

# 1 Numerical solution of The Non linear Shallow Water Equations

The one dimensional Non Linear Shallow Water Equations with flat bottom read in conservation form

$$\begin{aligned} h_t + (hu)_x &= 0 \\ (hu)_t + \left(hu^2 + \frac{1}{2}gh^2\right)_x &= 0 \end{aligned} \quad (1)$$

where subscripts denote partial derivatives respect to time and space variables  $t$  and  $x$ ;  $h$  denotes the water column height;  $u$  the horizontal velocity;  $g = 9.81$  the gravity acceleration. As a conservation law, the system (??) can be written as

$$U_t + F(U)_x = 0 \quad (2)$$

where  $U = (h, hu)^T$ ,  $F(U) = (hu, hu^2 + \frac{1}{2}gh^2)$ . Weak solutions are approximated using a Finite Volume scheme. After averaging the system (2) in a cell  $\Omega_i = [x_i - \Delta x/2, x_i + \Delta x/2]$ , and defining  $\bar{U} = \frac{1}{\Delta x} \int_{\Omega_i} U(x)dx$ , then a semidiscrete approximation to (2) is

$$\bar{U}_t + \frac{1}{\Delta x} (F(U_{i+1/2}) - F(U_{i-1/2})) = 0 \quad (3)$$

where  $U_{i\pm 1/2}$  corresponds to the values of the conserved variables at the interface of each cell. The system (3) is integrated in time using an Euler scheme with CFL condition

$$\Delta t = CFL \frac{\Delta x}{\max_i(|u_i| + c_i)} \quad (4)$$

with  $CFL = 0.45$ .

## 1.1 Riemann problem

At each time-step the the values at each interface  $U^* = U_{i+1/2}$  of system (??) are obtained from the solution to the Riemann problem of the non-conservative form of (2) between the two neighbor states  $U_L = U_i$  and  $U_R = U_{i+1}$

$$\begin{aligned} U_t + A(U)U_x &= 0 \\ U(t=0, x) &= \begin{cases} U_l & , \text{ if } x \leq 0. \\ U_r & , \text{ if } x > 0 \end{cases} \end{aligned} \quad (5)$$

where  $A$  is the jacobian matrix of  $F(U)$ . The solution to this Riemann problem is found using the approximate Riemann solver of Roe that is described in

reference [1]. It consists first of a change of variables that allows to write (5) for  $h > 0$  as

$$\begin{aligned} V_t + C(V)V_x &= 0 \\ V(t=0, x) &= \begin{cases} V_l & , \text{ if } x \leq 0. \\ V_r & , \text{ if } x > 0 \end{cases} \end{aligned} \quad (6)$$

with  $V = (2c, u)^T$  and  $C(V) = \begin{pmatrix} u & c \\ c & u \end{pmatrix}$ . Second, instead of using the exact formulation, a linearized problem is solved using  $C(\hat{V})$  in place of  $C(V)$ , with  $\hat{V} = (V_L + V_R)/2$ . The matrix  $C(\hat{V})$  is diagonalizable and thus, a decoupled system can be obtained in the form

$$\begin{aligned} (w_1)_t + \hat{\lambda}_1 (w_1)_x &= 0 \\ (w_2)_t + \hat{\lambda}_2 (w_2)_x &= 0 \\ (w_1, w_2)^T(t=0, x) &= \begin{cases} ((w_1)_L, (w_2)_L)^T & , \text{ if } x \leq 0. \\ ((w_1)_R, (w_2)_R)^T & , \text{ if } x > 0 \end{cases} \end{aligned} \quad (7)$$

where  $\hat{\lambda}_1 = \hat{u} - \hat{c}$ ,  $\hat{\lambda}_2 = \hat{u} + \hat{c}$ ,  $w_1 = u - 2c$ ,  $w_2 = u + 2c$  and  $(w_1)_L = u_L - 2c_L$ ,  $(w_2)_L = u_L + 2c_L$ ,  $(w_1)_R = u_R - 2c_R$ ,  $(w_2)_R = u_R + 2c_R$ . Writing  $W = (w_1, w_2)$  and noticing that  $\hat{\lambda}_1 \leq \hat{\lambda}_2$ , the solution can be found for three separate cases:

- If  $\lambda_1 > 0$ , then  $W^* = W_L$
- If  $\lambda_1 \leq 0$  and  $\lambda_2 > 0$ ,  $W^* = ((w_R)_1, (w_L)_2)^T$
- If  $\lambda_2 \leq 0$ ,  $W^* = W_R$

and values at the interface can then be recovered setting the inverse transformation

$$\begin{aligned} u^* &= \frac{1}{2}(w_1^* + w_2^*) \\ h^* &= \frac{1}{16g}(w_2^* - w_1^*)^2 \end{aligned} \quad (8)$$

A third step is necessary, which consists on an entropy fix to select only weak solutions that are physically consistent. This is simply obtained by setting  $W^* = \hat{W}$  whenever  $(\lambda_1)_L < 0$  and  $(\lambda_1)_R > 0$ , or  $(\lambda_2)_L < 0$  and  $(\lambda_2)_R > 0$ .

## 1.2 Second order Finite Volume Scheme

To obtain second order convergence for smooth solutions a MUSCL (Monotonic Upstream-Centered) scheme is used. This means that instead of solving a Riemann problem between  $U_L = U_i$  and  $U_R = U_{i+1}$  one must solve for  $U_L = U_{i,r}$  and  $U_R = U_{i+1,l}$ , where  $U_{i,r} = U_i + \frac{\Delta x}{2}s$ ,  $U_{i,l} = U_i - \frac{\Delta x}{2}s$   $s = \minmod(s_L, s_R)$ ,  $s_L = \frac{U_i - U_{i-1}}{\Delta x}$ ,  $s_R = \frac{U_{i+1} - U_i}{\Delta x}$  and

$$\minmod(s_1, s_2) = \begin{cases} \min(s_1, s_2) & \text{if } s_1 > 0 \text{ and } s_2 > 0 \\ \max(s_1, s_2) & \text{if } s_1 < 0 \text{ and } s_2 < 0 \\ 0 & \text{elsewhere} \end{cases} \quad (9)$$

## References

- [1] F. Marche, P. Bonneton, P. Fabrice, and N. Seguin. Evaluation of well-balanced bore-capturing schemes for 2d wetting and drying processes. *International Journal for Numerical Methods in Fluids*, 53:867–894, 2006.