

# **Review of Chapter 1**

## **Wave Nature of Light**

# EXAMPLE: Group and phase velocity

Consider a light traveling in a pure SiO<sub>2</sub> glass medium. If the wavelength of light is 1μm and the refractive index at this wavelength is 1.450, what is the phase velocity, group index (N<sub>g</sub>) and group velocity (V<sub>g</sub>)?

**Solution:**

The phase velocity is given by:

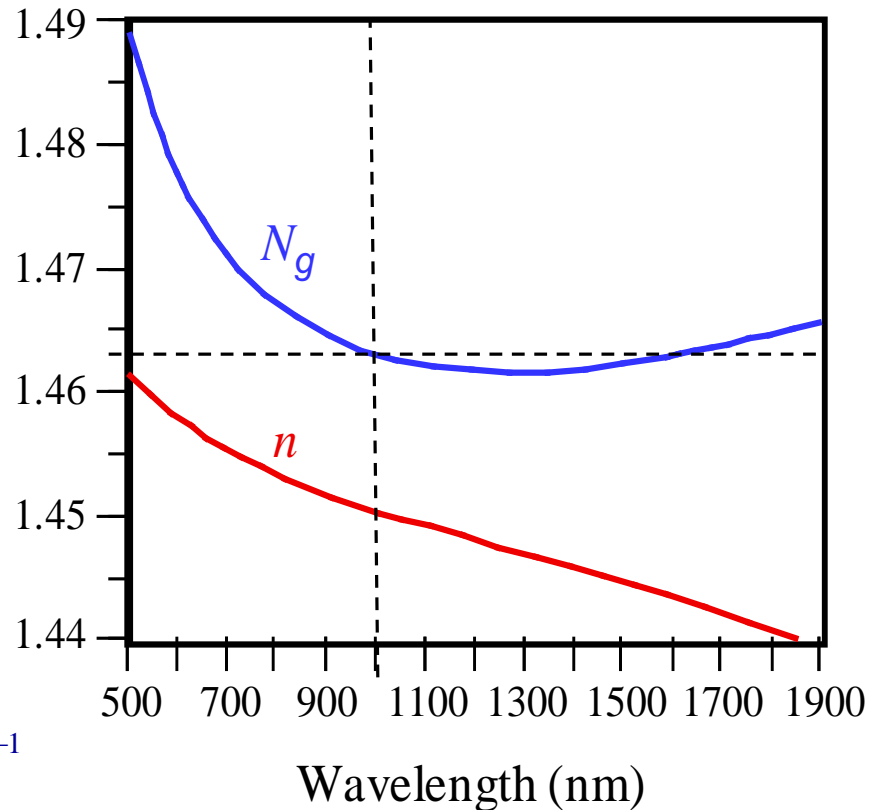
$$v = \frac{c}{n} = \frac{3 \times 10^8}{1.450} = 2.069 \times 10^8 \text{ m/s}$$

**From Fig.:**

when  $\lambda = 1\mu\text{m}$

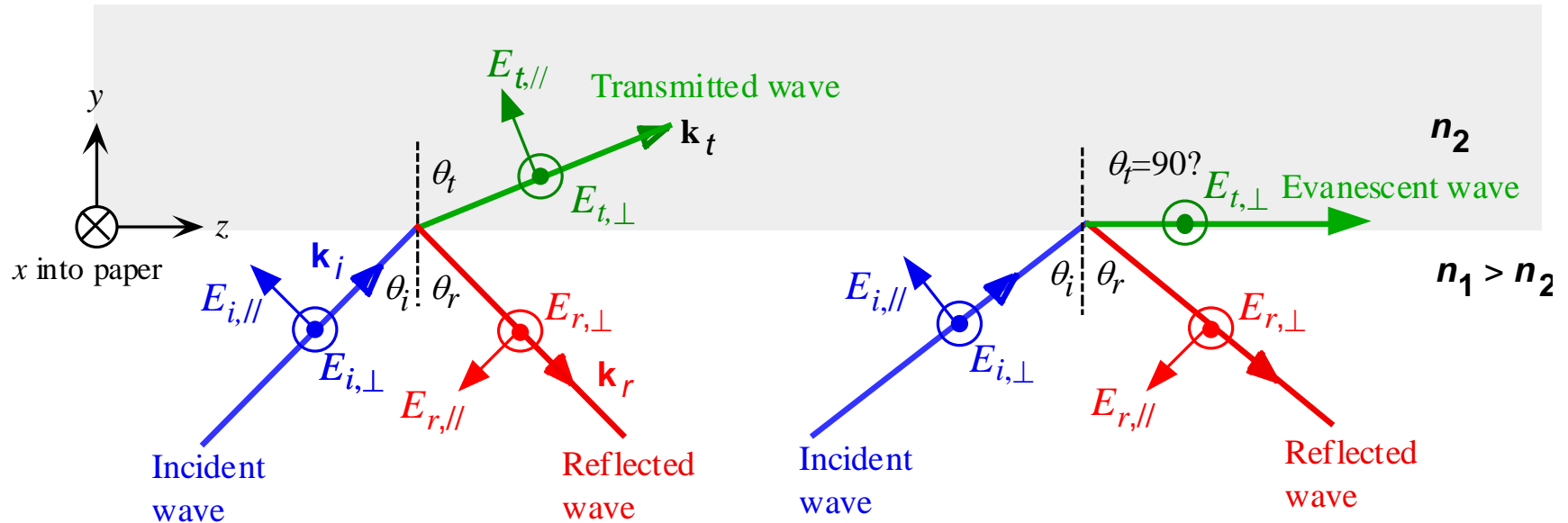
$$N_g = 1.463$$

**thus** 
$$v_g = \frac{c}{N_g} = \frac{3 \times 10^8}{1.463} = 2.051 \times 10^8 \text{ ms}^{-1}$$



Refractive index  $n$  and the group index  $N_g$  of pure SiO<sub>2</sub> (silica) glass as a function of wavelength.

# Fresnel's Equations



(a)  $\theta_i < \theta_c$  then some of the wave is transmitted into the less dense medium. Some of the wave is reflected.

(b)  $\theta_i > \theta_c$  then the incident wave suffers total internal reflection. However, there is an evanescent wave at the surface of the medium.

Light wave travelling in a more dense medium strikes a less dense medium. The plane of incidence is the plane of the paper and is perpendicular to the flat interface between the two media. The electric field is normal to the direction of propagation. It can be resolved into perpendicular ( $\perp$ ) and parallel ( $\parallel$ ) components

at normal incidence:  $\theta_i = 0$   $r_{//} = r_{\perp} = \frac{n_1 - n_2}{n_1 + n_2}$

**Brewster's angle**  
(Polarization angle)  $\tan \theta_p = \frac{n_2}{n_1}$

the phase change  
of reflected wave

$$\left\{ \begin{array}{l} \tan\left(\frac{1}{2}\phi_{\perp}\right) = \frac{\sqrt{\sin^2 \theta_i - n^2}}{\cos \theta_i} \\ \tan\left(\frac{1}{2}\phi_{//} + \frac{1}{2}\pi\right) = \frac{\sqrt{\sin^2 \theta_i - n^2}}{n^2 \cos \theta_i} \end{array} \right.$$

## EXAMPLE: Reflection at interface

Consider the reflection of light at normal incidence on a boundary between a glass medium of refractive index 1.5 and air of refractive index 1.

- (1). If light is traveling from air to glass, what is the reflection coefficient and the intensity of the reflected light with respects to that of the incident light?
- (2). If light is traveling from glass to air, what is the reflection coefficient and the intensity of the reflected light with respect to that of the incident light?

$$(1) \quad r_{//} = r_{\perp} = \frac{n_1 - n_2}{n_1 + n_2} = \frac{1 - 1.5}{1 + 1.5} = -0.2 \quad R_{//} = R_{\perp} = |r_{\perp}|^2 = 0.04$$

$$(2) \quad r_{//} = r_{\perp} = \frac{n_1 - n_2}{n_1 + n_2} = \frac{1.5 - 1}{1.5 + 1} = 0.2 \quad R_{//} = R_{\perp} = |r_{//}|^2 = 0.04$$

# **Review of Chapter 2**

## **Dielectric Waveguides and Optical Fiber**

# Single and Multimode Waveguides

**Maximum number of  
mode being allowed  
in the waveguide**

$$m \leq \frac{2V - \phi}{\pi}$$

**V-number**

$$V = \frac{2\pi a}{\lambda} \sqrt{n_1^2 - n_2^2}$$

## EXAMPLE V-Number and the number of mode

Estimate the number of modes that can be supported in a planar dielectric waveguide that is  $100\mu m$  wide and has  $n_1 = 1.490$  and  $n_2 = 1.470$  at the free-space source wavelength(  $\lambda = 1\mu m$  ) .

**Solution:**

$$m \leq \frac{2V - \phi}{\pi} = \frac{2V}{\pi} - \frac{\phi}{\pi}$$

$$V = \frac{2\pi a}{\lambda} \sqrt{n_1^2 - n_2^2} = \frac{2 \times 3.14 \times 50 \times 10^{-6}}{1 \times 10^{-6}} \sqrt{1.49^2 - 1.47^2}$$
$$= 76.44$$

$$\because \frac{\phi}{\pi} < 1 \quad \therefore m \leq \frac{2V}{\pi} = \frac{2 \times 76.44}{3.14} = 48$$

**Including  $m = 0$  :**  $\therefore M = 48 + 1 = 49$



## **V-number of step index fiber**

$$V = \frac{2\pi a}{\lambda} \sqrt{n_1^2 - n_2^2}$$

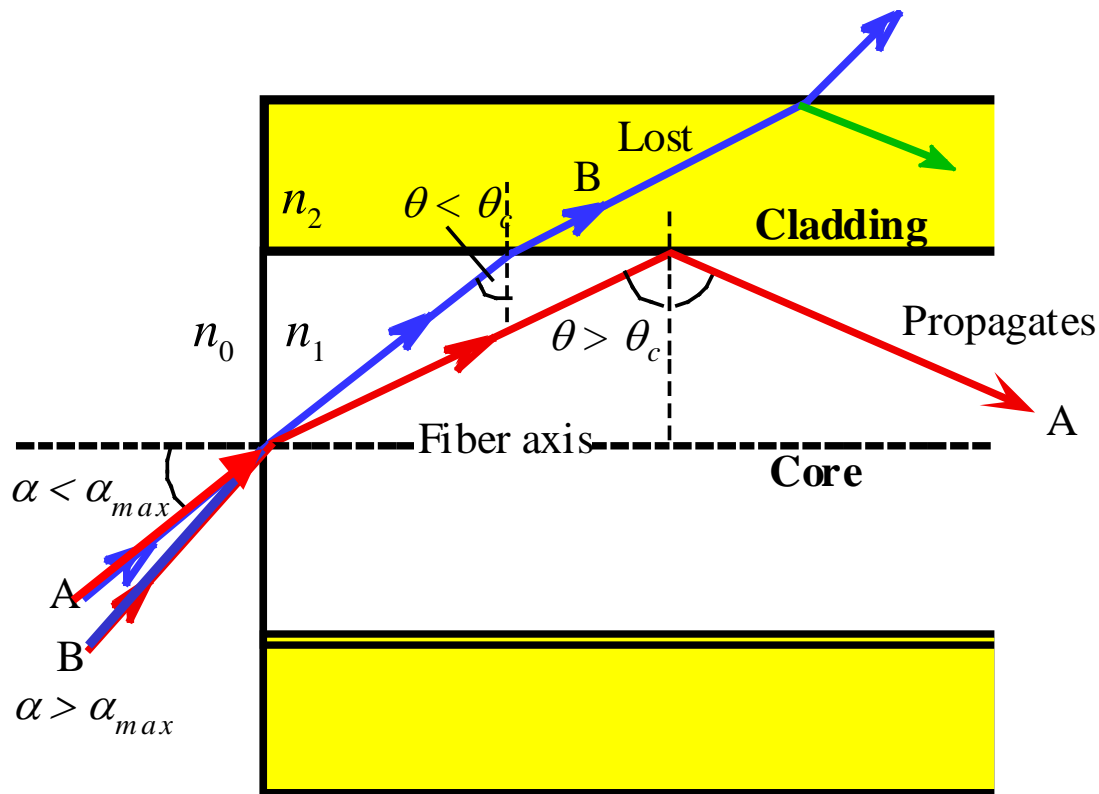
## **Cut-off wavelength of step index fiber**

$$V_{cut-off} = \frac{2\pi a}{\lambda_c} \sqrt{n_1^2 - n_2^2} = 2.045$$

## **Normalized propagation constant**

$$b = \frac{(\beta/k)^2 - n_2^2}{n_1^2 - n_2^2}$$

# NUMERICAL APERTURE



Maximum acceptance angle  $\alpha_{max}$  is that which just gives total internal reflection at the core-cladding interface, i.e. when  $\alpha = \alpha_{max}$  then  $\theta = \theta_c$ . Rays with  $\alpha > \alpha_{max}$  (e.g. ray B) become refracted and penetrate the cladding and are eventually lost.

**maximum acceptance angle**  $\alpha_{\max}$

**Snell's law:** 
$$\frac{\sin \alpha_{\max}}{\sin(90^\circ - \theta_c)} = \frac{n_1}{n_2}$$

$$\theta_c = \frac{n_2}{n_1} \quad \sin \alpha_{\max} = \frac{\sqrt{n_1^2 - n_2^2}}{n_0}$$

**Numerical aperture:** 
$$NA = \sqrt{n_1^2 - n_2^2}$$

**maximum acceptance angle:** 
$$\sin \alpha_{\max} = \frac{NA}{n_0}$$

**V-number and NA:** 
$$V = \frac{2\pi a}{\lambda} NA$$

## EXAMPLE: Multimode fiber

Consider a multimode fiber with a core diameter of  $100\mu m$ , core refractive index of 1.480, and a cladding refractive index of 1.460. Consider operating this fiber at  $\lambda = 850nm$

- (1). Calculate the V-number for the fiber.
- (2). Calculate the wavelength below which the fiber becomes multimode.
- (3). Calculate the numerical aperture.
- (4). Calculate the maximum acceptance angle

$$(1) \quad V = \frac{2\pi a}{\lambda} \sqrt{n_1^2 - n_2^2} = \frac{2 \times 3.14 \times 50 \times 10^{-6}}{850 \times 10^{-9}} \sqrt{1.48^2 - 1.46^2} =$$

$$(2) \quad \lambda < \frac{2\pi a}{2.405} \sqrt{n_1^2 - n_2^2} = \frac{2 \times 3.14 \times 50 \times 10^{-6}}{2.405} \sqrt{1.48^2 - 1.46^2} =$$

$$(3) \quad NA = \sqrt{n_1^2 - n_2^2} = \sqrt{1.48^2 - 1.46^2} = 0.2425$$

$$(4) \quad \sin \alpha_{\max} = \frac{NA}{n_0} = \frac{0.2425}{1} = 0.2425 \quad \alpha_{\max} = 14^\circ$$

## EXAMPLE: Doppler broadened linewidth

For an He-Ne laser, the Doppler broadened linewidth  $\Delta\nu_{1/2}$  of  $632.8nm$  radiation is about  $1.51GHz$ , Calculated the Doppler broadened width in the wavelength.

**Solution:**

$$\lambda = \frac{c}{\nu}$$

$$\nu = \frac{c}{\lambda} = \frac{3 \times 10^8}{632.8 \times 10^{-9}} = 4.74 \times 10^{14}$$

$$d\lambda = -\frac{c}{\nu^2} d\nu;$$

$$\frac{\Delta\lambda}{\Delta\nu} = \left| -\frac{c}{\nu^2} \right| = \frac{c}{\nu};$$

$$\Delta\lambda_{1/2} \approx \Delta\nu_{1/2} \frac{\lambda}{\nu} = 1.51 \times 10^9 \frac{632.8 \times 10^{-9}}{4.74 \times 10^{14}} =$$

## EXAMPLE: Modes in a laser

Consider an AlGaAs laser diode which has an optical cavity of length 200 microns. The peak radiation is at 870nm and the refractive index of InGaAsP is 3.7. The optical gain width is 6nm.

- (1) What is the mode number  $m$  value of the peak radiation?
- (2) What is the separation  $\delta\lambda_m$  between the modes of cavity?
- (3) How many modes are there in the cavity?

Modes in an optical cavity:  $m \frac{\lambda}{2n} = L$  ; wavelength:  $\lambda = 870 \times 10^{-9} m$

Cavity length:  $L = 200 \times 10^{-6} m$  ; index: 3.7

linewidth:  $\Delta\lambda_{1/2} = 6nm$

**Solution:**

$$(1) \quad m = \frac{2nL}{\lambda} = \frac{2 \times 3.7 \times 200 \times 10^{-6}}{870 \times 10^{-9}} = 1644 \times 10^3 = 1644$$

$$(2) \quad \delta\lambda_m = \lambda_m - \lambda_{m+1} = \frac{2nL}{m} - \frac{2nL}{m+1} = \frac{2nL}{m(m+1)} \approx \frac{2nL}{m^2} = \frac{2nL}{(2nL/\lambda)^2}$$
$$= \frac{\lambda^2}{2nL} = \frac{(870 \times 10^{-9})^2}{2 \times 3.7 \times 200 \times 10^{-6}} = 0.547 nm$$

$$(3) \quad Modes = \frac{\Delta\lambda_{1/2}}{\delta\lambda_m} = \frac{6nm}{0.547nm} = 10.97 \quad \text{So, there is 10 mode in the cavity}$$

## EXAMPLE: laser output wavelength variations

Given that the refractive index  $n$  of GsAs has a temperature dependence  $dn/dT = 1.5 \times 10^{-4} K^{-1}$  estimate the change in the emitted wavelength 870nm per degree change in the temperature between mode hops.

$$m \frac{\lambda}{2n} = L$$

$$\lambda = \frac{2nL}{m}$$

$$d\lambda = \frac{2L}{m} dn$$

$$\frac{d\lambda}{dT} = \frac{2L}{m} \frac{dn}{dT} = \frac{\lambda}{n} \frac{dn}{dT} = \frac{870nm}{3.7} (1.5 \times 10^{-4}) = 0.035nmK^{-1}$$