

Member *ed*:

$$[k]:$$

$$200 \begin{bmatrix} u_e & v_e & \theta_{ze} & u_d & v_d & \theta_{zd} \\ 0.0048 & 0 & -12.00 & -0.0048 & 0 & -12.00 \\ & 0.800 & 0 & 0 & -0.800 & 0 \\ & & 0.4 \times 10^5 & 12.00 & 0 & 0.2 \times 10^5 \\ & & & 0.0048 & 0 & 12.00 \\ \text{Sym.} & & & & 0.800 & 0 \\ & & & & & 0.4 \times 10^5 \end{bmatrix}$$

Assembled global stiffness equation:

$$[P_{xx} \ P_{xy} \ P_{mx} \ P_{yx} \ P_{yy} \ P_{my} \ P_{xc} \ P_{yc} \ P_{mx} \ P_{xd} \ P_{yd} \ P_{md} \ P_{xe} \ P_{ye} \ P_{me}]^T =$$

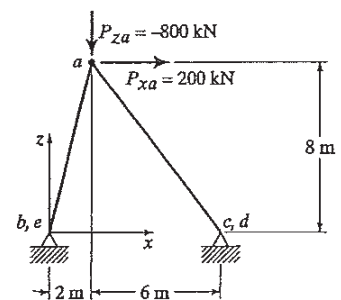
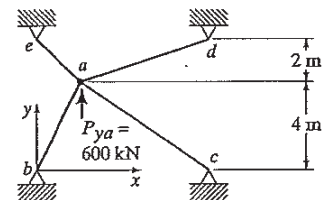
$$200 \begin{bmatrix} u_a & v_a & \theta_{za} & u_b & v_b & \theta_{zb} & u_c & v_c & \theta_{zc} & u_d & v_d & \theta_{zd} & u_e & v_e & \theta_{ze} \\ 0.0048 & 0 & -12.00 & -0.0048 & 0 & -12.00 & & & & & & & & & \\ & 0.800 & 0 & 0 & -0.800 & 0 & & & & & & & & & \\ & & 0.4 \times 10^5 & 12.00 & 0 & 0.2 \times 10^5 & & & & & & & & & \\ & & & 0.6500 & 0.2591 & 4.969 & -0.6452 & -0.2591 & -7.0313 & & & & & & \\ & & & & 0.9095 & 17.381 & -0.2591 & -0.1095 & 17.381 & & & & & & \\ & & & & & 1.4 \times 10^5 & 7.0313 & -17.381 & 0.5 \times 10^5 & & & & & & \\ & & & & & & 1.1589 & -0.1226 & 14.231 & -0.5137 & 0.3817 & 7.200 & & & \\ & & & & & \text{Sym} & & 0.4006 & -7.781 & 0.3817 & -0.2911 & 9.600 & & & \\ & & & & & & & & 1.4 \times 10^5 & -7.200 & -9.600 & 0.2 \times 10^5 & & & \\ & & & & & & & & & 0.5185 & -0.3817 & 4.80 & -0.0048 & 0 & 12.00 \\ & & & & & & & & & & 1.0911 & -9.60 & 0 & -0.800 & 0 \\ & & & & & & & & & & & 0.8 \times 10^5 & -12.00 & 0 & 0.2 \times 10^5 \\ & & & & & & & & & & & & 0.0048 & 0 & -12.00 \\ & & & & & & & & & & & & & 0.800 & 0 \\ & & & & & & & & & & & & & & 0.4 \times 10^5 \end{bmatrix} \begin{bmatrix} u_a \\ v_a \\ \theta_{za} \\ u_b \\ v_b \\ \theta_{zb} \\ u_c \\ v_c \\ \theta_{zc} \\ u_d \\ v_d \\ \theta_{zd} \\ u_e \\ v_e \\ \theta_{ze} \end{bmatrix}$$

EXAMPLE 5.4

A pin-jointed space truss is supported and loaded as shown. $E = 200,000$ MPa. Bar areas are:

$$\begin{aligned} A_{ab} &= 20 \times 10^3 \text{ mm}^2 \\ A_{ac} &= 30 \times 10^3 \text{ mm}^2 \\ A_{ad} &= 40 \times 10^3 \text{ mm}^2 \\ A_{ae} &= 30 \times 10^3 \text{ mm}^2 \end{aligned}$$

1. Calculate the displacement at *a*.
2. Calculate the reactions.



Develop the three-dimensional stiffness matrix for an axial force member. Stating Equation 4.34 in the local coordinates shown and eliminating all irrelevant degrees of freedom,

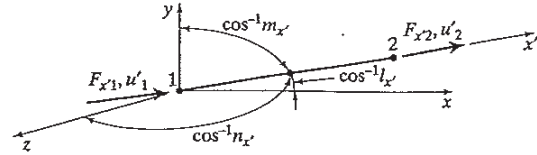
$$\begin{Bmatrix} F_{x'1} \\ F_{x'2} \end{Bmatrix} = \frac{EA}{L} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix} \begin{Bmatrix} u'_1 \\ u'_2 \end{Bmatrix} = [k'] \begin{Bmatrix} u'_1 \\ u'_2 \end{Bmatrix}$$

In Equation 5.7 delete all columns except those corresponding to F_{x1} , F_{y1} , F_{z1} , F_{x2} , F_{y2} , and F_{z2} and all rows except those corresponding to $F_{x'1}$ and $F_{x'2}$ (compare Example 5.1) yielding

$$[\Gamma] = \begin{bmatrix} l_{x'} & m_{x'} & n_{x'} & 0 & 0 & 0 \\ 0 & 0 & 0 & l_{x'} & m_{x'} & n_{x'} \end{bmatrix}$$

Using Equation 5.16, $[k] = [\Gamma]^T [k'] [\Gamma]$,

$$[k] = \frac{EA}{L} \begin{bmatrix} u_1 & v_1 & w_1 & u_2 & v_2 & w_2 \\ \begin{bmatrix} l_{x'}^2 & l_{x'}m_{x'} & l_{x'}n_{x'} \\ m_{x'}^2 & m_{x'}n_{x'} & n_{x'}^2 \end{bmatrix} & \begin{bmatrix} -l_{x'}^2 & -l_{x'}m_{x'} & -l_{x'}n_{x'} \\ -l_{x'}m_{x'} & -m_{x'}^2 & -m_{x'}n_{x'} \\ -l_{x'}n_{x'} & -m_{x'}n_{x'} & -n_{x'}^2 \end{bmatrix} \\ \text{Sym} & \begin{bmatrix} l_{x'}^2 & l_{x'}m_{x'} & l_{x'}n_{x'} \\ m_{x'}^2 & m_{x'}n_{x'} & n_{x'}^2 \end{bmatrix} \end{bmatrix}$$



1. **Displacements.** Record direction cosines for each member. Locate local origin for each member at a .

Member	x	y	z	L	$l_{x'}$	$m_{x'}$	$n_{x'}$
ab	-2	-4	-8	9.165	-0.2182	-0.4364	-0.8729
ac	6	-4	-8	10.770	0.5571	-0.3714	-0.7428
ad	6	2	-8	10.198	0.5883	0.1961	-0.7845
ae	-2	2	-8	8.485	-0.2357	0.2357	-0.9428

Record direction cosine products multiplied by A/L . (Values of A/L are in mm.)

Member	(A/L)	\times	$l_{x'}^2$	$m_{x'}^2$	$n_{x'}^2$	$l_{x'}m_{x'}$	$l_{x'}n_{x'}$	$m_{x'}n_{x'}$
ab	2.182		0.1034	0.4156	1.663	0.2078	0.4156	0.8312
ac	2.785		0.8643	0.3841	1.537	-0.5762	-1.1525	0.7683
ad	3.922		1.3574	0.1508	2.414	0.4524	-1.8101	-0.6034
ae	3.536		0.1964	0.1964	3.143	-0.1964	0.7858	-0.7858
Σ			2.5215	1.1469	8.757	-0.1124	-1.7612	0.2103

Referring to the $[k]$ matrix and adding stiffnesses in the usual way, the global stiffness equations for the nonzero degrees of freedom are

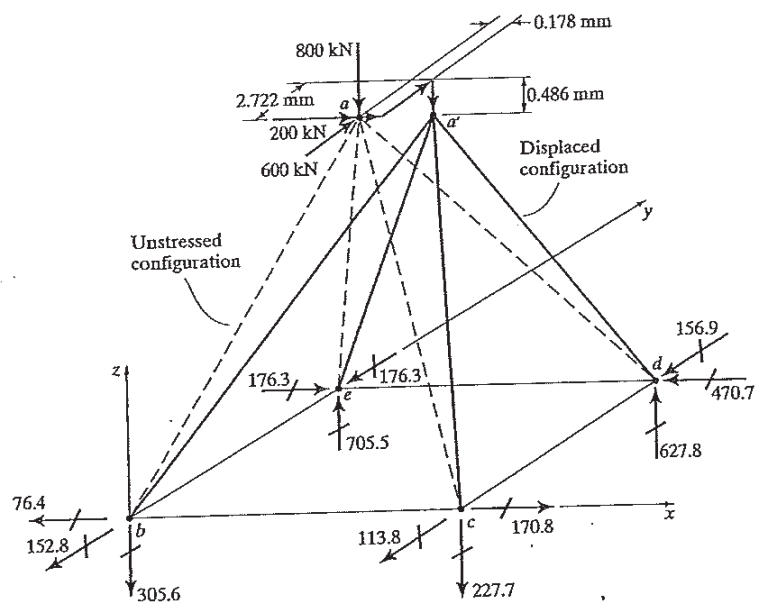
$$\begin{Bmatrix} P_{xa} \\ P_{ya} \\ P_{za} \end{Bmatrix} = \begin{Bmatrix} 200 \\ 600 \\ -800 \end{Bmatrix} = 200 \begin{bmatrix} 2.522 & -0.1124 & -1.7612 \\ & 1.147 & 0.2103 \\ \text{Sym.} & & 8.757 \end{bmatrix} \begin{Bmatrix} u_a \\ v_a \\ w_a \end{Bmatrix}$$

Solving for the displacements,

$$[\Delta] = [u_a \ v_a \ w_a] = [0.1783 \ 2.722 \ -0.4863] \text{ mm}$$

2. *Reactions.* Using the properties of the element stiffness matrices (see above table), the global components of the reactions are

$$\begin{Bmatrix} R_{xb} \\ R_{yb} \\ R_{zb} \\ R_{xc} \\ R_{yc} \\ R_{zc} \\ R_{xd} \\ R_{yd} \\ R_{zd} \\ R_{xe} \\ R_{ye} \\ R_{ze} \\ R_{te} \end{Bmatrix} = -200 \begin{Bmatrix} 0.1034 & 0.2078 & 0.4156 \\ 0.2078 & 0.4156 & 0.8312 \\ 0.4156 & 0.8312 & 1.663 \\ 0.8643 & -0.5762 & -1.1525 \\ -0.5762 & 0.3841 & 0.7683 \\ -1.1525 & 0.7683 & 1.537 \\ 1.3574 & 0.4524 & -1.8101 \\ 0.4524 & 0.1508 & -0.6034 \\ -1.810 & -0.6034 & 2.414 \\ 0.1964 & -0.1964 & 0.7858 \\ -0.1964 & 0.1964 & -0.7858 \\ 0.7858 & -0.7858 & 3.143 \end{Bmatrix} \begin{Bmatrix} -76.4 \\ -152.8 \\ -305.6 \\ 170.8 \\ -113.8 \\ -227.7 \\ -470.7 \\ -156.9 \\ 627.8 \\ 176.3 \\ -176.3 \\ 705.5 \end{Bmatrix} \text{ kN}$$



EXAMPLE 5.5

Find the direction cosines of the member shown. x and z are horizontal; y is vertical. The x' axis is along the member. The $x'y'$ plane makes a dihedral angle of 30° with a vertical plane through the member axis. Demonstrate that the matrix of direction cosines $[\gamma]$ can be generated by three successive rotations.

