



# "Event 4 Report"

# Submitted for the fulfillment of the CIE (Event-4) for the course CONTROL SYSTEMS

(EC540)

## Submitted by

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#### **Probelm Statement**

For the plant G(s) = 1/s(s+6) design a phase-lead controller for damping ratio  $\zeta = 0.4$  and natural frequency 15 rad/sec.

What is the phase margin and gain margin of the compensated system?

#### Solution

#### **Clearing Workspace**

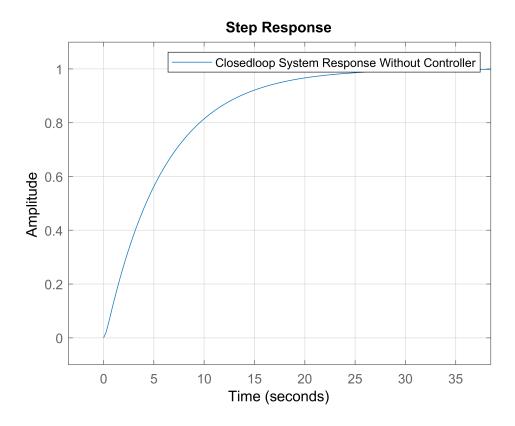
```
close all;
clear;
clc;
```

#### System without a controller

```
s=tf('s');
G=1/(s*(s+6));
```

#### Gcl = Closedloop Transfer Function

```
Gcl = G/(1+G); % system without controller
step(Gcl); % plotting step response
grid on;
setAxisLimits(axis);
legend('Closedloop System Response Without Controller');
```



Poles fo the system without controller

```
disp(pole(Gcl));

0
-6.0000
-5.8284
-0.1716
```

One of the pole is on the imaginary axis, and therefore, the system without controller is marginally stable.

Time domain parameters of system

```
stepinfo(Gcl)
```

```
ans = struct with fields:
    RiseTime: 12.8096
SettlingTime: 22.9766
SettlingMin: 0.9016
SettlingMax: 0.9993
    Overshoot: 0
    Undershoot: 0
    Peak: 0.9993
PeakTime: 42.6770
```

# Designing a Phase Lead Controller

```
\zeta = 0.4
```

 $\omega n = 15$ 

```
zita = 0.4;
wn = 15;
desiredPoles = roots([1 2*zita*wn wn^2]);
```

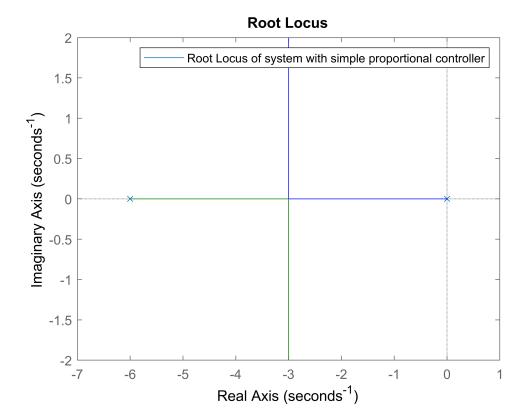
Root Locus must pass throught desired poles.

```
disp(desiredPoles);
```

```
-6.0000 +13.7477i
-6.0000 -13.7477i
```

Root Locus of a system with a simple proportional controller

```
figure;
rlocus(G);
legend('Root Locus of system with simple proportional controller');
```



We can see that no matter what, the root locus doesn't pass through desired poles.

```
syms s1
G1=1/(s1*(s1+6));
phi=double(angle(subs(G1,s1,-6+13.74i)))*180/pi;
sphi=180-phi;
```

The zero of the controller is usually taken just below the desired poles, but as in this system, a pole already exists at S = -6.

 $\therefore$  We take the zero of the controller slightly towards left of -6. i.e S = -7 or **Z = 7**.

```
z=-7;
p=z-13.7477/tand(90-sphi);
disp(p);
```

-13.0034

And thus we the pole of the controller as -13 or P = 13.

Then we find out **k** using magnitude criteria.

```
Ds=(s1-z)/(s1-p);
k=1/(double(abs(subs(Ds*G1,-6+13.7477i))))
```

k = 230.8210

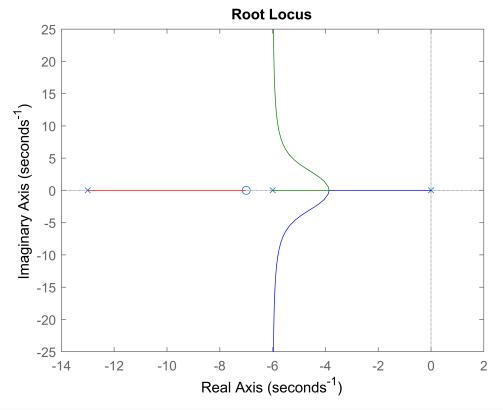
Thus at k = 230.5863, the RL passes through the desired pole location.

#### Verification of design

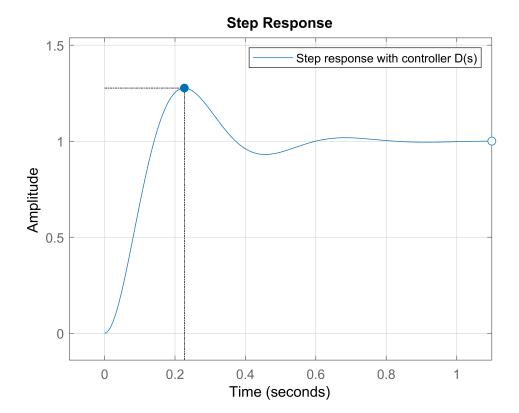
Ds = Controller Transfer Function

Ls = Closedloop Transfer Function with Controller

```
Ds = (s-z)/(s-p);
Ls = k*Ds*G/(1+k*Ds*G);
figure;
rlocus(Ds*G);
```



```
figure;
response = stepplot(Ls);
grid on;
response.showCharacteristic('PeakResponse');
response.showCharacteristic('SettlingTime');
response.showCharacteristic('RiseTime');
response.showCharacteristic('SteadyState');
setAxisLimits(axis);
legend('Step response with controller D(s)');
```



Time Domain parameters of system with controller.

```
stepinfo(Ls)

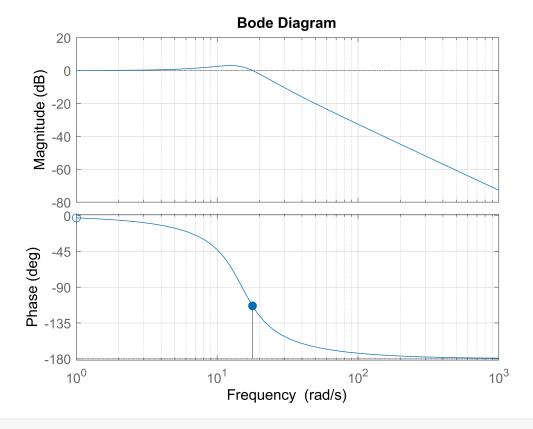
ans = struct with fields:
    RiseTime: 0.0952
SettlingTime: 0.5612
SettlingMin: 0.9312
SettlingMax: 1.2771
    Overshoot: 27.7119
Undershoot: 0
    Peak: 1.2771
PeakTime: 0.2267
```

```
[gainMargin, phaseMargin, wcg, wcp] = margin(Ls)
```

```
Warning: The closed-loop system is unstable.
gainMargin = Inf
phaseMargin = 66.5761
wcg = Inf
wcp = 17.8151
```

### **Bode Plot of the closed loop transfer function.**

```
response = bodeplot(Ls);
response.showCharacteristic('AllStabilityMargins');
grid on;
```

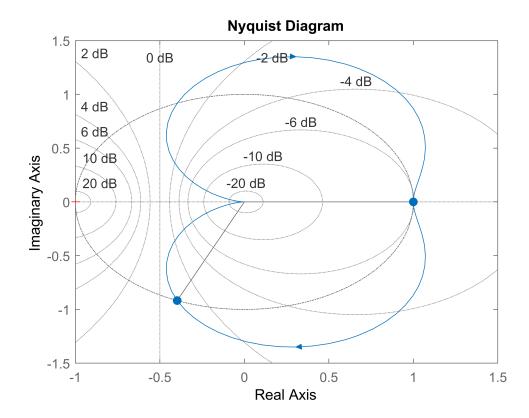


We can see from the **bode plot** that once the gain crossed the **0db** point, it never crosses it back again, hence no matter what the gain is, the system is going to remain stable.

Where as the phase when the gain crosses the **0db** is the **phase margin** and it's angle is 66.57°

#### Nyquist Plot of the closed loop transfer function

```
response = nyquistplot(Ls);
response.showCharacteristic('AllStabilityMargins');
grid on;
```



#### Inference

Since the **Gain Margin is infinity**, any amount of gain will not result in system getting unstable, this can be shown in the Nyquist plot.

**Phase Margin is 66.5761**, this means that the system is stable for any value on phase but not 66.5761. As seen on the Nyquist plot, At a gain of **0db**, the plot touches the -1 point at an angle of 66.5761 degrees.

(Simm: P(8) = 1 To Do: Design a phase lead Z=0.4 Wn= 15 wad/s. Sd= - 7 Wn + Wn \( 1 - \frac{7}{2} = -6 \pm 3\sqrt{21 y'}. We check if a simple proportional controlles can salue.  $\propto (8) = 1 + R G(8) = 1 + R = 8^{2} + 68 + R$   $8(8+6) = 8^{2} + 68 + R$ Funding wats & 32+68+12. Poles are  $-b \pm \sqrt{b^2 - 4ac}$  $= -6 \pm \sqrt{36 - 4R} = -3 \pm \sqrt{9 - R}$ Since the real part is always -3, it never passes though Sol vie -6 ± 3 √21 ij. So me use a phase dead contidles.

```
Phase lead Controller.
   Sites 2:
                D(8)= R(8+Z) Zero à the controller cis
8+P. Chosen below Sd, but un this
                                   system, a fide already exists at 8=-6.
                       . We chose the pde location to be -\frac{7}{2}
                                     ue Z=7.
-> Funding During angle exileria.
                    in 10 (sd) + 16, (sd) =+180°.
             me 18d+z - 18d+b - 18d - 18d+6 = ± 180°
             2-6+3\sqrt{21}y^{2}+7-24+2-24+2-26+3\sqrt{21}y^{2}-2-6+3\sqrt{21}y^{2}+6=\pm 180^{\circ}
        ± 180= 85.839° - 18/14 - 113.54° - 90 = ±180
                           28d+P = 62.269 = \tan^{-1}\left(\frac{3\sqrt{21}}{P-6}\right)
                    P = \frac{3\sqrt{21}}{\tan(62.269)} + 6 = \frac{13.22}{100}
                                                 L(s) = \frac{K(s+7)}{8(s+6)(s+13.22)}
Funding Rusing magnitude criteria.
       R = \frac{1}{|L(s)|} = \frac{|Sd||Sd+6||Sd+13.22|}{|Sd|+7|}
   R = \left| -6 + 3\sqrt{21} \mathring{y} \right| \left| 3\sqrt{21} \mathring{y} \right| \left| -6 + 3\sqrt{21} \mathring{y} + 13.22 \right| = \boxed{232.31}
                     1-6+3/214+71.
```

2(8) = 232.31 (847) 8(8+6) (8+13.22)

Eteteling the RL & L(≤) aboute, we can see that the point -6 ± 31/21 y passes through.