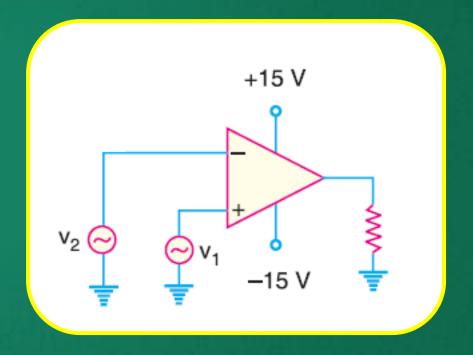
Basic Electronic Circuits (IEC-103)

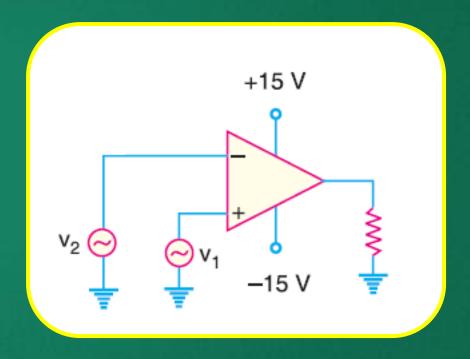
Lecture-08

Nonlinear Applications of Operational Amplifiers

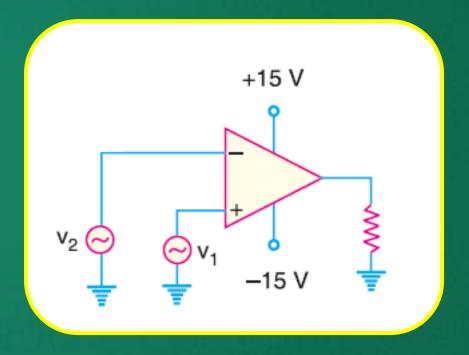
Non-Linear Op-Amp Applications

- ☐ Applications using saturation
 - Comparators
 - Comparator with hysteresis (Schmitt trigger)
 - Square wave and triangular wave generators
- ☐ Applications using active feedback components
 - Log, antilog, squaring etc. amplifiers
 - Precision rectifier





☐ A comparator is an op-amp circuit without negative feedback and takes the advantage of very high open-loop gain.

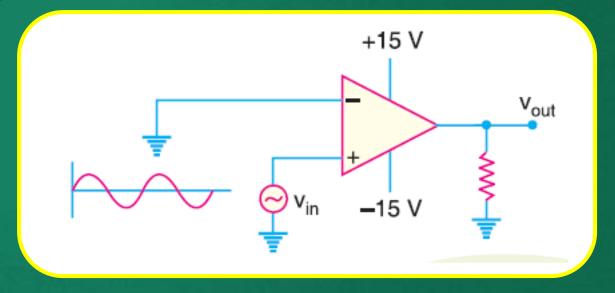


- ☐ A comparator is an op-amp circuit without negative feedback and takes the advantage of very high open-loop gain.
- ☐ It is operated in a non-linear mode.

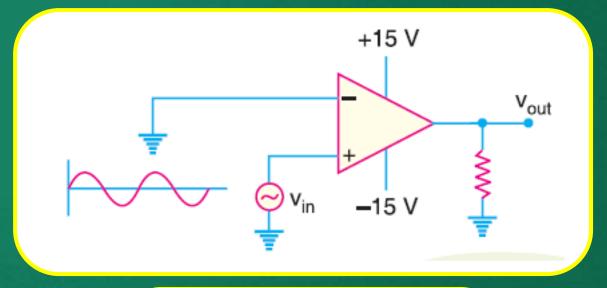
$$+V_{sat} = +V_{supply} - 2 = 15 - 2 = +13 \text{ V}$$

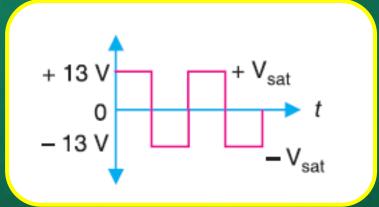
 $-V_{sat} = -V_{supply} + 2 = -15 + 2 = -13 \text{ V}$

Comparator (Square Wave Generator)

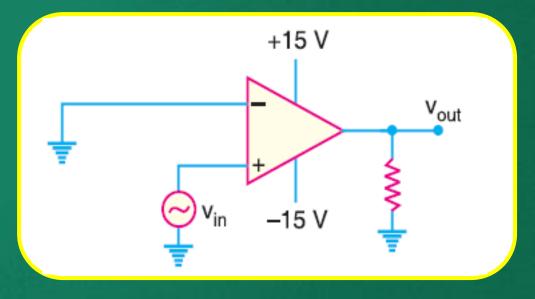


Comparator (Square Wave Generator)

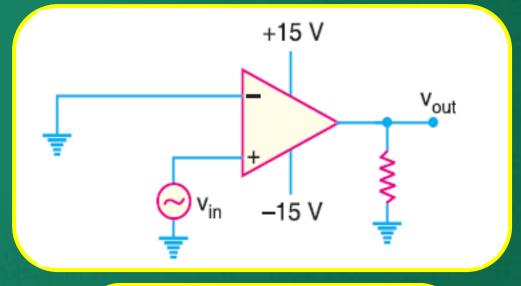


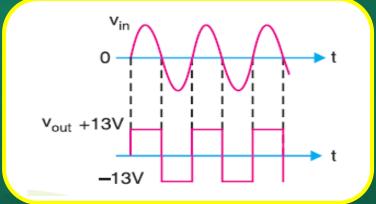


Comparator (Zero Crossing Detector)

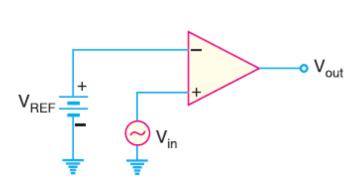


Comparator (Zero Crossing Detector)

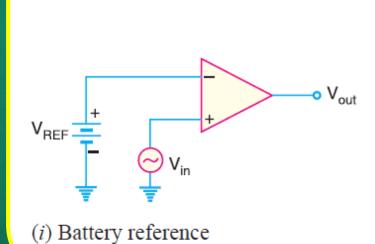


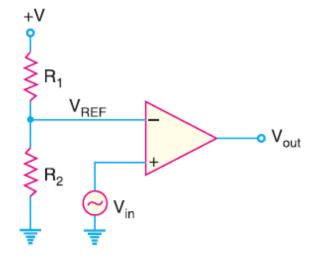


Comparator (Level Detector)



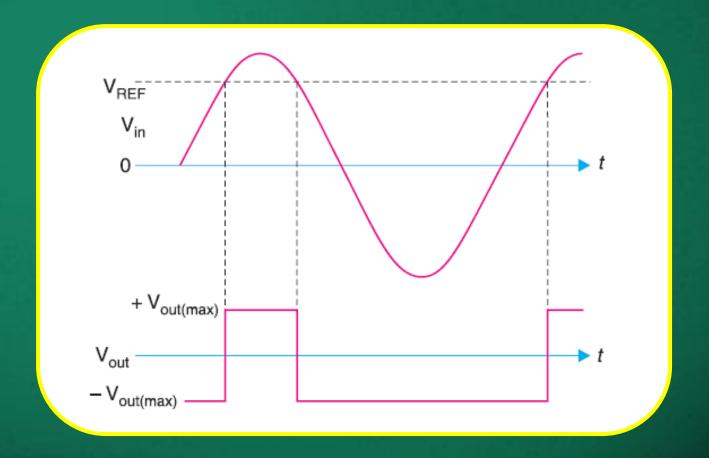
Comparator (Level Detector)





(ii) Voltage-divider reference

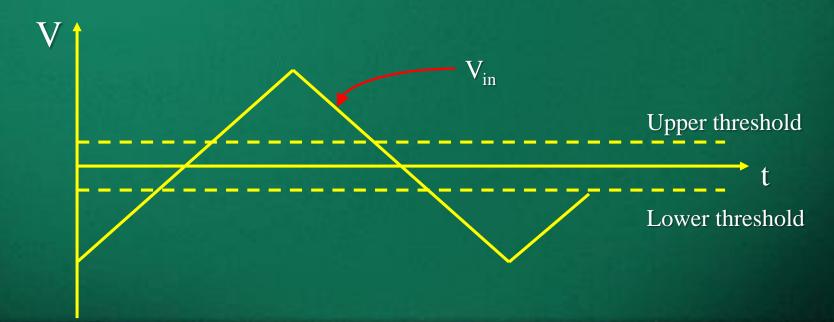
Comparator (Level Detector)



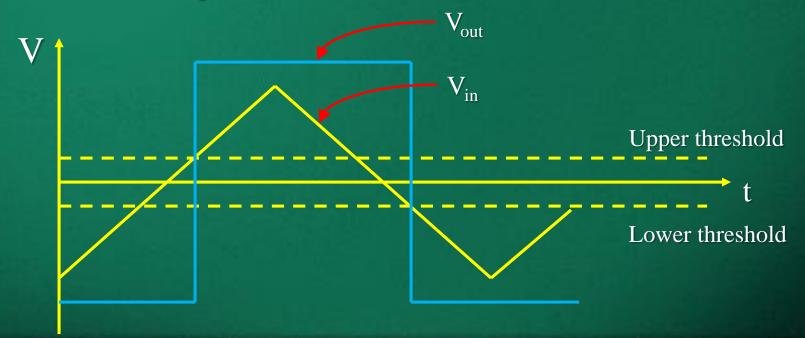
☐ A comparator with hysteresis has a safety margin.

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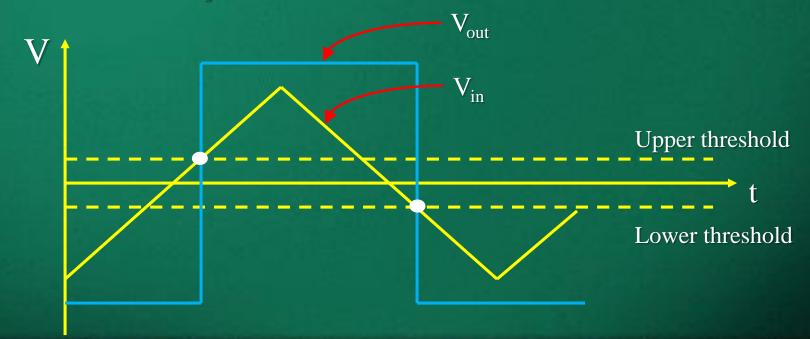
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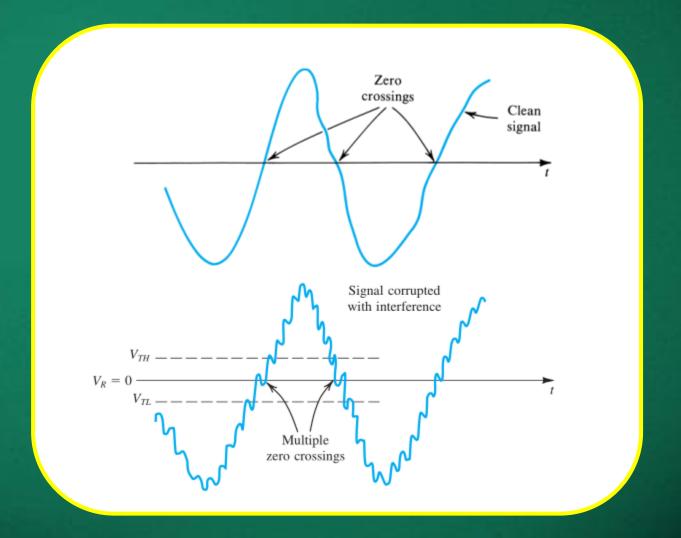
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- ☐ The advantage is immunity against small noise spikes.
- ☐ It takes at minimum the hysteresis range to make it switch.

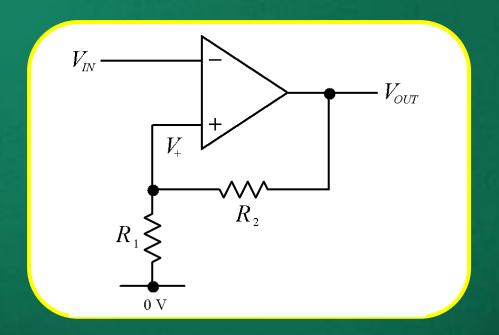
Rejecting Interference

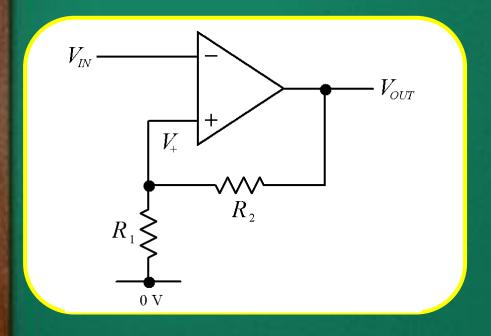


☐ The Schmitt trigger is an op-amp comparator circuit featuring hysteresis.

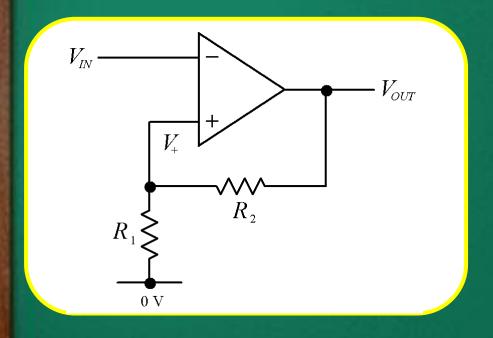
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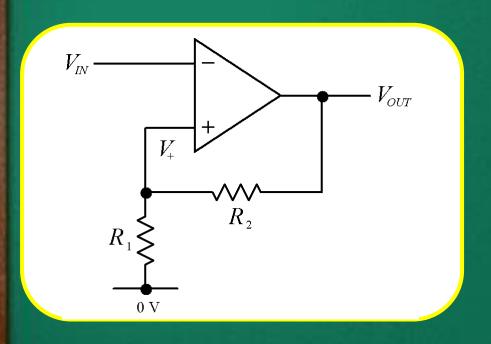




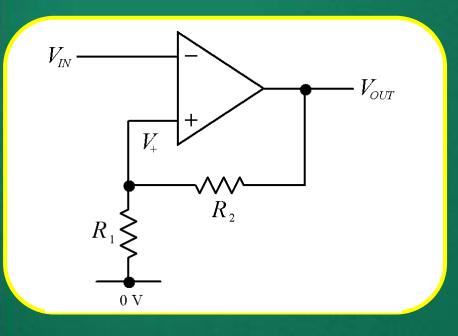
Switching occurs when:



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$$V_{IN} = V_{-} = V_{+} = V_{OUT} \frac{R_{1}}{R_{1} + R_{2}}$$



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But,

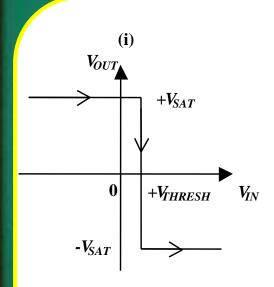
$$V_{OUT} = \pm V_{SAT}$$

$$\therefore V_{THRESH} = \pm V_{SAT} \frac{R_1}{R_1 + R_2}$$

Input-Output Relationship

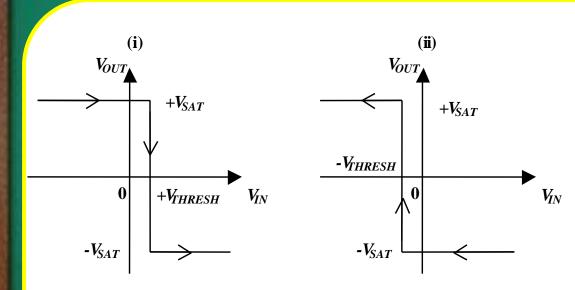


Input-Output Relationship



V_{IN} increasing

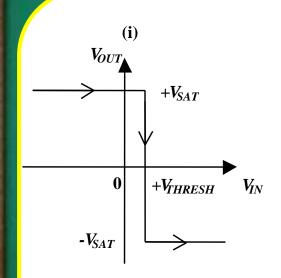
Input-Output Relationship

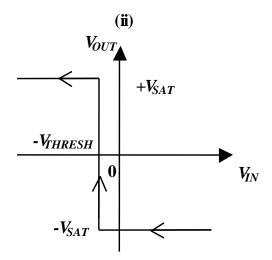


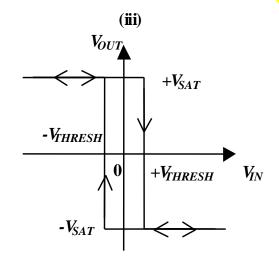
 V_{IN} increasing

V_{IN} decreasing

Input-Output Relationship







V_{IN} increasing

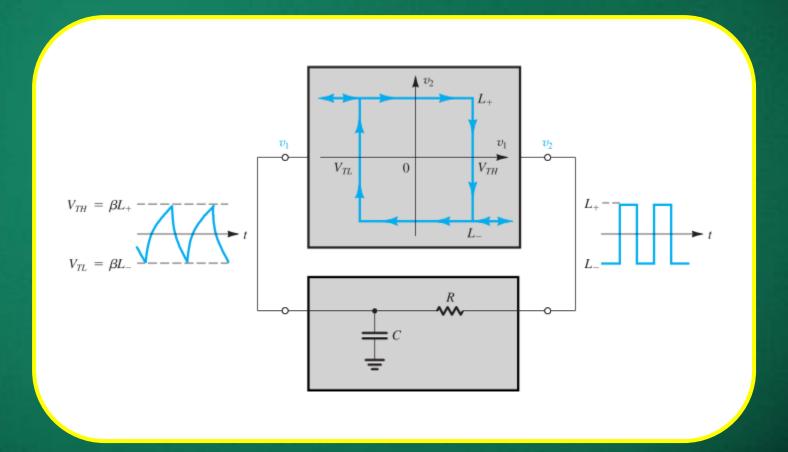
V_{IN} decreasing

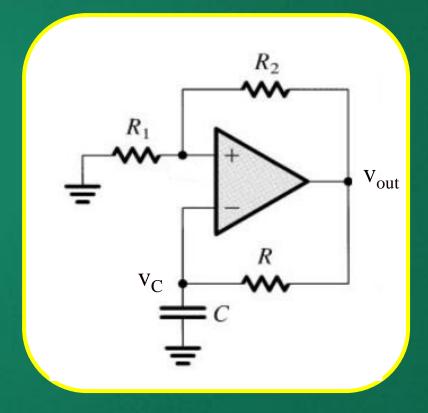
(i) & (ii) combined

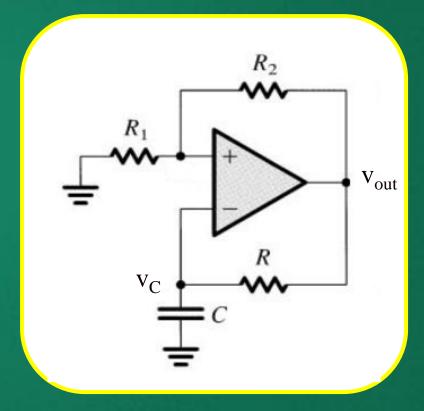
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- ☐ The circuits generating a square wave can be called as relaxation oscillator or astable multivibrator.

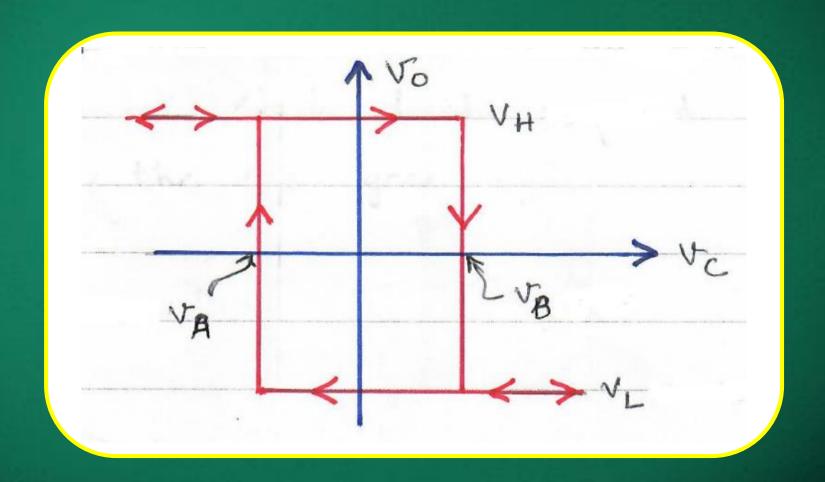




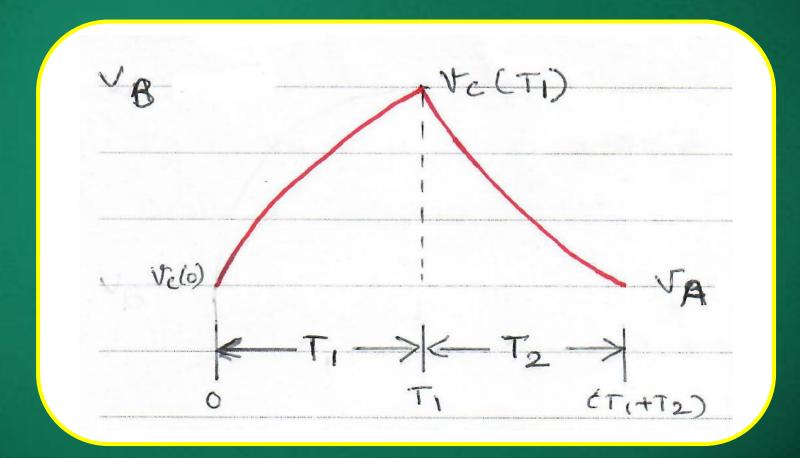


The circuit's frequency of oscillation will depend on the charging and discharging of capacitor C through feedback resistor R.

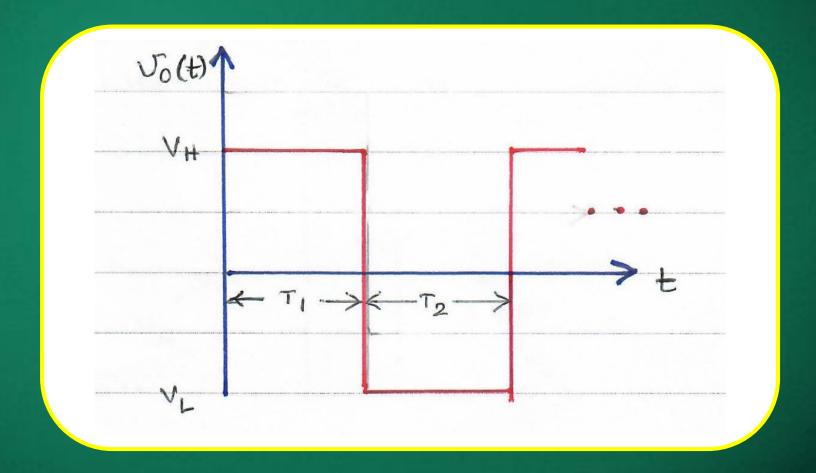
Hysteresis Loop

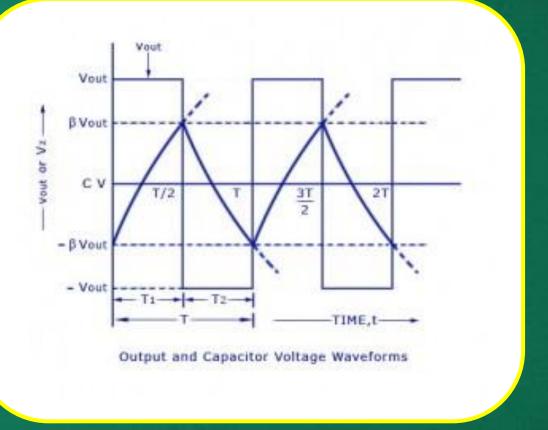


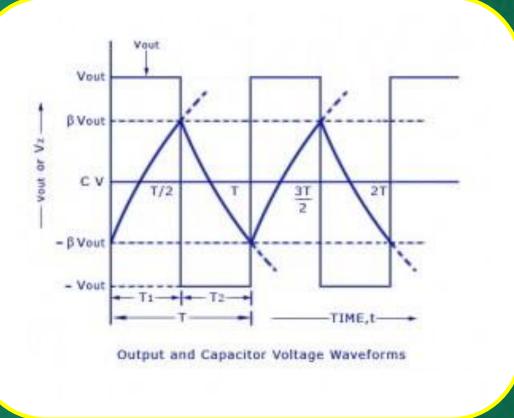
Capacitor Voltage



Output Voltage







$$T_1 = RC \ln \left(\frac{1+\beta}{1-\beta} \right)$$
 where $\beta = \frac{R_1}{R_1 + R_2}$

$$T_2 = RC \ln \left(\frac{1+\beta}{1-\beta} \right)$$
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If
$$R_1 = R_2 = R$$
 then $\beta = 0.5$

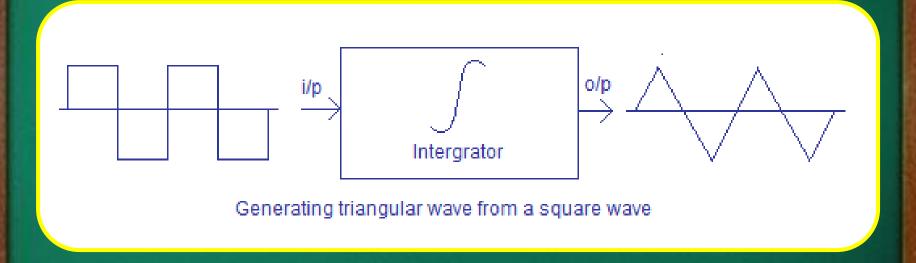
$$T_2 = RC \ln \left(\frac{1+\beta}{1-\beta} \right)$$
 where $\beta = \frac{R_1}{R_1 + R_2}$

$$T_1 = T_2$$

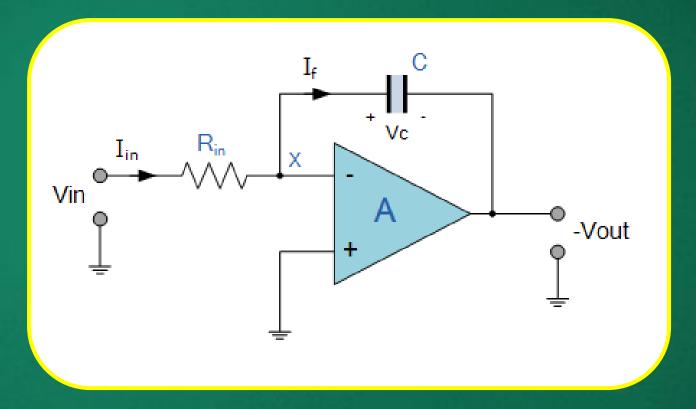
$$T = T_1 + T_2 = 2RC \ln \left(\frac{1+\beta}{1-\beta} \right)$$

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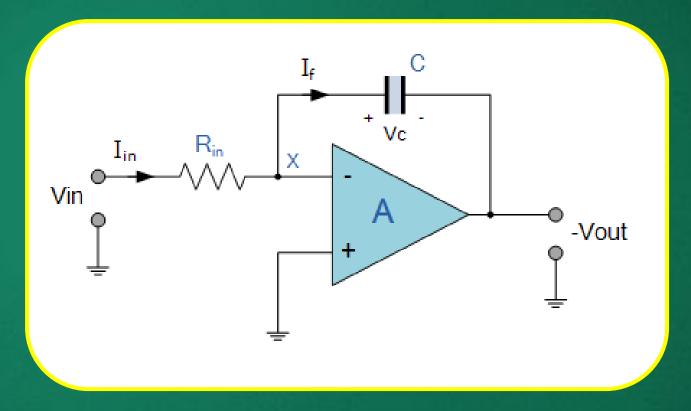
$$\Rightarrow T = 2RC \ln \left(\frac{1+0.5}{1-0.5} \right) = 2RC \ln(3) = 2.197RC$$



Integrator Circuit

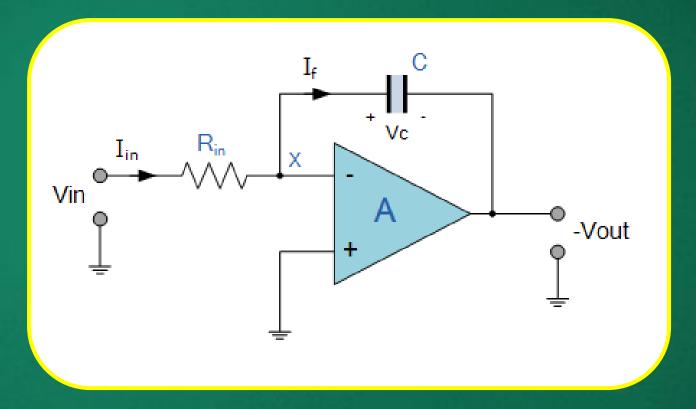


Integrator Circuit



$$V_{\text{out}}(t) = -\frac{1}{R_{\text{in}}C} \int_0^t V_{\text{in}}(t) dt$$

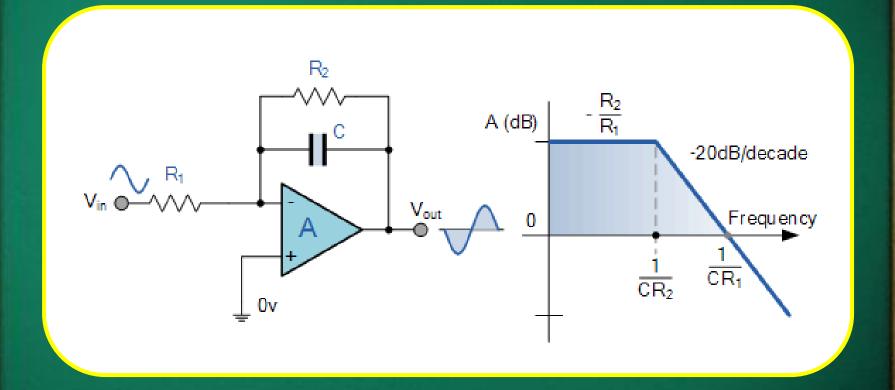
Integrator Circuit



$$V_{\text{out}}(t) = -\frac{1}{R_{\text{in}}C} \int_0^t V_{\text{in}}(t) dt$$

$$V_{out}(\omega) = -\frac{1}{j\omega R_{in}C} V_{in}(\omega)$$

Practical Integrator Circuit

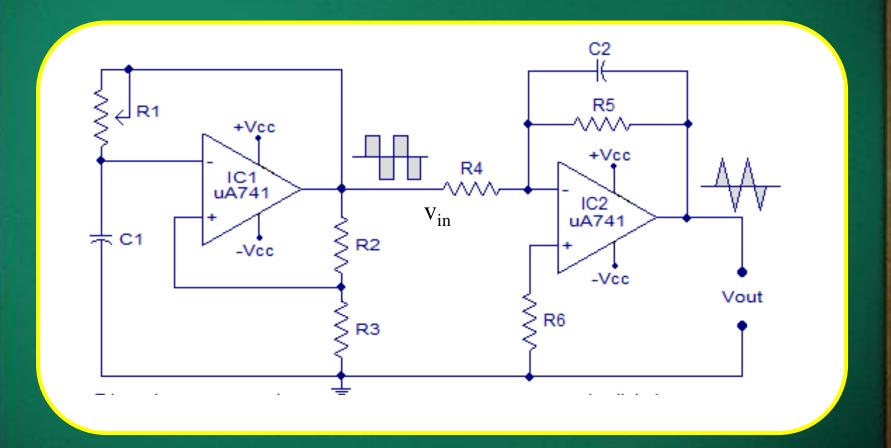


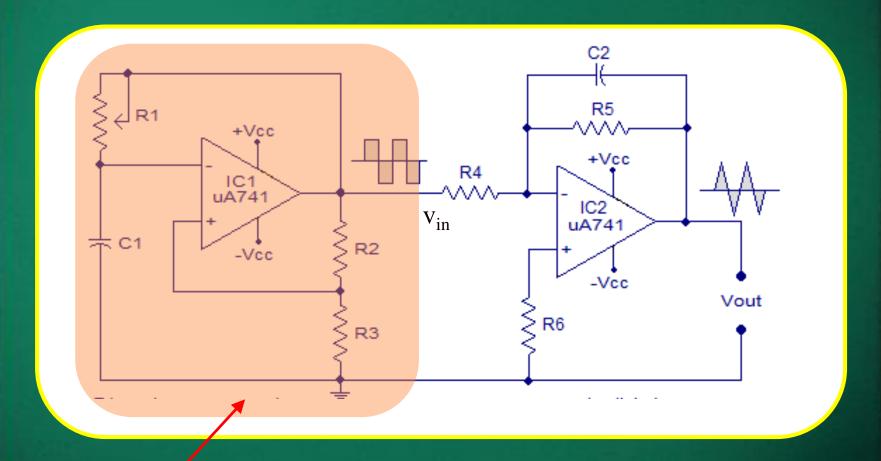
Practical Integrator Circuit

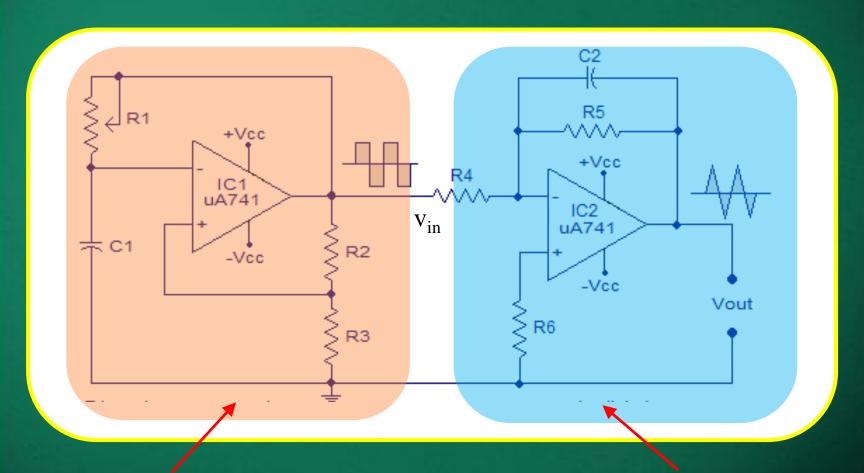
DC Voltage Gain
$$(A_{v0}) = -\frac{R_2}{R_1}$$

$$AC Voltage Gain $(A_v) = -\frac{R_2}{R_1} \times \frac{1}{(1 + \omega CR_2)}$

$$Corner Frequency $(\omega_0) = \frac{1}{CR_2}$$$$$

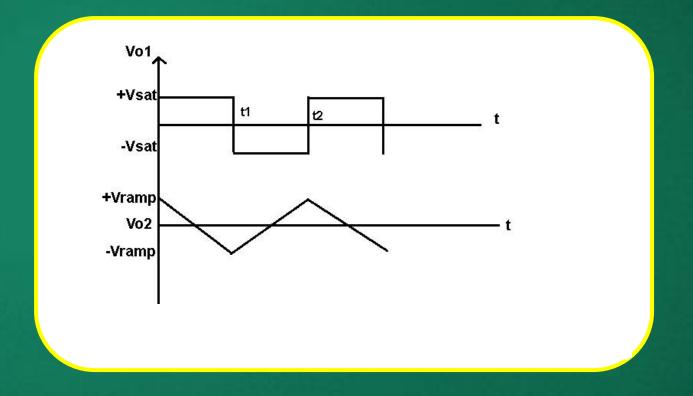


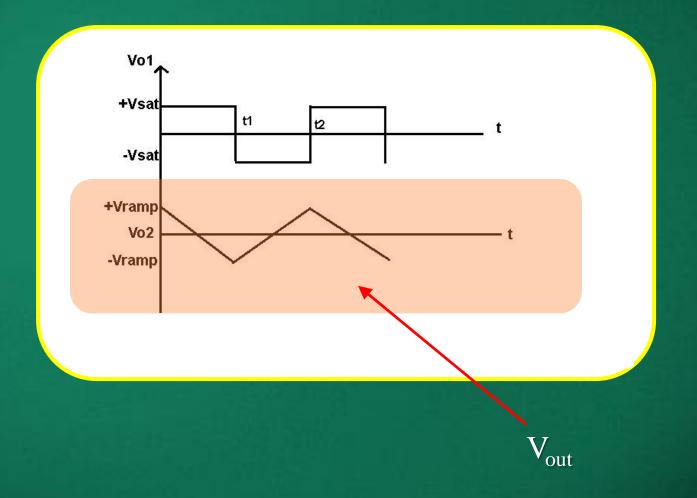


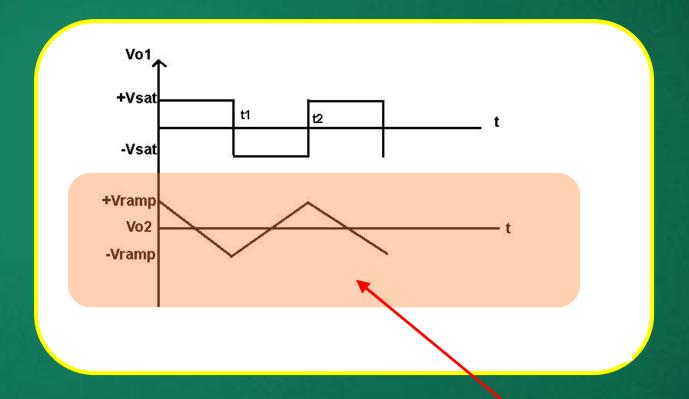


Square Wave Generator

Integrator

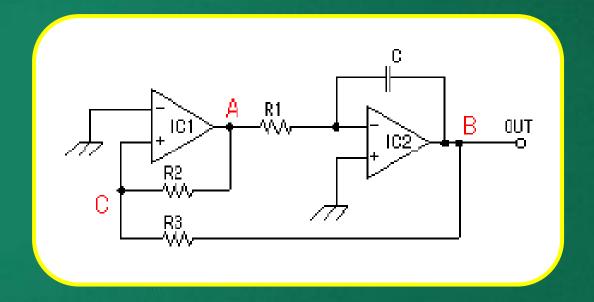


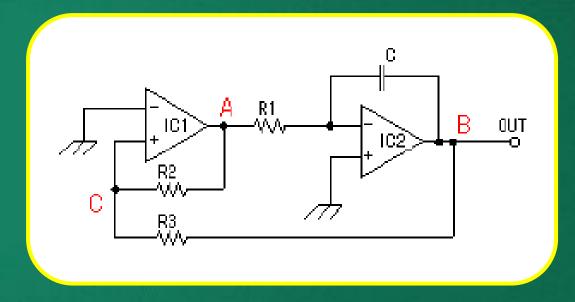


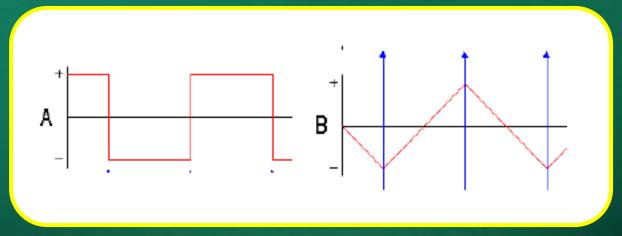


$$V_{\text{out}} = \left(\frac{-R_5 / R_4}{R_5 C_2 s + 1}\right) V_{\text{in}}$$

Vout

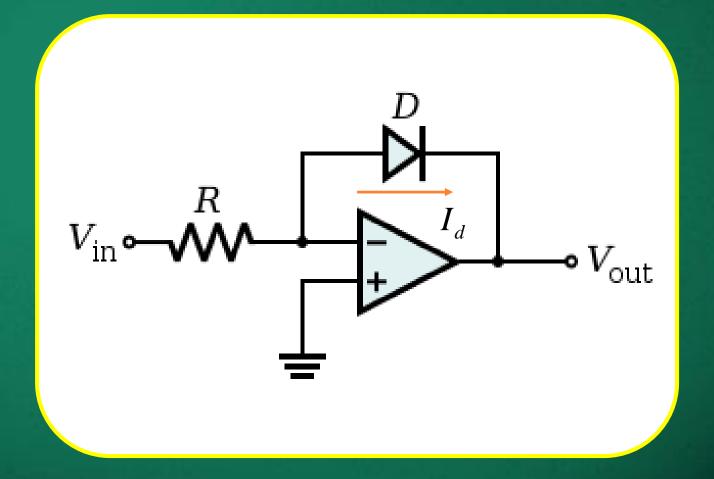






Log and Antilog Amplifier

Logarithmic Amplifier



Diode Equation

$$i_D = I_0 \left(e^{\frac{qv_D}{nKT}} - 1 \right)$$

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 i_D = the net current flowing through the diode;

 I_0 = "dark saturation current", the diode leakage current in the absence of light;

 v_D = applied voltage across the terminals of the diode;

q = absolute value of electron charge (1.6x10⁻¹⁹ C);

 $k = Boltzmann's constant (1.38x10^{-23} J/K);$

T = absolute temperature in Kelvin (K); and

n = empirical constant, 1 for Ge and 2 for Si diode.

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At 300 K, kT/q = 26 mV, the thermal voltage.

Diode Equation

$$i_D = I_0 \left(e^{\left(\frac{v_D}{0.026}\right)} - 1 \right)$$

where v_D is the voltage applied across diode in volts.

If diode is forward biased

$$i_D \cong I_0 e^{\left(\frac{v_D}{0.026}\right)}$$

Applying KCL at inverting input

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$$\frac{0 - V_{in}}{R} + I_d = 0 \Longrightarrow I_d = \frac{V_{in}}{R}$$

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$$e^{\left(-v_{\text{out}}/v_{T}\right)} = \frac{V_{\text{in}}}{I_{0}R}$$

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$$\mathbf{v}_{\text{out}} = -v_T \ln \left(\frac{\mathbf{V}_{\text{in}}}{I_0 \mathbf{R}} \right) = k_1 \ln \left(\frac{\mathbf{V}_{\text{in}}}{k_2} \right)$$

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where

$$\mathbf{k}_1 = -\mathbf{v}_T$$
 and $\mathbf{k}_2 = \mathbf{I}_0 \mathbf{R}$