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Dynamic Aeroelastic Scaling of the CRM Wing via Multidisciplinary Optimization

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WCSMO12



Braunschweig, Germany
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Introduction - Similarity and Optimization



Reference aircraft

Introduction - Similarity and Optimization



Reference aircraft



Scaled model

Introduction - Similarity and Optimization



Reference aircraft



Scaled model

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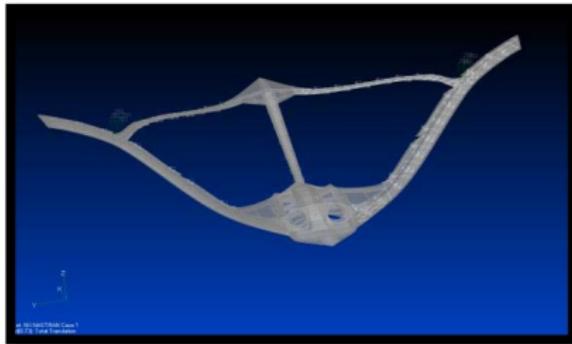


Reference aircraft

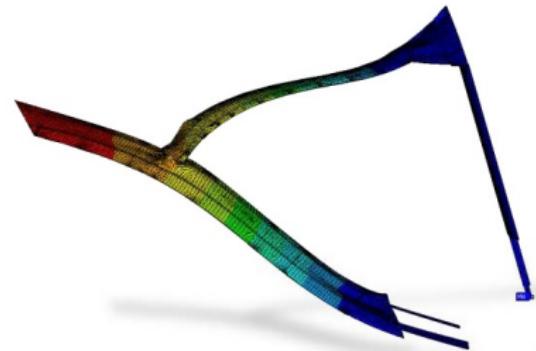


Scaled model

Introduction - Dynamic Aeroelastic Similarity



Reference aircraft mode shape*



Optimized scale demonstrator mode shape*



*[Richards et al., AIAA/ATIO Conference, 2010]

- 1 Tools
- 2 Dynamic Aeroelastic Scaling
- 3 CRM wing modal optimization
- 4 Aerodynamic Flutter Optimization
- 5 Conclusion
- 6 Perspectives

1 Tools

2 Dynamic Aeroelastic Scaling

3 CRM wing modal optimization

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6 Perspectives

- Nastran 95*: Normal Modes and Flutter Analysis

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- Panair/a502[†]: Static aerodynamics

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- OpenMDAO[‡] Framework



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- Panair/a502[†]: Static aerodynamics
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- Optimizer: SLSQP (Gradient-based, from Scipy library)

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 *[github.com/nasa/NASTRAN-95]

 †[pdas.com/panair.html]

 ‡[Gray et al., AIAA/ISSMO, 2014]

1 Tools

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3 CRM wing modal optimization

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Dynamic Aeroelastic Scaling

Aeroelastic equations of motion:

$$[\mathbf{M}]\{\ddot{x}\} + [\mathbf{K}]\{x\} = [\mathbf{A}_k]\{x\} + [\mathbf{A}_c]\{\dot{x}\} + [\mathbf{A}_m]\{\ddot{x}\} + [\mathbf{M}]\{a_g\}$$

Dynamic Aeroelastic Scaling

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In modal coordinates ($\{x\} = [\Phi]\{\eta\}$):

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$$\begin{aligned} [\Phi]^T [\mathbf{M}] [\Phi] \{\ddot{\eta}\} + [\Phi]^T [\mathbf{K}] [\Phi] \{\eta\} &= [\Phi]^T [\mathbf{A}_k] [\Phi] \{\eta\} + \\ &[\Phi]^T [\mathbf{A}_c] [\Phi] \{\dot{\eta}\} + [\Phi]^T [\mathbf{A}_m] [\Phi] \{\ddot{\eta}\} + \frac{1}{b} [\Phi]^T [\mathbf{M}] \{a_g\} \end{aligned}$$

Dynamic Aeroelastic Scaling

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[Ricciardi et al., Journal of Aircraft, 2014]

Dynamic Aeroelastic Scaling

Adimensionalize with reference quantities:

$$\langle \bar{\mathbf{m}} \rangle \{ \ddot{\eta}^* \} + \langle \bar{\mathbf{m}} \bar{\omega}^2 \rangle \{ \eta \} = \underbrace{\frac{V^2}{b^2 \omega_1^2}}_{1/\kappa_1^2} \underbrace{\frac{gb}{V^2}}_{1/Fr^2} \langle \bar{\mathbf{m}} \rangle [\Phi]^{-1} \{ \bar{a}_g \}$$
$$+ \underbrace{\frac{1}{2} \frac{\rho S b}{m_1} \frac{V^2}{\omega_1^2 b^2}}_{\mu_1} \left([\bar{\mathbf{a}}_k] \{ \eta \} + \underbrace{\frac{\omega_1 b}{V}}_{\kappa_1} [\bar{\mathbf{a}}_c] \{ \dot{\eta}^* \} + \underbrace{\frac{\omega_1^2 b^2}{V^2}}_{\kappa_1^2} [\bar{\mathbf{a}}_m] \{ \ddot{\eta}^* \} \right)$$

Traditional Dynamic Aeroelastic Scaling

Nondimensional aeroelastic equations of motion (harmonic solution):

Reference aircraft: \mathbf{r}

Scaled model: \mathbf{m}

$$\langle \bar{\mathbf{m}}_{\mathbf{r}} \rangle \{ \dot{\eta}^{\star\star} \} + \langle \bar{\mathbf{m}}_{\mathbf{r}} \bar{\omega}_{\mathbf{r}}^2 \rangle \{ \eta \} = \frac{1}{2} \frac{\mu_{1r}}{\kappa_{1r}^2} [\bar{\mathbf{a}}_{\mathbf{hr}}(\mathbf{X}_{\mathbf{ar}}, \kappa, M_{\mathbf{r}})] \{ \eta \}$$

$$\langle \bar{\mathbf{m}}_{\mathbf{m}} \rangle \{ \dot{\eta}^{\star\star} \} + \langle \bar{\mathbf{m}}_{\mathbf{m}} \bar{\omega}_{\mathbf{m}}^2 \rangle \{ \eta \} = \frac{1}{2} \frac{\mu_{1m}}{\kappa_{1m}^2} [\bar{\mathbf{a}}_{\mathbf{hm}}(\mathbf{X}_{\mathbf{am}}, \kappa, M_{\mathbf{m}})] \{ \eta \}$$

Traditional Dynamic Aeroelastic Scaling

Nondimensional aeroelastic equations of motion (harmonic solution):

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$$\underbrace{\langle \bar{m}_r \rangle \{ \dot{\eta}^* \} + \langle \bar{m}_r \bar{\omega}_r^2 \rangle \{ \eta \}}_{\text{Match } [\Phi], \langle \bar{\omega} \rangle, \langle \bar{m} \rangle \\ (\text{from the problem}) \\ K - \omega^2 [M] \{ \phi \} = 0 \\ \text{through optimization}} = \frac{1}{2} \frac{\mu_{1r}}{\kappa_{1r}^2} \underbrace{[\bar{a}_{hr}(X_{ar}, \kappa, M_r)]}_{\text{Equal if same aerodynamic shape and flow similarity}} \{ \eta \}$$

Match $[\Phi]$, $\langle \bar{\omega} \rangle$, $\langle \bar{m} \rangle$
(from the problem
 $K - \omega^2 [M] \{ \phi \} = 0$)
through optimization

Equal if same aerodynamic
shape and flow similarity

$$\underbrace{\langle \bar{m}_m \rangle \{ \dot{\eta}^* \} + \langle \bar{m}_m \bar{\omega}_m^2 \rangle \{ \eta \}}_{\text{Match } [\Phi], \langle \bar{\omega} \rangle, \langle \bar{m} \rangle \\ (\text{from the problem}) \\ K - \omega^2 [M] \{ \phi \} = 0 \\ \text{through optimization}} = \frac{1}{2} \frac{\mu_{1m}}{\kappa_{1m}^2} \underbrace{[\bar{a}_{hm}(X_{am}, \kappa, M_m)]}_{\text{Equal if same aerodynamic shape and flow similarity}} \{ \eta \}$$

1 Tools

2 Dynamic Aeroelastic Scaling

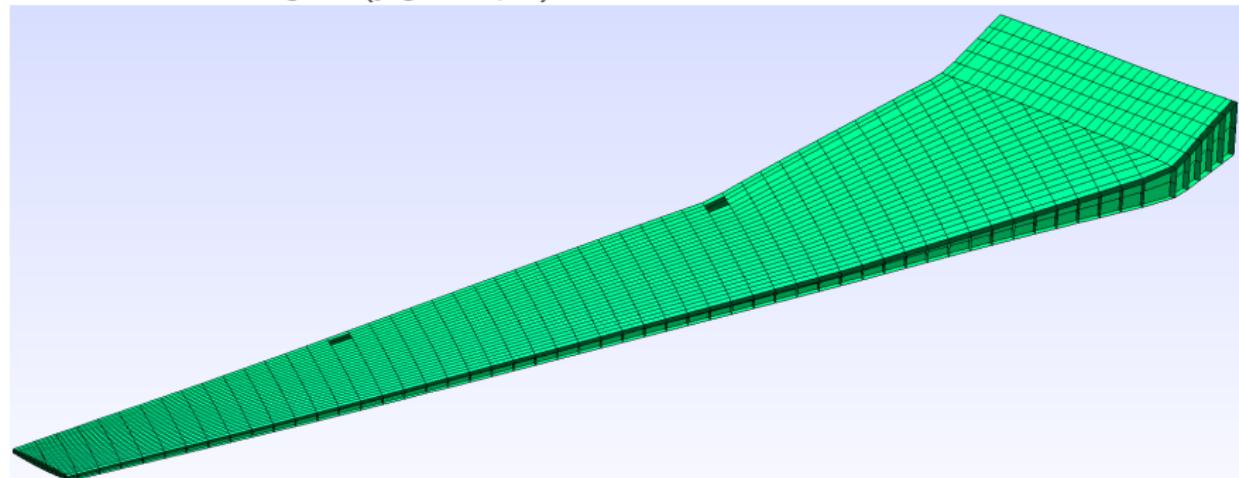
3 CRM wing modal optimization

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Reference Design* (jig shape): For all elements $t_r = 8.89mm$



X
Y
Z

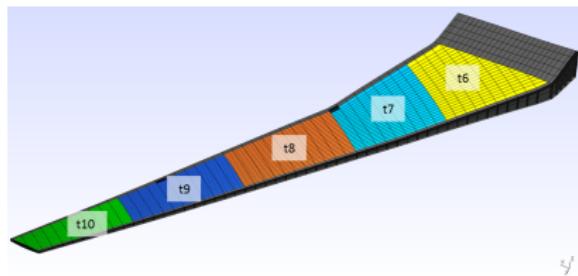
Model provided by T. Achard and C. Blondeau*

[ Achard et al., AIAA/ISSMO, 2016]

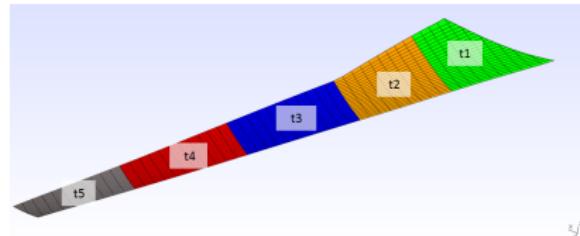
CRM modal optimization: Problem definition

Hypothesis: Flow similarity assumed

Objective Function		Dimension	Bounds
Mode shape difference minimization	$\min(N - \text{trace}(\text{MAC}([\Phi_r], [\Phi_m])))$	\mathbb{R}	
Design Variables			
Skin thicknesses vector	$[t]$	\mathbb{R}^{10}	$[0.0889, 26.67]$ mm
Constraints			
Reduced frequency matching	$\ \omega_r - \omega_m\ = 0$	\mathbb{R}	
Mass matching	$M_r - M_m = 0$	\mathbb{R}	
Generalized masses matching	$\ m_r - m_m\ = 0$	\mathbb{R}	



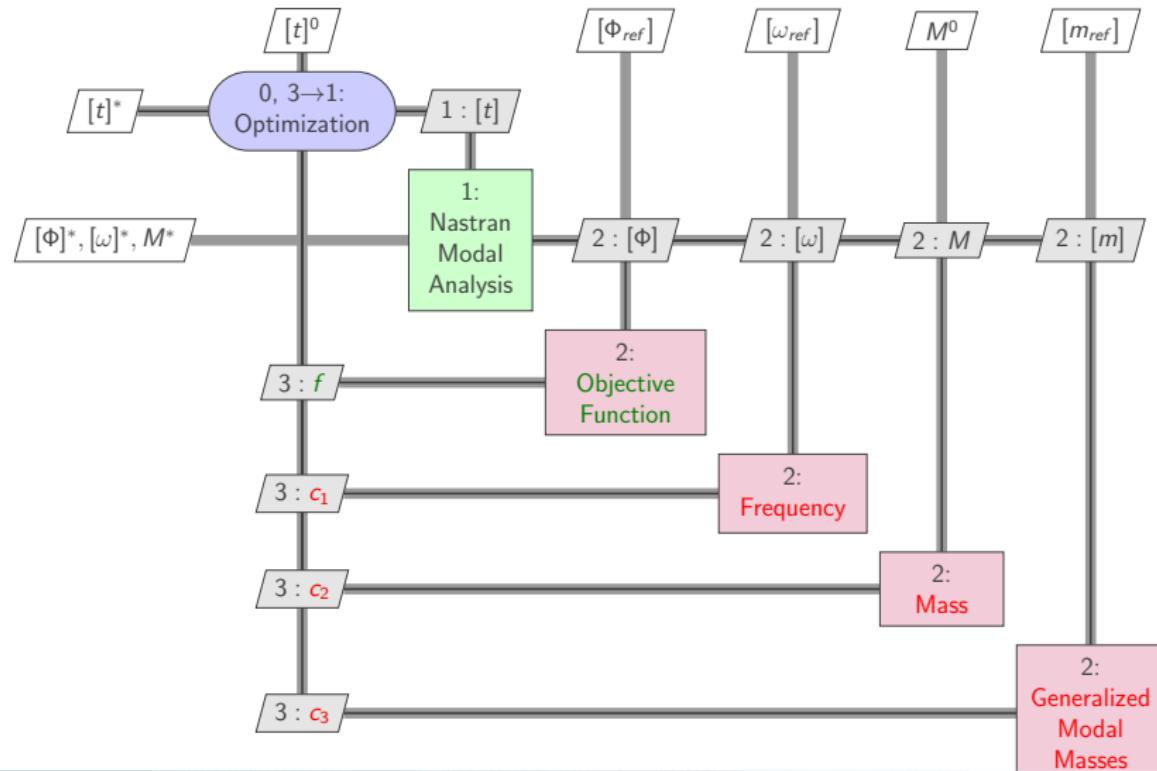
→ Upper skin panels



Lower skin panels ←

Traditional Modal Optimization

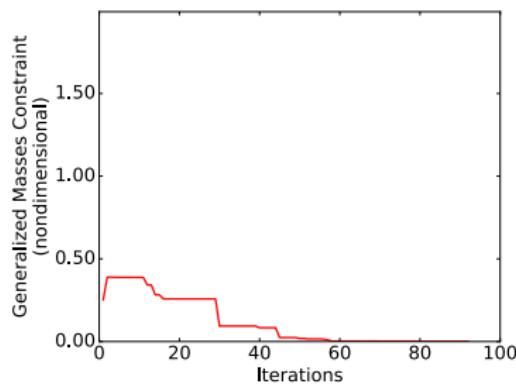
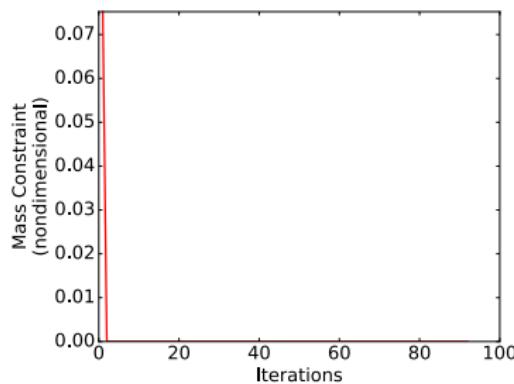
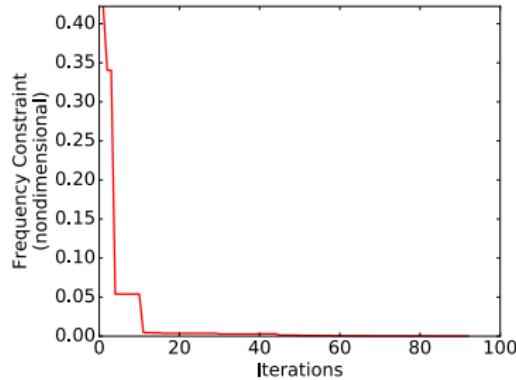
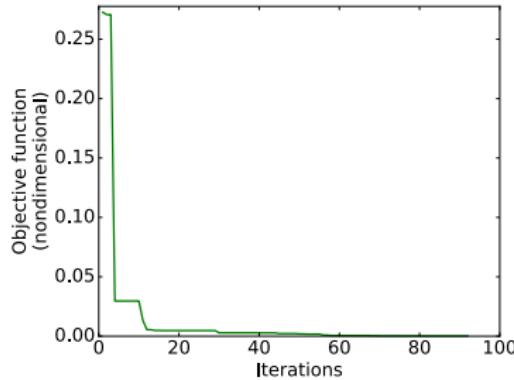
Hypothesis: Flow similarity assumed



CRM Modal Optimization: Results

Best Found Point vs Iteration

Criterion: Point with best objective function AND sum of constraints



1 Tools

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What if the flow is not similar?

Reference aircraft: r

Scaled model: m

$$\langle \bar{\mathbf{m}}_r \rangle \{ \dot{\eta}^* \} + \langle \bar{\mathbf{m}}_r \bar{\omega}_r^2 \rangle \{ \eta \} = \frac{1}{2} \frac{\mu_{1r}}{\kappa_{1r}^2} [\bar{\mathbf{a}}_{hr}(X_{ar}, \kappa, M_r)] \{ \eta \}$$

$$\langle \bar{\mathbf{m}}_m \rangle \{ \dot{\eta}^* \} + \langle \bar{\mathbf{m}}_m \bar{\omega}_m^2 \rangle \{ \eta \} = \frac{1}{2} \frac{\mu_{1m}}{\kappa_{1m}^2} [\bar{\mathbf{a}}_{hm}(X_{am}, \kappa, M_m)] \{ \eta \}$$

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$$\underbrace{\langle \bar{m}_r \rangle \{ \hat{\eta}^* \} + \langle \bar{m}_r \bar{\omega}_r^2 \rangle \{ \eta \}}_{\text{Reference aircraft equations}} = \frac{1}{2} \frac{\mu_{1r}}{\kappa_{1r}^2} \underbrace{[\bar{a}_{hr}(X_{ar}, \kappa, M_r)]}_{\text{Reference aircraft aerodynamics}} \{ \eta \}$$

matched through modal optimization

$$\underbrace{\langle \bar{m}_m \rangle \{ \hat{\eta}^* \} + \langle \bar{m}_m \bar{\omega}_m^2 \rangle \{ \eta \}}_{\text{Scaled model equations}} = \frac{1}{2} \frac{\mu_{1m}}{\kappa_{1m}^2} \underbrace{[\bar{a}_{hm}(X_{am}, \kappa, M_m)]}_{?} \{ \eta \}$$

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$$\underbrace{\langle \bar{m}_r \rangle \{ \hat{\eta}^* \} + \langle \bar{m}_r \bar{\omega}_r^2 \rangle \{ \eta \}}_{\text{matched through modal optimization}} = \frac{1}{2} \frac{\mu_{1r}}{\kappa_{1r}^2} \underbrace{[\bar{a}_{hr}(X_{ar}, \kappa, M_r)]}_{\text{optimize w.r.t. } X_{ar}} \{ \eta \}$$

matched through modal optimization

$$\underbrace{\langle \bar{m}_m \rangle \{ \hat{\eta}^* \} + \langle \bar{m}_m \bar{\omega}_m^2 \rangle \{ \eta \}}_{\text{optimize w.r.t. } X_{am}} = \frac{1}{2} \frac{\mu_{1m}}{\kappa_{1m}^2} \underbrace{[\bar{a}_{hm}(X_{am}, \kappa, M_m)]}_{\text{optimize w.r.t. } X_{am}} \{ \eta \}$$

What if the flow is not similar? Aerodynamic Optimization

- Reference aircraft: r
- Scale model: m

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- Reference aircraft: r
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- Mach number: M

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Objective function:

What if the flow is not similar? Aerodynamic Optimization

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$$f = \sum_i (\|[\bar{a}_{hr}(X_{ar}, \kappa_i, M_r)] - [\bar{a}_{hm}(X_{am}, \kappa_i, M_m)]\|)$$

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Design variables:

What if the flow is not similar? Aerodynamic Optimization

- Reference aircraft: r
- Scale model: m
- Reduced frequency: κ
- Mach number: M

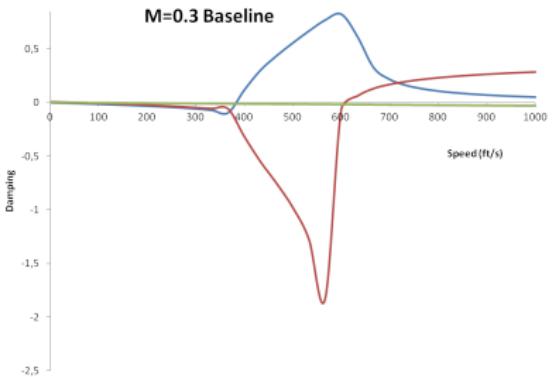
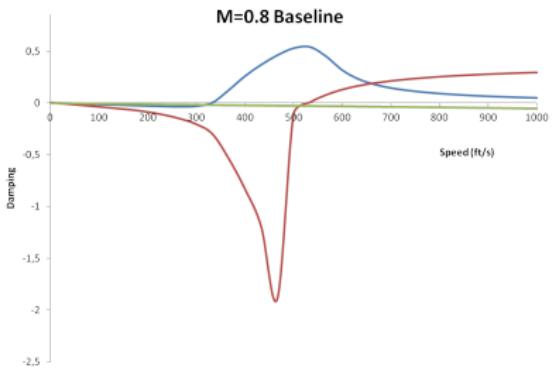
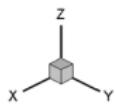
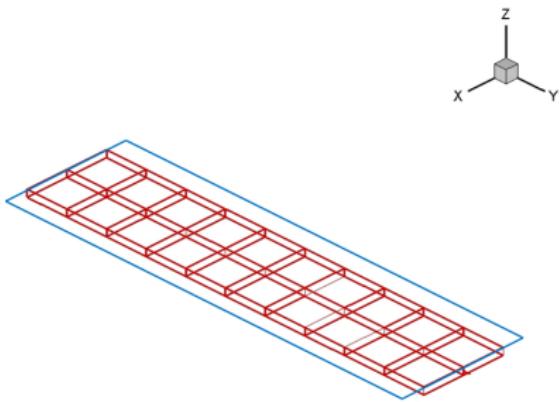
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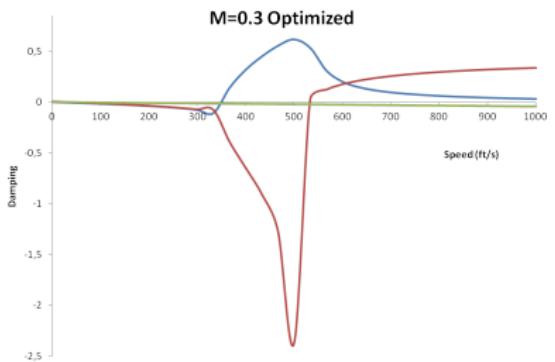
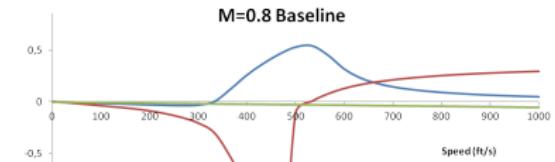
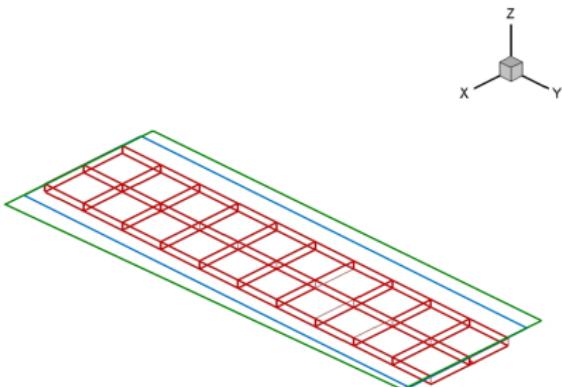
Design variables:

- X_{am} : Parameters defining the wing planform

Aerodynamic Optimization: Goland Wing Test Case



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6 Perspectives

Conclusion

- Review of the traditional dynamic aeroelastic scaling approach

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- Review of the traditional dynamic aeroelastic scaling approach
- Modal optimization for similarity

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- Modal optimization for similarity
- Application to the CRM test case

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- Modal optimization for similarity
- Application to the CRM test case
- Importance of no flow similarity
- Wing planform optimization for flutter similarity

1 Tools

2 Dynamic Aeroelastic Scaling

3 CRM wing modal optimization

4 Aerodynamic Flutter Optimization

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6 Perspectives

- Perform flutter-based wing planform optimization with the CRM model

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- From the optimized planform, optimize wing twist distribution and structure properties to match static deflection

This work has been supported by the EU project 658570 - NextGen Airliners funded by Marie Skłodowska-Curie actions (MSCA).

Thanks for your attention!

Questions?