

Ego motion estimation from vehicle wheel speed

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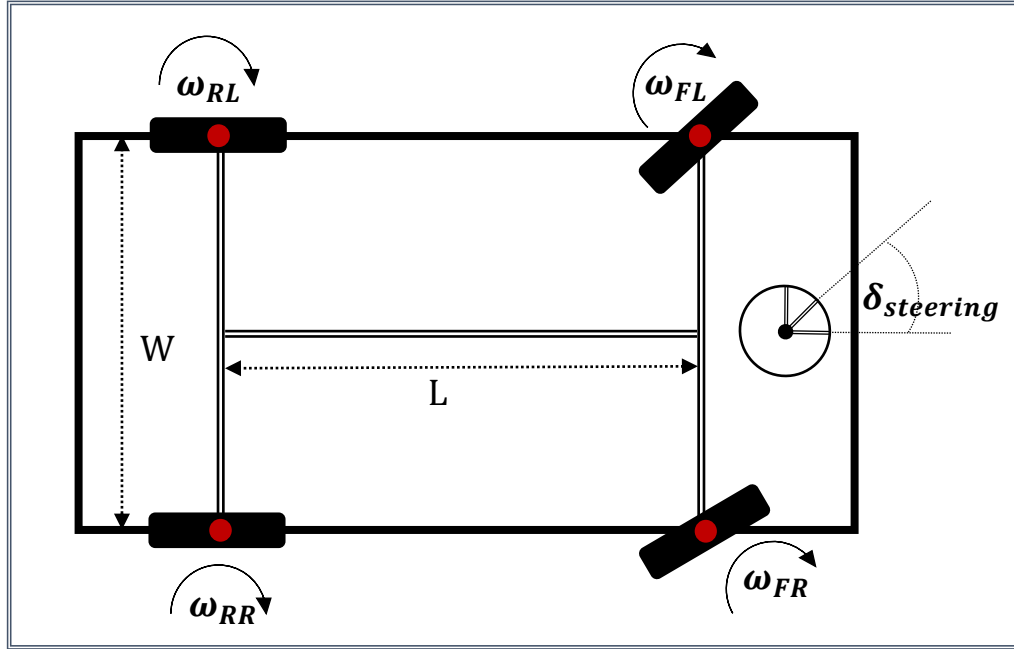
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CLOSING REMARKS

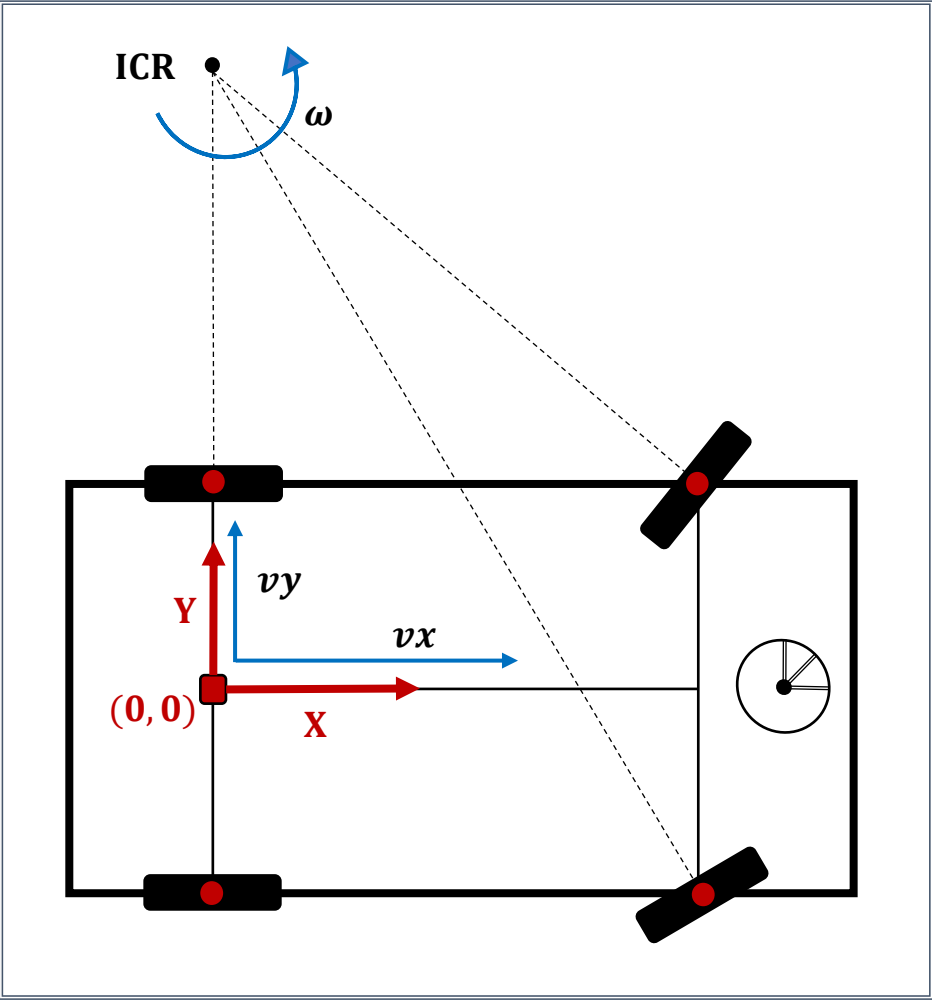
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Inputs Considered



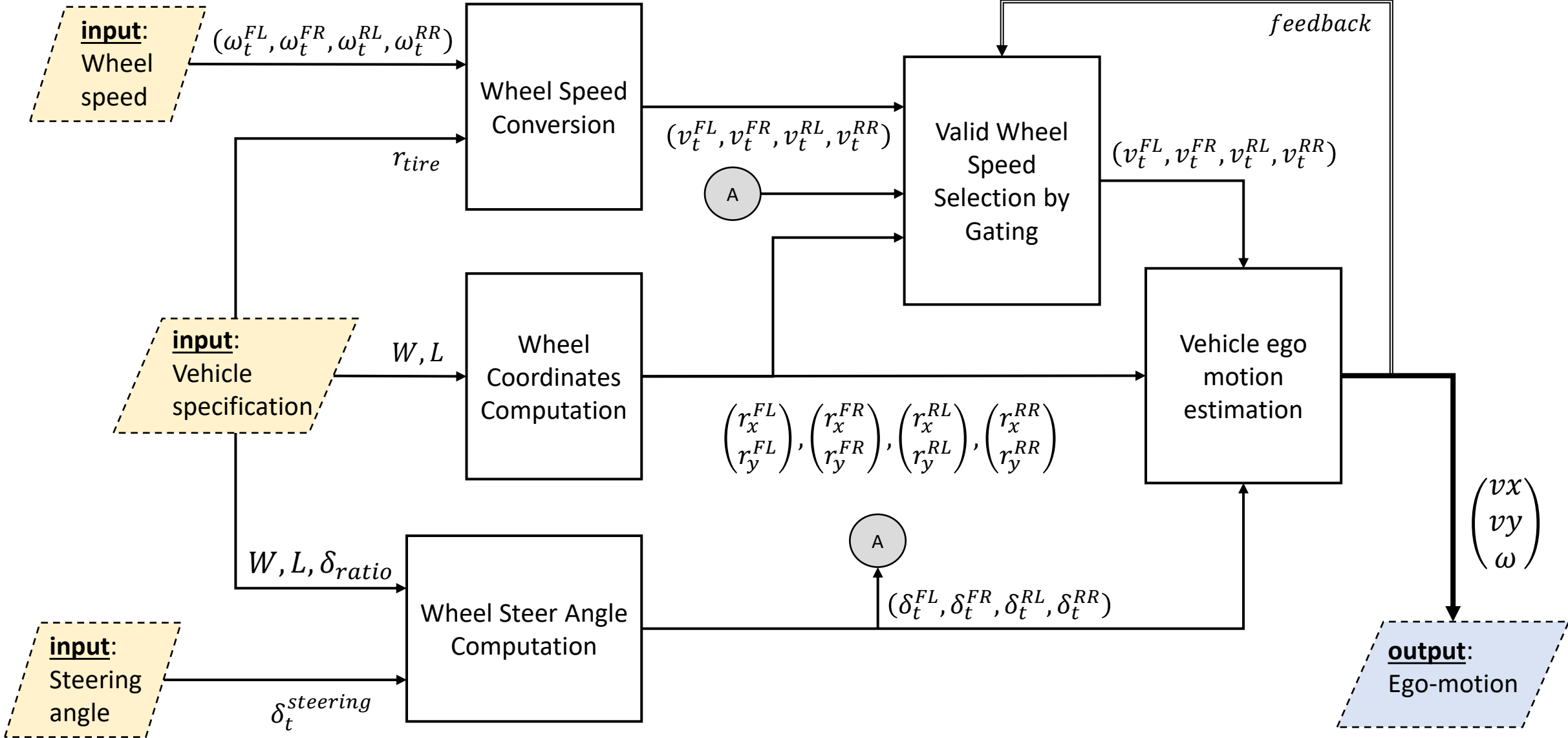
Inputs	notations	unit
Inputs from ego-vehicle speed and steering sensor		
Steering angle	$\delta_{steering}$	radian
Front Left wheel speed	ω_{FL}	rpm
Front Right wheel speed	ω_{FR}	rpm
Rear Right wheel speed	ω_{RR}	rpm
Rear Left wheel speed	ω_{RL}	rpm
Ego-vehicle constant parameters		
Wheel Base	W	m
Track Length	L	m
Steering ratio	δ_{ratio}	-
Tire radius	r_{tire}	m

Required Output



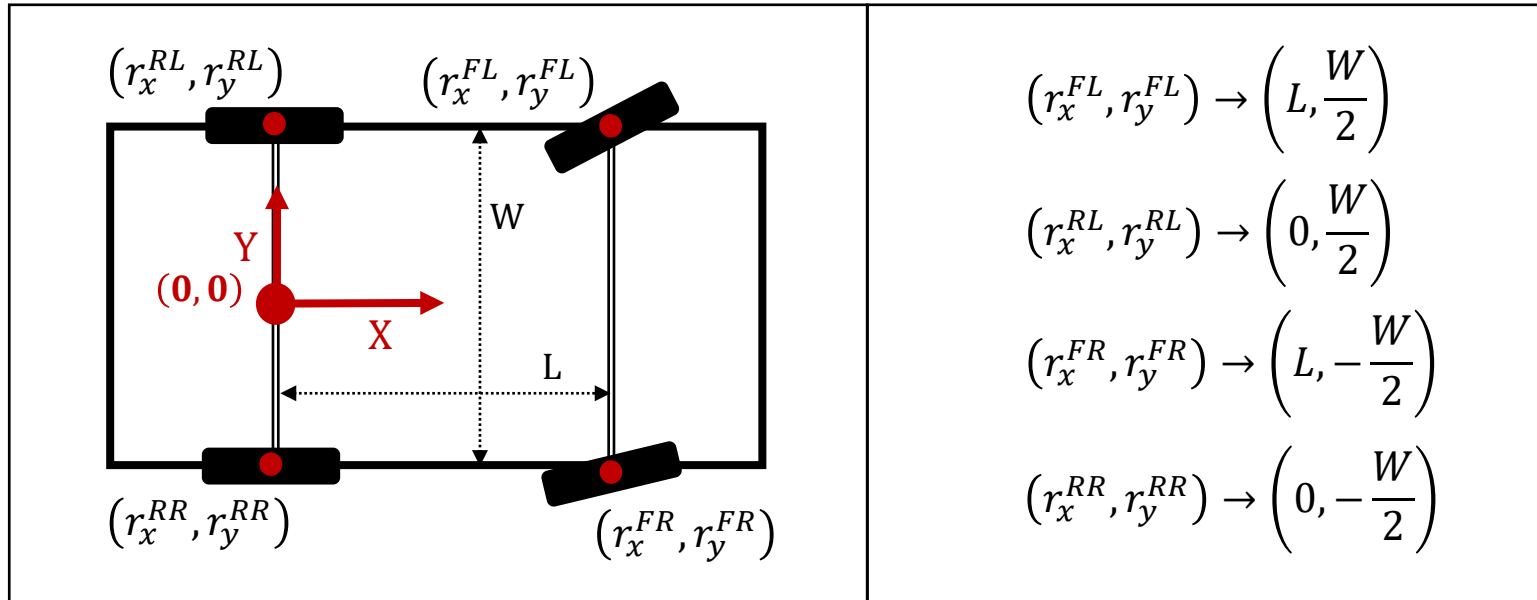
Estimated Outputs	notations	unit
Ego-vehicle Motion parameters		
Body frame longitudinal velocity w.r.t rear wheel base centre	v_x	m/s
Body frame lateral velocity w.r.t rear wheel base centre	v_y	m/s
Yaw rate	ω	rad/s

High Level Architecture



Wheel Speed Conversion & Wheel Coordinate Computation

The coordinates of the wheel locations are as follows assuming the vehicle wheel base centre to be the point of origin

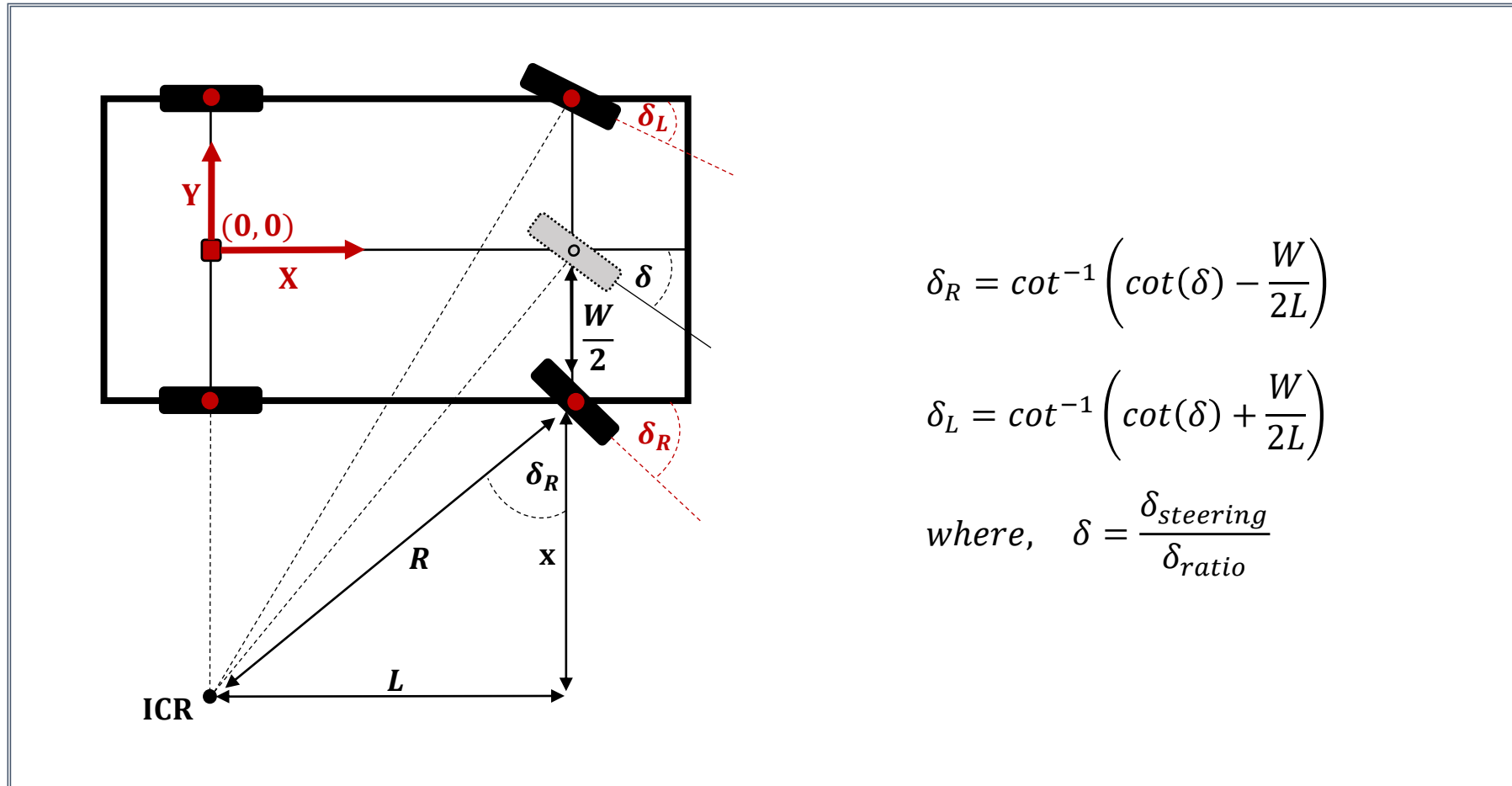


The wheel speed are in rpm (rotations per minute) which needs to be converted to m/s

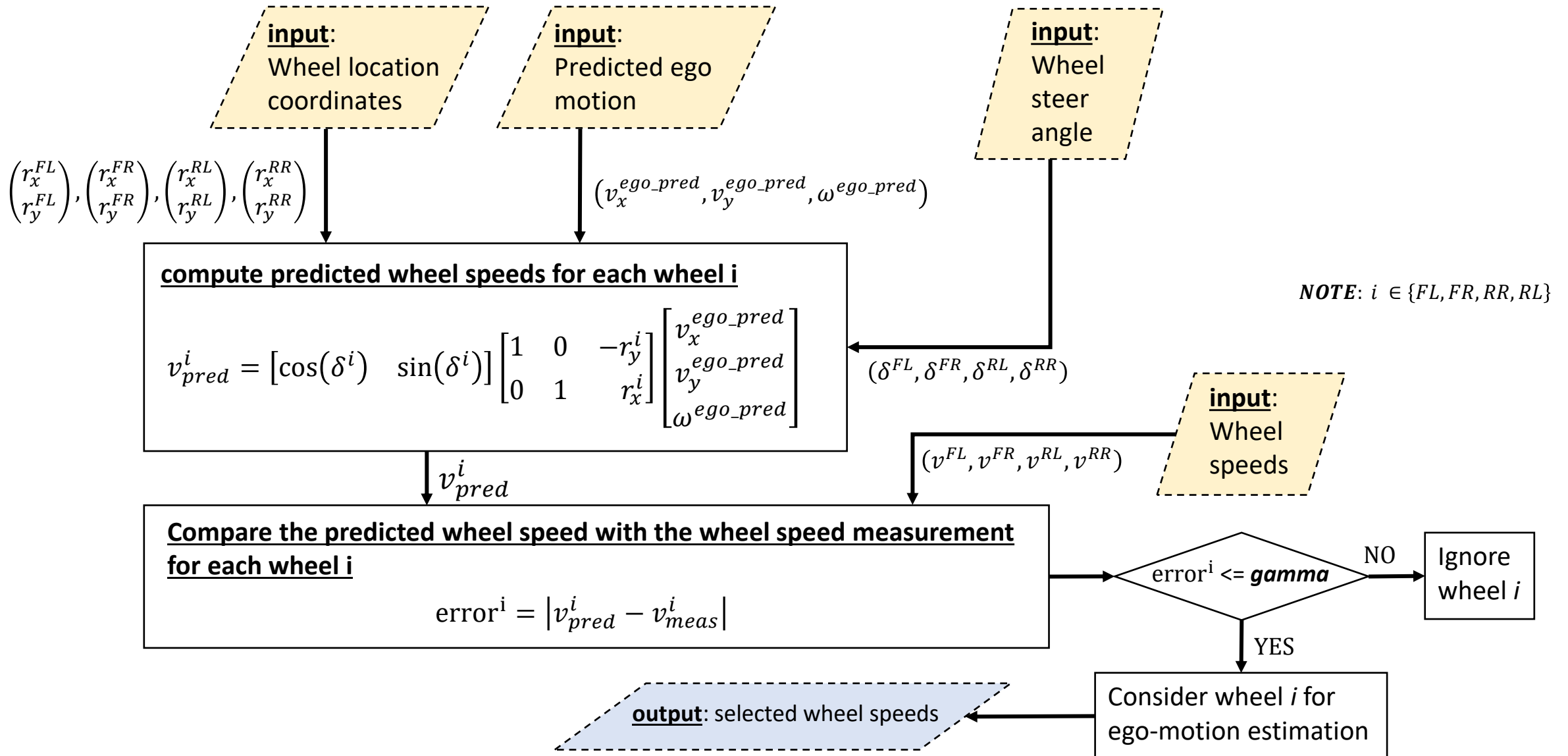
$$v_i = \frac{2\pi r_{tire} \omega_i}{60}, \quad \text{where } i \in \{FL, FR, RR, RL\}$$

Wheel Steer angle Computation

By imposing Ackerman's constraints and assuming that the vehicle is **2WD** (2 wheel drive) we can derive the following expressions for the right and left wheel steering angle

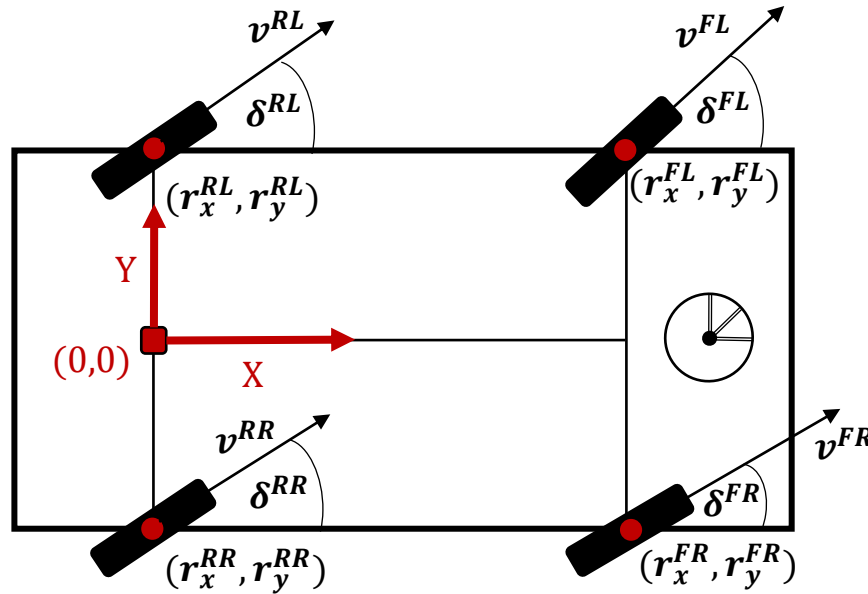


Valid Wheel Speed selection by Gating



Ego-Motion Estimation : measurement model 3DOF

Assuming that the ego vehicle has **4 wheels**. Let the corresponding **wheel locations** , **wheel speeds** and the **wheel steer angles** are as follows:



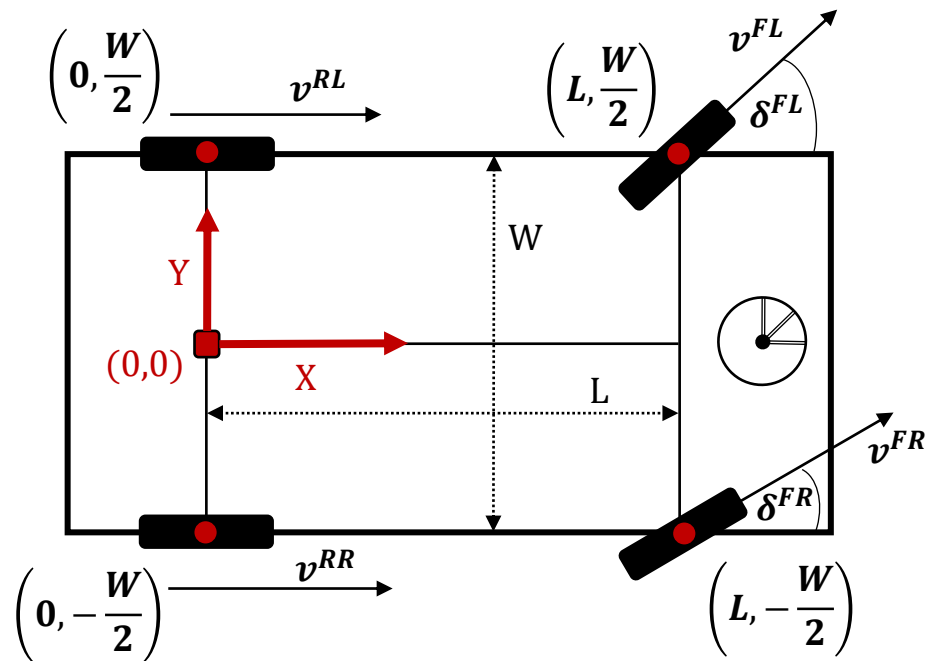
Wheel	Location x coordinate	Location y coordinate	Wheel Speed	Wheel Steer Angle
Front Left (FL)	r_x^{FL}	r_y^{FL}	v^{FL}	δ^{FL}
Front Right (FR)	r_x^{FR}	r_y^{FR}	v^{FR}	δ^{FR}
Rear Left (RL)	r_x^{RL}	r_y^{RL}	v^{RL}	δ^{RL}
Rear Right (RR)	r_x^{RR}	r_y^{RR}	v^{RR}	δ^{RR}

From the well known kinematic expression $\vec{v} = \vec{\omega} \times \vec{r}$, and under the assumption of **no wheel sleep**, the expression below can be derived

$$\begin{bmatrix} 1 & 0 & -r_y^{FL} \\ 0 & 1 & r_x^{FL} \\ 1 & 0 & -r_y^{FR} \\ 0 & 1 & r_x^{FR} \\ 1 & 0 & -r_y^{RL} \\ 0 & 1 & r_x^{RL} \\ 1 & 0 & -r_y^{RR} \\ 0 & 1 & r_x^{RR} \end{bmatrix} \begin{bmatrix} v_x \\ v_y \\ \omega \end{bmatrix} = \begin{bmatrix} v^{FL} \cos(\delta^{FL}) \\ v^{FL} \sin(\delta^{FL}) \\ v^{FR} \cos(\delta^{FR}) \\ v^{FR} \sin(\delta^{FR}) \\ v^{RL} \cos(\delta^{RL}) \\ v^{RL} \sin(\delta^{RL}) \\ v^{RR} \cos(\delta^{RR}) \\ v^{RR} \sin(\delta^{RR}) \end{bmatrix}$$

Ego-Motion Estimation : measurement model 2DOF

Under the assumption of no side slip and 2 wheel drive, if we compute the vehicle ego-motion w.r.t the rear wheel base centre the lateral component of the ego motion can be considered to be zero ($v_y = 0$). Under such conditions the measurement model reduces as follows:



$$\begin{bmatrix} 1 & -\frac{W}{2} \\ 0 & L \\ 1 & \frac{W}{2} \\ 0 & L \\ 1 & -\frac{W}{2} \\ 1 & \frac{W}{2} \end{bmatrix} \begin{bmatrix} v_x \\ \omega \end{bmatrix} = \begin{bmatrix} v^{FL} \cos(\delta^{FL}) \\ v^{FL} \sin(\delta^{FL}) \\ v^{FR} \cos(\delta^{FR}) \\ v^{FR} \sin(\delta^{FR}) \\ v_{RL} \\ v_{RR} \end{bmatrix}$$

$$\Rightarrow AX = b$$

Ego-Motion Estimation : covariance computation

The covariance is computed as follows

Given the measurement
noise covariance of the
wheel speed sensor

$$R_{vel} = \begin{bmatrix} \sigma_{v^{FL}}^2 & 0 & 0 & 0 \\ 0 & \sigma_{v^{FR}}^2 & 0 & 0 \\ 0 & 0 & \sigma_{v^{RL}}^2 & 0 \\ 0 & 0 & 0 & \sigma_{v^{RR}}^2 \end{bmatrix}$$

We can compute the covariance of
the pseudo-measurement (the right
hand-side of the equation in the
previous slide)

$$\Sigma_{FL} = \begin{bmatrix} (\sigma_{v^{FL}}^2) \cos^2(\delta^{FL}) & (\sigma_{v^{FL}}^2) \sin(\delta^{FL}) \cos(\delta^{FL}) \\ (\sigma_{v^{FL}}^2) \sin(\delta^{FL}) \cos(\delta^{FL}) & (\sigma_{v^{FL}}^2) \sin^2(\delta^{FL}) \end{bmatrix}$$

$$\Sigma_{FR} = \begin{bmatrix} (\sigma_{v^{FR}}^2) \cos^2(\delta^{FR}) & (\sigma_{v^{FR}}^2) \sin(\delta^{FR}) \cos(\delta^{FR}) \\ (\sigma_{v^{FR}}^2) \sin(\delta^{FR}) \cos(\delta^{FR}) & (\sigma_{v^{FR}}^2) \sin^2(\delta^{FR}) \end{bmatrix}$$

$$\Sigma_R = \begin{bmatrix} \sigma_{v^{RL}}^2 & 0 \\ 0 & \sigma_{v^{RR}}^2 \end{bmatrix}$$

$$\Sigma_b = \begin{bmatrix} \Sigma_{FL} & 0 & 0 \\ 0 & \Sigma_{FR} & 0 \\ 0 & 0 & \Sigma_R \end{bmatrix}$$

Ego-Motion Estimation : Ordinary Least Squares

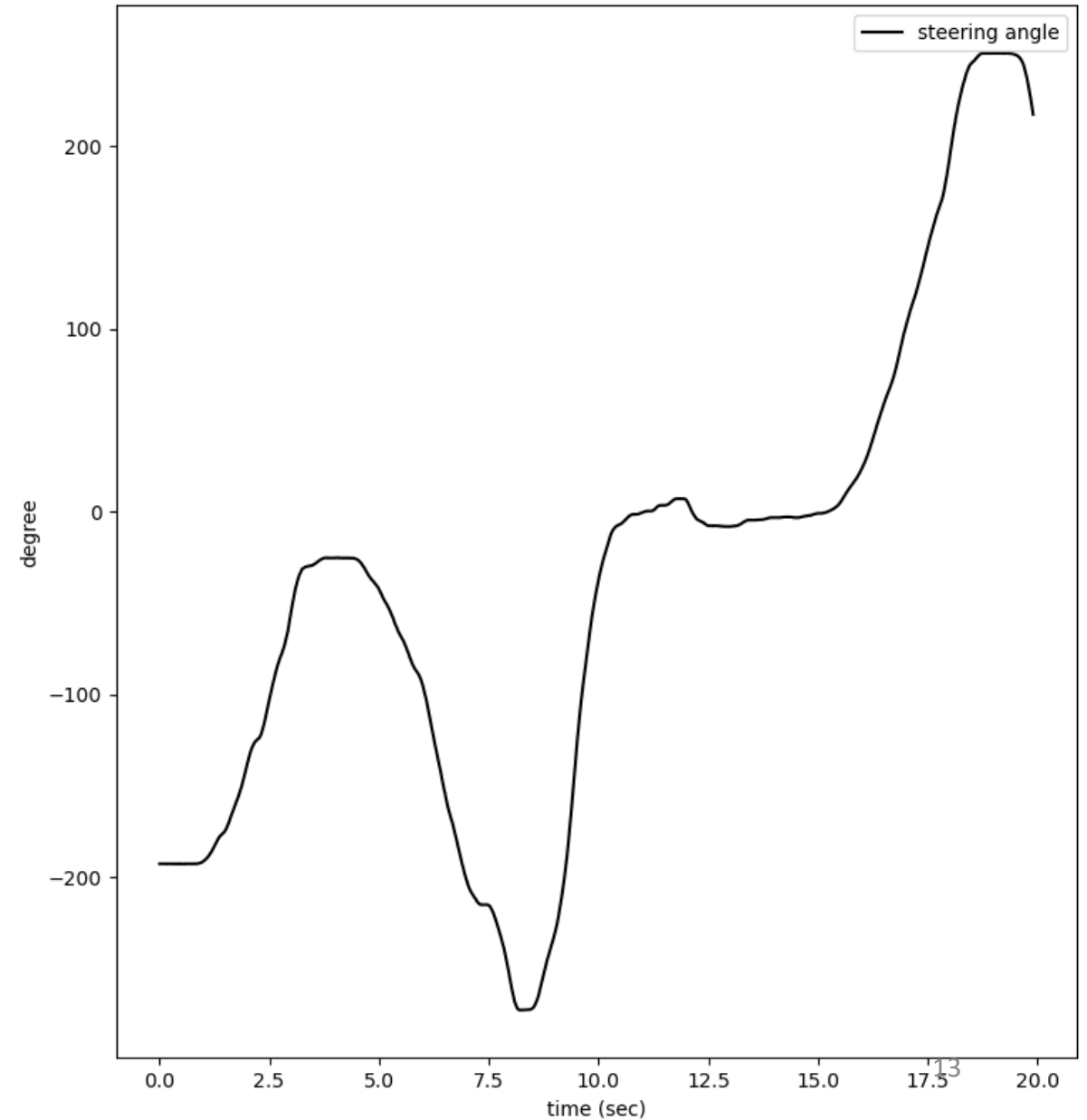
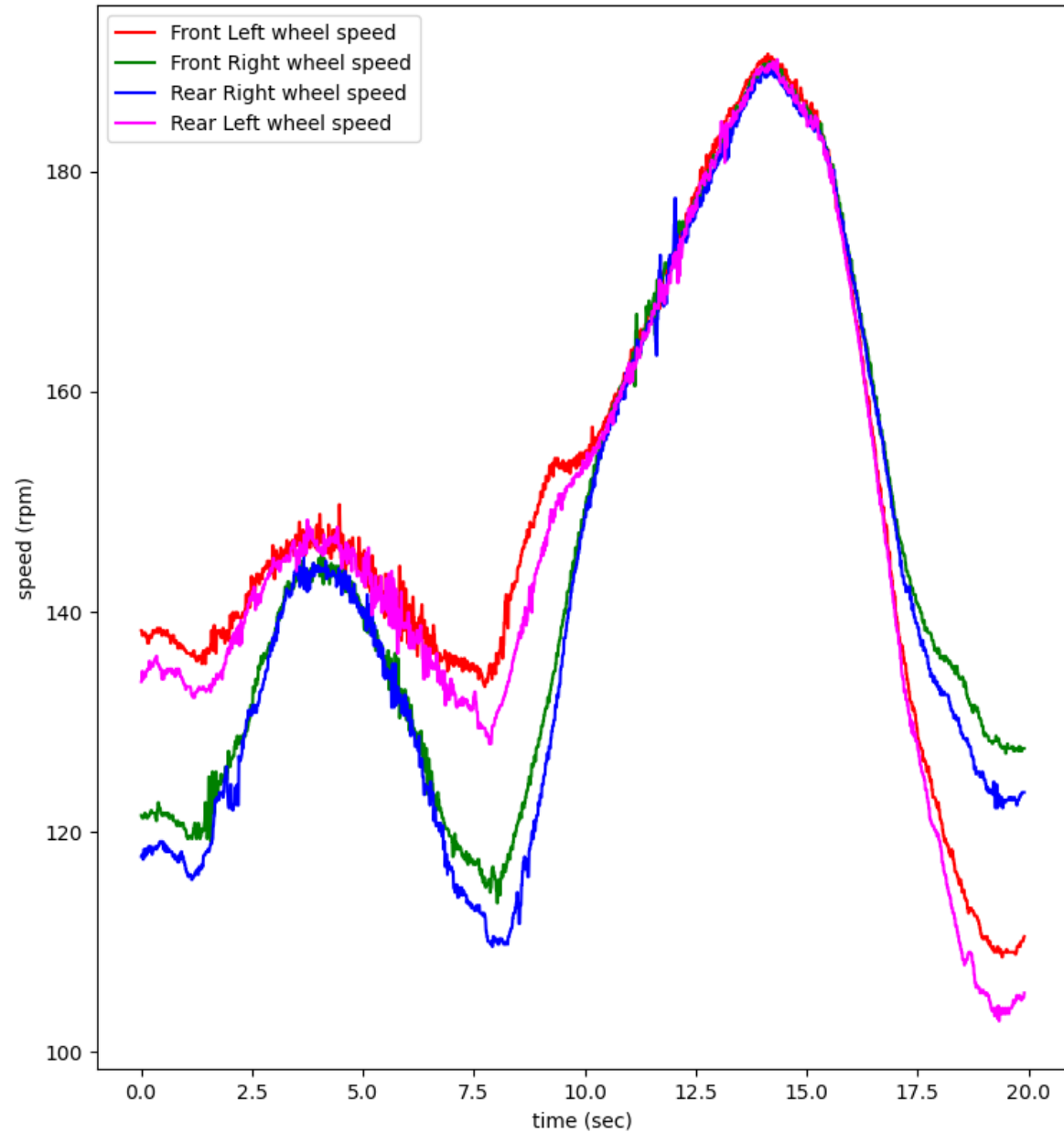
The ego-motion is computed using ordinary least squares as follows

$$\text{let, } B = (A^T A)^{-1} A^T$$

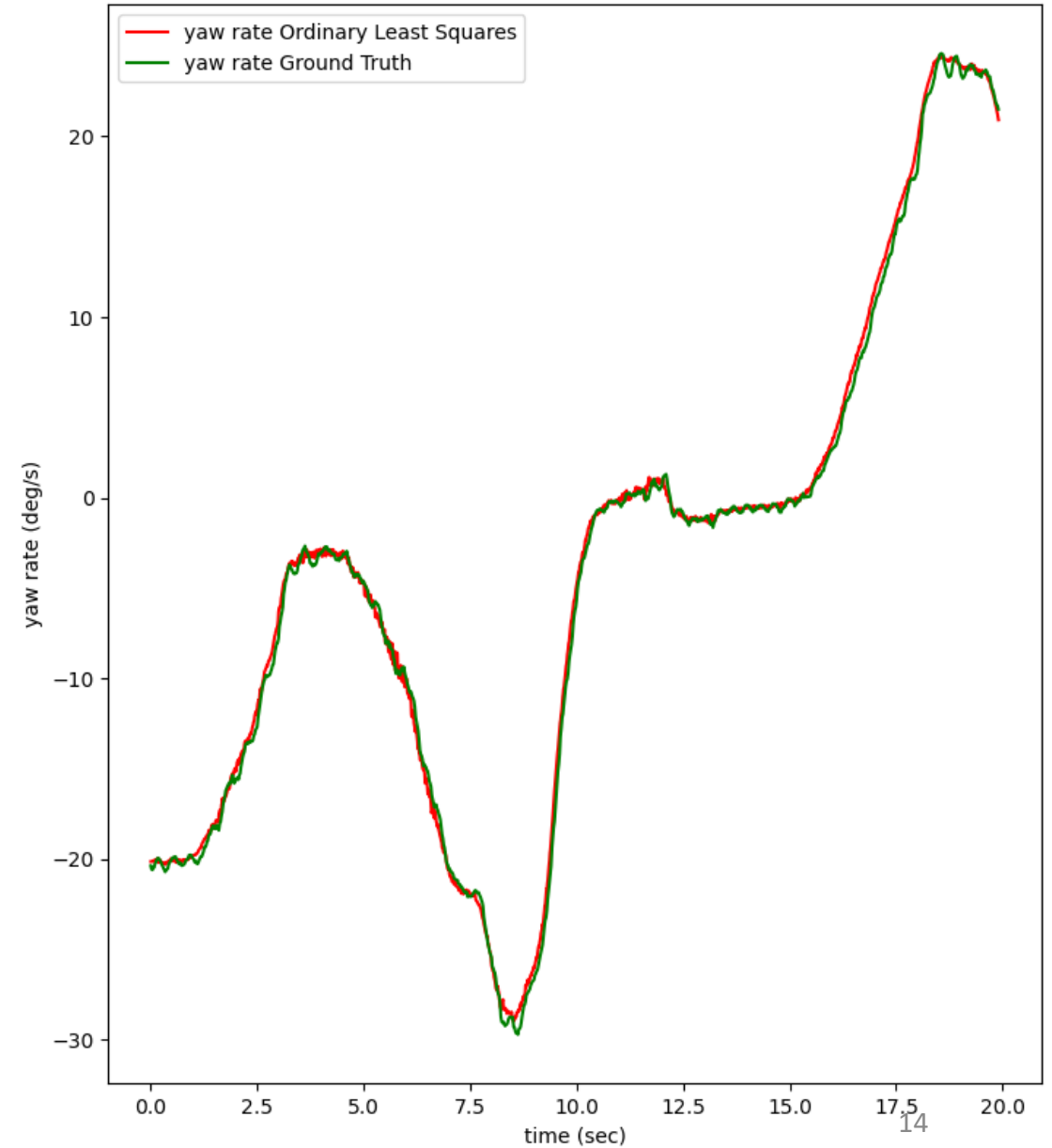
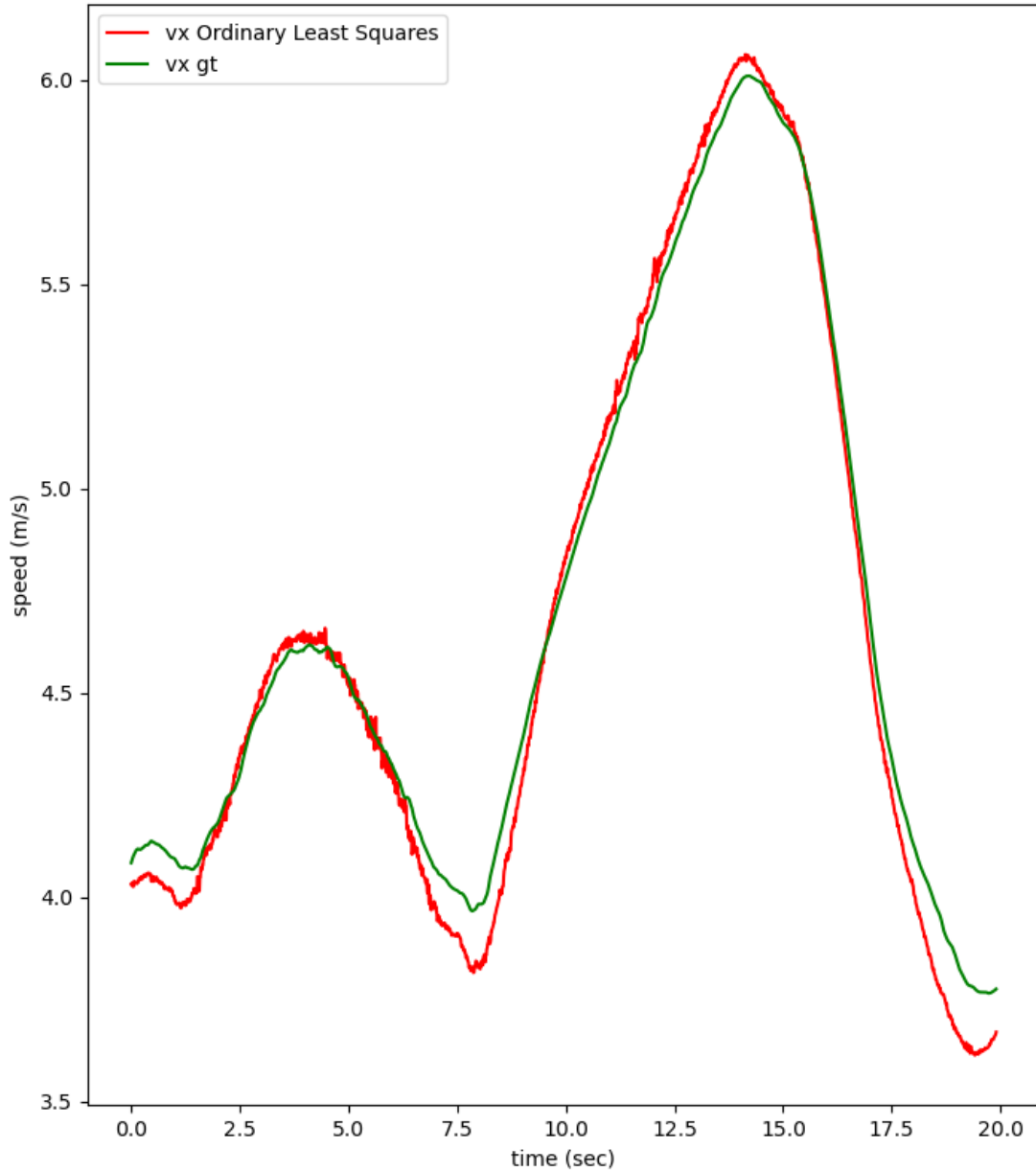
$$\hat{X} = Bb$$

$$\hat{\Sigma} = B\Sigma_b B^T$$

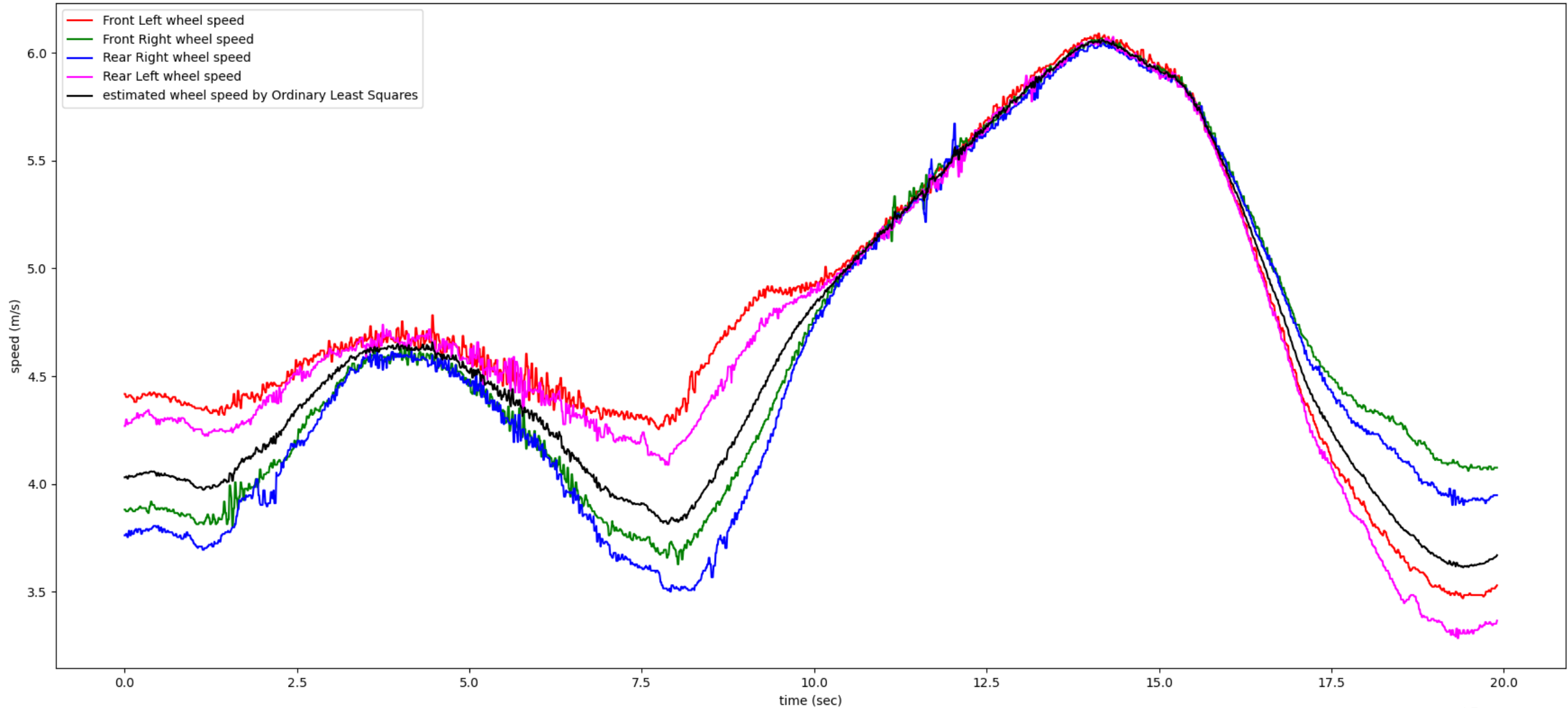
NuScenes Mini – scene 0916 : Input Signals Plot



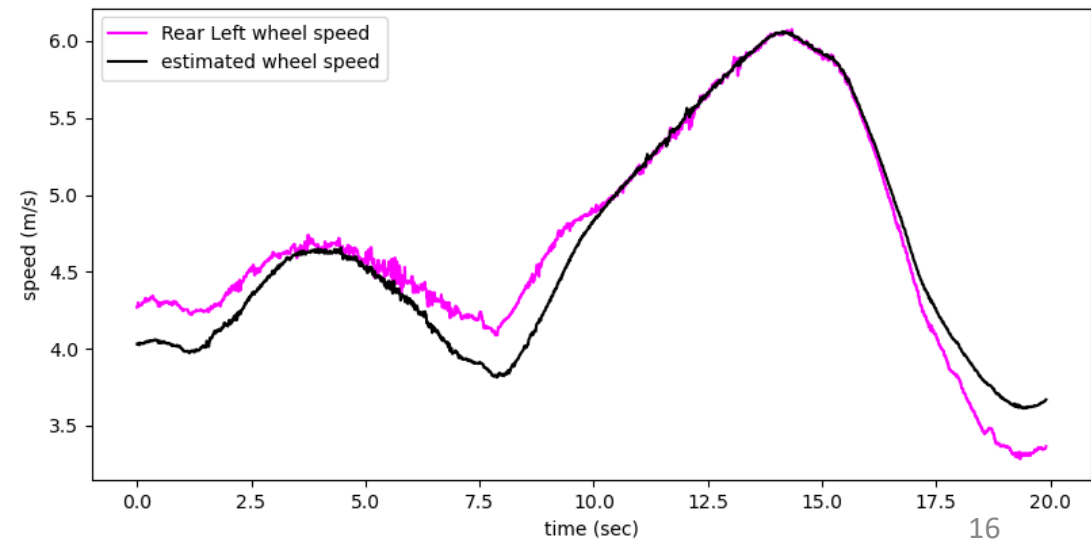
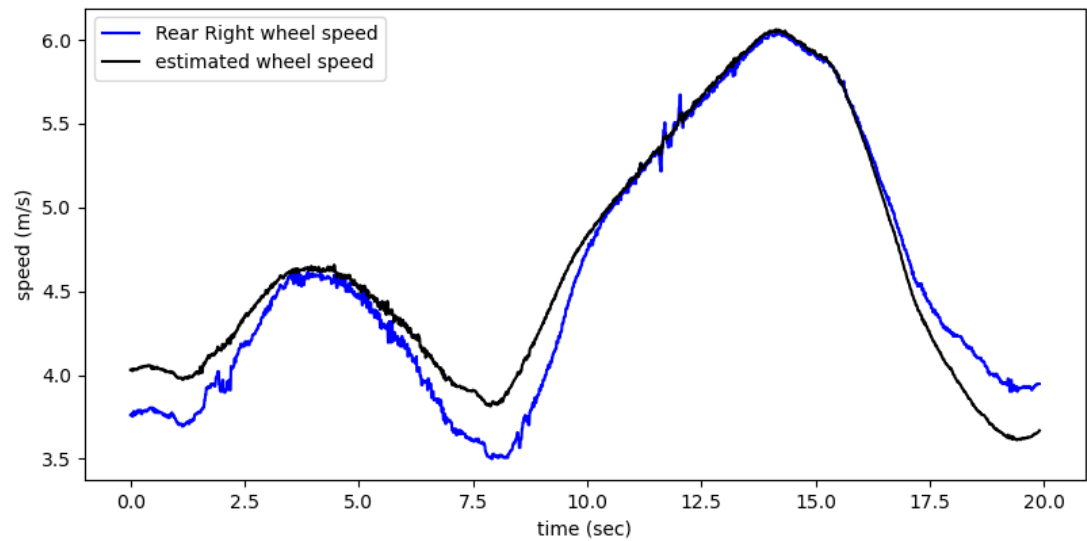
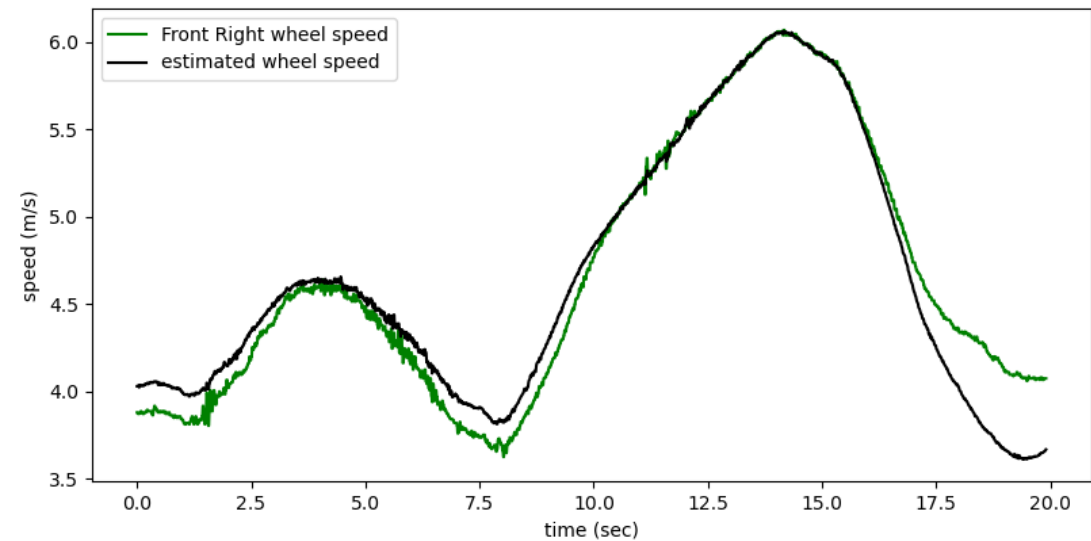
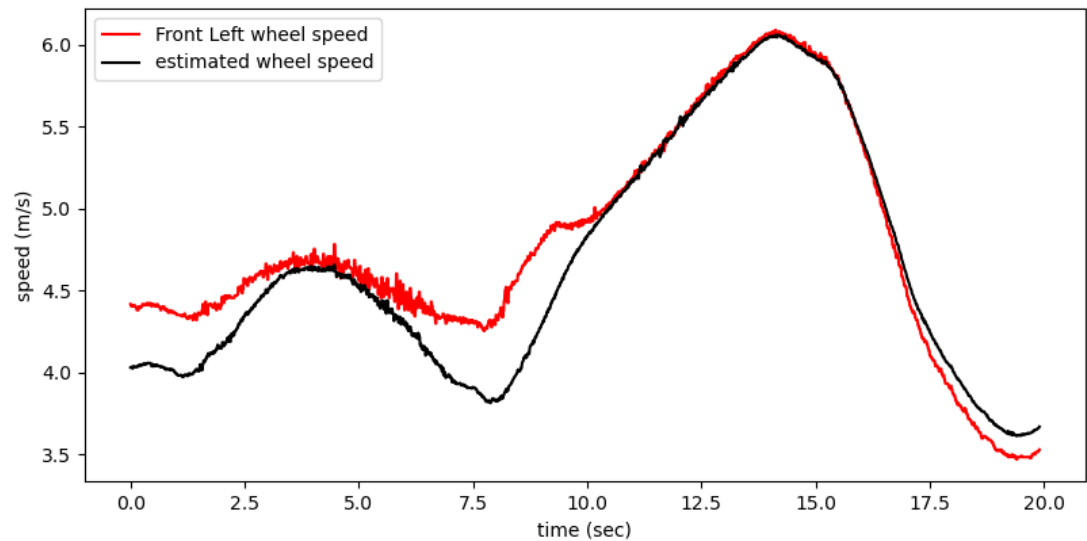
NuScenes Mini – scene 0916 : Ego motion estimation output plot



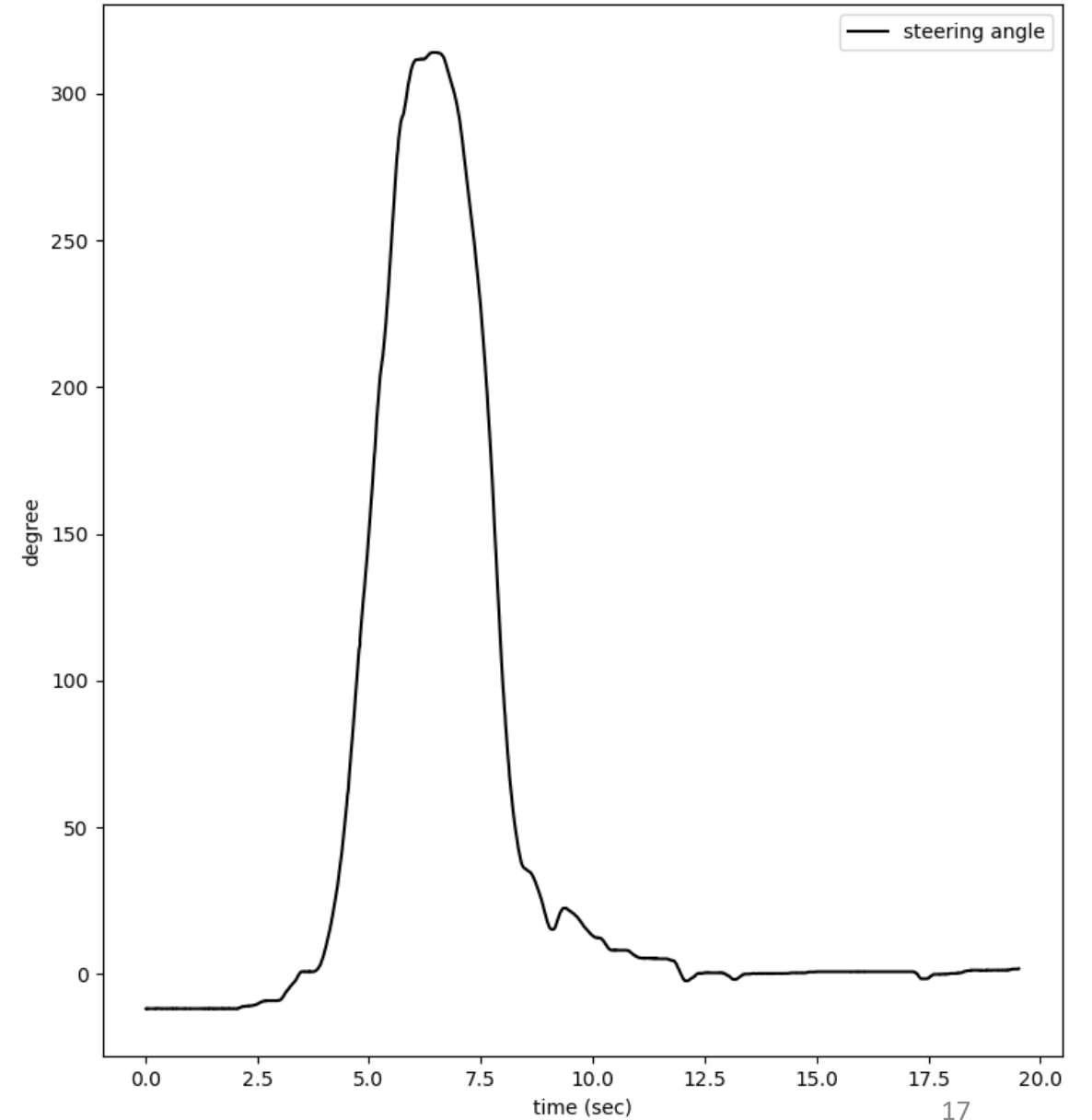
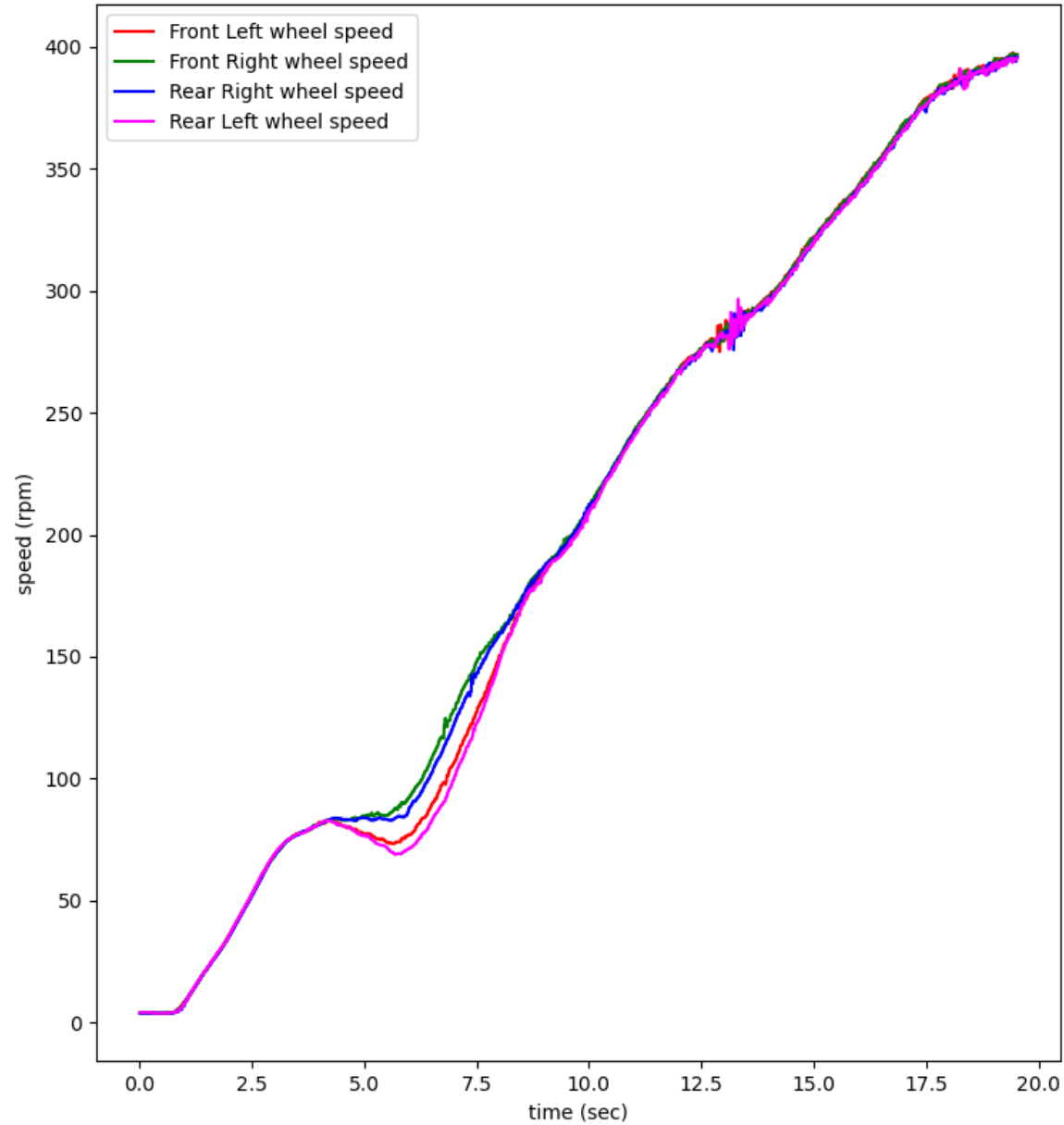
NuScenes Mini – scene 0916 : velocity comparison consolidated plot



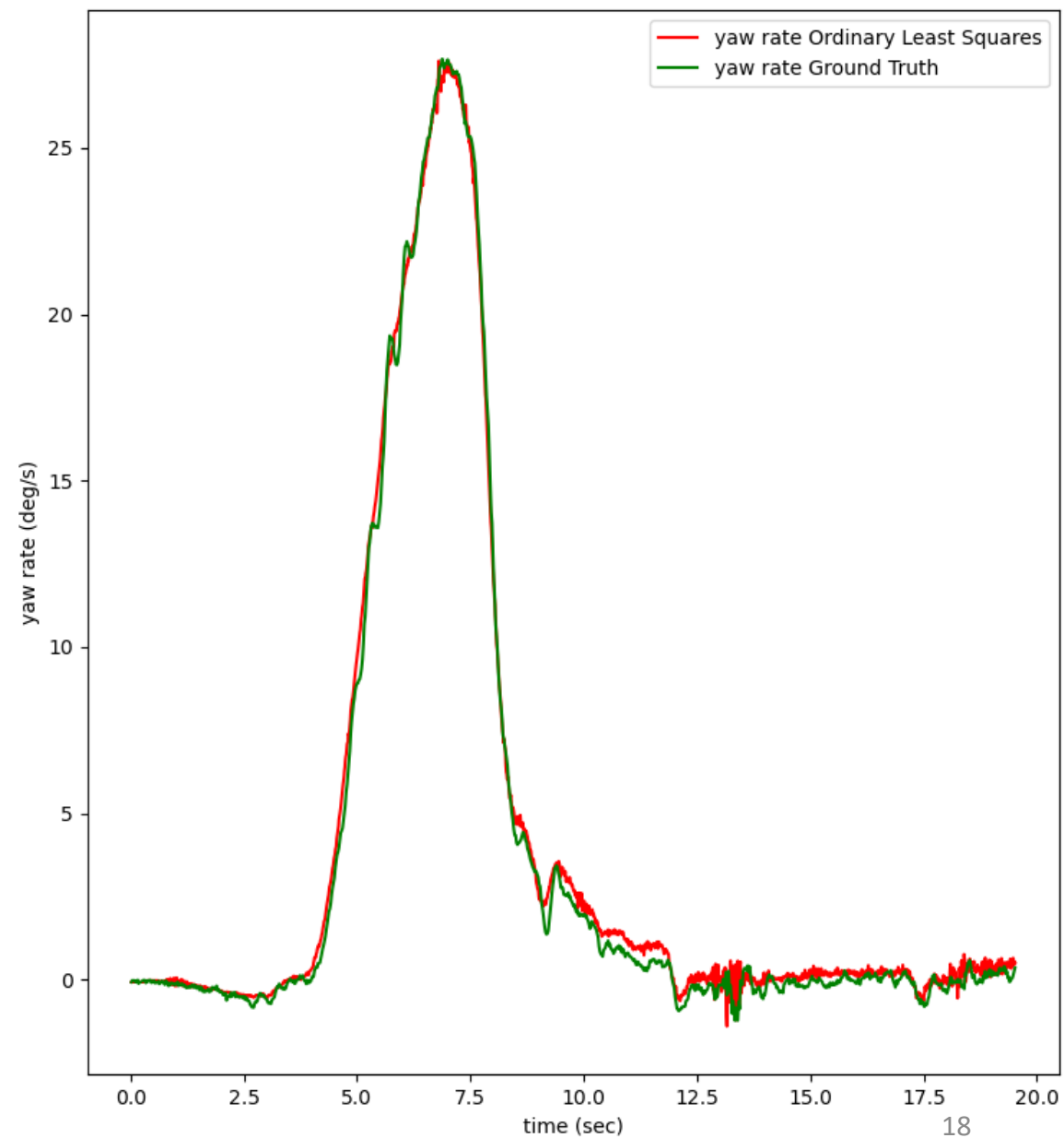
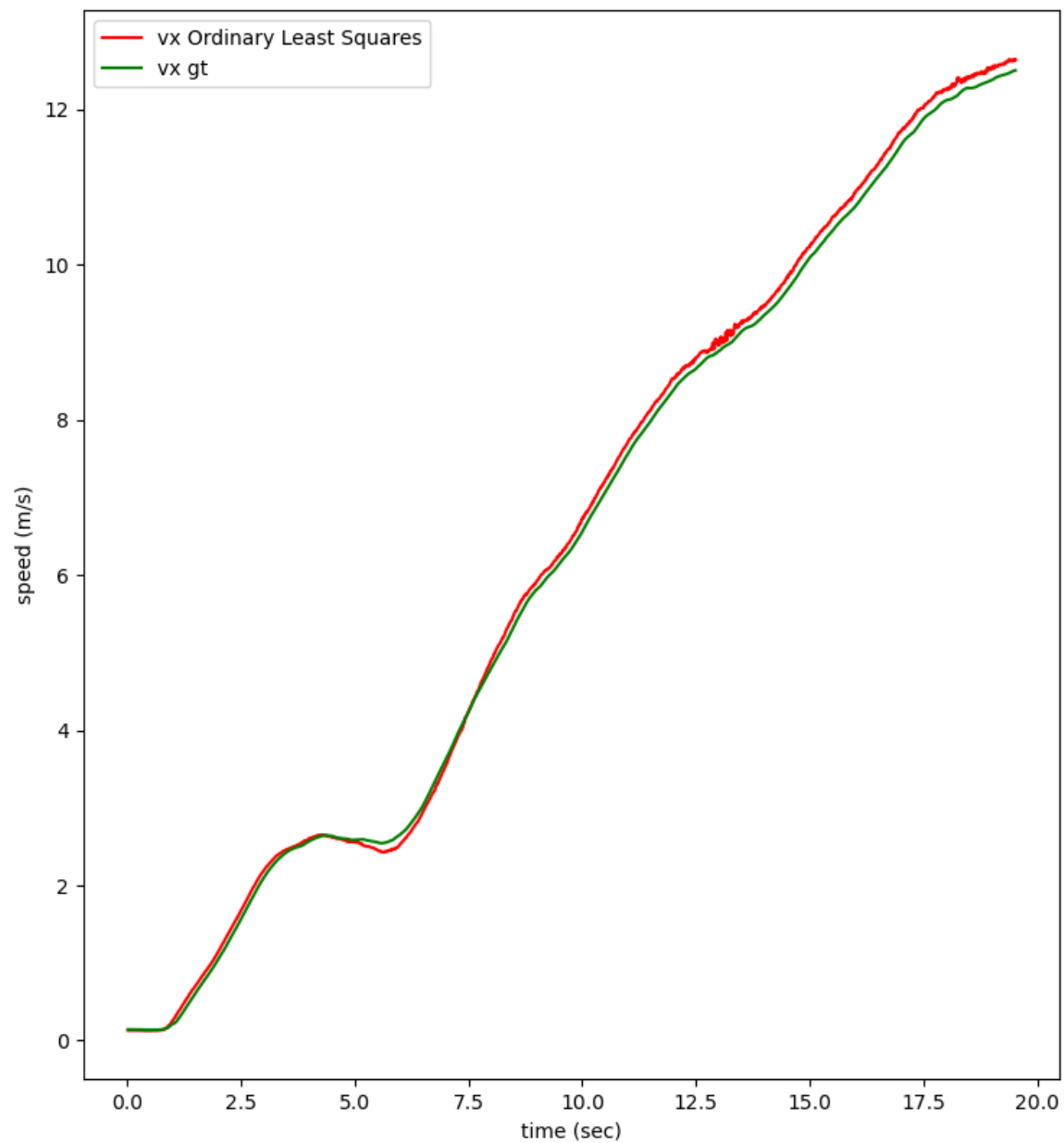
NuScenes Mini – scene 0916 : velocity comparison plot



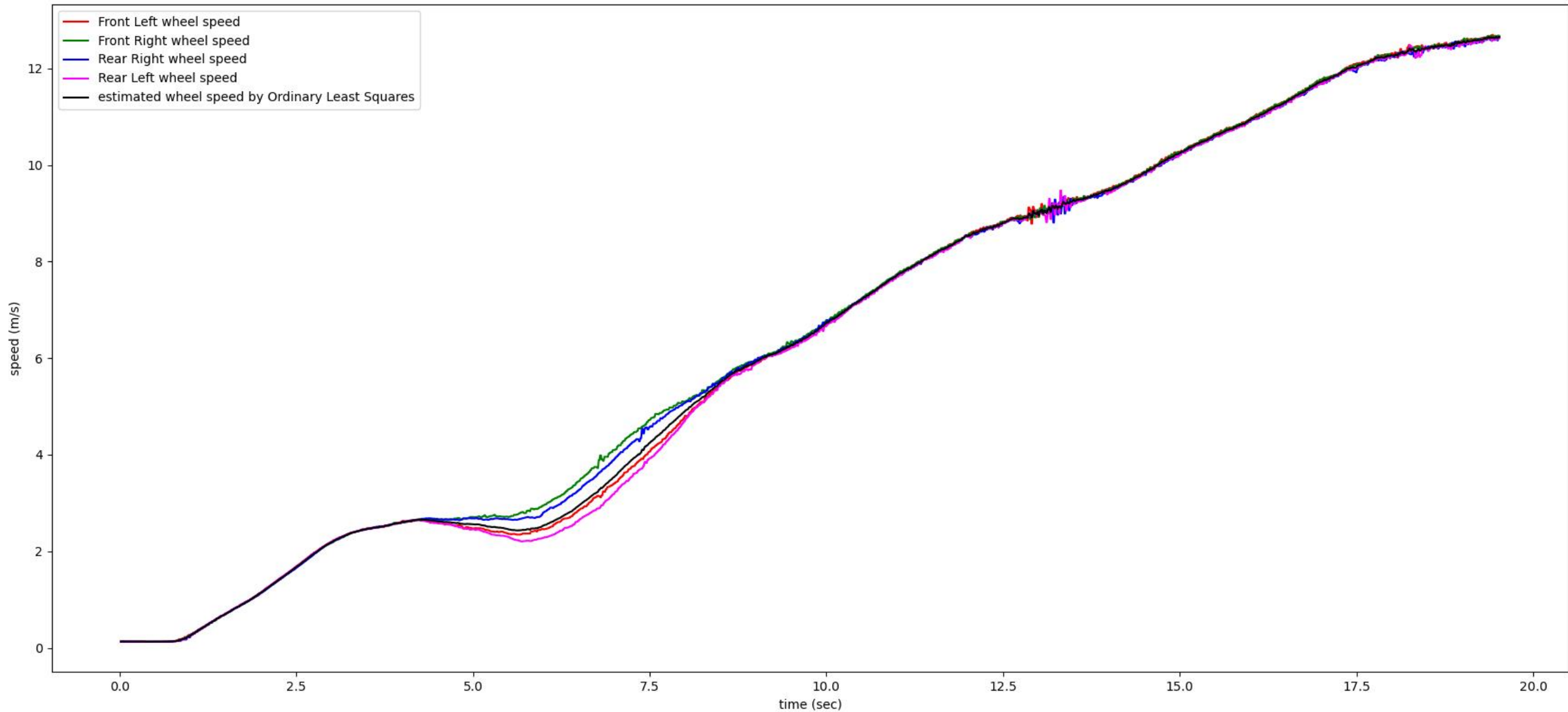
NuScenes Mini – scene 1094 : Input Signals Plot



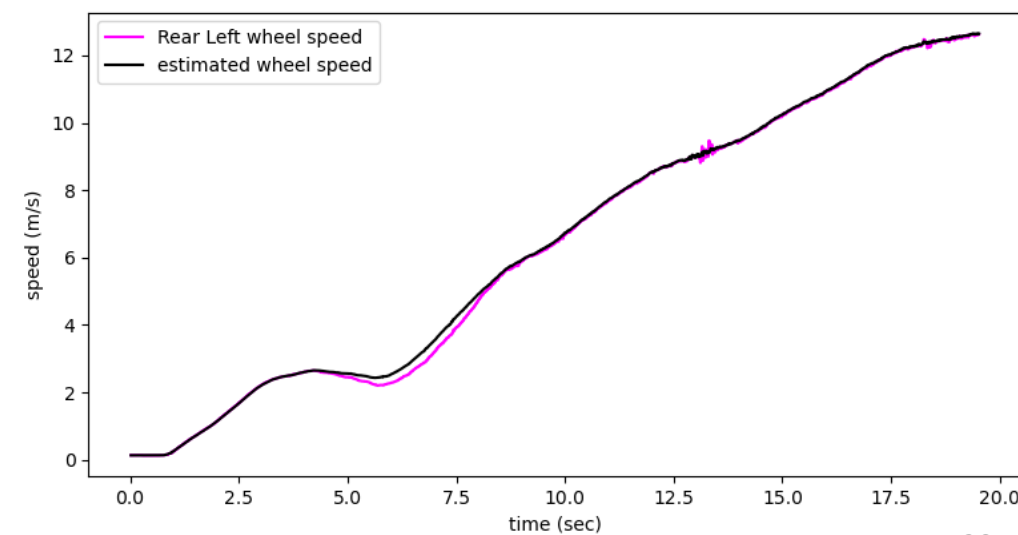
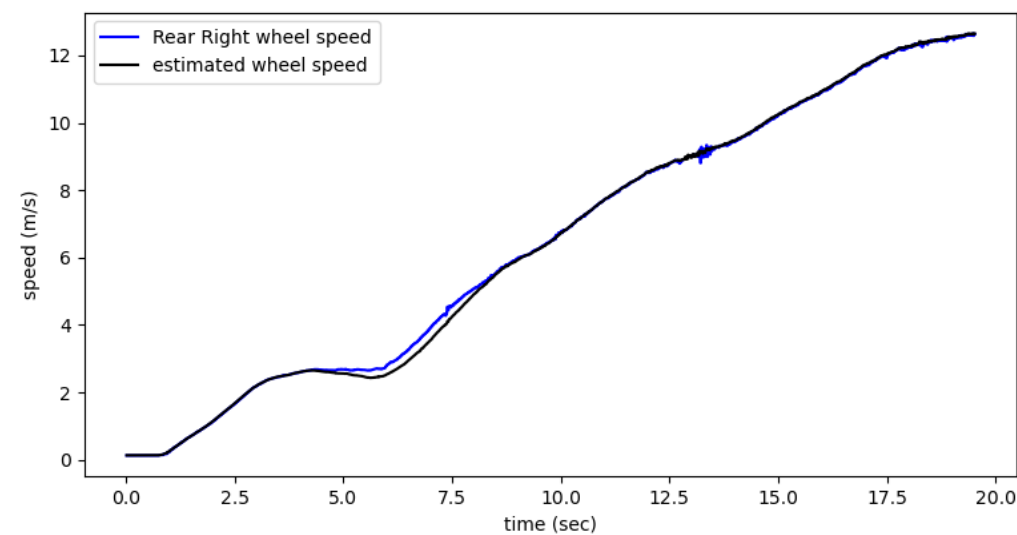
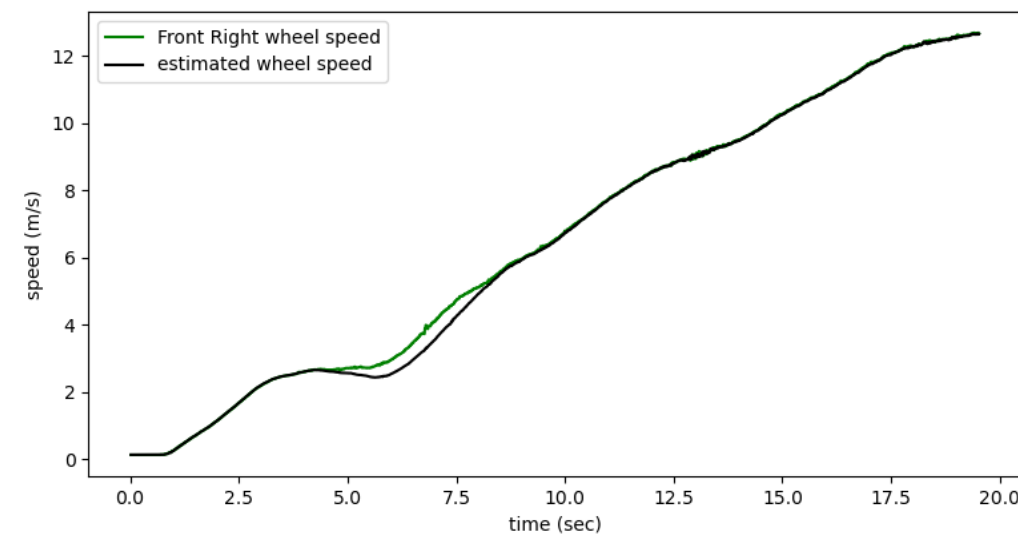
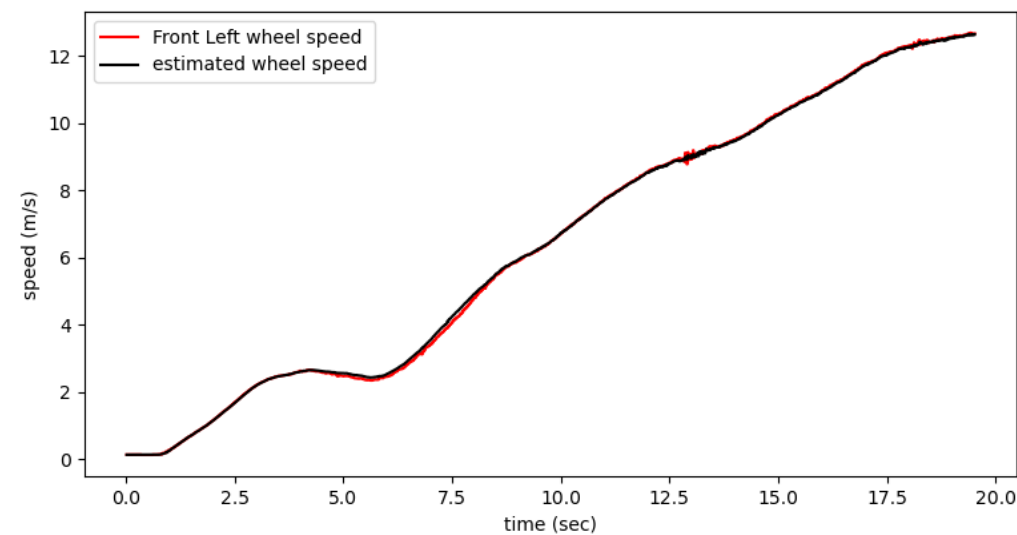
NuScenes Mini – scene 1094 : Ego motion estimation output plot



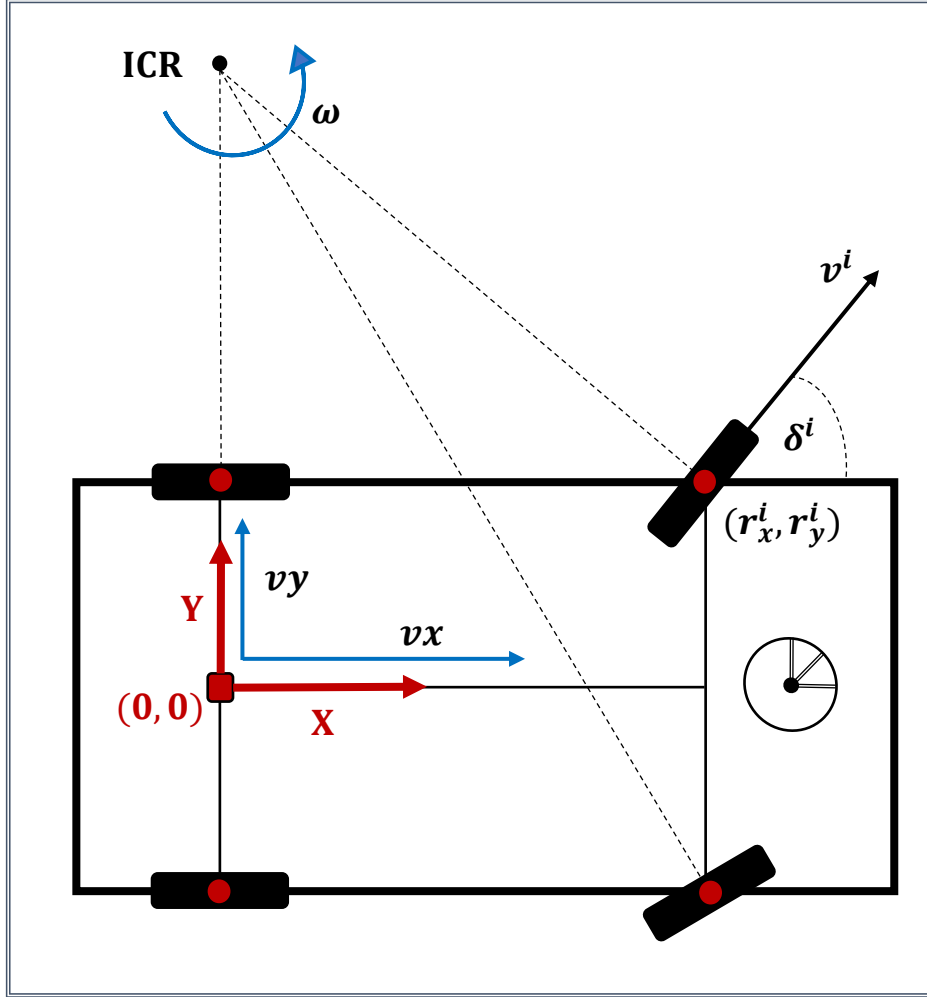
NuScenes Mini – scene 1094 : velocity comparison consolidated plot



NuScenes Mini – scene 1094 : velocity comparison plot



Alternative Measurement model



$$\begin{bmatrix} \cos(\delta^i) & \sin(\delta^i) \end{bmatrix} \begin{bmatrix} 1 & 0 & -r_y^i \\ 0 & 1 & r_x^i \end{bmatrix} \begin{bmatrix} v_x \\ v_y \\ \omega \end{bmatrix} = v^i$$

$$\Rightarrow \begin{bmatrix} \cos(\delta^i) & \sin(\delta^i) & r_x^i \sin(\delta^i) - r_y^i \cos(\delta^i) \end{bmatrix} \begin{bmatrix} v_x \\ v_y \\ \omega \end{bmatrix} = v^i$$

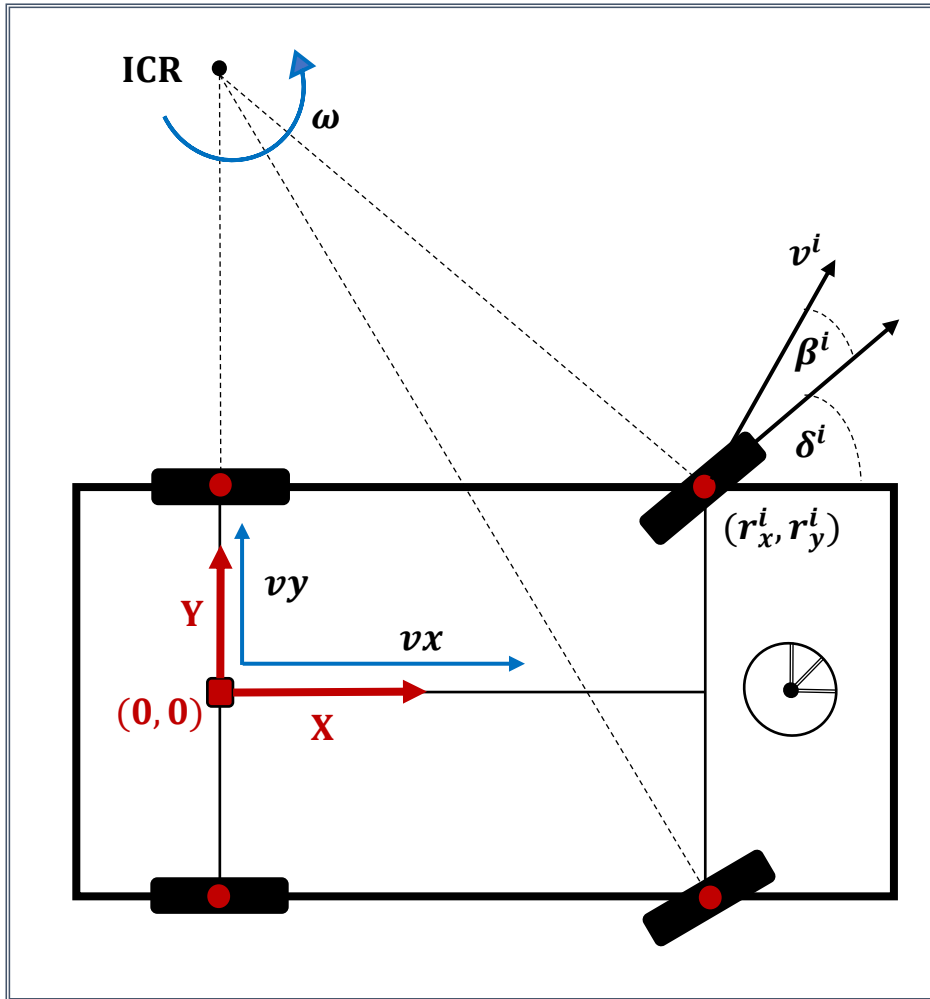
3-DOF Measurement model

$$\begin{bmatrix} \cos(\delta^{FL}) & \sin(\delta^{FL}) & r_x^{FL} \sin(\delta^{FL}) - r_y^{FL} \cos(\delta^{FL}) \\ \cos(\delta^{FR}) & \sin(\delta^{FR}) & r_x^{FR} \sin(\delta^{FR}) - r_y^{FR} \cos(\delta^{FR}) \\ \cos(\delta^{RL}) & \sin(\delta^{RL}) & r_x^{RL} \sin(\delta^{RL}) - r_y^{RL} \cos(\delta^{RL}) \\ \cos(\delta^{RR}) & \sin(\delta^{RR}) & r_x^{RR} \sin(\delta^{RR}) - r_y^{RR} \cos(\delta^{RR}) \end{bmatrix} \begin{bmatrix} v_x \\ v_y \\ \omega \end{bmatrix} = \begin{bmatrix} v^{FL} \\ v^{FR} \\ v^{RL} \\ v^{RR} \end{bmatrix}$$

2-DOF Measurement model

$$\begin{bmatrix} \cos(\delta^{FL}) & r_x^{FL} \sin(\delta^{FL}) - r_y^{FL} \cos(\delta^{FL}) \\ \cos(\delta^{FR}) & r_x^{FR} \sin(\delta^{FR}) - r_y^{FR} \cos(\delta^{FR}) \\ \cos(\delta^{RL}) & r_x^{RL} \sin(\delta^{RL}) - r_y^{RL} \cos(\delta^{RL}) \\ \cos(\delta^{RR}) & r_x^{RR} \sin(\delta^{RR}) - r_y^{RR} \cos(\delta^{RR}) \end{bmatrix} \begin{bmatrix} v_x \\ \omega \end{bmatrix} = \begin{bmatrix} v^{FL} \\ v^{FR} \\ v^{RL} \\ v^{RR} \end{bmatrix}$$

Applicability of the alternative measurement model



$$\begin{bmatrix} \cos(\delta^i + \beta^i) & \sin(\delta^i + \beta^i) \end{bmatrix} \begin{bmatrix} 1 & 0 & -r_y^i \\ 0 & 1 & r_x^i \end{bmatrix} \begin{bmatrix} v_x \\ v_y \\ \omega \end{bmatrix} = v^i$$

Although the **alternative measurement model** is a more accurate representation of the vehicle kinematics, but without a **direct measurement of the wheel-slip angle** (β^i), the ego-motion estimation becomes noisy especially the yaw rate.

Hence in this project this alternative formulation is not used

Use-cases

- Short-term wheel odometry
- Can be used as a prior for localization
- Integrate multiple sensor scans by temporal alignment.
etc..

The End