

Derivation of EOMs for $N_p + 1$ Connected Panels using Kane's Method

I Introduction

$\theta_i = \theta_{i,d} + \theta_{i,0}$ positive angle is in the upward direction.

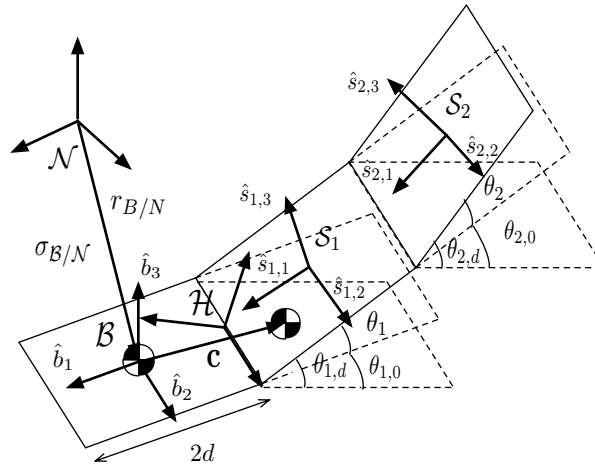


Figure 1: Frame and variable definitions for the system discussed here, where $N_p = 2$.

II Derivation of Equations of Motion - Kane's Method

The choice of state variables and their respective chosen generalized speeds are:

$$\mathbf{X} = \begin{bmatrix} \mathbf{r}_{B/N} \\ \boldsymbol{\sigma}_{B/N} \\ \theta_1 \\ \vdots \\ \theta_{N_p} \end{bmatrix} \quad \mathbf{u} = \begin{bmatrix} \dot{\mathbf{r}}_{B/N} \\ \boldsymbol{\omega}_{B/N} \\ \dot{\theta}_1 \\ \vdots \\ \dot{\theta}_{N_p} \end{bmatrix} \quad (1)$$

To create the partial velocity table, some velocities first need to be defined

$$\dot{\mathbf{r}}_{B/N} = \dot{\mathbf{r}}_{B/N} \quad (2)$$

$$\dot{\mathbf{r}}_{C/N} = \dot{\mathbf{r}}_{B/N} + \dot{\mathbf{c}} \quad (3)$$

$$\boldsymbol{\omega}_{B/N} = \boldsymbol{\omega}_{B/N} \quad (4)$$

$$\boldsymbol{\omega}_{S_i/N} = \boldsymbol{\omega}_{B/N} + \left(\sum_{k=1}^i \dot{\theta}_k \right) \hat{\mathbf{s}}_{i,2} \quad (5)$$

$$\mathbf{r}_{S_i/N} = \mathbf{r}_{B/N} + \mathbf{r}_{S_i/B} = \mathbf{r}_{B/N} + \mathbf{r}_{H/B} - [d\hat{\mathbf{s}}_{i,1} + \sum_{n=1}^{i-1} 2d\hat{\mathbf{s}}_{n,1}] \quad (6)$$

$$\dot{\mathbf{r}}_{S_i/N} = \dot{\mathbf{r}}_{B/N} + \mathbf{r}'_{S_i/B} + \boldsymbol{\omega}_{B/N} \times \mathbf{r}_{S_i/B} = \dot{\mathbf{r}}_{B/N} + d \left[\left(\sum_{k=1}^i \dot{\theta}_k \right) \hat{\mathbf{s}}_{i,3} + \sum_{n=1}^{i-1} 2\hat{\mathbf{s}}_{n,3} \left(\sum_{k=1}^n \dot{\theta}_k \right) \right] - [\tilde{\mathbf{r}}_{S_i/B}] \boldsymbol{\omega}_{B/N} \quad (7)$$

Where

$$\hat{\mathbf{s}}'_{i,j} = \boldsymbol{\omega}_{S_i/B} \times \hat{\mathbf{s}}_{i,j} = \left(\sum_{k=1}^i \dot{\theta}_k \right) \hat{\mathbf{s}}_{i,2} \times \hat{\mathbf{s}}_{i,j} \quad (8)$$

is used to get the derivative.

The summation in equation 6 and 7 can be out of bounds for certain values of i . When this occurs, the summation becomes equal to zero. c is defined as the position vector between the body frame and the COM of the system:

$$\mathbf{c} = \frac{1}{m_{sc}} \left[\sum_{i=1}^{N_p} m_p \mathbf{r}_{S_i/B} \right] \quad (9)$$

$$\dot{\mathbf{c}} = \mathbf{c}' - [\tilde{\mathbf{c}}] \boldsymbol{\omega}_{B/N} \quad (10)$$

$$\mathbf{c}' = \frac{m_p d}{m_{sc}} \sum_{i=1}^{N_p} \left[\left(\sum_{k=1}^i \dot{\theta}_k \right) \hat{\mathbf{s}}_{i,3} + \sum_{n=1}^{i-1} 2\hat{\mathbf{s}}_{n,3} \left(\sum_{k=1}^n \dot{\theta}_k \right) \right] \quad (11)$$

$$\mathbf{c}' = \frac{m_p d}{m_{sc}} \left[\sum_{i=1}^{N_p} \dot{\theta}_i \sum_{n=i}^{N_p} (2[N_p - n] + 1) \hat{\mathbf{s}}_{n,3} \right] \quad (12)$$

Now the following partial velocity table can be created (here: $j = r - 6$):

Table 1: Partial Velocity Table

r	\mathbf{v}_r^C	\mathbf{v}_r^B	$\boldsymbol{\omega}_r^B$	$\mathbf{v}_r^{S_i}$	$\boldsymbol{\omega}_r^{S_i}$
1 – 3	$[I_{3 \times 3}]$	$[I_{3 \times 3}]$	$[0_{3 \times 3}]$	$[I_{3 \times 3}]$	$[0_{3 \times 3}]$
4 – 6	$-\tilde{\mathbf{c}}$	$[0_{3 \times 3}]$	$[I_{3 \times 3}]$	$-\tilde{\mathbf{r}}_{S_i/B}$	$[I_{3 \times 3}]$
$7 - N_p$	$\sum_{n=j}^{N_p} (2[N_p - n] + 1) \hat{\mathbf{s}}_{n,3}$	$[0_{3 \times 1}]$	$[0_{3 \times 1}]$	if $j \leq i$: $d[\hat{\mathbf{s}}_{i,3} + \sum_{n=j}^{i-1} 2\hat{\mathbf{s}}_{n,3}]$ else: $[0_{3 \times 1}]$	if $j \leq i$: $\hat{\mathbf{s}}_{i,2}$ else: $[0_{3 \times 1}]$

Using these partial velocity definitions, the follow sections will step through the formulation for the translational, rotational and panel EOMs developed using Kane's method.

II.A Hub Translational Motion

Starting with the definition of a generalized force:

$$\mathbf{F}_r = \sum_r^N \mathbf{v}_r^T \mathbf{F} \quad (13)$$

Using this definition the external force applied on the system for the translational equations is defined as:

$$\mathbf{F}_{1-3} = [\mathbf{v}_{1-3}^C]^T \mathbf{F}_{\text{ext}} = \mathbf{F}_{\text{ext}} \quad (14)$$

Using the definition of generalized inertia forces,

$$\mathbf{F}_r^* = \sum_r^N \left[\boldsymbol{\omega}_r^T \mathbf{T}^* + \mathbf{v}_r^T (-m_r \mathbf{a}_r) \right] \quad (15)$$

the inertia forces for the hub translational motion are defined as

$$\mathbf{F}_{1-3}^* = [\mathbf{v}_{1-3}^B]^T (-m_{\text{hub}} \ddot{\mathbf{r}}_{B/N}) + \sum_{i=1}^{N_p} [\mathbf{v}_{1-3}^{S_i}]^T (-m_{\mathbf{p}_i} \ddot{\mathbf{r}}_{S_i/N}) = -m_{\text{hub}} \ddot{\mathbf{r}}_{B/N} + \sum_{i=1}^{N_p} -m_{\mathbf{p}_i} \ddot{\mathbf{r}}_{S_i/N} \quad (16)$$

Finally, Kane's equation is:

$$\mathbf{F}_r + \mathbf{F}_r^* = 0 \quad (17)$$

therefore

$$\mathbf{F}_{\text{ext}} - m_{\text{hub}} \ddot{\mathbf{r}}_{B/N} + \sum_{i=1}^{N_p} -m_{\mathbf{p}_i} \ddot{\mathbf{r}}_{S_i/N} = 0 \quad (18)$$

Expanding and rearranging results in

$$m_{\text{hub}} \ddot{\mathbf{r}}_{B/N} + \sum_{i=1}^{N_p} m_{\mathbf{p}} (\ddot{\mathbf{r}}_{B/N} + \ddot{\mathbf{r}}_{S_i/B}) = \mathbf{F}_{\text{ext}} \quad (19)$$

Where

$$\ddot{\mathbf{r}}_{S_i/B} = \mathbf{r}_{S_i/B}'' + 2\boldsymbol{\omega}_{B/N} \times \mathbf{r}_{S_i/B}' + \dot{\boldsymbol{\omega}}_{B/N} \times \mathbf{r}_{S_i/B} + \boldsymbol{\omega}_{B/N} \times (\boldsymbol{\omega}_{B/N} \times \mathbf{r}_{S_i/B}) \quad (20)$$

Plugging Eq. (20) into Eq. (19) results in

$$m_{\text{hub}} \ddot{\mathbf{r}}_{B/N} + \sum_{i=1}^{N_p} m_{\mathbf{p}} \left[\ddot{\mathbf{r}}_{B/N} + \mathbf{r}_{S_i/B}'' + 2\boldsymbol{\omega}_{B/N} \times \mathbf{r}_{S_i/B}' + \dot{\boldsymbol{\omega}}_{B/N} \times \mathbf{r}_{S_i/B} + \boldsymbol{\omega}_{B/N} \times (\boldsymbol{\omega}_{B/N} \times \mathbf{r}_{S_i/B}) \right] = \mathbf{F}_{\text{ext}} \quad (21)$$

The body frame derivative can be written explicitly using the simplification used in Eqs. 11 and 12 (this simplification only works when $\mathbf{r}_{S_i/B}''$ is summed over all panels)

$$m_{\mathbf{p}} \sum_{i=1}^{N_p} \mathbf{r}_{S_i/B}'' = \sum_{i=1}^{N_p} \left[\ddot{\theta}_i \sum_{k=i}^{N_p} (2[N_p - k] + 1) dm_{\mathbf{p}} \hat{\mathbf{s}}_{k,3} + \left(\sum_{k=1}^i \dot{\theta}_k \right)^2 (2[N_p - i] + 1) dm_{\mathbf{p}} \hat{\mathbf{s}}_{i,1} \right] \quad (22)$$

Combining like terms and rearranging results in

$$m_{\text{sc}} \ddot{\mathbf{r}}_{B/N} - m_{\text{sc}} [\tilde{\mathbf{c}}] \dot{\boldsymbol{\omega}}_{B/N} + \sum_{i=1}^{N_p} \left[\sum_{k=i}^{N_p} (2[N_p - k] + 1) dm_{\mathbf{p}} \hat{\mathbf{s}}_{k,3} \right] \ddot{\theta}_i = \mathbf{F}_{\text{ext}} - 2m_{\text{sc}} [\tilde{\boldsymbol{\omega}}_{B/N}] \mathbf{c}' - m_{\text{sc}} [\tilde{\boldsymbol{\omega}}_{B/N}] [\tilde{\boldsymbol{\omega}}_{B/N}] \mathbf{c} - \sum_{i=1}^{N_p} \left[\left(\sum_{k=1}^i \dot{\theta}_k \right)^2 (2[N_p - i] + 1) dm_{\mathbf{p}} \hat{\mathbf{s}}_{i,1} \right] \quad (23)$$

II.B Hub Rotational Motion

The torque acting on the spacecraft, \mathbf{L}_B needs to be defined as a general active force. Using Eq. (13) active forces acting on the spacecraft for the rotational equations can be defined as:

$$\mathbf{F}_{4-6} = [\boldsymbol{\omega}_{4-6}^B]^T \mathbf{L}_B = \mathbf{L}_B \quad (24)$$

To define the generalized inertia forces, using Eq. (15) the definition of \mathbf{T}^* needs to be defined for a rigid body:

$$\mathbf{T}^* = -[I_c]\dot{\boldsymbol{\omega}} - [\tilde{\boldsymbol{\omega}}][I_c]\boldsymbol{\omega} \quad (25)$$

$$\begin{aligned} \mathbf{F}_{4-6}^* &= [\boldsymbol{\omega}_{4-6}^B]^T \mathbf{T}_{\text{hub}}^* + [\mathbf{v}_{4-6}^B]^T (-m_{\text{hub}} \ddot{\mathbf{r}}_{B/N}) + \sum_{i=1}^{N_p} \left([\mathbf{v}_{4-6}^{S_i}]^T (-m_p \ddot{\mathbf{r}}_{S_i/N}) + [\boldsymbol{\omega}_{4-6}^{S_i}]^T \mathbf{T}_{p_i}^* \right) \\ &= -[I_{\text{hub},B}] \dot{\boldsymbol{\omega}}_{B/N} - [\tilde{\boldsymbol{\omega}}_{B/N}][I_{\text{hub},B}] \boldsymbol{\omega}_{B/N} + \sum_{i=1}^{N_p} \left(-m_p [\tilde{\mathbf{r}}_{S_i/B}] \ddot{\mathbf{r}}_{S_i/N} - [I_{p_i,S_i}] \dot{\boldsymbol{\omega}}_{S_i/N} - [\tilde{\boldsymbol{\omega}}_{S_i/N}][I_{p_i,S_i}] \boldsymbol{\omega}_{S_i/N} \right) \end{aligned} \quad (26)$$

Using Kane's equation, Eq. (17), the following equations of motion for the rotational dynamics are defined:

$$\begin{aligned} \mathbf{L}_B - [I_{\text{hub},B}] \dot{\boldsymbol{\omega}}_{B/N} - [\tilde{\boldsymbol{\omega}}_{B/N}][I_{\text{hub},B}] \boldsymbol{\omega}_{B/N} \\ + \sum_{i=1}^{N_p} \left(-m_p [\tilde{\mathbf{r}}_{S_i/B}] \ddot{\mathbf{r}}_{S_i/N} - [I_{p_i,S_i}] \dot{\boldsymbol{\omega}}_{S_i/N} - [\tilde{\boldsymbol{\omega}}_{S_i/N}][I_{p_i,S_i}] \boldsymbol{\omega}_{S_i/N} \right) = 0 \end{aligned} \quad (27)$$

$$\dot{\boldsymbol{\omega}}_{S_i/N} = \dot{\boldsymbol{\omega}}_{B/N} + \sum_{k=i}^i \ddot{\theta}_k \hat{\mathbf{s}}_{i,1} + \sum_{k=i}^i \dot{\theta}_k (\boldsymbol{\omega}_{B/N} \times \hat{\mathbf{s}}_{i,2}) \quad (28)$$

Plugging Eq. (28) into Eq. (27)

$$\begin{aligned} \mathbf{L}_B - [I_{\text{hub},B}] \dot{\boldsymbol{\omega}}_{B/N} - [\tilde{\boldsymbol{\omega}}_{B/N}][I_{\text{hub},B}] \boldsymbol{\omega}_{B/N} \\ + \sum_{i=1}^{N_p} \left(-m_p [\tilde{\mathbf{r}}_{S_i/B}] \ddot{\mathbf{r}}_{S_i/N} - [I_{p_i,S_i}] \dot{\boldsymbol{\omega}}_{B/N} - I_{S_i,2} \sum_{k=i}^i \ddot{\theta}_k \hat{\mathbf{s}}_{i,2} + [I_{p_i,S_i}] \sum_{k=i}^i \dot{\theta}_k (\hat{\mathbf{s}}_{i,2} \times \boldsymbol{\omega}_{B/N}) \right. \\ \left. - [\tilde{\boldsymbol{\omega}}_{B/N}][I_{p_i,S_i}] \boldsymbol{\omega}_{B/N} - [\tilde{\boldsymbol{\omega}}_{B/N}][I_{p_i,S_i}] \left(\sum_{k=i}^i \dot{\theta}_k \right) \hat{\mathbf{s}}_{i,2} - \left(\sum_{k=i}^i \dot{\theta}_k \right) \hat{\mathbf{s}}_{i,2} \times [I_{p_i,S_i}] \boldsymbol{\omega}_{B/N} \right) = 0 \end{aligned} \quad (29)$$

$$\begin{aligned} \mathbf{L}_B - [I_{\text{hub},B}] \dot{\boldsymbol{\omega}}_{B/N} - \sum_{i=1}^{N_p} [I_{p_i,S_i}] \dot{\boldsymbol{\omega}}_{B/N} - \sum_{i=1}^{N_p} I_{S_i,2} \sum_{k=i}^i \ddot{\theta}_k \hat{\mathbf{s}}_{i,2} - [\tilde{\boldsymbol{\omega}}_{B/N}][I_{\text{hub},B}] \boldsymbol{\omega}_{B/N} - \sum_{i=1}^{N_p} [\tilde{\boldsymbol{\omega}}_{B/N}][I_{p_i,S_i}] \boldsymbol{\omega}_{B/N} \\ + \sum_{i=1}^{N_p} \left(-m_p [\tilde{\mathbf{r}}_{S_i/B}] [\ddot{\mathbf{r}}_{B/N} + \ddot{\mathbf{r}}_{S_i/B}] - I_{S_i,2} \sum_{k=i}^i \dot{\theta}_k [\tilde{\boldsymbol{\omega}}_{B/N}] \hat{\mathbf{s}}_{i,2} \right. \\ \left. + \sum_{k=i}^i \dot{\theta}_k [I_{S_i,1} \hat{\mathbf{s}}_{i,1} \hat{\mathbf{s}}_{i,3}^T - I_{S_i,3} \hat{\mathbf{s}}_{i,3} \hat{\mathbf{s}}_{i,1}^T] \boldsymbol{\omega}_{B/N} - \sum_{k=i}^i \dot{\theta}_k [I_{S_i,3} \hat{\mathbf{s}}_{i,1} \hat{\mathbf{s}}_{i,3}^T - I_{S_i,1} \hat{\mathbf{s}}_{i,3} \hat{\mathbf{s}}_{i,1}^T] \boldsymbol{\omega}_{B/N} \right) = 0 \end{aligned} \quad (30)$$

$$\sum_{i=1}^{N_p} -m_p [\tilde{\mathbf{r}}_{S_i/B}] \mathbf{r}_{S_i/B}'' = -m_p d \sum_{i=1}^{N_p} \left(\ddot{\theta} \sum_{k=i}^{N_p} [\tilde{\mathbf{r}}_{S_k/B}] + \sum_{n=k+1}^{N_p} 2[\tilde{\mathbf{r}}_{S_n/B}] \right) \hat{\mathbf{s}}_{k,3} + \left(\sum_{k=1}^i \dot{\theta} \right)^2 [\tilde{\mathbf{r}}_{S_i/B}] + \sum_{n=i+1}^{N_p} 2[\tilde{\mathbf{r}}_{S_n/B}] \hat{\mathbf{s}}_{i,1} \quad (31)$$

$$\begin{aligned}
& \mathbf{L}_B - m_{sc}[\tilde{\mathbf{c}}]\ddot{\mathbf{r}}_{B/N} - [I_{hub,B}]\dot{\boldsymbol{\omega}}_{B/N} - \sum_{i=1}^{N_p} [I_{sp_i,S_i}]\dot{\boldsymbol{\omega}}_{B/N} - \sum_{i=1}^{N_p} \ddot{\theta}_i \sum_{k=i}^{N_p} I_{s_{k,2}} \hat{\mathbf{s}}_{k,2} - [\tilde{\boldsymbol{\omega}}_{B/N}][I_{hub,B}]\boldsymbol{\omega}_{B/N} - \sum_{i=1}^{N_p} [\tilde{\boldsymbol{\omega}}_{B/N}][I_{p_i,S_i}]\boldsymbol{\omega}_{B/N} \\
& + \sum_{i=1}^{N_p} \left(-\ddot{\theta} \sum_{k=i}^{N_p} [\tilde{\mathbf{r}}_{S_k/B}] + \sum_{n=k+1}^{N_p} 2[\tilde{\mathbf{r}}_{S_n/B}] \right) m_p d\hat{\mathbf{s}}_{k,3} - \left(\sum_{k=1}^i \dot{\theta} \right)^2 [\tilde{\mathbf{r}}_{S_i/B}] + \sum_{n=i+1}^{N_p} 2[\tilde{\mathbf{r}}_{S_n/B}] m_p d\hat{\mathbf{s}}_{i,1} \\
& - m_p[\tilde{\mathbf{r}}_{S_i/B}] \left[2\boldsymbol{\omega}_{B/N} \times \mathbf{r}'_{S_i/B} + \dot{\boldsymbol{\omega}}_{B/N} \times \mathbf{r}_{S_i/B} + \boldsymbol{\omega}_{B/N} \times (\boldsymbol{\omega}_{B/N} \times \mathbf{r}_{S_i/B}) \right] - I_{s_{i,2}} \sum_{k=i}^i \dot{\theta}_k [\tilde{\boldsymbol{\omega}}_{B/N}] \hat{\mathbf{s}}_{i,2} \\
& - \sum_{k=i}^i \dot{\theta}_k (I_{s_{i,3}} - I_{s_{i,1}}) (\hat{\mathbf{s}}_{i,1} \hat{\mathbf{s}}_{i,3}^T + \hat{\mathbf{s}}_{i,3} \hat{\mathbf{s}}_{i,1}^T) \boldsymbol{\omega}_{B/N} \Big) = 0 \quad (32)
\end{aligned}$$

$$\begin{aligned}
& \mathbf{L}_B - m_{sc}[\tilde{\mathbf{c}}]\ddot{\mathbf{r}}_{B/N} - [I_{sc,B}]\dot{\boldsymbol{\omega}}_{B/N} - \sum_{i=1}^{N_p} \left[\sum_{k=i}^{N_p} I_{s_{k,2}} \hat{\mathbf{s}}_{k,2} + \sum_{k=i}^{N_p} [\tilde{\mathbf{r}}_{S_k/B}] + \sum_{n=k+1}^{N_p} 2[\tilde{\mathbf{r}}_{S_n/B}] \right] m_p d\hat{\mathbf{s}}_{k,3} \Big] \ddot{\theta}_i - [\tilde{\boldsymbol{\omega}}_{B/N}][I_{sc,B}]\boldsymbol{\omega}_{B/N} \\
& + \sum_{i=1}^{N_p} \left(-2m_p[\tilde{\mathbf{r}}_{S_i/B}] [\boldsymbol{\omega}_{B/N} \times \mathbf{r}'_{S_i/B}] - \left(\sum_{k=1}^i \dot{\theta}_k \right) (I_{s_{i,3}} - I_{s_{i,1}}) (\hat{\mathbf{s}}_{i,1} \hat{\mathbf{s}}_{i,3}^T + \hat{\mathbf{s}}_{i,3} \hat{\mathbf{s}}_{i,1}^T) \boldsymbol{\omega}_{B/N} \right. \\
& \left. - \left(\sum_{k=1}^i \dot{\theta} \right)^2 [\tilde{\mathbf{r}}_{S_i/B}] + \sum_{n=i+1}^{N_p} 2[\tilde{\mathbf{r}}_{S_n/B}] \right] m_p d\hat{\mathbf{s}}_{i,1} - I_{s_{i,2}} \left(\sum_{k=1}^i \dot{\theta}_k \right) [\tilde{\boldsymbol{\omega}}_{B/N}] \hat{\mathbf{s}}_{i,2} \Big) = 0 \quad (33)
\end{aligned}$$

Moving things to the correct sides

$$\begin{aligned}
& m_{sc}[\tilde{\mathbf{c}}]\ddot{\mathbf{r}}_{B/N} + [I_{sc,B}]\dot{\boldsymbol{\omega}}_{B/N} + \sum_{i=1}^{N_p} \left[\sum_{k=i}^{N_p} I_{s_{k,2}} \hat{\mathbf{s}}_{k,2} + \sum_{k=i}^{N_p} [\tilde{\mathbf{r}}_{S_k/B}] + \sum_{n=k+1}^{N_p} 2[\tilde{\mathbf{r}}_{S_n/B}] \right] m_p d\hat{\mathbf{s}}_{k,3} \Big] \ddot{\theta}_i \\
& = -[\tilde{\boldsymbol{\omega}}_{B/N}][I_{sc,B}]\boldsymbol{\omega}_{B/N} - \sum_{i=1}^{N_p} \left(2m_p[\tilde{\mathbf{r}}_{S_i/B}] [\boldsymbol{\omega}_{B/N} \times \mathbf{r}'_{S_i/B}] + \left(\sum_{k=1}^i \dot{\theta}_k \right) (I_{s_{i,3}} - I_{s_{i,1}}) (\hat{\mathbf{s}}_{i,1} \hat{\mathbf{s}}_{i,3}^T + \hat{\mathbf{s}}_{i,3} \hat{\mathbf{s}}_{i,1}^T) \boldsymbol{\omega}_{B/N} \right. \\
& \left. + \left(\sum_{k=1}^i \dot{\theta} \right)^2 [\tilde{\mathbf{r}}_{S_i/B}] + \sum_{n=i+1}^{N_p} 2[\tilde{\mathbf{r}}_{S_n/B}] \right] m_p d\hat{\mathbf{s}}_{i,1} + I_{s_{i,2}} \left(\sum_{k=1}^i \dot{\theta}_k \right) [\tilde{\boldsymbol{\omega}}_{B/N}] \hat{\mathbf{s}}_{i,2} \Big) + \mathbf{L}_B \quad (34)
\end{aligned}$$

$$\begin{aligned}
& m_{sc}[\tilde{\mathbf{c}}]\ddot{\mathbf{r}}_{B/N} + [I_{sc,B}]\dot{\boldsymbol{\omega}}_{B/N} + \sum_{i=1}^{N_p} \left[\sum_{k=i}^{N_p} I_{s_{k,2}} \hat{\mathbf{s}}_{k,2} + \sum_{k=i}^{N_p} [\tilde{\mathbf{r}}_{S_k/B}] + \sum_{n=k+1}^{N_p} 2[\tilde{\mathbf{r}}_{S_n/B}] \right] m_p d\hat{\mathbf{s}}_{k,3} \Big] \ddot{\theta}_i \\
& = -[\tilde{\boldsymbol{\omega}}_{B/N}][I_{sc,B}]\boldsymbol{\omega}_{B/N} - \sum_{i=1}^{N_p} \left(-m_p [\tilde{\mathbf{r}}'_{S_i/B}][\tilde{\mathbf{r}}_{S_i/B}] + [\tilde{\mathbf{r}}_{S_i/B}][\tilde{\mathbf{r}}'_{S_i/B}] \right) \boldsymbol{\omega}_{B/N} + \left(\sum_{k=1}^i \dot{\theta}_k \right) (I_{s_{i,3}} - I_{s_{i,1}}) (\hat{\mathbf{s}}_{i,1} \hat{\mathbf{s}}_{i,3}^T + \hat{\mathbf{s}}_{i,3} \hat{\mathbf{s}}_{i,1}^T) \boldsymbol{\omega}_{B/N} \\
& + m_p[\tilde{\boldsymbol{\omega}}_{B/N}][\tilde{\mathbf{r}}_{S_i/B}]\mathbf{r}'_{S_i/B} + \left(\sum_{k=1}^i \dot{\theta} \right)^2 [\tilde{\mathbf{r}}_{S_i/B}] + \sum_{n=i+1}^{N_p} 2[\tilde{\mathbf{r}}_{S_n/B}] m_p d\hat{\mathbf{s}}_{i,1} + I_{s_{i,2}} \left(\sum_{k=1}^i \dot{\theta}_k \right) [\tilde{\boldsymbol{\omega}}_{B/N}] \hat{\mathbf{s}}_{i,2} \Big) + \mathbf{L}_B \quad (35)
\end{aligned}$$

End

$$\begin{aligned}
& m_{sc}[\tilde{\mathbf{c}}]\ddot{\mathbf{r}}_{B/N} + [I_{sc,B}]\dot{\boldsymbol{\omega}}_{B/N} + \sum_{i=1}^{N_p} \left[\sum_{k=i}^{N_p} I_{s_{k,2}} \hat{\mathbf{s}}_{k,2} + \sum_{k=i}^{N_p} [\tilde{\mathbf{r}}_{S_k/B}] + \sum_{n=k+1}^{N_p} 2[\tilde{\mathbf{r}}_{S_n/B}] \right] m_p d\hat{\mathbf{s}}_{k,3} \Big] \ddot{\theta}_i = -[\tilde{\boldsymbol{\omega}}_{B/N}][I_{sc,B}]\boldsymbol{\omega}_{B/N} \\
& - [I'_{sc,B}]\boldsymbol{\omega}_{B/N} - \sum_{i=1}^{N_p} \left(m_p[\tilde{\boldsymbol{\omega}}_{B/N}][\tilde{\mathbf{r}}_{S_i/B}]\mathbf{r}'_{S_i/B} + \left(\sum_{k=1}^i \dot{\theta} \right)^2 [\tilde{\mathbf{r}}_{S_i/B}] + \sum_{n=i+1}^{N_p} 2[\tilde{\mathbf{r}}_{S_n/B}] \right] m_p d\hat{\mathbf{s}}_{i,1} + I_{s_{i,2}} \left(\sum_{k=1}^i \dot{\theta}_k \right) [\tilde{\boldsymbol{\omega}}_{B/N}] \hat{\mathbf{s}}_{i,2} \Big) + \mathbf{L}_B \quad (36)
\end{aligned}$$

II.C Panel Motions

Following the similar pattern for translational and rotational equations the generalized active forces are defined, where $j = r - 6$:

$$\begin{aligned} \mathbf{F}_r = & \boldsymbol{\omega}_r^{S_j} \cdot (-k_j(\theta_j - \theta_{j,0})\hat{\mathbf{s}}_{j,2} - c_j\dot{\theta}_j\hat{\mathbf{s}}_{j,2} + k_{j+1}(\theta_{j+1} - \theta_{j+1,0})\hat{\mathbf{s}}_{j,2} + c_{j+1}\dot{\theta}_{j+1}\hat{\mathbf{s}}_{j+1,2}) \\ & + 2d\hat{\mathbf{s}}_{j,3} \cdot (\mathbf{F}_{ext,j+1} - m_{conn,j}\ddot{\mathbf{r}}_{conn,j}) = -k_j(\theta_j - \theta_{j,0}) - c_j\dot{\theta}_j + k_{j+1}(\theta_{j+1} - \theta_{j+1,0}) + c_{j+1}\dot{\theta}_{j+1} \\ & + 2d\hat{\mathbf{s}}_{j,3} \cdot (\mathbf{F}_{ext,j+1} - m_{conn,j}\ddot{\mathbf{r}}_{conn,j}) = K + 2d\hat{\mathbf{s}}_{j,3} \cdot (\mathbf{F}_{ext,j+1} - m_{conn,j}\ddot{\mathbf{r}}_{conn,j}) \end{aligned} \quad (37)$$

Where $m_{conn,j}$ and $\ddot{\mathbf{r}}_{conn,j}$ are the mass and acceleration of the connected panels after the j th panel, and:

$$K = -k_j(\theta_j - \theta_{j,0}) - c_j\dot{\theta}_j + k_{j+1}(\theta_{j+1} - \theta_{j+1,0}) + c_{j+1}\dot{\theta}_{j+1} \quad (38)$$

The generalized inertia forces are defined as:

$$\begin{aligned} \mathbf{F}_r^* = & \boldsymbol{\omega}_r^{S_j} \cdot \mathbf{T}_{p_j}^* + \mathbf{v}_r^{S_j} \cdot (-m_p\ddot{\mathbf{r}}_{S_j/N}) = \\ & \boldsymbol{\omega}_r^{S_j} \cdot \left[-[I_{p_j,S_j}]\dot{\boldsymbol{\omega}}_{S_j/N} - [\tilde{\boldsymbol{\omega}}_{S_j/N}][I_{p_j,S_j}]\boldsymbol{\omega}_{S_j/N} \right] + \mathbf{v}_r^{S_j} \cdot (-m_p\ddot{\mathbf{r}}_{S_j/N}) \end{aligned} \quad (39)$$

Using Kane's equation the following equations of motion are defined:

$$\begin{aligned} K + 2d\hat{\mathbf{s}}_{j,3} \cdot (\mathbf{F}_{ext,j+1} - m_{conn,j}\ddot{\mathbf{r}}_{conn,j}) + \hat{\mathbf{s}}_{i,2} \cdot \left[-[I_{p_i,S_i}]\dot{\boldsymbol{\omega}}_{S_i/N} - [\tilde{\boldsymbol{\omega}}_{S_i/N}][I_{p_i,S_i}]\boldsymbol{\omega}_{S_i/N} \right] \\ + d\hat{\mathbf{s}}_{j,3} \cdot (-m_p\ddot{\mathbf{r}}_{S_j/N}) = 0 \end{aligned} \quad (40)$$

Defining the inertial derivative:

$$\dot{\boldsymbol{\omega}}_{S_j/N} = \dot{\boldsymbol{\omega}}_{B/N} + \sum_{i=1}^{N_p} \ddot{\theta}_i \hat{\mathbf{s}}_{j,2} + \sum_{i=1}^{N_p} \dot{\theta}_i \boldsymbol{\omega}_{B/N} \times \hat{\mathbf{s}}_{j,2} \quad (41)$$

Which can be plugged into Eq. (40):

$$\begin{aligned} K - I_{s_j,2}\hat{\mathbf{s}}_{j,2}^T \dot{\boldsymbol{\omega}}_{B/N} - I_{s_j,2} \sum_{i=1}^{N_p} \ddot{\theta}_i - (I_{s_{j,1}} - I_{s_{j,3}}) \omega_{s_{j,3}} \omega_{s_{j,1}} \\ + 2d\hat{\mathbf{s}}_{j,3}^T \mathbf{F}_{ext,j+1} - 2d\hat{\mathbf{s}}_{j,3}^T \sum_{i=j+1}^{N_p} m_p \ddot{\mathbf{r}}_{S_i/N} - d\hat{\mathbf{s}}_{j,3}^T m_p \ddot{\mathbf{r}}_{S_j/N} = 0 \end{aligned} \quad (42)$$

$$\begin{aligned} K - I_{s_j,2}\hat{\mathbf{s}}_{j,2}^T \dot{\boldsymbol{\omega}}_{B/N} - I_{s_j,2} \sum_{i=1}^{N_p} \ddot{\theta}_i - (I_{s_{j,1}} - I_{s_{j,3}}) \omega_{s_{j,3}} \omega_{s_{j,1}} \\ + 2d\hat{\mathbf{s}}_{j,3}^T \mathbf{F}_{ext,j+1} - 2d\hat{\mathbf{s}}_{j,3}^T \sum_{i=j+1}^{N_p} m_p [\ddot{\mathbf{r}}_{B/N} + \ddot{\mathbf{r}}_{S_i/B}] - d\hat{\mathbf{s}}_{j,3}^T m_p [\ddot{\mathbf{r}}_{B/N} + \ddot{\mathbf{r}}_{S_j/B}] = 0 \end{aligned} \quad (43)$$

$$\begin{aligned} K - [d\hat{\mathbf{s}}_{j,3}^T + \sum_{i=j+1}^{N_p} 2d\hat{\mathbf{s}}_{j,3}^T] \ddot{\mathbf{r}}_{B/N} - I_{s_j,2}\hat{\mathbf{s}}_{j,2}^T \dot{\boldsymbol{\omega}}_{B/N} - I_{s_j,2} \sum_{i=1}^{N_p} \ddot{\theta}_i - (I_{s_{j,1}} - I_{s_{j,3}}) \omega_{s_{j,3}} \omega_{s_{j,1}} \\ + 2d\hat{\mathbf{s}}_{j,3}^T \mathbf{F}_{ext,j+1} - 2d\hat{\mathbf{s}}_{j,3}^T \sum_{i=j+1}^{N_p} m_p [\mathbf{r}_{S_i/B}'' + 2\boldsymbol{\omega}_{B/N} \times \mathbf{r}_{S_i/B}' + \dot{\boldsymbol{\omega}}_{B/N} \times \mathbf{r}_{S_i/B} + \boldsymbol{\omega}_{B/N} \times (\boldsymbol{\omega}_{B/N} \times \mathbf{r}_{S_i/B})] \\ - d\hat{\mathbf{s}}_{j,3}^T m_p [\mathbf{r}_{S_j/B}'' + 2\boldsymbol{\omega}_{B/N} \times \mathbf{r}_{S_j/B}' + \dot{\boldsymbol{\omega}}_{B/N} \times \mathbf{r}_{S_j/B} + \boldsymbol{\omega}_{B/N} \times (\boldsymbol{\omega}_{B/N} \times \mathbf{r}_{S_j/B})] = 0 \end{aligned} \quad (44)$$

$$\begin{aligned}
K - \left[dm_p \hat{\mathbf{s}}_{j,3}^T + \sum_{i=j+1}^{N_p} 2dm_p \hat{\mathbf{s}}_{j,3}^T \right] \ddot{\mathbf{r}}_{B/N} - \left[I_{s_j,2} \hat{\mathbf{s}}_{j,2}^T - m_p d\hat{\mathbf{s}}_{j,3}^T [\tilde{\mathbf{r}}_{S_i/B}] - \sum_{i=j+1}^{N_p} 2m_p d\hat{\mathbf{s}}_{j,3}^T [\tilde{\mathbf{r}}_{S_i/B}] \right] \dot{\boldsymbol{\omega}}_{B/N} - \\
I_{s_j,2} \sum_{i=1}^{N_p} \ddot{\theta}_i - (I_{s_{j,1}} - I_{s_{j,3}}) \omega_{s_{j,3}} \omega_{s_{j,1}} + 2d\hat{\mathbf{s}}_{j,3}^T \mathbf{F}_{ext,j+1} - m_p d\hat{\mathbf{s}}_{j,3}^T [\mathbf{r}_{S_j/B}'' + \sum_{i=1}^{N_p} 2\mathbf{r}_{S_i/B}''] \\
- m_p d\hat{\mathbf{s}}_{j,3}^T \left[2[\tilde{\boldsymbol{\omega}}_{B/N}] \mathbf{r}_{S_j/B}' + [\tilde{\boldsymbol{\omega}}_{B/N}] [\tilde{\boldsymbol{\omega}}_{B/N}] \mathbf{r}_{S_j/B} + \sum_{i=j+1}^{N_p} \left(4[\tilde{\boldsymbol{\omega}}_{B/N}] \mathbf{r}_{S_j/B}' + 2[\tilde{\boldsymbol{\omega}}_{B/N}] [\tilde{\boldsymbol{\omega}}_{B/N}] \mathbf{r}_{S_j/B} \right) \right] = 0
\end{aligned} \tag{45}$$

The $\mathbf{r}_{S_j/B}''$ terms contain $\ddot{\theta}$ terms and thus need to be rewritten to a usable form. This is done by writing it out for several panels and finding a pattern, the result of this is shown next:

$$\begin{aligned}
K - \left[dm_p \hat{\mathbf{s}}_{j,3}^T + \sum_{i=j+1}^{N_p} 2dm_p \hat{\mathbf{s}}_{j,3}^T \right] \ddot{\mathbf{r}}_{B/N} - \left[I_{s_j,2} \hat{\mathbf{s}}_{j,2}^T - m_p d\hat{\mathbf{s}}_{j,3}^T [\tilde{\mathbf{r}}_{S_i/B}] - \sum_{i=j+1}^{N_p} 2m_p d\hat{\mathbf{s}}_{j,3}^T [\tilde{\mathbf{r}}_{S_i/B}] \right] \dot{\boldsymbol{\omega}}_{B/N} - \\
I_{s_j,2} \sum_{i=1}^{N_p} \ddot{\theta}_i - (I_{s_{j,1}} - I_{s_{j,3}}) \omega_{s_{j,3}} \omega_{s_{j,1}} + 2d\hat{\mathbf{s}}_{j,3}^T \mathbf{F}_{ext,j+1} \\
- m_p d\hat{\mathbf{s}}_{j,3}^T \left[2[\tilde{\boldsymbol{\omega}}_{B/N}] \mathbf{r}_{S_j/B}' + [\tilde{\boldsymbol{\omega}}_{B/N}] [\tilde{\boldsymbol{\omega}}_{B/N}] \mathbf{r}_{S_j/B} + \sum_{i=j+1}^{N_p} \left(4[\tilde{\boldsymbol{\omega}}_{B/N}] \mathbf{r}_{S_j/B}' + 2[\tilde{\boldsymbol{\omega}}_{B/N}] [\tilde{\boldsymbol{\omega}}_{B/N}] \mathbf{r}_{S_j/B} \right) \right] \\
- m_p d^2 \hat{\mathbf{s}}_{j,3}^T \sum_{i=1}^{N_p} \left[\ddot{\theta}_i \sum_{k=i}^{N_p} (2\hat{s}_{k,3} + 4\hat{s}_{k,3}(N_p - j) - H[k - j]4\hat{s}_{k,3}(k - j)) - H[j - i]\hat{s}_{j,3} + \right. \\
\left. \left(\sum_{n=1}^i \dot{\theta}_n \right)^2 (2\hat{s}_{i,1} + 4\hat{s}_{i,1}(N_p - j) - H[i - j]4\hat{s}_{i,1}(i - j)) - \left(\sum_{n=1}^i \dot{\theta}_n \right)^2 \hat{s}_{j,1} \right] = 0 \tag{46}
\end{aligned}$$

This finally leads to:

$$\begin{aligned}
\left[dm_p \hat{\mathbf{s}}_{j,3}^T + \sum_{i=j+1}^{N_p} 2dm_p \hat{\mathbf{s}}_{j,3}^T \right] \ddot{\mathbf{r}}_{B/N} + \left[I_{s_j,2} \hat{\mathbf{s}}_{j,2}^T - m_p d\hat{\mathbf{s}}_{j,3}^T [\tilde{\mathbf{r}}_{S_i/B}] - \sum_{i=j+1}^{N_p} 2m_p d\hat{\mathbf{s}}_{j,3}^T [\tilde{\mathbf{r}}_{S_i/B}] \right] \dot{\boldsymbol{\omega}}_{B/N} + \\
\sum_{i=1}^{N_p} \left[I_{s_j,2} H[j - i] + m_p d^2 \hat{\mathbf{s}}_{j,3}^T \sum_{k=i}^{N_p} (2\hat{s}_{k,3} + 4\hat{s}_{k,3}(N_p - j) - H[k - j]4\hat{s}_{k,3}(k - j)) - H[j - i]\hat{s}_{j,3} \right] \ddot{\theta}_i \\
= K + 2d\hat{\mathbf{s}}_{j,3}^T \mathbf{F}_{ext,j+1} - (I_{s_{j,1}} - I_{s_{j,3}}) \omega_{s_{j,3}} \omega_{s_{j,1}} - m_p d\hat{\mathbf{s}}_{j,3}^T \left[2[\tilde{\boldsymbol{\omega}}_{B/N}] \mathbf{r}_{S_j/B}' + [\tilde{\boldsymbol{\omega}}_{B/N}] [\tilde{\boldsymbol{\omega}}_{B/N}] \mathbf{r}_{S_j/B} + \right. \\
\left. \sum_{i=j+1}^{N_p} \left(4[\tilde{\boldsymbol{\omega}}_{B/N}] \mathbf{r}_{S_j/B}' + 2[\tilde{\boldsymbol{\omega}}_{B/N}] [\tilde{\boldsymbol{\omega}}_{B/N}] \mathbf{r}_{S_j/B} \right) + \left(\sum_{n=1}^i \dot{\theta}_n \right)^2 (2\hat{s}_{i,1} + 4\hat{s}_{i,1}(N_p - j) - H[i - j]4\hat{s}_{i,1}(i - j)) - \left(\sum_{n=1}^i \dot{\theta}_n \right)^2 \hat{s}_{j,1} \right]
\end{aligned} \tag{47}$$

Where $H[x]$ is the Heaviside function.

III Back Substitution Method

The Back substitution method is used to gain a simpler expression that combines the three equations of motion. First, Eq. (47) is rearranged so that the second order state variables for the panel motions are isolated on the left hand

side:

$$\begin{aligned}
& \sum_{i=1}^{N_p} \left[I_{s_j,2} H[j-i] + m_p d^2 \hat{s}_{j,3}^T \sum_{k=i}^{N_p} (2\hat{s}_{k,3} + 4\hat{s}_{k,3}(N_p-j) - H[k-j]4\hat{s}_{k,3}(k-j)) - H[j-i]\hat{s}_{j,3} \right] \ddot{\theta}_i = \\
& - \left[dm_p \hat{s}_{j,3}^T + \sum_{i=j+1}^{N_p} 2dm_p \hat{s}_{j,3}^T \right] \ddot{\mathbf{r}}_{B/N} - \left[I_{s_j,2} \hat{s}_{j,2}^T - m_p d \hat{s}_{j,3}^T [\tilde{\mathbf{r}}_{S_i/B}] - \sum_{i=j+1}^{N_p} 2m_p d \hat{s}_{j,3}^T [\tilde{\mathbf{r}}_{S_i/B}] \right] \dot{\boldsymbol{\omega}}_{B/N} + \\
& K + 2d \hat{s}_{j,3}^T \mathbf{F}_{ext,j+1} - (I_{s_{j,1}} - I_{s_{j,3}}) \omega_{s_{j,3}} \omega_{s_{j,1}} - m_p d \hat{s}_{j,3}^T \left[2[\tilde{\boldsymbol{\omega}}_{B/N}] \mathbf{r}'_{S_j/B} + [\tilde{\boldsymbol{\omega}}_{B/N}] [\tilde{\boldsymbol{\omega}}_{B/N}] \mathbf{r}_{S_j/B} + \right. \\
& \left. \sum_{i=j+1}^{N_p} \left(4[\tilde{\boldsymbol{\omega}}_{B/N}] \mathbf{r}'_{S_j/B} + 2[\tilde{\boldsymbol{\omega}}_{B/N}] [\tilde{\boldsymbol{\omega}}_{B/N}] \mathbf{r}_{S_j/B} \right) + \left(\sum_{n=1}^i \dot{\theta}_i \right)^2 (2\hat{s}_{i,1} + 4\hat{s}_{i,1}(N_p-j) - H[i-j]4\hat{s}_{i,1}(i-j)) - \left(\sum_{n=1}^i \dot{\theta}_i \right)^2 \hat{s}_{j,1} \right]
\end{aligned} \tag{48}$$

Now, defining the elements of a matrix $[A]$ as:

$$a_{j,i} = I_{s_j,2} H[j-i] + m_p d^2 \hat{s}_{j,3}^T \sum_{k=i}^{N_p} \left(2\hat{s}_{k,3} + 4\hat{s}_{k,3}(N_p-j) - H[k-j]4\hat{s}_{k,3}(k-j) \right) - H[j-i]\hat{s}_{j,3} \tag{49}$$

And defining the row elements of a matrix $[F]$ as:

$$\mathbf{f}_{j,1} = -[dm_p \hat{s}_{j,3}^T + \sum_{i=j+1}^{N_p} 2dm_p \hat{s}_{j,3}^T] \tag{50}$$

With a matrix $[G]$ which has row elements defined as:

$$\mathbf{g}_{j,1} = -[I_{s_j,2} \hat{s}_{j,2}^T - m_p d \hat{s}_{j,3}^T [\tilde{\mathbf{r}}_{S_i/B}] - \sum_{i=j+1}^{N_p} 2m_p d \hat{s}_{j,3}^T [\tilde{\mathbf{r}}_{S_i/B}] \tag{51}$$

Also defining the vector \mathbf{v}

$$\begin{aligned}
\mathbf{v}_{j,1} = & K + 2d \hat{s}_{j,3}^T \mathbf{F}_{ext,j+1} - (I_{s_{j,1}} - I_{s_{j,3}}) \omega_{s_{j,3}} \omega_{s_{j,1}} - m_p d \hat{s}_{j,3}^T \left[2[\tilde{\boldsymbol{\omega}}_{B/N}] \mathbf{r}'_{S_j/B} + [\tilde{\boldsymbol{\omega}}_{B/N}] [\tilde{\boldsymbol{\omega}}_{B/N}] \mathbf{r}_{S_j/B} + \right. \\
& \left. \sum_{i=j+1}^{N_p} \left(4[\tilde{\boldsymbol{\omega}}_{B/N}] \mathbf{r}'_{S_j/B} + 2[\tilde{\boldsymbol{\omega}}_{B/N}] [\tilde{\boldsymbol{\omega}}_{B/N}] \mathbf{r}_{S_j/B} \right) + \left(\sum_{n=1}^i \dot{\theta}_i \right)^2 (2\hat{s}_{i,1} + 4\hat{s}_{i,1}(N_p-j) - H[i-j]4\hat{s}_{i,1}(i-j)) - \left(\sum_{n=1}^i \dot{\theta}_i \right)^2 \hat{s}_{j,1} \right]
\end{aligned} \tag{52}$$

Eq. (48) can then be written in matrix form to utilize some linear algebra techniques.

$$[A] \begin{bmatrix} \ddot{\theta}_1 \\ \vdots \\ \ddot{\theta}_{N_p} \end{bmatrix} = [F] \ddot{\mathbf{r}}_{B/N} + [G] \dot{\boldsymbol{\omega}}_{B/N} + \mathbf{v} \tag{53}$$

Eq. (53) can now be solved by inverting matrix $[A]$. Note the definition $[E] = [A]^{-1}$.

$$\begin{bmatrix} \ddot{\theta}_1 \\ \vdots \\ \ddot{\theta}_{N_p} \end{bmatrix} = [E][F] \ddot{\mathbf{r}}_{B/N} + [E][G] \dot{\boldsymbol{\omega}}_{B/N} + [E]\mathbf{v} \tag{54}$$

And the subcomponents of $[E]$ are defined as

$$[E] = \begin{bmatrix} \mathbf{e}_1^T \\ \vdots \\ \mathbf{e}_{N_p}^T \end{bmatrix} \tag{55}$$

Since the modified Euler's equation, Eq. (36), has $\ddot{\theta}_i$ terms, it is more convenient to use the expression for $\ddot{\theta}_i$ as

$$\ddot{\theta}_i = e_i^T [F] \ddot{\mathbf{r}}_{B/N} + e_i^T [G] \dot{\boldsymbol{\omega}}_{B/N} + e_i^T \mathbf{v} \quad (56)$$

The next step in the back substitution method is to analytically substitute Eq. (56) into the translational and rotational EOMs. Performing this substitution for translation yields:

$$\begin{aligned} m_{sc} \ddot{\mathbf{r}}_{B/N} - m_{sc} [\tilde{\mathbf{c}}] \dot{\boldsymbol{\omega}}_{B/N} + \sum_{i=1}^{N_p} \left[\sum_{k=i}^{N_p} (2[N_p - k] + 1) dm_p \hat{\mathbf{s}}_{k,3} [e_i^T [F] \ddot{\mathbf{r}}_{B/N} + e_i^T [G] \dot{\boldsymbol{\omega}}_{B/N} + e_i^T \mathbf{v}] \right] &= \mathbf{F}_{ext} - 2m_{sc} [\tilde{\boldsymbol{\omega}}_{B/N}] \mathbf{c}' \\ &- m_{sc} [\tilde{\boldsymbol{\omega}}_{B/N}] [\tilde{\boldsymbol{\omega}}_{B/N}] \mathbf{c} - \sum_{i=1}^{N_p} \left[\left(\sum_{k=1}^i \dot{\theta}_k \right)^2 (2[N_p - i] + 1) dm_p \hat{\mathbf{s}}_{i,1} \right] \end{aligned} \quad (57)$$

Combining like terms yields:

$$\begin{aligned} &\left\{ m_{sc} [I_{3 \times 3}] + \sum_{i=1}^{N_p} \left[\sum_{k=i}^{N_p} (2[N_p - k] + 1) dm_p \hat{\mathbf{s}}_{k,3} \right] e_i^T [F] \right\} \ddot{\mathbf{r}}_{B/N} + \left\{ -m_{sc} [\tilde{\mathbf{c}}] + \sum_{i=1}^{N_p} \left[\sum_{k=i}^{N_p} (2[N_p - k] + 1) dm_p \hat{\mathbf{s}}_{k,3} \right] e_i^T [G] \right\} \dot{\boldsymbol{\omega}}_{B/N} \\ &= \mathbf{F}_{ext} - 2m_{sc} [\tilde{\boldsymbol{\omega}}_{B/N}] \mathbf{c}' - m_{sc} [\tilde{\boldsymbol{\omega}}_{B/N}] [\tilde{\boldsymbol{\omega}}_{B/N}] \mathbf{c} - \sum_{i=1}^{N_p} \left[\left(\sum_{k=1}^i \dot{\theta}_k \right)^2 (2[N_p - i] + 1) dm_p \hat{\mathbf{s}}_{i,1} \right] \\ &\quad - \sum_{i=1}^{N_p} \left[\sum_{k=i}^{N_p} (2[N_p - k] + 1) dm_p \hat{\mathbf{s}}_{k,3} e_i^T \mathbf{v} \right] \end{aligned} \quad (58)$$

Substitution into the rotational equation of motion:

$$\begin{aligned} &m_{sc} [\tilde{\mathbf{c}}] \ddot{\mathbf{r}}_{B/N} + [I_{sc,B}] \dot{\boldsymbol{\omega}}_{B/N} + \sum_{i=1}^{N_p} \left[\sum_{k=i}^{N_p} (I_{s_{k,2}} \hat{\mathbf{s}}_{k,2} + [\tilde{\mathbf{r}}_{S_k/B}] + \sum_{n=k+1}^{N_p} 2[\tilde{\mathbf{r}}_{S_n/B}]) m_p d\hat{\mathbf{s}}_{k,3} \right] [e_i^T [F] \ddot{\mathbf{r}}_{B/N} + e_i^T [G] \dot{\boldsymbol{\omega}}_{B/N} + e_i^T \mathbf{v}] \\ &= -[\tilde{\boldsymbol{\omega}}_{B/N}] [I_{sc,B}] \boldsymbol{\omega}_{B/N} - [I'_{sc,B}] \boldsymbol{\omega}_{B/N} - \sum_{i=1}^{N_p} \left(m_p [\tilde{\boldsymbol{\omega}}_{B/N}] [\tilde{\mathbf{r}}_{S_i/B}] \mathbf{r}'_{S_i/B} + \left(\sum_{k=1}^i \dot{\theta}_k \right)^2 [\tilde{\mathbf{r}}_{S_i/B}] + \sum_{n=i+1}^{N_p} 2[\tilde{\mathbf{r}}_{S_n/B}] \right) m_p d\hat{\mathbf{s}}_{i,1} \\ &\quad + I_{s_{i,2}} \left(\sum_{k=1}^i \dot{\theta}_k \right) [\tilde{\boldsymbol{\omega}}_{B/N}] \hat{\mathbf{s}}_{i,2} \Big) + \mathbf{L}_B \end{aligned} \quad (59)$$

And combining like terms yields:

$$\begin{aligned} &\left\{ m_{sc} [\tilde{\mathbf{c}}] + \sum_{i=1}^{N_p} \left[\sum_{k=i}^{N_p} (I_{s_{k,2}} \hat{\mathbf{s}}_{k,2} + [\tilde{\mathbf{r}}_{S_k/B}] + \sum_{n=k+1}^{N_p} 2[\tilde{\mathbf{r}}_{S_n/B}]) m_p d\hat{\mathbf{s}}_{k,3} \right] e_i^T [F] \right\} \ddot{\mathbf{r}}_{B/N} \\ &\quad + \left\{ [I_{sc,B}] + \sum_{i=1}^{N_p} \left[\sum_{k=i}^{N_p} (I_{s_{k,2}} \hat{\mathbf{s}}_{k,2} + [\tilde{\mathbf{r}}_{S_k/B}] + \sum_{n=k+1}^{N_p} 2[\tilde{\mathbf{r}}_{S_n/B}]) m_p d\hat{\mathbf{s}}_{k,3} \right] e_i^T [G] \right\} \dot{\boldsymbol{\omega}}_{B/N} \\ &= -[\tilde{\boldsymbol{\omega}}_{B/N}] [I_{sc,B}] \boldsymbol{\omega}_{B/N} - [I'_{sc,B}] \boldsymbol{\omega}_{B/N} - \sum_{i=1}^{N_p} \left(m_p [\tilde{\boldsymbol{\omega}}_{B/N}] [\tilde{\mathbf{r}}_{S_i/B}] \mathbf{r}'_{S_i/B} + \left(\sum_{k=1}^i \dot{\theta}_k \right)^2 [\tilde{\mathbf{r}}_{S_i/B}] + \sum_{n=i+1}^{N_p} 2[\tilde{\mathbf{r}}_{S_n/B}] \right) m_p d\hat{\mathbf{s}}_{i,1} \\ &\quad + I_{s_{i,2}} \left(\sum_{k=1}^i \dot{\theta}_k \right) [\tilde{\boldsymbol{\omega}}_{B/N}] \hat{\mathbf{s}}_{i,2} \Big) + \mathbf{L}_B - \sum_{i=1}^{N_p} \left[\sum_{k=i}^{N_p} (I_{s_{k,2}} \hat{\mathbf{s}}_{k,2} + [\tilde{\mathbf{r}}_{S_k/B}] + \sum_{n=k+1}^{N_p} 2[\tilde{\mathbf{r}}_{S_n/B}]) m_p d\hat{\mathbf{s}}_{k,3} \right] e_i^T \mathbf{v} \end{aligned} \quad (60)$$

With the following definitions:

$$[A_{contr}] = \sum_{i=1}^{N_p} \left[\sum_{k=i}^{N_p} (2[N_p - k] + 1) dm_p \hat{\mathbf{s}}_{k,3} \right] e_i^T [F] \quad (61)$$

$$[B_{\text{contr}}] = \sum_{i=1}^{N_p} \left[\sum_{k=i}^{N_p} (2[N_p - k] + 1) dm_p \hat{\mathbf{s}}_{k,3} \right] e_i^T [G] \quad (62)$$

$$\mathbf{v}_{\text{trans,contr}} = - \sum_{i=1}^{N_p} \left[\left(\sum_{k=1}^i \dot{\theta}_k \right)^2 (2[N_p - i] + 1) dm_p \hat{\mathbf{s}}_{i,1} \right] - \sum_{i=1}^{N_p} \left[\sum_{k=i}^{N_p} (2[N_p - k] + 1) dm_p \hat{\mathbf{s}}_{k,3} e_i^T \mathbf{v} \right] \quad (63)$$

$$[C_{\text{contr}}] = \sum_{i=1}^{N_p} \left[\sum_{k=i}^{N_p} (I_{s_{k,2}} \hat{\mathbf{s}}_{k,2} + [\tilde{\mathbf{r}}_{S_k/B}] + \sum_{n=k+1}^{N_p} 2[\tilde{\mathbf{r}}_{S_n/B}] m_p d\hat{\mathbf{s}}_{k,3} \right] e_i^T [F] \quad (64)$$

$$[D_{\text{contr}}] = \sum_{i=1}^{N_p} \left[\sum_{k=i}^{N_p} (I_{s_{k,2}} \hat{\mathbf{s}}_{k,2} + [\tilde{\mathbf{r}}_{S_k/B}] + \sum_{n=k+1}^{N_p} 2[\tilde{\mathbf{r}}_{S_n/B}] m_p d\hat{\mathbf{s}}_{k,3} \right] e_i^T [G] \quad (65)$$

$$\begin{aligned} [v_{\text{rot,contr}}] = & - \sum_{i=1}^{N_p} \left(m_p [\tilde{\boldsymbol{\omega}}_{\mathcal{B}/\mathcal{N}}] [\tilde{\mathbf{r}}_{S_i/B}] \mathbf{r}'_{S_i/B} + \left(\sum_{k=1}^i \dot{\theta} \right)^2 [\tilde{\mathbf{r}}_{S_i/B}] + \sum_{n=i+1}^{N_p} 2[\tilde{\mathbf{r}}_{S_n/B}] m_p d\hat{\mathbf{s}}_{i,1} + I_{s_{i,2}} \left(\sum_{k=1}^i \dot{\theta}_k \right) [\tilde{\boldsymbol{\omega}}_{\mathcal{B}/\mathcal{N}}] \hat{\mathbf{s}}_{i,2} \right) \\ & - \sum_{i=1}^{N_p} \left[\sum_{k=i}^{N_p} (I_{s_{k,2}} \hat{\mathbf{s}}_{k,2} + [\tilde{\mathbf{r}}_{S_k/B}] + \sum_{n=k+1}^{N_p} 2[\tilde{\mathbf{r}}_{S_n/B}] m_p d\hat{\mathbf{s}}_{k,3} \right] e_i^T \mathbf{v} \end{aligned} \quad (66)$$

The full back substitution matrices then become:

$$[A] = m_{\text{sc}} [I_{3 \times 3}] + [A_{\text{contr}}] \quad (67)$$

$$[B] = -m_{\text{sc}} [\tilde{\mathbf{c}}] + [B_{\text{contr}}] \quad (68)$$

$$\mathbf{v}_{\text{trans}} = \mathbf{F} - 2m_{\text{sc}} [\tilde{\boldsymbol{\omega}}_{\mathcal{B}/\mathcal{N}}] \mathbf{c}' - m_{\text{sc}} [\tilde{\boldsymbol{\omega}}_{\mathcal{B}/\mathcal{N}}] [\tilde{\boldsymbol{\omega}}_{\mathcal{B}/\mathcal{N}}] \mathbf{c} + \mathbf{v}_{\text{trans,contr}} \quad (69)$$

$$[C] = m_{\text{sc}} + [C_{\text{contr}}] \quad (70)$$

$$[D] = [I_{\text{sc},B}] + [D_{\text{contr}}] \quad (71)$$

$$\mathbf{v}_{\text{rot}} = -[\tilde{\boldsymbol{\omega}}_{\mathcal{B}/\mathcal{N}}] [I_{\text{sc},B}] \boldsymbol{\omega}_{\mathcal{B}/\mathcal{N}} - [I'_{\text{sc},B}] \boldsymbol{\omega}_{\mathcal{B}/\mathcal{N}} + \mathbf{L}_B + \mathbf{v}_{\text{rot,contr}} \quad (72)$$

This produces the following simplified equations:

$$\begin{bmatrix} [A] & [B] \\ [C] & [D] \end{bmatrix} \begin{bmatrix} \ddot{\mathbf{r}}_{B/N} \\ \dot{\boldsymbol{\omega}}_{\mathcal{B}/\mathcal{N}} \end{bmatrix} = \begin{bmatrix} \mathbf{v}_{\text{trans}} \\ \mathbf{v}_{\text{rot}} \end{bmatrix} \quad (73)$$

Solving the system-of-equations by

$$\dot{\boldsymbol{\omega}}_{\mathcal{B}/\mathcal{N}} = \left([D] - [C][A]^{-1}[B] \right)^{-1} (\mathbf{v}_{\text{rot}} - [C][A]^{-1}\mathbf{v}_{\text{trans}}) \quad (74)$$

$$\ddot{\mathbf{r}}_{B/N} = [A]^{-1} (\mathbf{v}_{\text{trans}} - [B]\dot{\boldsymbol{\omega}}_{\mathcal{B}/\mathcal{N}}) \quad (75)$$

Now Eq. (74) and (75) can be used to solve for $\dot{\boldsymbol{\omega}}_{\mathcal{B}/\mathcal{N}}$ and $\ddot{\mathbf{r}}_{B/N}$. Once these second order state variables are solved for, Eq. (56) can be used to directly solve for $\ddot{\theta}_i$. This shows that the back substitution method can work seamlessly for interconnected bodies.