



**Autonomous Vehicle Simulation (AVS) Laboratory,
University of Colorado**

Basilisk Technical Memorandum

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DERIVATION OF REACTION WHEEL JITTER BACK-SUBSTITUTION

Prepared by	J. Alcorn, C. Allard
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Scope/Contents
This document derives the back substitution method for reaction wheel jitter to conform with Basilisk's dynamics architecture.

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1 Introduction

The goal is to manipulate the reaction wheel equations of motion to conform to the following form

$$\begin{bmatrix} [A] & [B] \\ [C] & [D] \end{bmatrix} \begin{bmatrix} \ddot{\mathbf{r}}_{B/N} \\ \dot{\boldsymbol{\omega}}_{B/N} \end{bmatrix} = \begin{bmatrix} \mathbf{v}_{\text{trans}} \\ \mathbf{v}_{\text{rot}} \end{bmatrix} \quad (1)$$

Solving the system-of-equations by

$$\dot{\boldsymbol{\omega}}_{B/N} = \left([D] - [C][A]^{-1}[B] \right)^{-1} (\mathbf{v}_{\text{rot}} - [C][A]^{-1}\mathbf{v}_{\text{trans}}) \quad (2)$$

$$\ddot{\mathbf{r}}_{B/N} = [A]^{-1}(\mathbf{v}_{\text{trans}} - [B]\dot{\boldsymbol{\omega}}_{B/N}) \quad (3)$$

2 Balanced Reaction Wheel Back-Substitution

2.1 Equations of Motion

The translational equation of motion is not coupled with $\dot{\boldsymbol{\Omega}}$ as seen in the equation below.

$$m_{\text{sc}}[I_{3 \times 3}]\ddot{\mathbf{r}}_{B/N} - m_{\text{sc}}[\tilde{\mathbf{c}}]\dot{\boldsymbol{\omega}}_{B/N} = \mathbf{F}_{\text{ext}} - 2m_{\text{sc}}[\tilde{\boldsymbol{\omega}}_{B/N}]\mathbf{c}' - m_{\text{sc}}[\tilde{\boldsymbol{\omega}}_{B/N}][\tilde{\boldsymbol{\omega}}_{B/N}]\mathbf{c} \quad (4)$$

The rotational equation of motion includes $\dot{\boldsymbol{\Omega}}$ terms, and is thus coupled with wheel motion as seen below.

$$m_{\text{sc}}[\tilde{\mathbf{c}}]\ddot{\mathbf{r}}_{B/N} + [I_{\text{sc},B}]\dot{\boldsymbol{\omega}}_{B/N} + \sum_{i=1}^N J_{s_i} \hat{\mathbf{g}}_{s_i} \dot{\Omega}_i = -[\tilde{\boldsymbol{\omega}}_{B/N}][I_{\text{sc},B}]\boldsymbol{\omega}_{B/N} - \sum_{i=1}^N (\boldsymbol{\omega}_{B/N} \times J_{s_i} \Omega_i \hat{\mathbf{g}}_{s_i}) + \mathbf{L}_B \quad (5)$$

The motor torque equation can be seen below.

$$\dot{\Omega}_i = \frac{u_{s_i}}{J_{s_i}} - \hat{\mathbf{g}}_{s_i}^T \dot{\boldsymbol{\omega}}_{B/N} \quad (6)$$

2.2 Back-Substitution Derivation

Plugging Eq. (6) into Eq. (5)

$$m_{sc}[\tilde{\mathbf{c}}]\ddot{\mathbf{r}}_{B/N} + ([I_{sc,B}] - \sum_{i=1}^N J_{s_i} \hat{\mathbf{g}}_{s_i} \hat{\mathbf{g}}_{s_i}^T) \dot{\boldsymbol{\omega}}_{B/N} = -[\tilde{\boldsymbol{\omega}}_{B/N}][I_{sc,B}] \boldsymbol{\omega}_{B/N} - \sum_{i=1}^N (\hat{\mathbf{g}}_{s_i} u_{s_i} + \boldsymbol{\omega}_{B/N} \times J_{s_i} \Omega_i \hat{\mathbf{g}}_{s_i}) - [I'_{sc,B}] \boldsymbol{\omega}_{B/N} + \mathbf{L}_B \quad (7)$$

2.3 Back-Substitution Contribution Matrices

The following can be defined:

$$[A_{\text{contr}}] = [0_{3 \times 3}] \quad (8)$$

$$[B_{\text{contr}}] = [0_{3 \times 3}] \quad (9)$$

$$[C_{\text{contr}}] = [0_{3 \times 3}] \quad (10)$$

$$[D_{\text{contr}}] = - \sum_{i=1}^N J_{s_i} \hat{\mathbf{g}}_{s_i} \hat{\mathbf{g}}_{s_i}^T \quad (11)$$

$$\mathbf{v}_{\text{trans,contr}} = \mathbf{0} \quad (12)$$

$$\mathbf{v}_{\text{rot,contr}} = - \sum_{i=1}^N (\hat{\mathbf{g}}_{s_i} u_{s_i} + \boldsymbol{\omega}_{B/N} \times J_{s_i} \Omega_i \hat{\mathbf{g}}_{s_i}) \quad (13)$$

3 Imbalanced Reaction Wheel Back-Substitution

3.1 Equations of Motion

The translational equation of motion is

$$\ddot{\mathbf{r}}_{B/N} - [\tilde{\mathbf{c}}] \dot{\boldsymbol{\omega}}_{B/N} + \frac{1}{m_{sc}} \sum_{i=1}^N m_{rw_i} d_i \hat{\mathbf{w}}_{3_i} \dot{\Omega}_i = \ddot{\mathbf{r}}_{C/N} - 2[\tilde{\boldsymbol{\omega}}_{B/N}] \mathbf{c}' - [\tilde{\boldsymbol{\omega}}_{B/N}][\tilde{\boldsymbol{\omega}}_{B/N}] \mathbf{c} + \frac{1}{m_{sc}} \sum_{i=1}^N m_{rw_i} d_i \Omega_i^2 \hat{\mathbf{w}}_{2_i} \quad (14)$$

The rotational equation of motion is

$$\begin{aligned} m_{sc}[\tilde{\mathbf{c}}]\ddot{\mathbf{r}}_{B/N} + [I_{sc,B}] \dot{\boldsymbol{\omega}}_{B/N} + \sum_{i=1}^N \left([I_{rw_i, W_{c_i}}] \hat{\mathbf{g}}_{s_i} + m_{rw_i} d_i [\tilde{\mathbf{r}}_{W_{c_i}/B}] \hat{\mathbf{w}}_{3_i} \right) \dot{\Omega}_i \\ = \sum_{i=1}^N \left[m_{rw_i} [\tilde{\mathbf{r}}_{W_{c_i}/B}] d_i \Omega_i^2 \hat{\mathbf{w}}_{2_i} - [I_{rw_i, W_{c_i}}]' \Omega_i \hat{\mathbf{g}}_{s_i} - [\tilde{\boldsymbol{\omega}}_{B/N}] \left([I_{rw_i, W_{c_i}}] \Omega_i \hat{\mathbf{g}}_{s_i} + m_{rw_i} [\tilde{\mathbf{r}}_{W_{c_i}/B}] \mathbf{r}'_{W_{c_i}/B} \right) \right] \\ - [\tilde{\boldsymbol{\omega}}_{B/N}][I_{sc,B}] \boldsymbol{\omega}_{B/N} - [I_{sc,B}]' \boldsymbol{\omega}_{B/N} + \mathbf{L}_B \end{aligned} \quad (15)$$

The motor torque equation is

$$\begin{aligned} [m_{rw_i} d_i \hat{\mathbf{w}}_{3_i}^T] \ddot{\mathbf{r}}_{B/N} + [(J_{11_i} + m_{rw_i} d_i^2) \hat{\mathbf{g}}_{s_i}^T + J_{13_i} \hat{\mathbf{w}}_{3_i}^T - m_{rw_i} d_i \hat{\mathbf{w}}_{3_i}^T [\tilde{\mathbf{r}}_{W_i/B}]] \dot{\boldsymbol{\omega}}_{B/N} + [J_{11_i} + m_{rw_i} d_i^2] \dot{\Omega}_i \\ = -J_{13_i} \omega_{w_{2_i}} \omega_{s_i} + \omega_{w_{2_i}} \omega_{w_{3_i}} (J_{22_i} - J_{33_i} - m_{rw_i} d_i^2) - m_{rw_i} d_i \hat{\mathbf{w}}_{3_i}^T [\tilde{\boldsymbol{\omega}}_{B/N}] [\tilde{\boldsymbol{\omega}}_{B/N}] \mathbf{r}_{W_i/B} + u_{s_i} \end{aligned} \quad (16)$$

3.2 Derivation of Back-Substitution

$$\begin{aligned} \dot{\Omega}_i = & -\left(\frac{m_{rw_i} d_i \hat{\mathbf{w}}_{3_i}^T}{J_{11_i} + m_{rw_i} d_i^2}\right) \ddot{\mathbf{r}}_{B/N} - \frac{1}{J_{11_i} + m_{rw_i} d_i^2} \left[(J_{11_i} + m_{rw_i} d_i^2) \hat{\mathbf{g}}_{s_i}^T + J_{13_i} \hat{\mathbf{w}}_{3_i}^T - m_{rw_i} d_i \hat{\mathbf{w}}_{3_i}^T [\tilde{\mathbf{r}}_{W_i/B}] \right] \dot{\boldsymbol{\omega}}_{B/N} \\ & + \frac{1}{J_{11_i} + m_{rw_i} d_i^2} \left(\omega_{w_{2_i}} \omega_{w_{3_i}} (J_{22_i} - J_{33_i} - m_{rw_i} d_i^2) - J_{13_i} \omega_{w_{2_i}} \omega_{s_i} - m_{rw_i} d_i \hat{\mathbf{w}}_{3_i}^T [\tilde{\boldsymbol{\omega}}_{B/N}] [\tilde{\boldsymbol{\omega}}_{B/N}] \mathbf{r}_{W_i/B} + u_{s_i} \right) \end{aligned} \quad (17)$$

$$\mathbf{a}_{\Omega_i} = -\frac{m_{rw_i} d_i}{J_{11_i} + m_{rw_i} d_i^2} \hat{\mathbf{w}}_{3_i} \quad (18)$$

$$\mathbf{b}_{\Omega_i} = -\frac{1}{J_{11_i} + m_{rw_i} d_i^2} \left[(J_{11_i} + m_{rw_i} d_i^2) \hat{\mathbf{g}}_{s_i} + J_{13_i} \hat{\mathbf{w}}_{3_i} + m_{rw_i} d_i [\tilde{\mathbf{r}}_{W_i/B}] \hat{\mathbf{w}}_{3_i} \right] \quad (19)$$

$$c_{\Omega_i} = \frac{1}{J_{11_i} + m_{rw_i} d_i^2} \left(\omega_{w_{2_i}} \omega_{w_{3_i}} (J_{22_i} - J_{33_i} - m_{rw_i} d_i^2) - J_{13_i} \omega_{w_{2_i}} \omega_{s_i} - m_{rw_i} d_i \hat{\mathbf{w}}_{3_i}^T [\tilde{\boldsymbol{\omega}}_{B/N}] [\tilde{\boldsymbol{\omega}}_{B/N}] \mathbf{r}_{W_i/B} + u_{s_i} \right) \quad (20)$$

$$\dot{\Omega}_i = \mathbf{a}_{\Omega_i}^T \ddot{\mathbf{r}}_{B/N} + \mathbf{b}_{\Omega_i}^T \dot{\boldsymbol{\omega}}_{B/N} + c_{\Omega_i} \quad (21)$$

Plugging the equation above into Eq. (14) and multiplying both sides by m_{sc} ,

$$\begin{aligned} & \left[m_{sc} [I_{3 \times 3}] + \sum_{i=1}^N m_{rw_i} d_i \hat{\mathbf{w}}_{3_i} \mathbf{a}_{\Omega_i}^T \right] \ddot{\mathbf{r}}_{B/N} + \left[-m_{sc} [\tilde{\mathbf{c}}] + \sum_{i=1}^N m_{rw_i} d_i \hat{\mathbf{w}}_{3_i} \mathbf{b}_{\Omega_i}^T \right] \dot{\boldsymbol{\omega}}_{B/N} \\ & = \mathbf{F} - 2m_{sc} [\tilde{\boldsymbol{\omega}}_{B/N}] \mathbf{c}' - m_{sc} [\tilde{\boldsymbol{\omega}}_{B/N}] [\tilde{\boldsymbol{\omega}}_{B/N}] \mathbf{c} + \sum_{i=1}^N \left[m_{rw_i} d_i \Omega_i^2 \hat{\mathbf{w}}_{2_i} - m_{rw_i} d_i c_{\Omega_i} \hat{\mathbf{w}}_{3_i} \right] \end{aligned} \quad (22)$$

Moving on to rotation...

$$\begin{aligned} & \left[m_{sc} [\tilde{\mathbf{c}}] + \sum_{i=1}^N \left([I_{rw_i, W_{c_i}}] \hat{\mathbf{g}}_{s_i} + m_{rw_i} d_i [\tilde{\mathbf{r}}_{W_{c_i}/B}] \hat{\mathbf{w}}_{3_i} \right) \mathbf{a}_{\Omega_i}^T \right] \ddot{\mathbf{r}}_{B/N} \\ & + \left[[I_{sc, B}] + \sum_{i=1}^N \left([I_{rw_i, W_{c_i}}] \hat{\mathbf{g}}_{s_i} + m_{rw_i} d_i [\tilde{\mathbf{r}}_{W_{c_i}/B}] \hat{\mathbf{w}}_{3_i} \right) \mathbf{b}_{\Omega_i}^T \right] \dot{\boldsymbol{\omega}}_{B/N} \\ & = -[\tilde{\boldsymbol{\omega}}_{B/N}] [I_{sc, B}] \boldsymbol{\omega}_{B/N} - [I_{sc, B}]' \boldsymbol{\omega}_{B/N} + \mathbf{L}_B \\ & + \sum_{i=1}^N \left[m_{rw_i} [\tilde{\mathbf{r}}_{W_{c_i}/B}] d_i \Omega_i^2 \hat{\mathbf{w}}_{2_i} - [I_{rw_i, W_{c_i}}]' \Omega_i \hat{\mathbf{g}}_{s_i} - [\tilde{\boldsymbol{\omega}}_{B/N}] \left([I_{rw_i, W_{c_i}}] \Omega_i \hat{\mathbf{g}}_{s_i} + m_{rw_i} [\tilde{\mathbf{r}}_{W_{c_i}/B}] \mathbf{r}'_{W_{c_i}/B} \right) \right. \\ & \quad \left. - \left([I_{rw_i, W_{c_i}}] \hat{\mathbf{g}}_{s_i} + m_{rw_i} d_i [\tilde{\mathbf{r}}_{W_{c_i}/B}] \hat{\mathbf{w}}_{3_i} \right) c_{\Omega_i} \right] \end{aligned} \quad (23)$$

3.3 Back-Substitution Contribution Matrices

$$[A_{\text{contr}}] = \sum_{i=1}^N m_{rw_i} d_i \hat{\mathbf{w}}_{3_i} \mathbf{a}_{\Omega_i}^T \quad (24)$$

$$[B_{\text{contr}}] = \sum_{i=1}^N m_{\text{rw}_i} d_i \hat{\mathbf{w}}_{3_i} \mathbf{b}_{\Omega_i}^T \quad (25)$$

$$[C_{\text{contr}}] = \sum_{i=1}^N \left([I_{\text{rw}_i, W_{c_i}}] \hat{\mathbf{g}}_{s_i} + m_{\text{rw}_i} d_i [\tilde{\mathbf{r}}_{W_{c_i}/B}] \hat{\mathbf{w}}_{3_i} \right) \mathbf{a}_{\Omega_i}^T \quad (26)$$

$$[D_{\text{contr}}] = \sum_{i=1}^N \left([I_{\text{rw}_i, W_{c_i}}] \hat{\mathbf{g}}_{s_i} + m_{\text{rw}_i} d_i [\tilde{\mathbf{r}}_{W_{c_i}/B}] \hat{\mathbf{w}}_{3_i} \right) \mathbf{b}_{\Omega_i}^T \quad (27)$$

$$\mathbf{v}_{\text{trans,contr}} = \sum_{i=1}^N \left[m_{\text{rw}_i} d_i \Omega_i^2 \hat{\mathbf{w}}_{2_i} - m_{\text{rw}_i} d_i c_{\Omega_i} \hat{\mathbf{w}}_{3_i} \right] \quad (28)$$

$$\begin{aligned} \mathbf{v}_{\text{rot,contr}} = \sum_{i=1}^N \left[m_{\text{rw}_i} [\tilde{\mathbf{r}}_{W_{c_i}/B}] d_i \Omega_i^2 \hat{\mathbf{w}}_{2_i} - [I_{\text{rw}_i, W_{c_i}}]' \Omega_i \hat{\mathbf{g}}_{s_i} - [\tilde{\boldsymbol{\omega}}_{\mathcal{B}/\mathcal{N}}] \left([I_{\text{rw}_i, W_{c_i}}] \Omega_i \hat{\mathbf{g}}_{s_i} + m_{\text{rw}_i} [\tilde{\mathbf{r}}_{W_{c_i}/B}] \mathbf{r}_{W_{c_i}/B}' \right) \right. \\ \left. - \left([I_{\text{rw}_i, W_{c_i}}] \hat{\mathbf{g}}_{s_i} + m_{\text{rw}_i} d_i [\tilde{\mathbf{r}}_{W_{c_i}/B}] \hat{\mathbf{w}}_{3_i} \right) c_{\Omega_i} \right] \quad (29) \end{aligned}$$