

# WILEY

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## **Fundamentals of Momentum, Heat, and Mass Transfer**

**Sixth Edition**

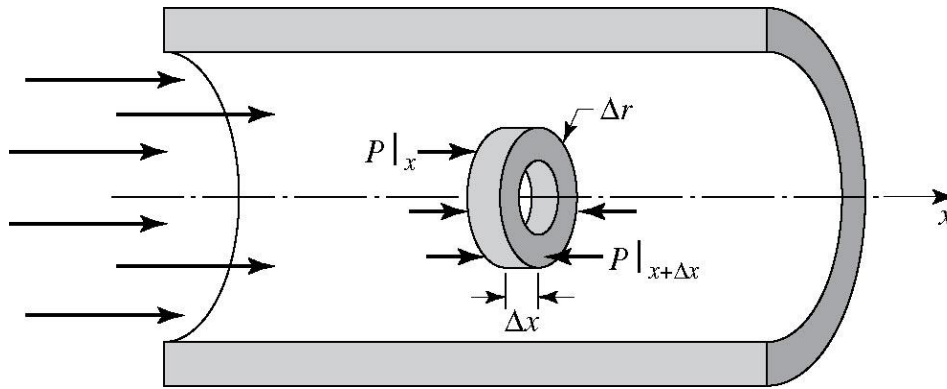
**Welty • Rorrer • Foster**

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### **Chapter 8**

*Analysis of a Differential Fluid Element in Laminar  
Flow*

## Fully developed laminar flow in a circular conduit

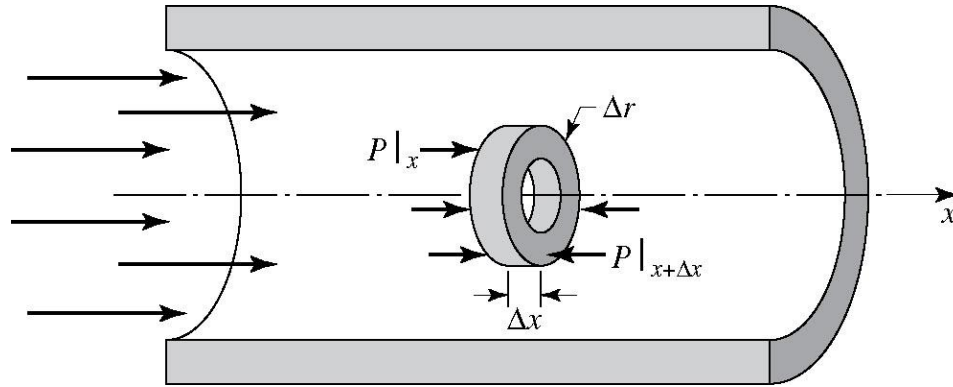


### Assumption:

1. The fluid behaves as a **continuum**.
2. The fluid is **incompressible** and **Newtonian**.
3. The flow is **laminar and fully developed**.
4. The flow is not influenced by entrance effects and represents a **steady-state** situation.

**Fully developed:** the velocity profile does not vary along the axis of flow

Conservation of **Mass** and **Momentum** should apply!!

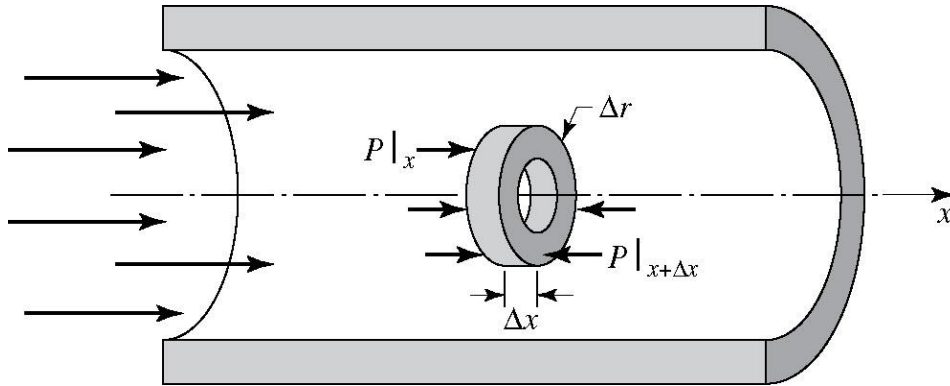


$$\Sigma F_x = \iint_{\text{c.s.}} \rho v_x (\mathbf{v} \cdot \mathbf{n}) dA + \frac{\partial}{\partial t} \iiint_{\text{c.v.}} \rho v_x dV \quad (5-5a)$$

$$-r \frac{dP}{dx} + \frac{d}{dr} (r \tau_{rx}) = 0 \quad (8-1)$$

$$\tau_{rx} = \left( \frac{dP}{dx} \right) \frac{r}{2} \quad (8-2)$$

$$\tau_{rx} = \mu \frac{dv_x}{dr} \quad (8-3)$$



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Flux integral

$\rho \mathbf{v}$ : mass flux

$\rho \mathbf{v} \mathbf{v}$ : convective momentum flux

$\tau$ : **stress**; **momentum flux** by molecular (viscous) transfer

$$v_x = -\left(\frac{dP}{dx}\right) \frac{1}{4\mu} (R^2 - r^2) \quad (8-4)$$

$$v_x = -\left(\frac{dP}{dx}\right) \frac{R^2}{4\mu} \left[1 - \left(\frac{r}{R}\right)^2\right] \quad (8-5)$$

$$v_{\max} = -\left(\frac{dP}{dx}\right) \frac{R^2}{4\mu} \quad (8-6)$$

$$v_x = v_{\max} \left[1 - \left(\frac{r}{R}\right)^2\right] \quad (8-7)$$

$$v_{\text{avg}} = \frac{v_{\max}}{2} = -\left(\frac{dP}{dx}\right) \frac{R^2}{8\mu} \quad (8-8)$$

### **Hagen-Poiseuille equation**

$$-\frac{dP}{dx} = \frac{8\mu v_{\text{avg}}}{R^2} = \frac{32\mu v_{\text{avg}}}{D^2} \quad (8-9)$$

## Hagen-Poiseuille equation

$$-\frac{dP}{dx} = \frac{8\mu v_{\text{avg}}}{R^2} = \frac{32\mu v_{\text{avg}}}{D^2} \quad (8-9)$$

**Reynolds number** for fluids flowing in tubes

$$\text{Re} = \frac{D v_{\text{avg}} \rho}{\mu}$$

Re < 2100, laminar flow

Re > 2100, turbulent flow

The shear stress components in cylindrical coordinates      The shear stress components in spherical coordinates

$$\tau_{r\theta} = \tau_{\theta r} = \mu \left[ r \frac{\partial}{\partial r} \left( \frac{v_\theta}{r} \right) + \frac{1}{r} \frac{\partial v_r}{\partial \theta} \right]$$

$$\tau_{z\theta} = \tau_{\theta z} = \mu \left[ \frac{\partial v_\theta}{\partial z} + \frac{1}{r} \frac{\partial v_z}{\partial \theta} \right]$$

$$\tau_{zr} = \tau_{rz} = \mu \left[ \frac{\partial v_z}{\partial r} + \frac{\partial v_r}{\partial z} \right]$$

$$\tau_{r\theta} = \tau_{\theta r} = \mu \left[ r \frac{\partial}{\partial r} \left( \frac{v_\theta}{r} \right) + \frac{1}{r} \frac{\partial v_r}{\partial \theta} \right]$$

$$\tau_{\phi\theta} = \tau_{\theta\phi} = \mu \left[ \frac{\sin \theta}{r} \frac{\partial}{\partial \theta} \left( \frac{v_\phi}{\sin \theta} \right) + \frac{1}{r \sin \theta} \frac{\partial v_\theta}{\partial \phi} \right]$$

$$\tau_{\phi r} = \tau_{r\phi} = \mu \left[ \frac{1}{r \sin \theta} \frac{\partial v_r}{\partial \phi} + r \frac{\partial}{\partial r} \left( \frac{v_\phi}{r} \right) \right]$$

## Hagen-Poiseuille equation

$$-\frac{dP}{dx} = \frac{8\mu v_{\text{avg}}}{R^2} = \frac{32\mu v_{\text{avg}}}{D^2} \quad (8-9)$$

Other forms?

Calculate the **force** of the fluid acting on the wetted surface of the pipe

Calculate the **mass rate of flow and average velocity**

## Experimental observation

**Reynolds number** for fluids flowing in tubes

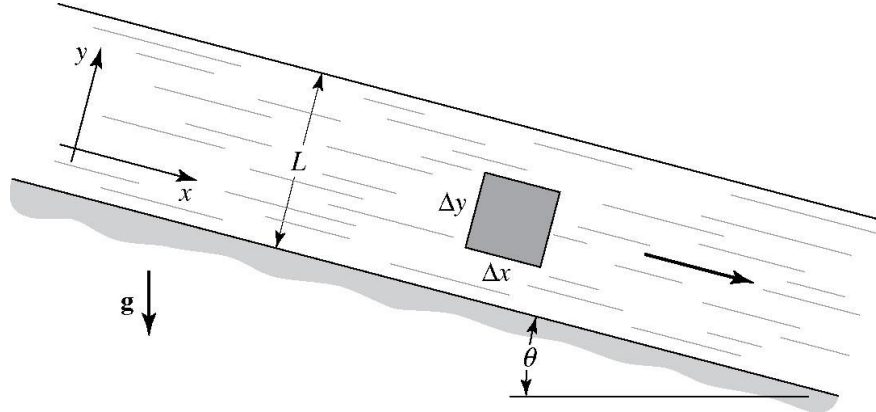
$$\text{Re} = \frac{D v_{\text{avg}} \rho}{\mu}$$

Re < **2100**, laminar flow

Re > **2100**, turbulent flow

Physical meaning of Re: **inertia force/viscous force**;  $\rho v^2 a^2 / \mu v a$

# Laminar flow of a Newtonian Fluid down on inclined-plane surface

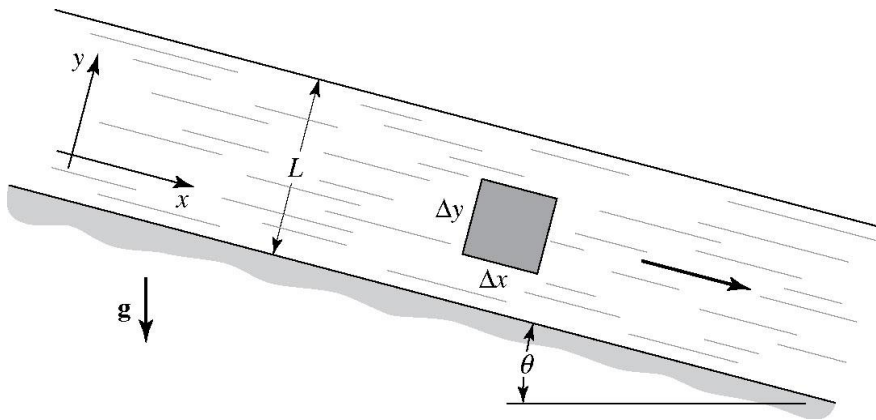


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Conservation of **Mass** and **Momentum** should apply!!





$$\frac{d}{dy} \tau_{yx} + \rho g \sin \theta = 0 \quad (8-10)$$

$$\tau_{yx} = \rho g L \sin \theta \left[ 1 - \frac{y}{L} \right] \quad (8-11)$$

$$v_x = \frac{\rho g L^2 \sin \theta}{\mu} \left[ \frac{y}{L} - \frac{1}{2} \left( \frac{y}{L} \right)^2 \right] \quad (8-12)$$

$$v_{\max} = \frac{\rho g L^2 \sin \theta}{2\mu} \quad (8-13)$$

Calculate the **force** of the fluid acting on the wetted surface of the wall

Calculate the **mass rate of flow and film thickness**

## Experimental observation

**Reynolds number** for fluids flowing in tubes

$$\text{Re} = \frac{4Lv_{\text{avg}}\rho}{\mu}$$

$\text{Re} < 20$ , **laminar flow** with negligible rippling

$20 < \text{Re} < 1500$ , laminar flow with pronounced rippling

$\text{Re} > 1500$ , **turbulent flow**

