I. 简多题

1.0复空包V=0图号温度梯度图温度梯度图旅楼的重直

2.
$$P_{Y}=1$$
, $S_{T}=S$
 $P_{Y}<1$, $S_{T}>S$
 $P_{Y}>1$, S_{T}

$$\frac{1}{3}: P_{Y} = \frac{1}{2}$$

$$\frac{S}{S_{T}} \sim P_{Y}^{\frac{1}{3}}$$

3. 因温度梯度万向与旅場方向垂直

4. (a) Reduction the numbers of control parameters. i成力控制参数的個數

(b) Establishment of similarity conditions 建之相似情况

when (Reynold's number) Re is very large, the viscous term is neglected.

6.

7.
$$(y=0, u=0)$$

 $y=8, u=0$
 $y=8, \frac{0}{2}$ = 0

8,

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Date.	

9. film temperature Tf = Tw+Too , 流体的温度由军板表面造产Tw 变化全 四界層四線 温度 Too, 含3 高乡地計算流体馆 温度变化的性質, 通常用薄膜温度(film temperature) Tf ま計算.

II. Explain the following terms

- (1) Film temperature: 展膜温度Tg=Tw+Tw, 车板表面温度Tw的流体边界唇温度Tw的车均,用兴計算流体的性質
- (2) Prandtl number: Pr=立, 量测速发现界管的影響传通与感识导

31 Boussinesq approximation:

Treat density p as a constant in all terms in the equations governing natural convection.

except in the buoyancy tem.

(a) 通常, 强制对流的作用比自然对流强,所以自然对流可忽略 (b) 在高温時,自然对流的作用含增多的

(c) 当 6r/定 >10,自然对流 is of primary importance

(5) Nusselt number: Nu = hL

Dream Come True

June 8, 2012 (1) 因为 24* 《 12 24* 所以 224* 可忽略 (2) 因常 32V* 《 52 3以* 32V* 3有物 1271 = 0 PX =0 (3) y=8, $u=V_{\infty}\left(\frac{\partial y}{\partial y}=0,-\cdot\right)$, V=0, $P=P_{\infty}$ and y=ST, T=Too (3T=0, ---) (a) o velocity fields: (y=0, dy=0) 1 y= W , U=0 3 temperature Sields: y=0, JJ=0, T=Tc y=w, T=Tw (b) TW-T Tiv-Tm is invariant in the flow direction and Tw, Im are function of & only 2 [TW-T] =0

$$\frac{1}{Tw-Tm} \left[\frac{dTw}{dz} - \frac{\partial T}{\partial z} \right] - \frac{Tw-T}{(Tw-Tm)^2} \left[\frac{dTw}{dz} - \frac{dTm}{dz} \right] = 0$$

$$\frac{dTw}{dz} - \frac{\partial T}{\partial z} - \frac{Tw-T}{Tv-Tm} \left(\frac{dTw}{dz} - \frac{dTm}{dz} \right) = 0$$

$$\frac{\partial T}{\partial z} = \frac{dTw}{dz} - \frac{Tw-T}{Tw-Tm} \left(\frac{dTw}{dz} - \frac{dTm}{dz} \right) = 0$$

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	121	
considering constant heat slur	7 1131	
(g''=h(Tw-Tm)=c	onstand T	
and h = constant	(-2-)	
=> Tw-Tm = constant	TM	
$\Rightarrow \frac{dTw}{dz} - \frac{dTm}{dz} = 0$	7"	
	pcV[(T+ST)-T]=	
$\Rightarrow \frac{dTw}{dz} = \frac{dTw}{dz} - 2$	THIN COME & 16	
のか代入の式、 3章 ot = dTw -	(2)	
0		+
\$ 3, 37 = dTw = d	Tm = constant = = = = constant	(Como
	13 - 10 - 10 - 10 - 10 - 10 - 10 - 10 -	
(C) (1) J J J J J J M M M M M M M M M M M M M	- 2 - 1 / 1 4 JT 1 4 4 7 1 7 4 7 1 2	
(C) $\left(\frac{1}{2}\right)^{\frac{1}{2}} + \sqrt{\frac{1}{2}} = 2\frac{1}{2}$ and $\left(\frac{1}{2}\right)^{\frac{1}{2}}$	$= \frac{2}{W} \left[\frac{1}{2} \left(2 \sqrt{\omega} \frac{\partial T}{\partial n} \right) \frac{1}{3} y^{3} + T_{c} y \right] \left[\frac{1}{0} \right]$	
. U=UW, V=0	= W (dVo dx) + TC+TC	
> Vo # = 2 3/12	k dt) k · W (200 dt)	
$\Rightarrow \frac{\partial^2 T}{\partial y^2} = \frac{\sqrt{\omega} \frac{\partial T}{\partial x}}{\sqrt{\omega} \frac{\partial T}{\partial x}}$	$N = \frac{k \frac{\partial T}{\partial y}}{T_W - T_M} = \frac{k \cdot \frac{W}{2} (2U_W \frac{\partial T}{\partial x})}{\frac{2}{24}W^2 (2U_W \frac{\partial T}{\partial x})}$	
较为 ot = (Viody) y+C,	$=\frac{\delta k}{W}$	1
Boundary condition: $y=0$, $\frac{\partial J}{\partial y}=0$	$N_{u_W} = \frac{h \cdot w}{k} = 6$	
\Rightarrow $C_1=0$	consider the same securities	
$\frac{\partial T}{\partial y} = (2 \frac{V_0}{2} \frac{\partial T}{\partial x}) y$	KIRLS FYTEN LINES	
	Agricultural State of the State	
表第 $T = \frac{1}{2} (2 \sqrt{27}) y^2 + Cz$ Boundary condition $y = 0$, $T = Tc$	File LCO INT. March Americani	
$\Rightarrow c_2 = Tc$	ET-sT1 6	
35 7= = (a Vh 2T) y2+Tc	W. M. W.	6
$x y = \frac{W}{Z}$, $T = Tw$	16 July 1	
$3\sqrt[3]{Tw} = \frac{W^2}{8}(2\sqrt{\log \frac{3}{2}}) + Tc$		
Tm = Lare SAC UTDAC	The state of the s	
Ac Mare JAC	AL SIL THE	
Describer Francisco Franci		

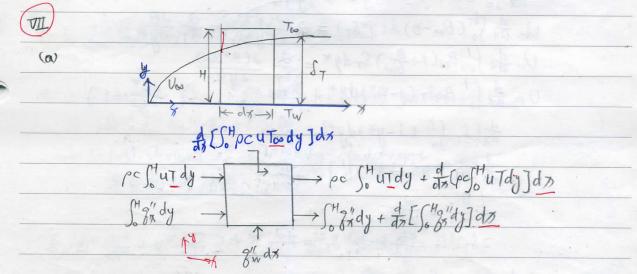
June 8, 2012 Tf = 110°(+10°(= 60°C ● 時義知. Tf=60°C, V=1896×10-5, K=0,02808, Pr=0.7>02 1) Re = VP = 8×0.1 = 4.22×104 指 Re, Pr 代入公式 电》以 【题目有公式, 控部本式 My】 x Nu = hD with = Nuxh [k=0.0808, D=0.1, Nu] 8 = hA (Tw-Ta) [9=8".A] 9= h. [(ZZY). L][TW-Tw) る)= h· T. D·(Tw-Too) (記) し直注=01m Too = 10°C h由 Nuxx 书等] 3 60 \$12 W/m] Dream Come Trus June 8, 20/2

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$$\frac{U_{SL}}{V} = \frac{[gB(Tw - T\omega)L]^{\frac{1}{2}}L}{V} = \frac{[gB(Tw - T\omega)L]^{3}}{V}^{\frac{1}{2}} = \frac{1}{6V^{2}}$$

Grashof number Gr = 3B(TW-TO)L3

$$\Rightarrow u^{+} \frac{\partial u^{+}}{\partial x^{+}} + v^{+} \frac{\partial u^{+}}{\partial y^{+}} = 0 + \frac{1}{\sqrt{6\pi}} \left(\frac{L^{2}}{S^{2}}\right) \frac{\partial^{2} u^{+}}{\partial y^{+}}$$



$$\frac{d}{d\pi} [pc \int_{0}^{H} u T dy] d\pi + \frac{d}{d\pi} [\int_{0}^{H} g_{\pi}' dy] d\pi = g_{u}'' d\pi + \frac{d}{d\pi} [\int_{0}^{H} pc u T \omega dy] d\pi$$

$$\frac{d}{d\pi} [pc \int_{0}^{H} U_{\omega} T dy] + \frac{d}{d\pi} [\int_{0}^{H} g_{\pi}'' dy] = g_{u}'' + \frac{d}{d\pi} [\int_{0}^{H} pc U_{\omega} T \omega dy]$$

$$\frac{d}{d\pi} [\int_{0}^{H} pc U_{\omega} T \omega dy] - \frac{d}{d\pi} [e \int_{0}^{H} U_{\omega} T dy] = -g_{u}'' + \frac{d}{d\pi} [\int_{0}^{H} g_{\pi}'' dy]$$

$$pc \frac{d}{d\pi} [\int_{0}^{H} U_{\omega} (T \omega - T) dy] = -g_{u}'' + \frac{d}{d\pi} [\int_{0}^{H} g_{\pi}'' dy]$$

Ada [5. 75/dy] 遠小於其地谈,可忽略. PC 気に「Uw(Tw-T)dy = - 3w" = - (- kogy)w)

$$\frac{\partial}{\partial \pi} \int_{0}^{6} U_{N} (T_{\infty} - T) dy = \frac{\partial}{\partial y} U_{N}$$

$$\frac{\partial}{\partial \pi} \int_{0}^{6T} (\theta_{\infty} - \theta) d(y * S_{T}) = \frac{\partial}{\partial y} \frac{\partial}{\partial y * S_{T}} = \frac{\partial}{\partial T} \frac{\partial}{\partial y}$$

$$\frac{\partial}{\partial \pi} \int_{0}^{6T} (\theta_{\infty} - \theta) d(y * S_{T}) = \frac{\partial}{\partial T} \frac{\partial}{\partial T} (\theta * \theta_{\infty})$$

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$$\frac{\partial}{\partial \pi} \int_{0}^{6T} (\theta_{\infty} - \theta) d(y * S_{T}) dy * = \frac{\partial}{\partial T} \frac{\partial}{\partial T} (\theta * \theta_{\infty})$$

$$\frac{\partial}{\partial \pi} \left[S_{T} \left(1 - \theta * \right) dy * = \frac{\partial}{\partial T} \frac{\partial}{\partial T} (\theta * \theta_{\infty})$$

$$\frac{\partial}{\partial \pi} \left[S_{T} \left(y * - \frac{1}{2} y *^{2} \right) \right]_{0}^{6T} = \frac{\partial}{\partial T}$$

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$$\frac{\partial}{\partial T} \left[S_{T} \left(y * - \frac{1}{2} y * - \frac{1}{2} y * \right) \right]_{0}^{6T} =$$

when
$$t = 0$$
, $S_T = 0 \Rightarrow C = 0$

$$S_T = \left(\frac{4\partial x}{V_{00}}\right)^{\frac{1}{2}} \Rightarrow \frac{S_T}{t} = 2\left(\frac{\partial}{V_{00}T}\right)^{\frac{1}{2}}$$

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$$S_T = \left(\frac{\partial}{\partial y}\right)_W = \frac{1}{S_T} = \frac{1}$$

$$Nu_{x} = \frac{hx}{k} = \frac{\pi}{\delta_{T}} = \frac{1}{z} \left(\frac{U\omega\pi}{a} \right)^{\frac{1}{z}}$$

$$\frac{U\omega\pi}{a} = \frac{U\omega\pi}{v} \frac{v}{a} = Re_{x} \cdot Pv$$

$$Nu_{x} = \frac{1}{z} P_{x}^{\frac{1}{z}} Re_{x}^{\frac{1}{z}}$$