

Last Time:

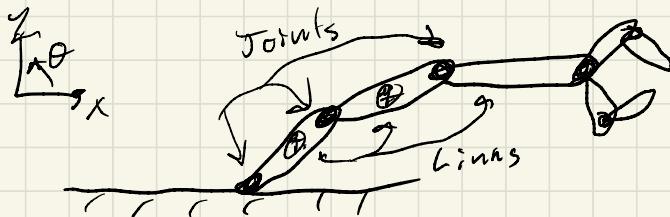
- Discrete Legendre Transform
- DCL with Constraints
- DCL with non-conservative forces

Today:

- Fixed-Base Manipulators
 - Floating-Base Systems
 - Least-Action with 3D Rotations
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Fixed - Base Manipulators:

- Classic serial/open-chain manipulators
(e.g. industrial robots/arms).



- Note (for now) we won't allow any joints that form closed loops.
- For systems like this, we can easily compute the position + orientation of each link in the world frame. from the joint angle. Called "forward kinematics".

- In 2D:

$$\text{link } \rightarrow \theta_1 = q_1$$

Orientation

in world

frame

$$r_1 = \underbrace{\begin{bmatrix} \cos(\theta) & \sin(\theta) \\ -\sin(\theta) & \cos(\theta) \end{bmatrix}}_{R(\theta)} \underbrace{a_1}_{\text{vector from joint 1 to Com of link 1}}$$

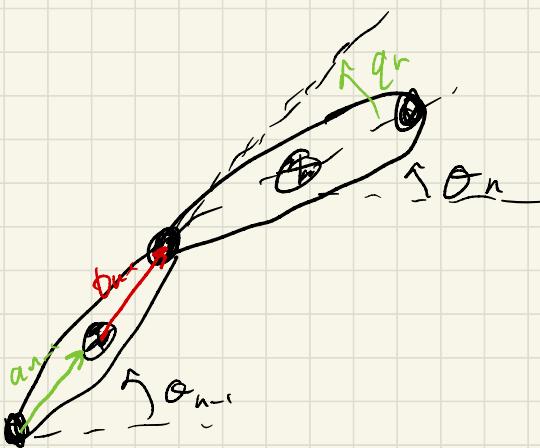
link COM
position in
world frame

for $K = 2:N$

$$\theta_n = \theta_{n-1} + q_n$$

$$r_n = r_{n-1} + R_{n-1} b_{n-1} + R(\theta_n) a_n$$

\uparrow
vector from COM
of link $n-1$ to point n



- In 3D:

$${}^N R_i^{B_i} = S_i(q_i)$$

$${}^N r_i = {}^N R_i^B a_i$$

$$R_n = R_{n-1} S_n(q_n)$$

$$r_n = r_{n-1} + R_{n-1} b_{n-1} + R_n a_n$$

- Let's focus on 2D for now. Let's write kinematics as a function:

$$\begin{bmatrix} r_1 \\ \theta_1 \\ r_2 \\ \theta_2 \\ \vdots \\ r_n \\ \theta_n \end{bmatrix} = k(q) \quad \text{--- } \mathbb{R}^n \text{ vector of joint angles}$$

- From this we can compute world-frame linear and angular velocity of each link:

$$\frac{d}{dt} \begin{bmatrix} r_1 \\ \theta_1 \\ \vdots \\ r_n \\ \theta_n \end{bmatrix} = \underbrace{\frac{\partial k(q)}{\partial q}}_{J} \dot{q}$$

$K(q) \in \mathbb{R}^{3n \times n}$

"Kinematic Jacobian"

- Given mass and inertia of each link, we can calculate kinetic energy:

$$T = \sum_{n=1}^N \frac{1}{2} m_n \dot{r}_n^T \dot{r}_n + \frac{1}{2} \sum J_n \dot{\theta}_n^2$$

$$= \frac{1}{2} \begin{bmatrix} \dot{r}_1 \\ \dot{\theta}_1 \\ \vdots \\ \dot{r}_n \\ \dot{\theta}_n \end{bmatrix}^T \underbrace{\begin{bmatrix} m_1 I & & & & \\ & \ddots & & & \\ & & G & & \\ & & & m_n I & \\ & & & & J_n \end{bmatrix}}_{\bar{M}} \begin{bmatrix} \dot{r}_1 \\ \dot{\theta}_1 \\ \vdots \\ \dot{r}_n \\ \dot{\theta}_n \end{bmatrix}$$

$$= \frac{1}{2} \dot{q}^T \underbrace{K(q) \bar{M} K(q)}_{M(q)} \dot{q} = \frac{1}{2} \dot{q}^T M(q) \dot{q}$$

- Similarly, we can compute $U(q)$ and $L(q, \dot{q})$

* Example: Forced Double Pendulum

- Joint torques are easy in this setup
- External forces applied to links take a little more work
- We can get this from the Lagrange-D'Alembert principle:

$$\frac{\partial}{\partial q(t)} \left[\int_{t_0}^{t_f} L(q, \dot{q}) dt + \int_{t_0}^{t_f} \underbrace{F(t)^T}_{\text{defined w.r.t. some coordinates } y} y(t) dt \right]$$

defined w.r.t. some coordinates y

- If we take the variational derivative:

$$\int_{t_0}^{t_f} \left[\frac{\partial L}{\partial q} - \frac{d}{dt} \left(\frac{\partial L}{\partial \dot{q}} \right) \right] \Delta q \, dt + \int_{t_0}^{t_f} F(t) \underbrace{\frac{\partial}{\partial q}}_{Y(q)} \Delta q \, dt$$

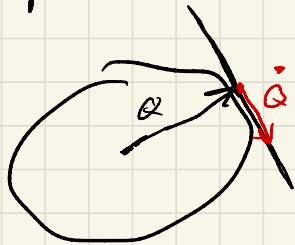
$$\Rightarrow M(q) \ddot{q} + C(q, \dot{q}) + \underline{F(q)} = Y(q)^T F$$

- * Example: double pendulum with external force

- To make this work in 3D we need some quaternion tricks.

Differentiating with Quaternions!

- Geometrically, a unit quaternion is confined to the unit sphere in \mathbb{R}^4 :



- Intuitively, derivatives of q live in local 3D tangent plane, just like ω :

$$\dot{Q} = \frac{1}{2} Q \times \hat{\omega} = \frac{1}{2} \underbrace{L(Q) H}_{\text{Left quaternion multiplication operator}} \omega$$

$\begin{bmatrix} 0 \\ \omega \end{bmatrix}$

Left quaternion multiplication operator

- I want a 3D gradient of $f(Q) : \mathbb{H} \rightarrow \mathbb{R}$
- We can parameterize a tiny rotation with an axis-angle vector ϕ :

$$\Delta Q = \begin{bmatrix} \cos(\|\phi\|) \\ \frac{\phi}{\|\phi\|} \sin(\|\phi\|) \end{bmatrix} \approx \begin{bmatrix} 1 \\ \phi \end{bmatrix} = \begin{bmatrix} 1 \\ 0 \end{bmatrix} + \begin{bmatrix} 0 \\ \phi \end{bmatrix}$$

- Now apply this to $f(Q)$:

$$\begin{aligned} f + \Delta f &= f(Q * \Delta Q) \approx f(Q * \begin{bmatrix} 1 \\ \phi \end{bmatrix}) = f(Q + Q * \hat{\phi}) \\ &\approx f(Q) + \frac{\partial f}{\partial Q} L(Q) H \phi \end{aligned}$$

$$\Rightarrow \Delta f = \frac{\partial f}{\partial Q} \underbrace{L(Q) H \phi}_{G(Q)}$$

$G(Q)$ "Attitude Jacobian"

$$\Rightarrow \frac{\partial f}{\partial \phi} = \frac{\partial f}{\partial Q} G(Q)$$

- Whenever we want to diff a function w.r.t. a quaternion input, take the standard Jacobian and right multiply by $G(Q)$
- We can play a similar trick on functions that output a quaternion:

$$Q = f(x) : \mathbb{R}^n \rightarrow \mathbb{H}$$

$$\begin{aligned}
 Q' &= Q + \Delta Q \approx Q + Q * \hat{\Delta \phi} = Q + L(Q) H \Delta \phi \\
 &\approx f(x + \Delta x) \approx f(x) + \frac{\partial f}{\partial x} \Delta x \\
 \Rightarrow \underbrace{L(Q) H \Delta \phi}_{\text{orthogonal}} &= \frac{\partial f}{\partial x} \Delta x \\
 \text{orthogonal} \Rightarrow L^T &= L^{-1}
 \end{aligned}$$

$$\begin{aligned}
 \Rightarrow H \Delta \phi &= L(Q)^T \frac{\partial f}{\partial x} \Delta x \\
 \Rightarrow \Delta \phi &= \underbrace{H^T L^T(Q)}_{G^T(Q)} \frac{\partial f}{\partial x} \Delta x
 \end{aligned}$$

- Whenever we want to diff a function with a quaternion output, take the standard Jacobian and left multiply by $G^T(Q)$.
- We can now compute kinetic energy of a 3D mechanism.
- Assume our kinematics function has the form:

$$\begin{bmatrix} {}^N r_i \\ {}^N Q_i \\ \vdots \\ r_n \\ Q_n \end{bmatrix} = k(q)$$

- Differentiate and apply $\bar{G}^T(q)$ to the output:

$$\begin{bmatrix} \Delta r_1 \\ \Delta \theta_1 \\ \vdots \\ \Delta r_n \\ \Delta \theta_n \end{bmatrix} = \begin{bmatrix} I & G^+(q, 1) & 0 \\ 0 & \ddots & \vdots \\ 0 & 0 & I & G^+(q, n) \end{bmatrix} \frac{\partial K}{\partial q} \Delta q$$

$\underbrace{\hspace{10em}}_{\bar{G}^T(q)}$

$$\Rightarrow \begin{bmatrix} V_1 \\ \dot{V}_1 \\ \vdots \\ V_n \\ \dot{V}_n \end{bmatrix} = \bar{G}^T(q) K(q) \dot{q}$$

- Now we can compute kinetic energy:

$$T = \frac{1}{2} \dot{q}^T \underbrace{K^T(q) \bar{G}(q) M \bar{G}^T(q) K(q)}_{M(q)} \dot{q}$$

$$\bar{M} = \begin{bmatrix} m_1 I & & \\ & \ddots & 0 \\ 0 & & m_n I & J_n \end{bmatrix}$$

J_n is the 3×3 inertia matrix of link K .