1) Mp: Viscous work

- (2) (a) Reduction the numbers of control parameters 1 (b) Establishment of similarity conditions
- B) liquid metal = Pr≪1 > S≪ST FIX Us = Va.

- (5) 子可, Re = 慢性项 ,在 Reynold number 很大時,大部分的黏滞烫可忽略,但在 四界層內的黏滯效並不可忽略
- (6) 自然対流的 continuity equation, momentum equation, energy equation中之户 會隨溫書下而变動,所以 very difficult to solved these equations
- (7) $G_{V}^{*} = G_{V} \times V_{U} = \frac{g\beta(T_{W} T_{W})L^{3}}{V^{2}} \times \frac{hL}{k} = \frac{g\beta L^{4} h(T_{W} T_{W})}{kV^{2}} = \frac{g\beta L^{4} g_{W}^{*}}{kV^{2}} (; g_{W}^{*} = h(T_{W} T_{W}))$
- (8) 在 y=8, 3y=0, T=11 dy = MXO=0, 改没有 shear stress 在y=ST, T=Tw, g"=h(Too-To)=0, tx没有heat flux.
- (9) Nu is constant in the fully-developed region for both the temperature and relocity fields. 因意 温度梯度与连度方向垂直,所以没有额对流.
- (10) (1) 真空(2) 整温发精度(3)建度=0(4)温度梯度可速度流垂直、

(11) 白智为定律 $P+ = PV^2 + Pgx = constant$, 因意 V=V(y), 对为微分後 部+0+Pg=0 => dp = -pg

I. nduration : 流体因温度的改变,等致 density 改变, 而使物体为Pg改变而(1) Free convection : 流体因温度的改变,等致 density 改变, 而使物体为Pg改变而 (自然対流) 数场活为(byoyany force), 李致流体流動。

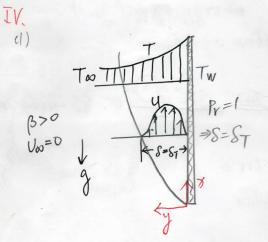
[分数考表: 36制文扩流 (forced convection: The fluid flow is caused by external forces, 初:电扇使空影流動)

(2) Bulk Sluid temperature:容積溫度,是面过管路流体的能量平均溫度下m Tm = 1 SACV SAC VT dAC & TAK mass-averaged temperature, VMixing-cup temperature.

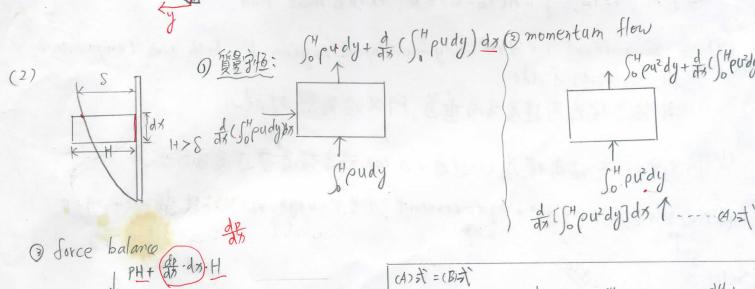
(3) Grashof number: Gr = gB(Tw-Tw)L³ 是活力ある。潜力的は值 定在自然对流的2万用就類似 Reynold number在張制对流的2万用

(4) Wind chill (temperature): 風寒效应, 人伴皮膚暴露在豬風中, 會感覺地當時氣溫更沒的效应.

(5) Boussinesz approximate: 在自然対影的 governing equation中, 好意为density 当作常权(constant), 降了景力项(buoyancy term)之外



速度曲线:由於不滑動(no-slip)倍件,使得平板壁上的 建度=0, 並逐渐增加至最大值,然度 逐渐减小, 直到四界層边缘, 其建及又 秀零, 国为感对流中, 流体是静止的.



PH+ dx dx = May yo dx

PH

T=0 \ W \ Twidx = May yo dx

PH

W = (She pg dy) dx

dp H dx + W + Twdx \
= (dx H) dx + (She pg dy) dx + (May y y = 0) dx \
- (B) = (dx H) dx + (She pg dy) dx + (May y y = 0) dx

(A) $\vec{x} = (B) \vec{x}$ $\frac{d}{dx} \left(\int_{0}^{H} \rho u^{2} dy \right) dx - \left(\frac{d\rho}{dx} + \right) dx - \left(\int_{0}^{H} \rho g dy \right) dx - M \frac{\partial u}{\partial y} \Big|_{y=0}$ $\frac{d}{dx} \left(\int_{0}^{H} \rho u^{2} dy \right) dx - \left(\frac{d\rho}{dx} + \right) dx - \left(\int_{0}^{H} \rho g dy \right) dx - M \frac{\partial u}{\partial y} \Big|_{y=0}$ $\frac{d}{dx} \left(\int_{0}^{H} \rho u^{2} dy \right) = \rho_{\infty} g + 1 - \int_{0}^{H} \rho g dy - M \frac{\partial u}{\partial y} \Big|_{y=0}$ $= \int_{0}^{H} \rho_{\infty} g dy - \int_{0}^{H} \rho g dy - M \frac{\partial u}{\partial y} \Big|_{y=0}$ $= \int_{0}^{H} (\rho_{\infty} - \rho) g dy - M \frac{\partial u}{\partial y} \Big|_{y=0}$ $3\frac{\partial}{\partial x} \left[\int_{0}^{H} \rho u^{2} dy \right] = \int_{0}^{H} \rho \left[\left(T - T_{\infty} \right) g dy - M \frac{\partial u}{\partial y} \right]_{y=0}$ $3\frac{\partial}{\partial x} \left[\int_{0}^{H} \rho u^{2} dy \right] = \int_{0}^{H} \rho \left[\left(T - T_{\infty} \right) g dy - M \frac{\partial u}{\partial y} \right]_{y=0}$

Date. To

III.

(1) if $\frac{Tw-T}{Tw-Tw}$ is invariant in the flow direction. $\frac{\partial (Tw-T)}{\partial v}|_{v=v_0} = constant$ $\frac{\partial T}{\partial v}|_{v=v_0} = constant$ Tw, Tw are function of z early $\Rightarrow \frac{\partial T}{\partial v}|_{v=v_0} = constant$ Tw-Tw $\frac{\partial T}{\partial v}|_{v=v_0} = constant$ $\frac{\partial T}{\partial v}|_{v=v_0} = k \cdot \frac{\partial T}{\partial v}|_{v=v_0} = k \cdot constant = constant$ $\frac{\partial T}{\partial v}|_{v=v_0} = k \cdot \frac{\partial T}{\partial v}|_{v=v_0} = k \cdot constant = constant$

$$\begin{array}{c} (2) \\ \hline \\ V \rightarrow \\ \hline \\ 2 \end{array}$$

$$\rho CV [(T+\Delta T)-T] \pi Y_0^2 = g''(2\pi Y_0) \Delta Z$$

$$\rho CV \Delta T \cdot Y_0 = 2g'' \Delta Z$$

$$\frac{\Delta T}{\Delta Z} = \frac{2}{Y_0} \frac{g''}{\rho CV}$$

Draw Come True K JJ) 27.

 $\frac{\partial V}{\partial t} = (\frac{9}{6}conV) - \frac{9}{6}conV^{2} + (\frac{9}{6}cond) - \frac{1}{6}cond^{2})$ $\frac{\partial V}{\partial t} = \frac{\partial (\frac{9}{6}cT)}{\partial t} \Delta y \Delta \xi$ $\frac{\partial ConV}{\partial t} = \frac{\partial (\frac{9}{6}cT)}{\partial t} \Delta y \Delta \xi$ $\frac{\partial ConV}{\partial t} = \frac{\partial (\frac{9}{6}cT)}{\partial t} \Delta y \Delta \xi$ $\frac{\partial ConV}{\partial t} = \frac{\partial (\frac{9}{6}cT)}{\partial t} \Delta y \Delta \xi$

 $C[\frac{\partial(\rho T)}{\partial t} + \frac{\partial}{\partial y}(\rho V T)] = k \frac{\partial^{2} T}{\partial y^{2}}$ $C[T_{f_{e}}^{2} + \rho F_{f_{e}}^{2} + \rho V_{f_{e}}^{2} + T \frac{\partial(\rho V)}{\partial y}] = k \frac{\partial^{2} T}{\partial y^{2}}$ $C[T_{f_{e}}^{2} + \rho F_{f_{e}}^{2} + \rho V_{f_{e}}^{2} + T \frac{\partial(\rho V)}{\partial y}] = k \frac{\partial^{2} T}{\partial y^{2}}$ $C[T_{f_{e}}^{2} + \rho F_{f_{e}}^{2} + \rho V_{f_{e}}^{2} + T \frac{\partial(\rho V)}{\partial y}] = k \frac{\partial^{2} T}{\partial y^{2}}$

国君YZS, T=Too且 U=0, 69以

(1)
$$\exists \frac{\partial^2 u^4}{\partial x^4 2} \geq \text{oxder} \ll \frac{L^2}{S^2} \frac{\partial^2 u^4}{\partial y^{4/2}} \geq \text{oxder}, \text{ fg. } \frac{\partial^2 u^4}{\partial x^4} \exists \hat{g} \hat{g}$$

$$\Rightarrow \begin{array}{c} O(1) & O(1) & O(1) & O(1) \\ U^* \frac{\partial U^*}{\partial \chi^*} + V^* \frac{\partial U^*}{\partial y^*} = -\frac{\partial p^*}{\partial \chi^*} + \frac{1}{Re} \frac{L^2}{8^2} \frac{\partial^2 U^*}{\partial y^*} \\ O(1) & O(1) & O(1) & O(\frac{1}{Re} \frac{L^2}{8^2}) & O(1) \\ 1 & + \frac{1}{2} \frac{2}{3} \frac{\partial^2 U^*}{\partial x^*} + \frac{1}{Re} \frac{L^2}{8^2} \frac{\partial^2 U^*}{\partial y^*} \\ \end{array}$$

上式各项之order为1

$$(2) \qquad \qquad U^{+} \frac{\partial V^{+}}{\partial x^{+}} + V^{+} \frac{\partial V^{+}}{\partial y^{+}} = -\frac{L^{2}}{S^{2}} \frac{\partial P^{+}}{\partial y^{+}} + \frac{1}{Re} \left[\frac{\partial^{2} V^{+}}{\partial x^{2}} + \frac{L^{2}}{S^{2}} \frac{\partial^{2} V^{+}}{\partial y^{+}} \right]$$

$$\frac{\partial^{2} V^{+}}{\partial x^{2}} = -\frac{L^{2}}{S^{2}} \frac{\partial P^{+}}{\partial y^{+}} + \frac{1}{Re} \left[\frac{\partial^{2} V^{+}}{\partial x^{2}} + \frac{L^{2}}{S^{2}} \frac{\partial^{2} V^{+}}{\partial y^{+}} \right]$$

$$\frac{\partial^{2} V^{+}}{\partial x^{2}} = 0$$

$$\Rightarrow V_{1} + V_{2} + V_{3} + V_{4} + V_$$

set
$$\frac{1}{Re} \frac{L^2}{S^2} \simeq 1$$

$$\Rightarrow U + \frac{\partial V}{\partial A} + V + \frac{\partial V}{\partial A} = \frac{\partial^2 V}{\partial A}$$

apply boundary layer theory,

$$\exists \begin{cases} y = \delta, \frac{\partial y}{\partial y} = 0, \ V = 0, \ P = P_{\infty} \\ y = S_{T}, \frac{\partial T}{\partial y} = 0 \end{cases}$$

$$\begin{cases}
\operatorname{gcond}_1 = -k \frac{\partial T}{\partial y} \Delta \xi \\
\operatorname{gcond}_2 = \left[-k \frac{\partial T}{\partial y} + \frac{\partial}{\partial x}\right]
\end{cases}$$

TW-TH DI

U= & Don = Tw-Tw

$$\frac{\partial(\rho c T)}{\partial t} = -\frac{\partial}{\partial y} (\rho (vT) = y = y + \frac{\partial}{\partial y} (k \frac{\partial T}{\partial y}) = y = y$$

$$C\left[\frac{d(PT)}{\partial t} + \frac{\partial}{\partial y}(PVT)\right] = k \frac{\partial^2 T}{\partial y^2}$$

$$C[T_{H}^{2}+\rho_{H}^{2}+\rho_{g}^{2}+T_{g}^{2}]=K_{g}^{2}$$

$$CT[\frac{3f}{ft} + \frac{3(pv)}{3y}] + cp[\frac{3T}{3t} + v\frac{3T}{3y}] = k\frac{3^2T}{3y^2}$$

連續方程式
$$\frac{\partial f}{\partial t} + \nabla \cdot \rho \vec{V} = 0$$

$$\Rightarrow \frac{\partial f}{\partial t} + \frac{\partial (\rho V)}{\partial y} = 0$$

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V亚(与另一份题目部间)