



A Numerical Investigation of Interface Deformation Forced by a Bluff Body

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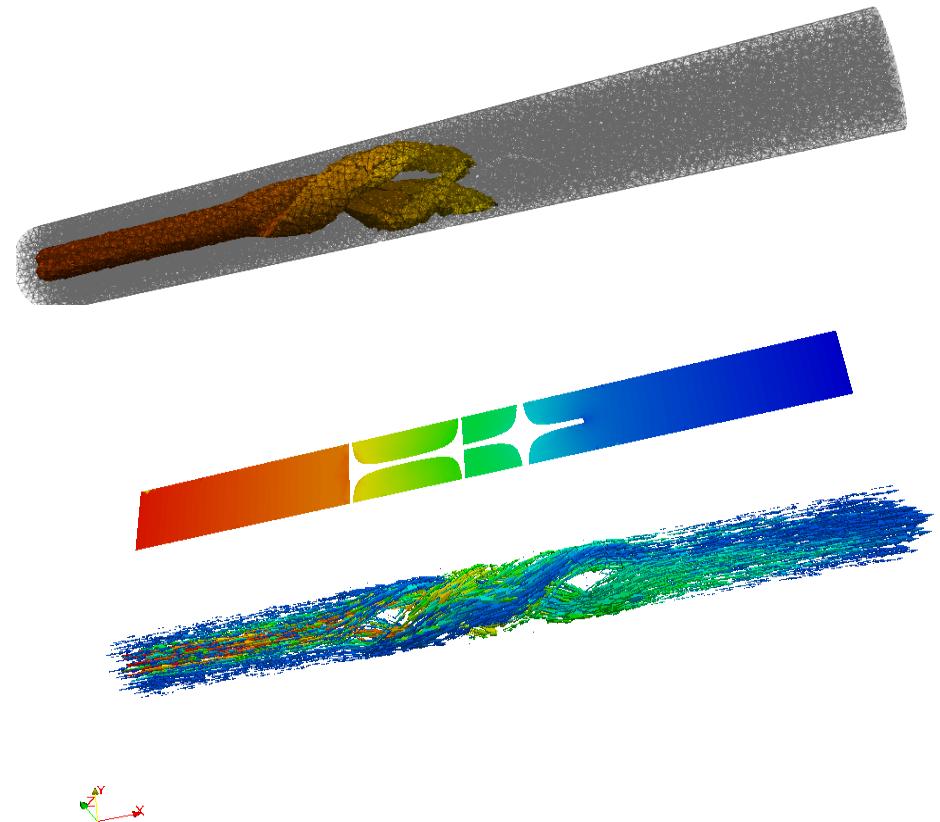
Prof Panagiota
Angeli

Overview

- Two phase flow in a pipe with interface deformation forced by a transverse bluff body
- Core problem part of experimental work at UCL Chemical Engineering Dept.
- Numerical investigation conducted at ICL in Applied Modelling & Computation Group using in-house code, Fluidity

FLUIDITY

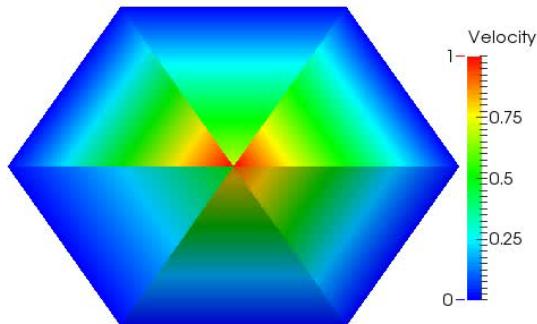
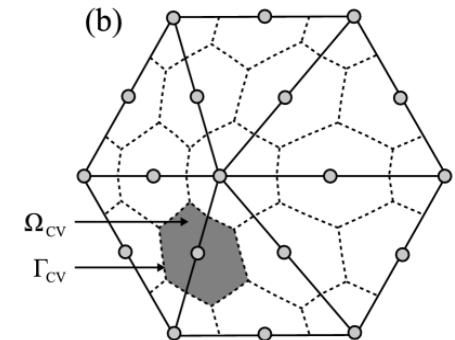
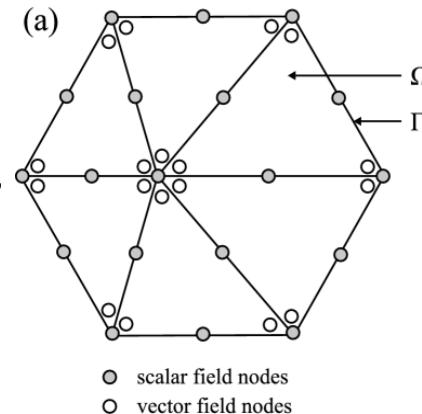
- Control volume-Finite element solver framework
- Mesh adaptivity capability
- Multiphase & multimaterial formulations (and both together)



CVDFEM methods

Control Volume Finite Element Method

- Solve weak form PDEs
- piecewise smooth fns for unconserved, unbounded variables
- piecewise flat fns for conserved & bounded tracers

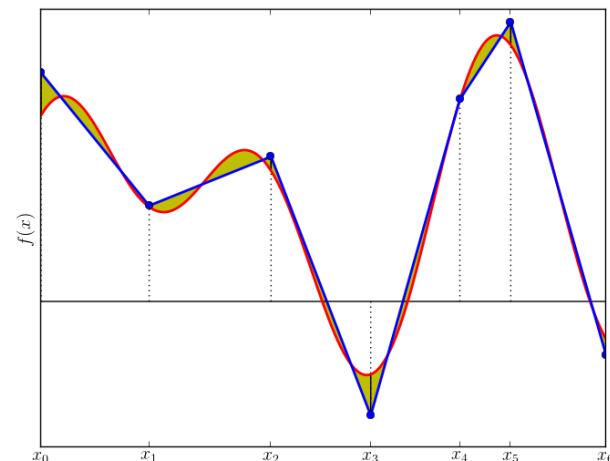
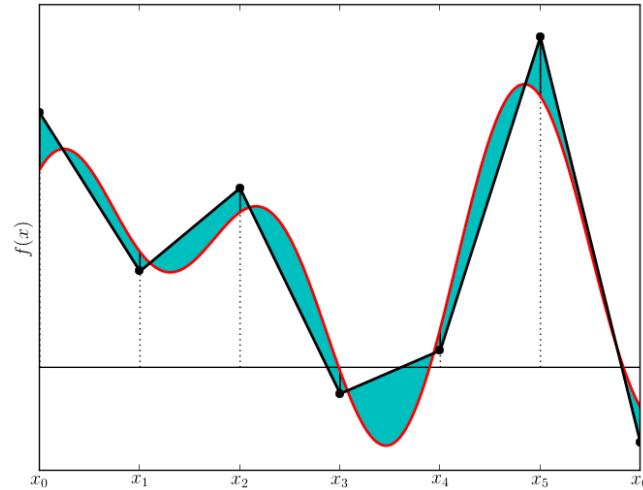


Discontinuous Galerkin Methods
Don't strongly enforce continuity of
the finite element variables across
finite element boundaries

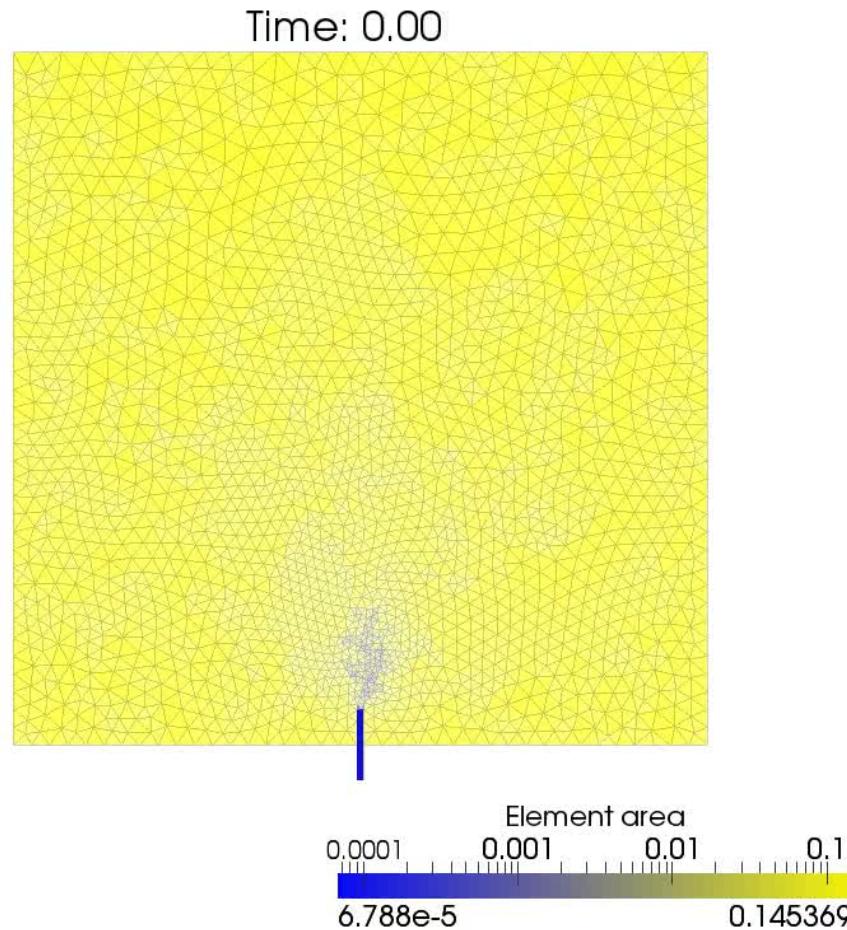
Mesh Adaptivity

- Minimise weighted sum of estimated linear interpolation error
- Estimate calculated from the data
- Place resolution in regions of solution curvature
 - Boundary layers
 - Filaments
 - Droplets
- Method is anisotropic
 - Aligns with flow

C.C. Pain, A.P. Umpleby,
 C.R.E. de Oliveira & A.J.H. Goddard (2001)
 Computer Methods in Applied
 Mechanics and Engineering



Mesh Adaptivity

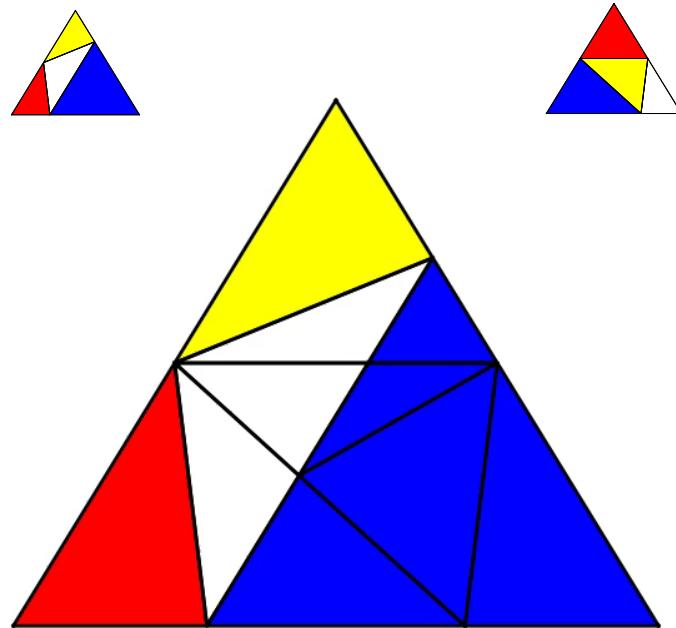


Supermeshing

FE solutions/test functions
piecewise smooth over mesh
elements

Elements of supermesh: old
variables and new test fns
both smooth.
No jumps.

Allows efficient
conservative mesh to
mesh interpolation via
projection methods

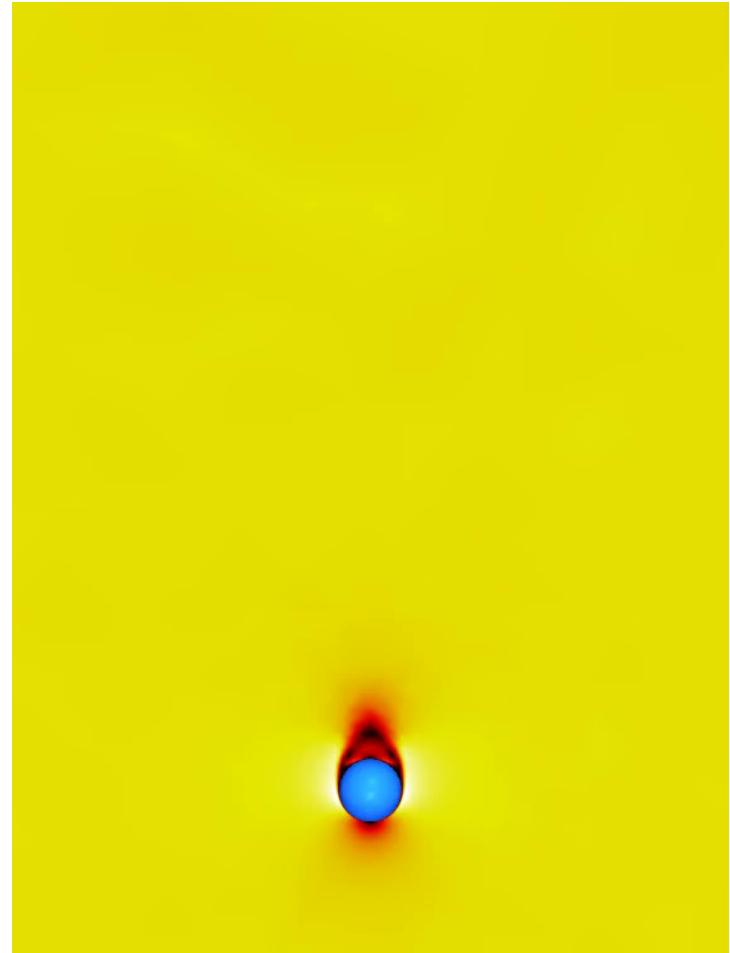


P. E. Farrell & J. R. Maddison (2011)
Computer Methods in Applied
Mechanics and Engineering

$$\sum_{k \in \{1, \dots, |T_3|\}} \int_{\Omega_k} N_{\sigma_i(k)} N_{\sigma_j(k)} \hat{\alpha}_{\sigma_j(k)} dA = \sum_{k \in \{1, \dots, |T_3|\}} \int_{\Omega_k} N_{\sigma_i(k)} N_{\pi_j(k)} \alpha_{\pi_j(k)} dA$$

Flow past a body

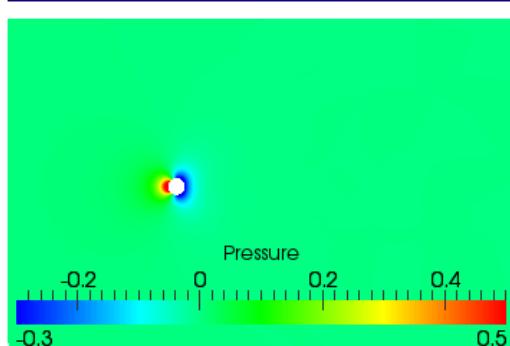
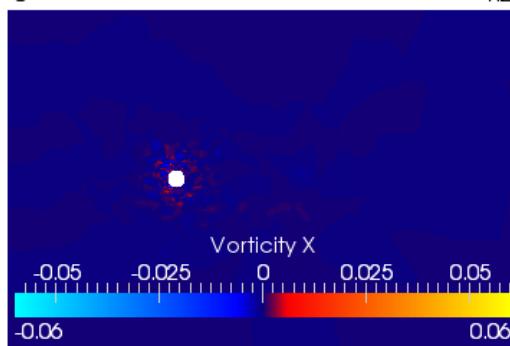
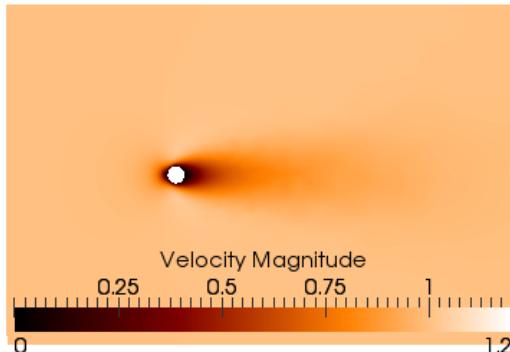
- Fixed solid body inserted into turbulent background flow
- Classic problem in single phase flow
- As flow becomes more turbulent object begins shedding sheet of alternating von Karman vortices.



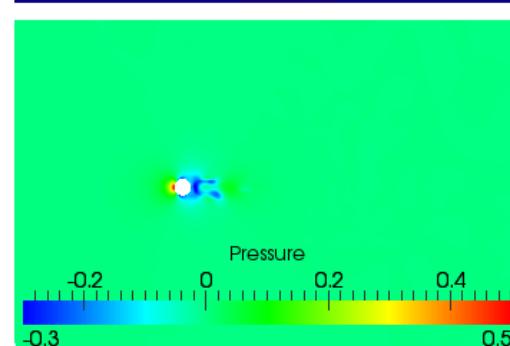
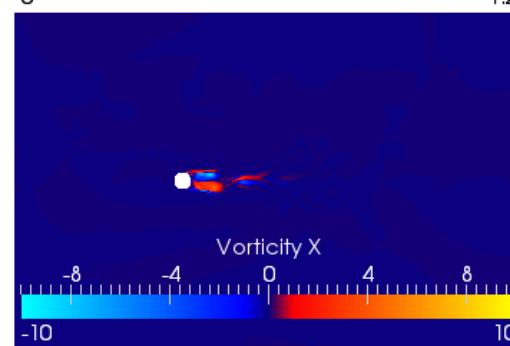
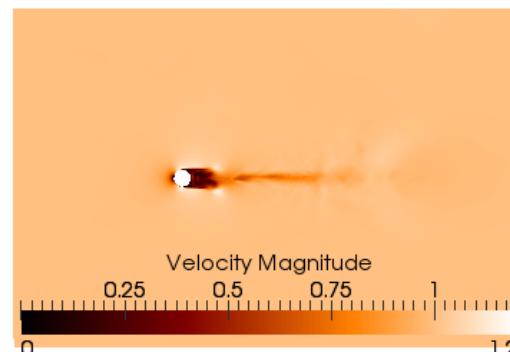


Flow Past a Body

Re
10



Re
1000

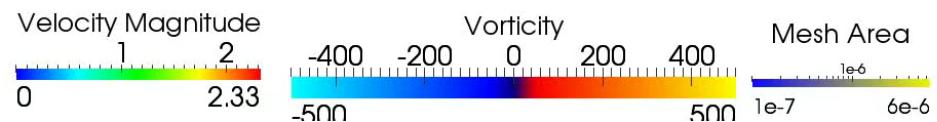
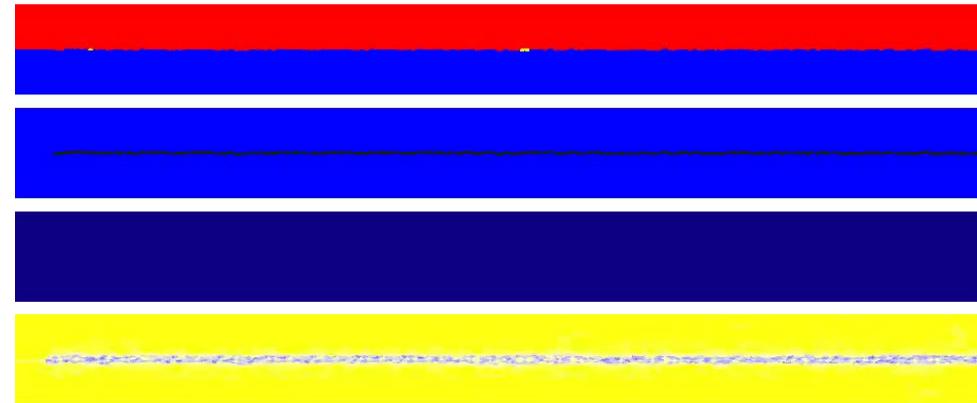


Two phase flow

Number of additional physical processes

Numerically “hard”

- Material Interfaces
- Viscosity differences
- Surface tension
- Droplets

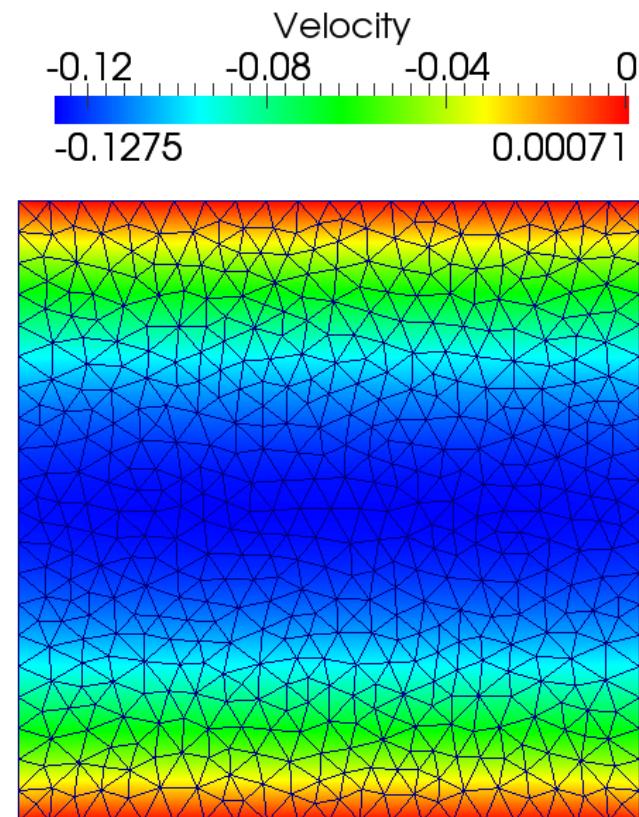
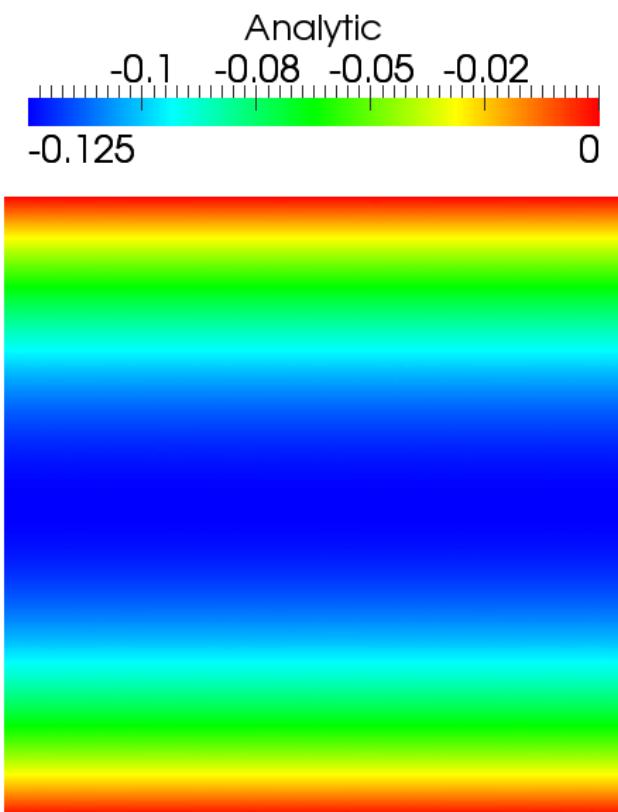


Verification of flow model

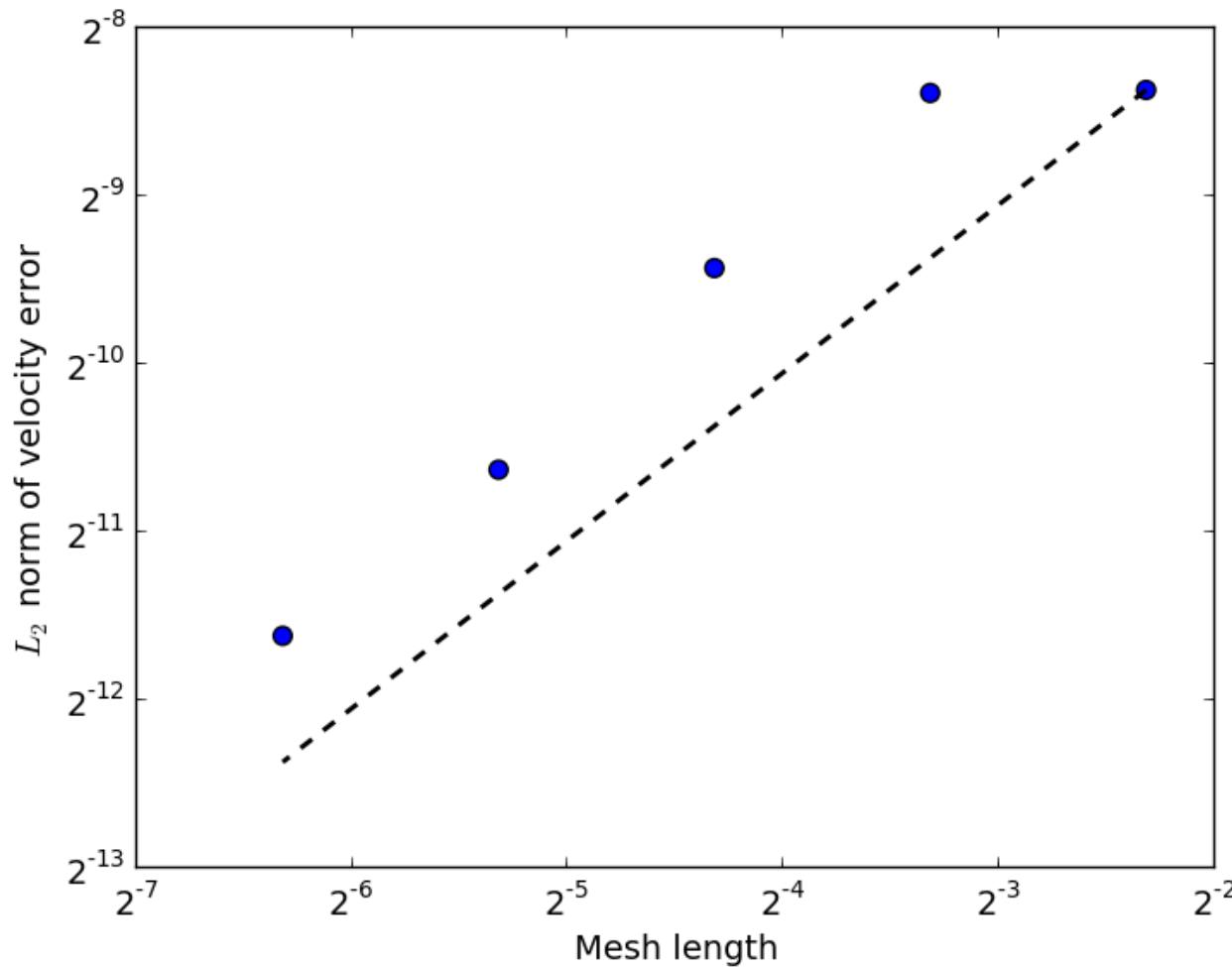
Single phase laminar channel flow

Spin up from
Pressure differential

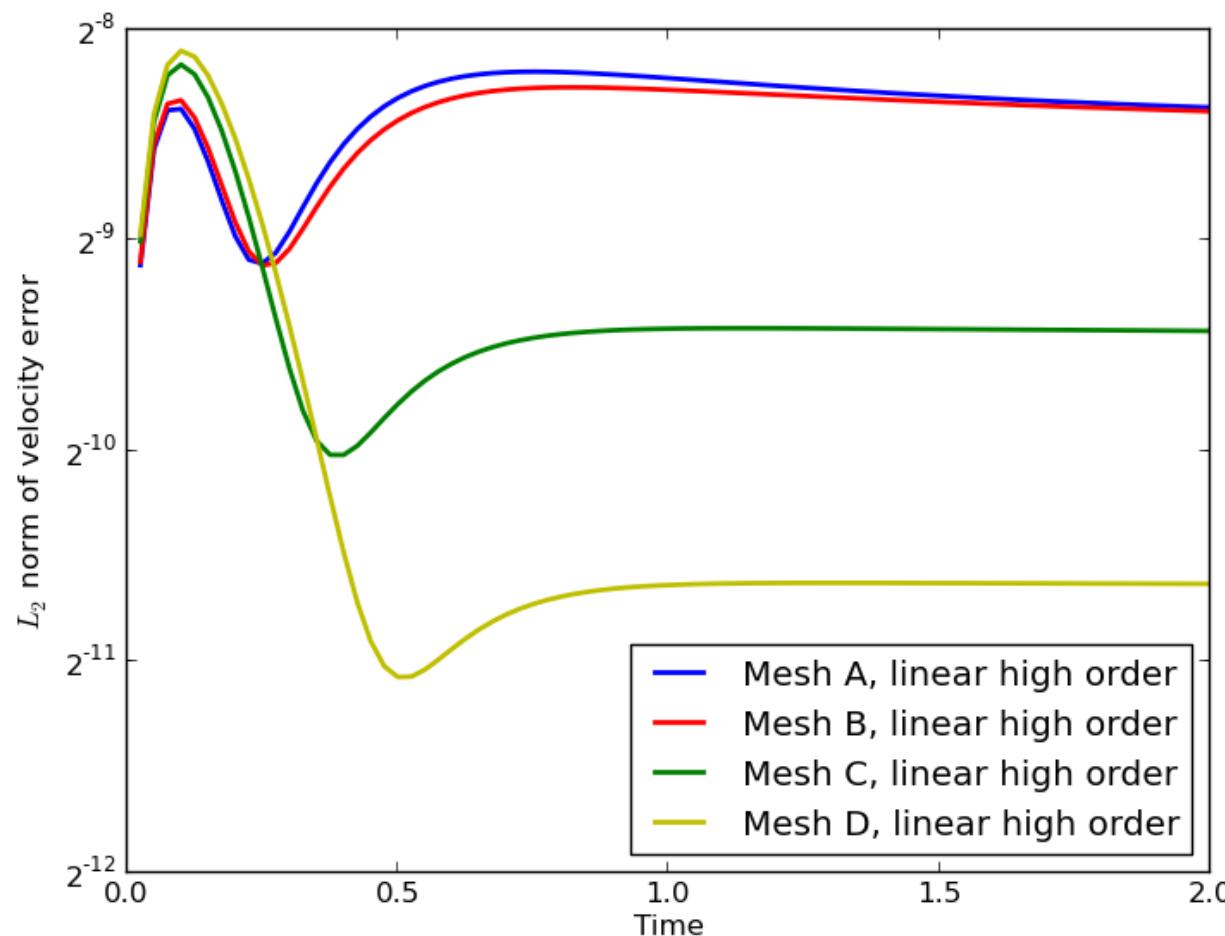
$$u(y) = -\frac{1}{2\mu} \frac{\partial p}{\partial x} (h^2 - y^2)$$



Verification of flow model



Verification of flow model



Verification of flow model

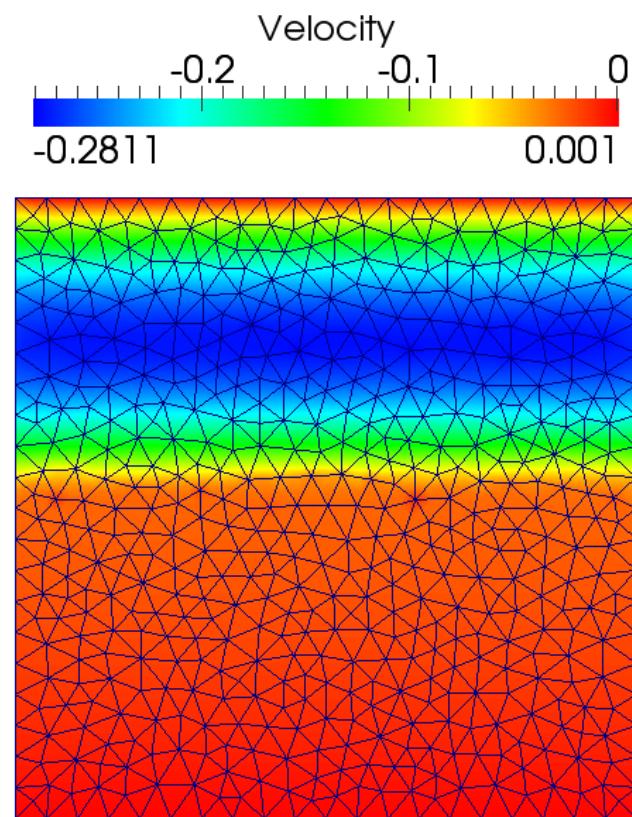
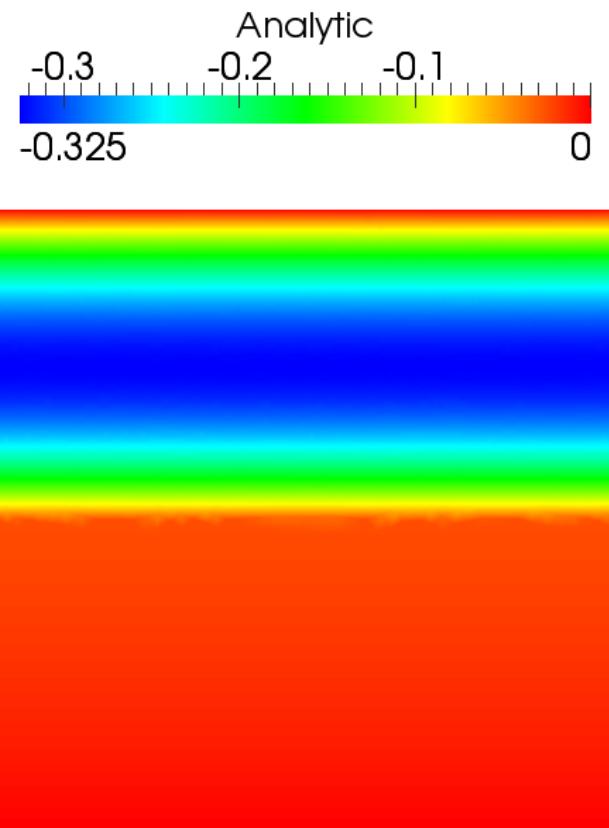
multiphase laminar channel flow

Spin up from
Pressure differential

$$c_0 = \frac{1}{2} \left[\frac{(\mu_1 - \mu_0) h_c^2 + \mu_0 h^2}{(\mu_1 - \mu_0) h_c + \mu_0 h} \right]$$

$$u(y) = -\frac{1}{2\mu_0} \frac{\partial p}{\partial x} [2c_0y - y^2]$$

$$u(y) = -\frac{1}{2\mu_1} \frac{\partial p}{\partial x} [2c_0(y-h) + h^2 - y^2]$$



Verification of flow model

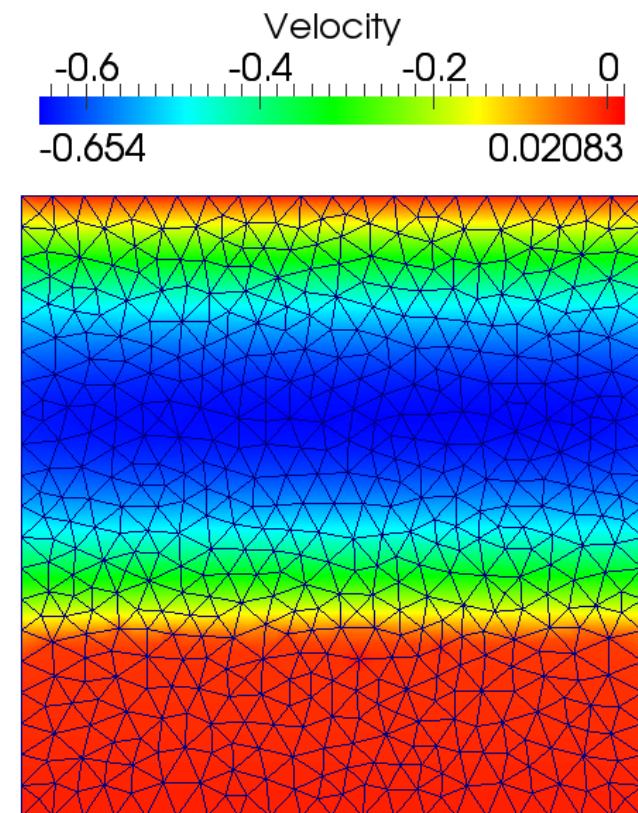
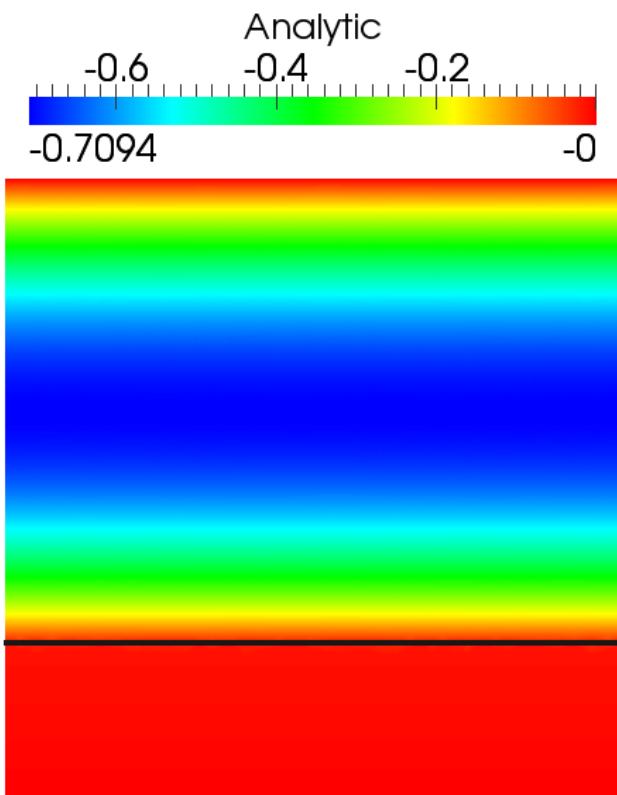
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Verification of flow model

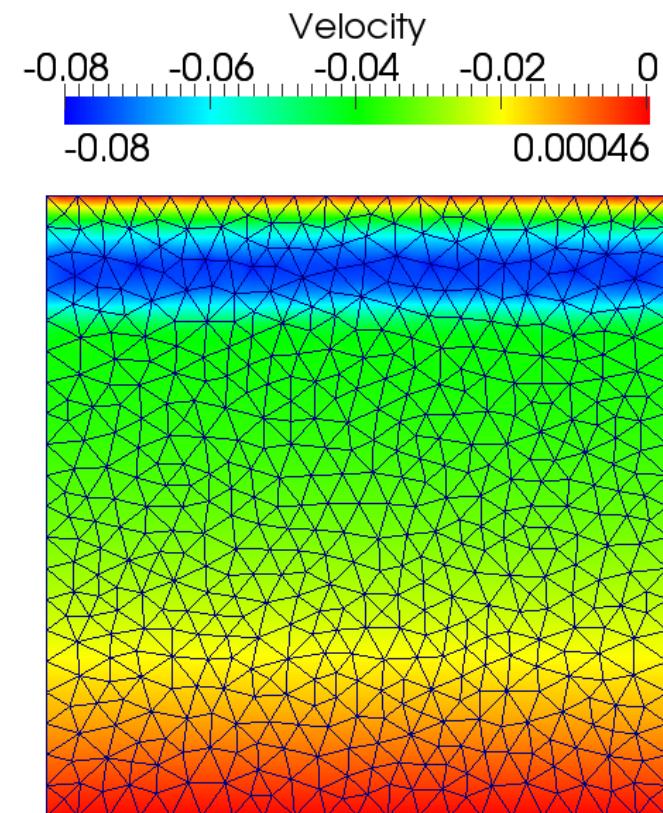
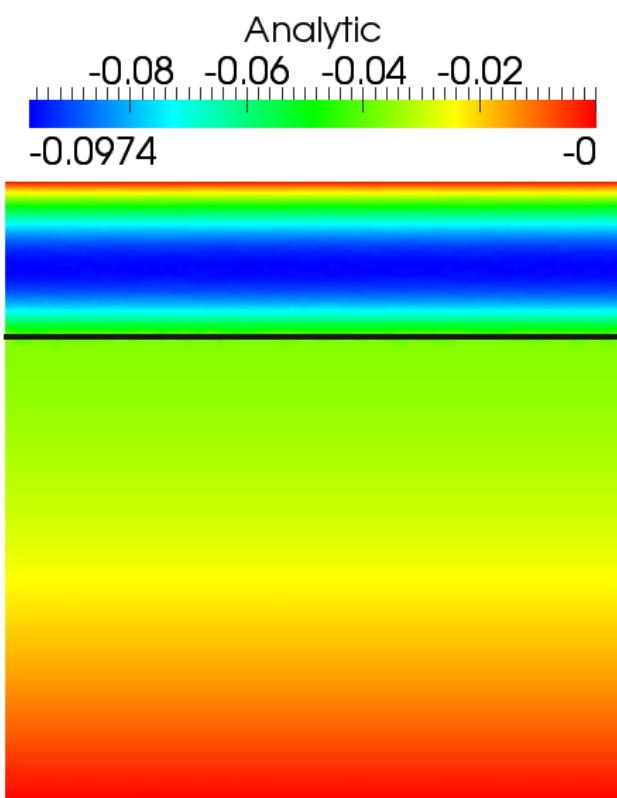
multiphase laminar channel flow

Spin up from
Pressure differential

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Verification of flow model

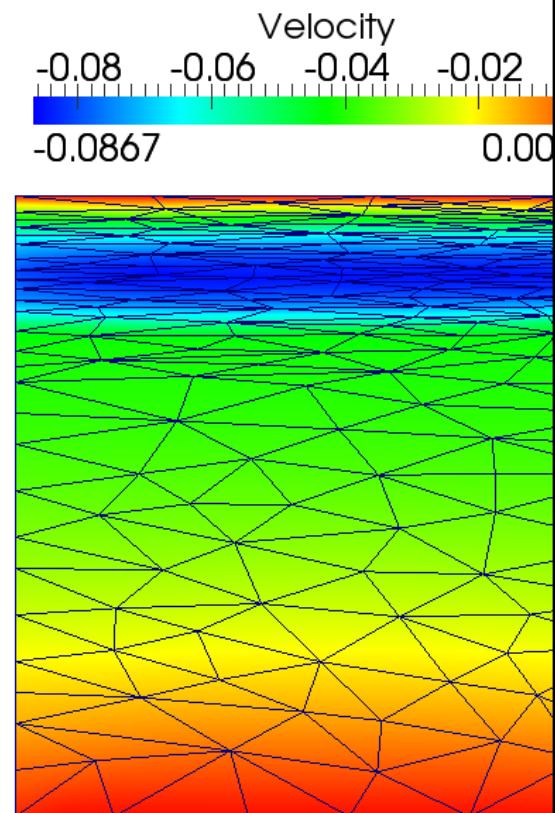
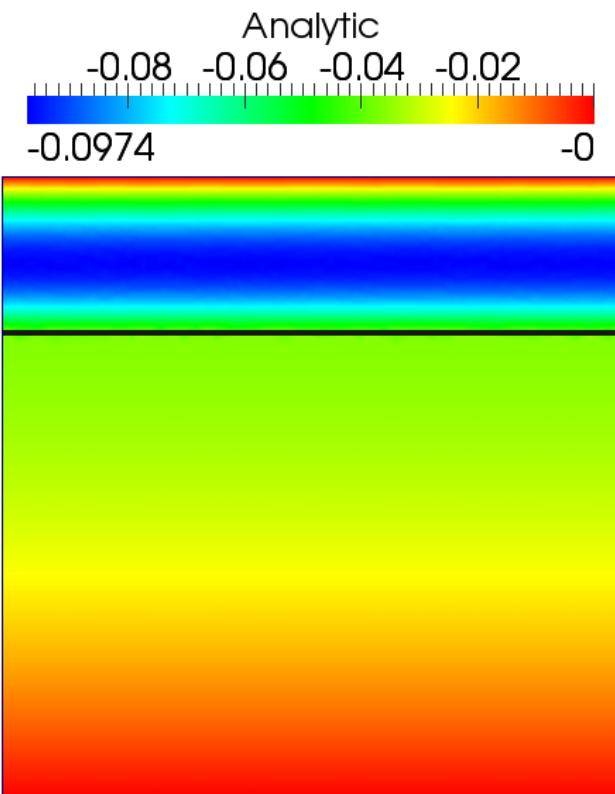
multiphase laminar channel flow

Spin up from
Pressure differential

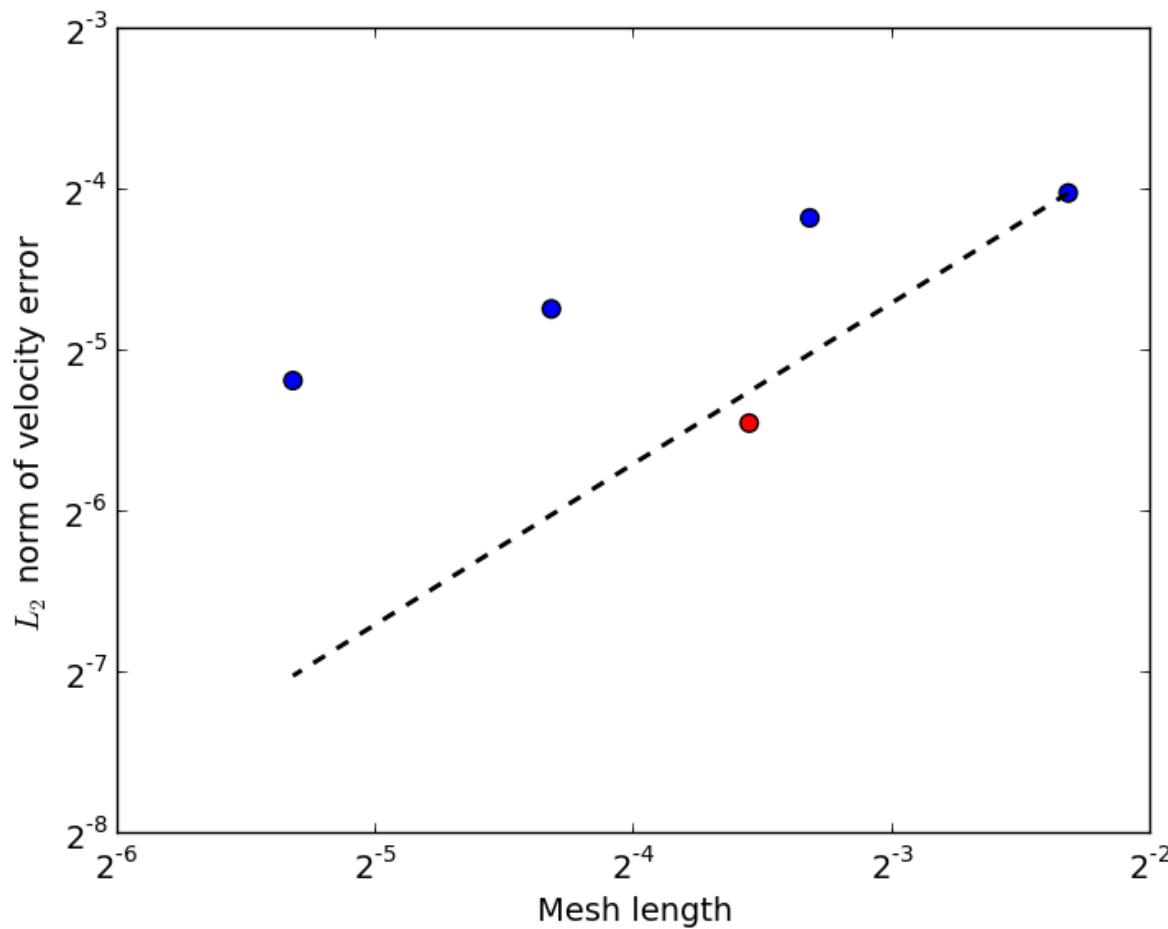
$$c_0 = \frac{1}{2} \left[\frac{(\mu_1 - \mu_0) h_c^2 + \mu_0 h^2}{(\mu_1 - \mu_0) h_c + \mu_0 h} \right]$$

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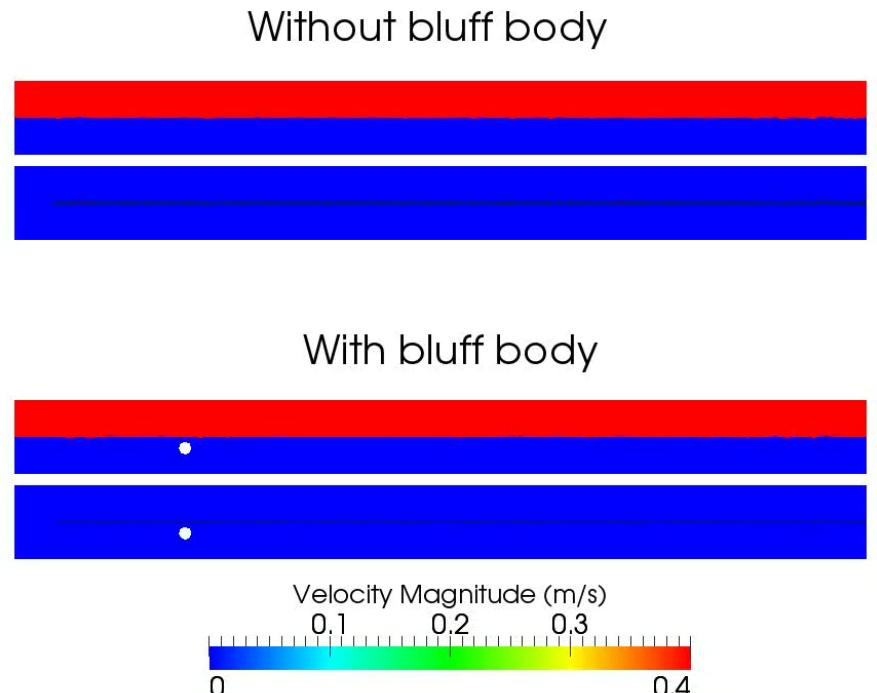


Verification of flow model



Two phase flow past a bluff body

- Combines both contribution of vortex shedding from the cylinder and interface instability
- Acts as an actuator for wave generation, wave breaking & droplet formation



Red = Exxsold140 oil
 $\rho = 830 \text{ kg.m}^{-3}$
 $\mu = 0.0055 \text{ kg.m}^{-1}\text{s}^{-1}$
 $\sigma=0.02 \text{ Nm}^{-1}$

Blue = Water
 $\rho = 1000 \text{ kg.m}^{-3}$
 $\mu = 0.001 \text{ kg.m}^{-1}\text{s}^{-1}$
 $\sigma=0.07 \text{ Nm}^{-1}$

$U_{\max} = 0.375$, velocity driven

Without body

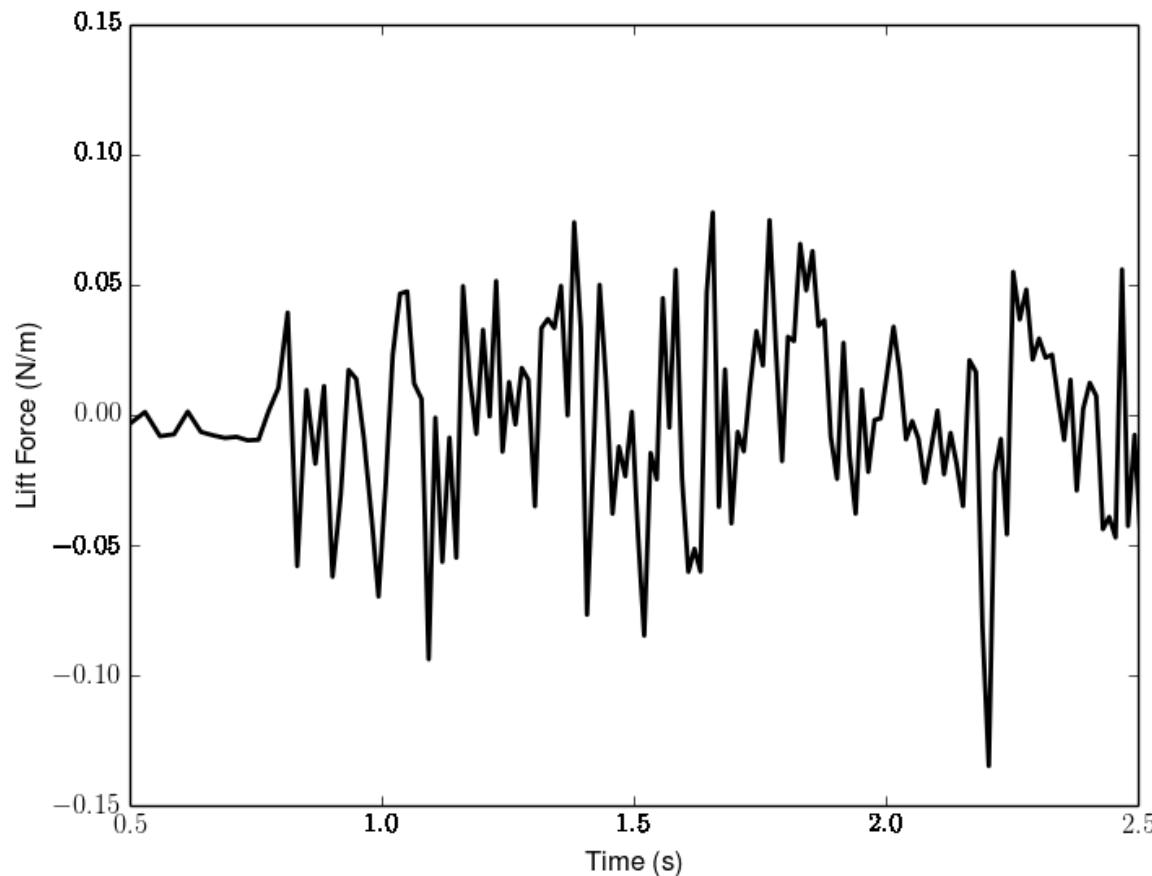


With body



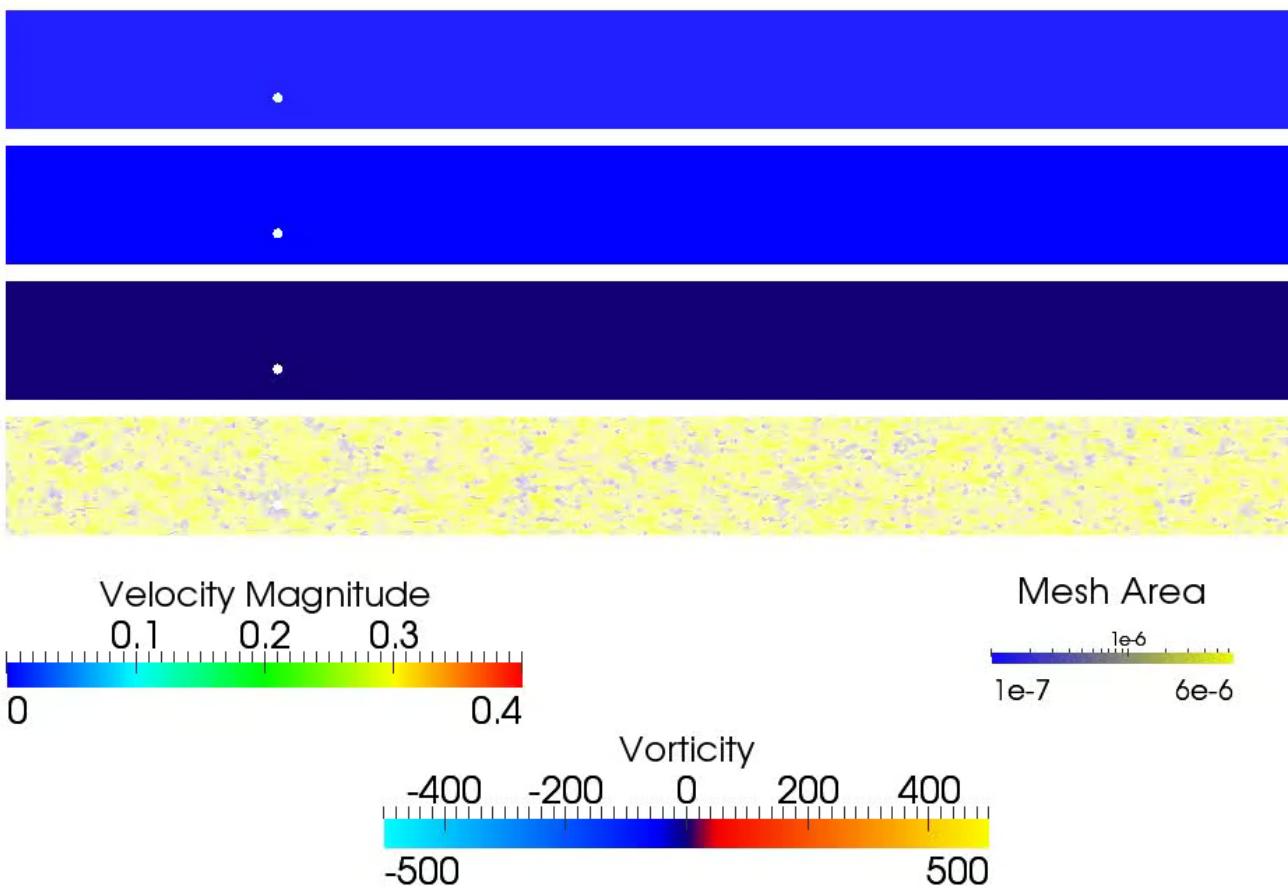
Forces on the body

Diagnostic: lift force on cylinder



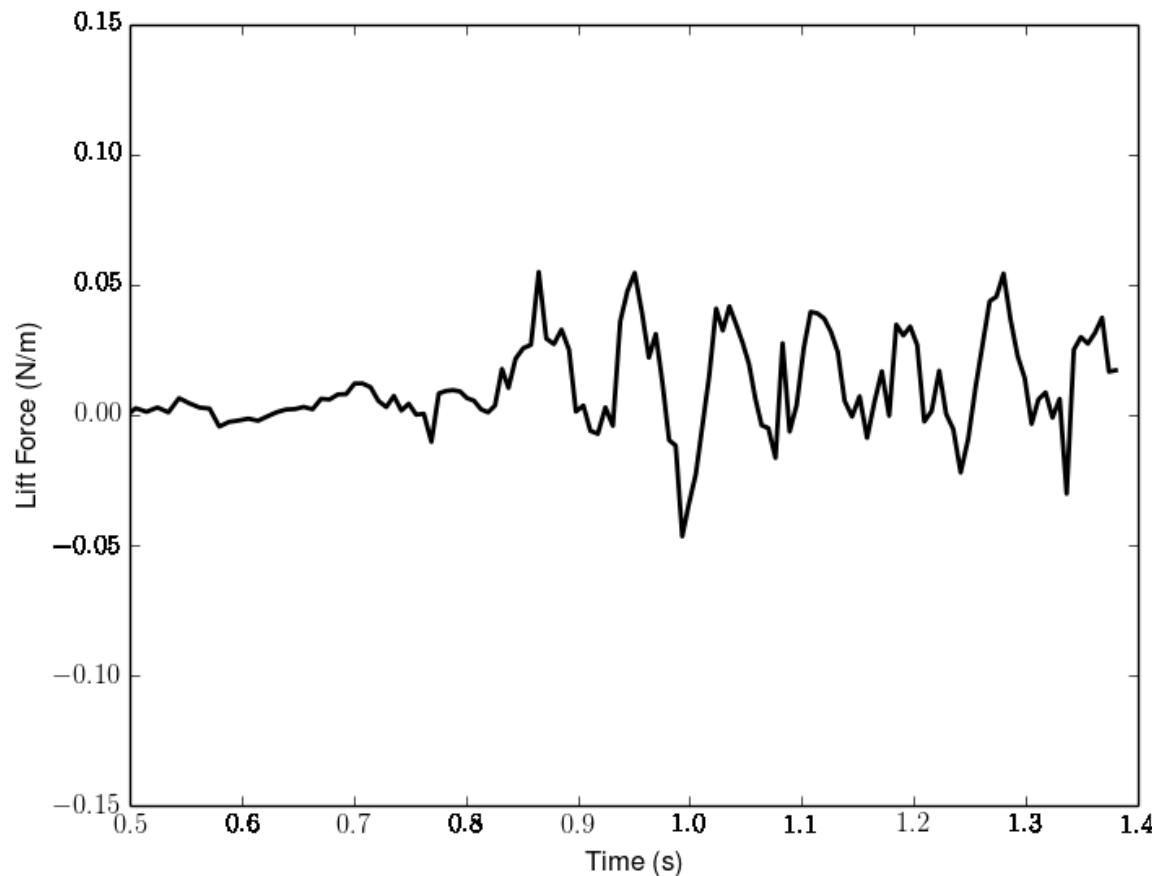


Comparison: Single Phase



Forces on the body

Diagnostic: lift force on cylinder

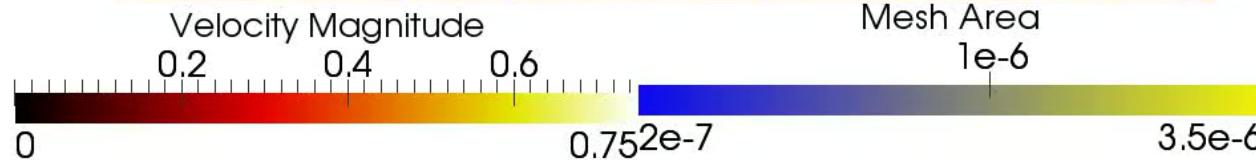
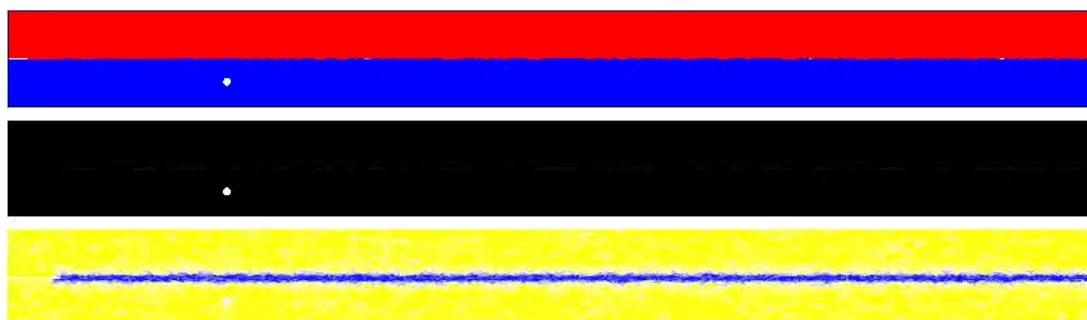


$U_{\max} = 0.75$, velocity driven

Without body

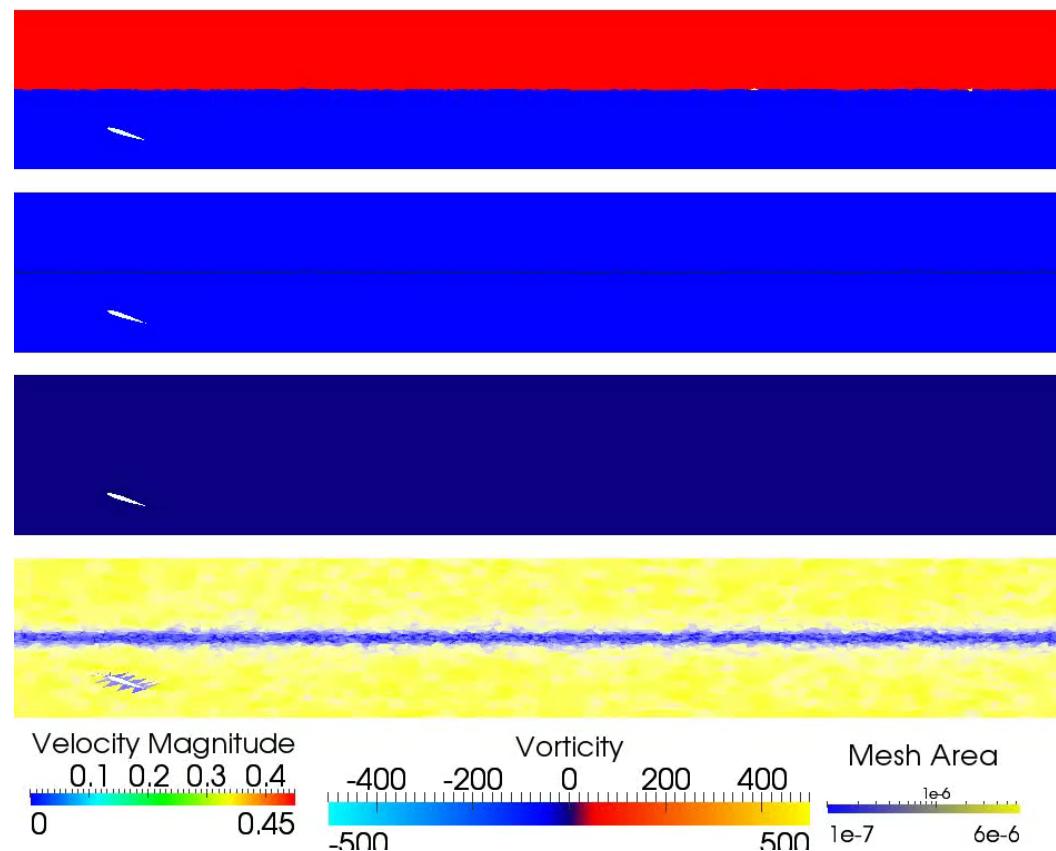
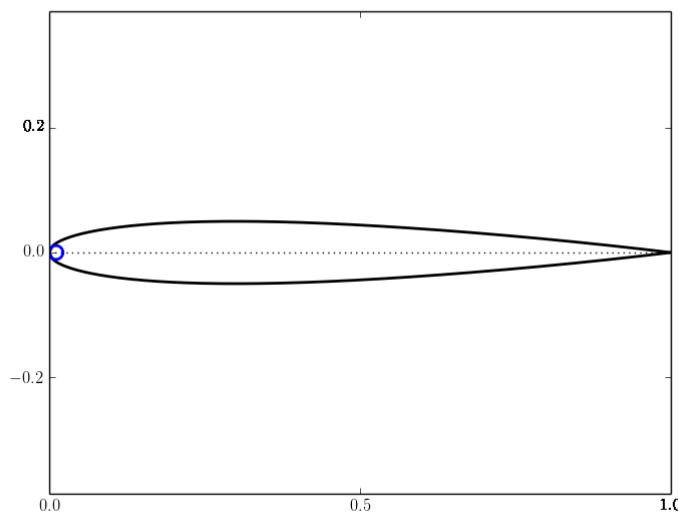


With body

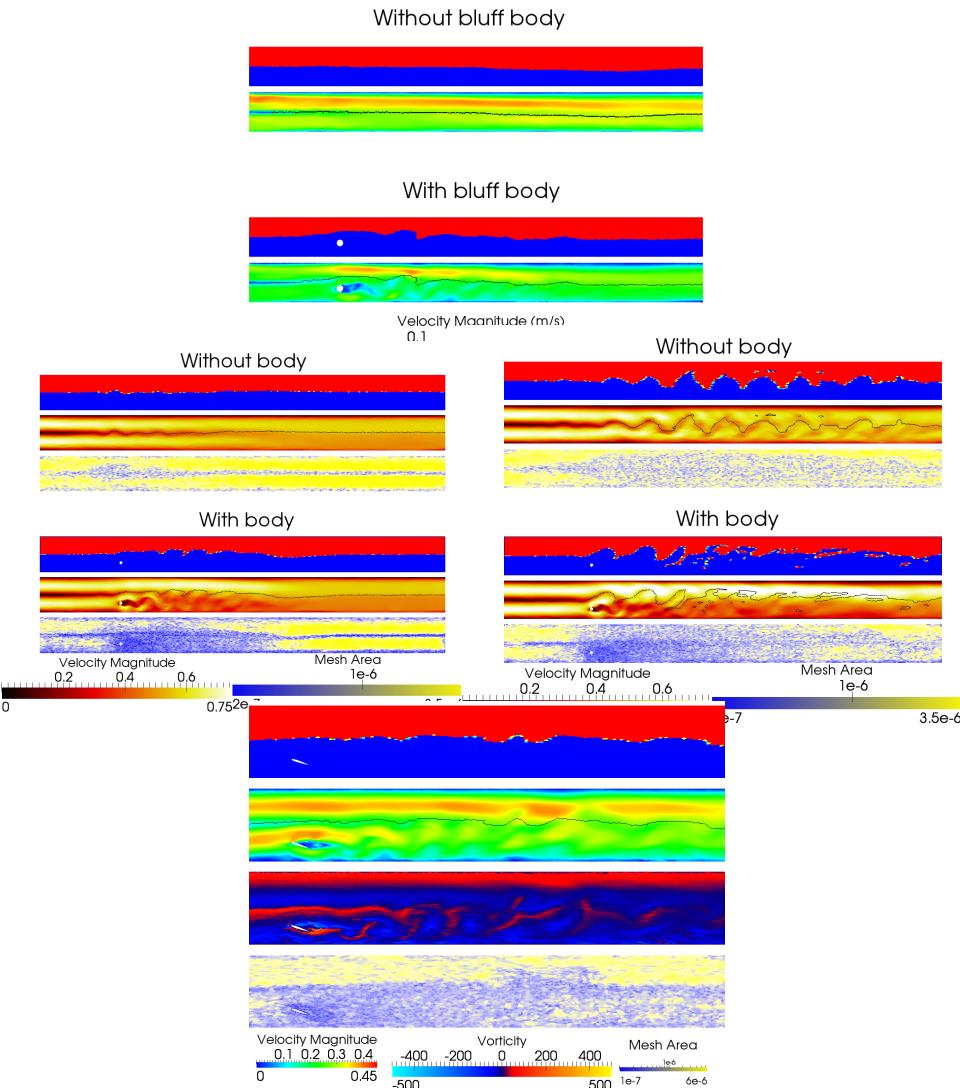


Noncylindrical bodies

- Trivial to investigate objects other than a cylinder numerically within Fluidity
- Eg. NACA modified airfoil



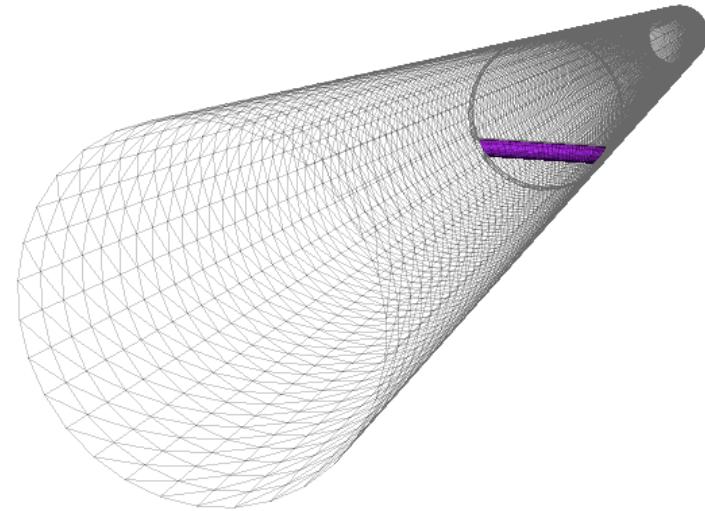
Summary



- Preliminary numerical study of two-phase oil-water interface deformation forced by a bluff body.
- In two dimensional experiments addition of a cylindrical body below a material interface is shown to variously
 - generate,
 - enhance,
 - or break interfacial waves
- depending on flow regime.
- Interaction between frequencies of KH instabilities at the interface & von Karman vortices shed from obstruction

Future work

- Full 3D modelling
 - Effects of the walls
- Investigate role of surface tension:
 - Qv talk by Z. Xie
 - Droplet formation due to forced wave breaking
- Detailed intercomparison with the experimental work of K.Park et. al





Thank you!

Any Questions?

Without body



With body

