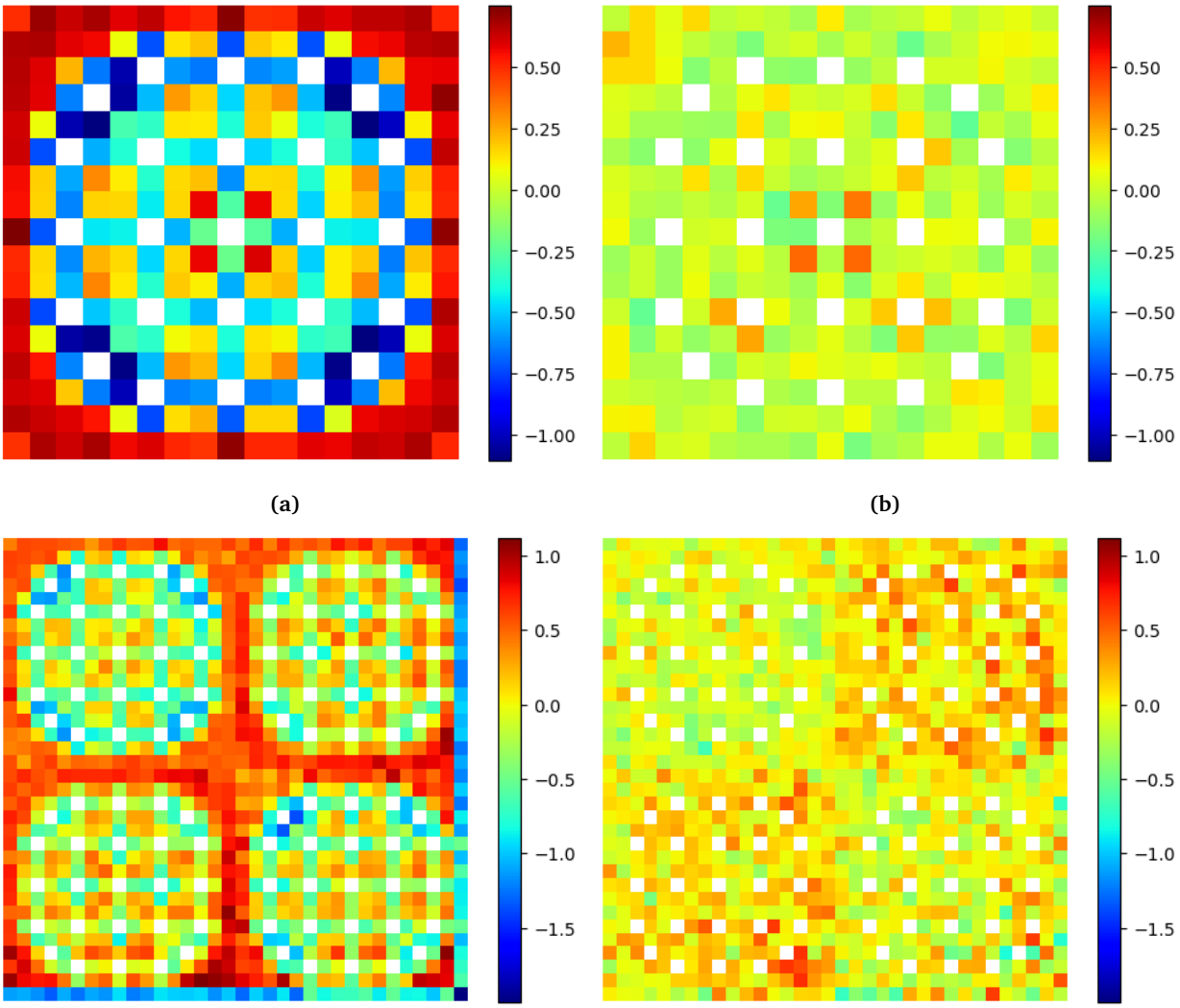

Figure 6. OpenMOC U-238 capture rate percent relative errors for the (a) assembly and (b) 2×2 colorset models.