University of Toronto Faculty of Applied Science and Engineering Final Examination, December 2001 Fourth Year - Programs 3, 4manu, 5ms

MIE 440F: Mechanical Design
Examiner: L. Shu
Exam Type: A
(No data other than information printed on examination paper permitted.)

- You may remove the last 2 pages (pictures) of the exam from the staple to help you work faster.
- Answer short-answer questions in 12 or fewer words per section. Verbosity will be penalized.

This is a 2.5-hour exam.

You may use a calculator.

Answer all parts of all questions.

To obtain the maximum credit on numerical problems, show all steps in your computations.

Point values are shown in [] for entire problems and parts of problems to help you allocate your time.

Clearly indicate your answers in the spaces provided on exam sheet.

If a question is ambiguous, state the necessary assumptions.

Student Last Name	
Student First Name	
Student ID number	

Problem	Points Possible	Points Obtained
I. Design for Assembly	90	
II. Design for Injection Molding	60	
III. Design for Stamping	40	
IV. Design for End-of-Life	40	
V. Product Liability	20	
Total	250	_

INSTRUCTIONS

You are studying for your final exams when you decide to take a break and head down to the local AYOF (Assemble Your Own Furniture) store. As you weave through the showroom maize, you trip over a stray unit called "Rulla," which you decide is your destiny to buy. You feel compelled to perform a design analysis on Rulla, because you love to apply what you learn in class to real life.

I. Design-for-Assembly [90]

As with all AYOF furniture, the Rulla requires assembly. Remove the last page from the back of the exam that contains the assembly diagrams. Calculate the assembly time of the Rulla by completing the table below.

- All dimensions in mm are given for smallest box/cylinder that surrounds part. All parts weigh < 10 lb.
- All parts over 300mm require two hands to handle.
- 1. Snap polypropylene anchors (30 x 10 x 5) into non-circular holes in one half of polypropylene box
- 2. Assemble other half (430 x 400 x 210) of polypropylene box
- 3. Assemble polypropylene shelf (400 x 400 x 15), whose top and bottom surfaces are different, into tight-fitting groove in box
- 4. Note: Perform in order described, not shown in diagram
 - a. Assemble by pressing steel caster-stems (7.5 dia x 50) into steel caster base
 - b. Assemble by pressing polypropylene casters (50 x 50 x 40) into steel stems in steel caster base
- 5. Punch holes on top of box
- 6. Assemble caster-base assembly (450 x 400 x 150) to box using screws (5 dia x 12)

Do NOT include final inversion of assembly so that wheels are on bottom.

Part/	Alpha	Beta	Handle	Handle	Insert	Insert	Handle	# times	Total	Additional
Opera	-		Code	Time	Code	Time	+ Insert	рег-	Time	Assumptions
-tion		[1			Time	formed	1	(none should be required)
1										
2			<u> </u>			<u>. </u>		<u> </u>		
3			 -					<u> </u>		
4a										
4b						 -				
5								<u> </u>		
6										
	 							<u> </u>		
Totals										

What is the minimum number of parts for this product that satisfy DFA criteria for separate parts?

Sketch/describe each of these parts.

II. Design for Injection Molding [60]

1. To injection mold one of the two identical box halves, sketch the most cost-effective mold closure direction relative to the part below [2].

2. Calculate the ABSOLUTE tooling cost to injection mold one of the two identical box halves using the most cost-effective mold closure direction. Use only details apparent from the assembly instructions and diagram. Assume standard finish and tolerances. Also complete table on next page for die detail. [42]

Injection Molding and Die Casting

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(a) Relative Die Construction Cost

Basic Shape: L =	B =; H =; => Box/Fint	L/H > 4?
Basic Complexity:	1st Digit =; 2nd Digit = => C _b =	
Subsidiary Comp:	3rd Digit =; 4th Digit = => C_s =	
T_a/R_a :	Sth Digit =; 6th Digit => C_ =	
Total Relative Die Con	nstruction Cost, $C_{dc} = C_b C_s C_t = $	

(b) Relative Die Material Cost:

$$L_{m} = \frac{1}{100}$$
; $B_{m} = \frac{1}{100}$; thus, $C = \frac{1}{100}$.

 $M_{ws} = \{0.006CH_{m}^{4}\}^{1/3} = \frac{1}{100}$
 $M_{wf} = 0.04L_{m}^{4/3} = \frac{1}{100}$
 $M_{a} = (2M_{ws} + L_{m})(2M_{ws} + B_{m}) = \frac{1}{100}$

$$M_1 = (H_m + 2M_w) =$$

Thus,
$$C_{dm}^-$$
 and $C_{d}^{=0.8C_{de}^+0.2C_{dm}^-}$

Absolute tooling cost:

Feat	ure	Number of Features	Penalty per Features	Penalty	SMALL PARTS (1, < 250 mm) Total Penalty (10 =) Low cavity detail
Holes	Circular	(n)	2n		10 < Total Penalty <20 -> Moderate cavity detail 20 < Total Penalty <40 -> High cavity detail Total Penalty >40 -> Very high cavity detail
Or	Rectangular		4n		MEDIUM PARTS (250 < L < 480 mm)
Depressions	lrregular		7n		Total Penalty <15 -> Low cavity data? 15 < Total Panalty <30 -> Moderate cavity data;
Bosses	Solid (8)		n		30 < Total Penaky <60° => High cavity detail Total Penally >60° => Very high cavity deta
DUSSES	Hollo w (8)		3n		LANCE DARKE LA . AM.
	ral ribs and/or rib clusters (6)		3n		LARGE PARTS { L > 480 mm} Total Penalty < 20 => Luw cavity detail
Side	Simple (9)		2.Sn		20 CTotal Penalty C40 => Moderate cavity detail 40 CTotal Penalty C90 => High cavity datail
Shutoffs	Complex (9)		4.5n		Total Penalty > 90 => Very high cavity detail
Let	tering (10)		n		1 in = 25.4 mm; 180 mm = 3.34 in)
		·	Total Penalty		

3. Why do you suppose the box and shelf are molded as 3 separate parts? [2]

4. Draw the most cost effective mold closure direction if the box and shelf were molded as a single part. [2]

5. If you look at the actual product, the box-half parts are hollow. Name the three components of cost for any manufactured part. State whether injection molding the box halves as hollow instead of solid will increase or decrease that component of cost, and why. [12]

	Cost component	Increase/ Decrease	Why
1			
2			
3			

Design for Stamping. [40] III.

If you wanted to mount Rulla to the wall, instead of using casters, two mounting brackets as shown on next last page of exam (remove) are used. Calculate the relative die construction cost to produce the bracket.

Feature	Number of Features (n)	Opposite Directions? (Y/N)	Penalty
Standard Hole		n n	
Non-standard Hote		2n 2n	
Coin		3n 3n	
Slandard Emboss		(n+1) n	
Non-standard Emboss		2(n+1) 2n	
Extruded Hole		2(n+1) 2n	_
Lance Form		3(n+1) 3n	
Curl		3(n+1) 3n	
Curl		3(n+1) 3n	
Hem		4(n·1) 4n	
Semi-Perl		(n+1) n	
Tab		3(n+1) 3n	
Lettering		2(n+1) 2n	
		Total Penalty	

Small Parts (L< 100 mm) Total Psealty of 4 -> Low Die Detail Cotal Penatty ≪ 8 → Medium Die Detail Total Panalty > 8 -> High Die Ostail

Medium Parts (100 mm < L << 200 mm) Total Penalty 4 6 *> Low Die Detail 4 Total Penalty 412=> Medium Die Detail Total Penalty >12=> High Die Detail

Large Parts (L > 200 mm) Total Penalty <10=> Low Die Detail
10 < Total Penalty <17=> Medium Die Detail Total Penalty >17=> High Die Detail

Relative Die Construction Cost

Peripheral Complexity:
$$L_{out} = \frac{1}{1200}$$
; $L_S = L_{out} / 2 (L_{ul} + L_{uw}) = \frac{1}{1200}$

Shear Complexity:

1st Digit = ____; 2nd Digit = ____ =>
$$C_{b1}$$
 = ____; N_{a1} =. ____

Wipe Form Complexity:

7th Digit=___;
$$F_{mc}$$
=___; F_{mb} =___; F_{mf} =___

Effect of sheet thickness:

8th Digit = ____;
$$F_t = ___; F_{dm} = ____$$

Basic Complexity,
$$C_b = C_{b1}F_{mc} + C_{b2}F_{mb} + C_{b3}F_{mf}$$

IV. Design for End-of-life [40]

Calculate the time required to disassemble Rulla for recycling based on information given in the assembly problem. By using the assembly data tables, we are assuming that disassembly will be related to assembly, e.g., a particular disassembly step is simply the reverse of the corresponding assembly step, i.e., the time it takes to untighten a screw is the same as it takes to tighten it.

1.	Will all the assembly steps in Problem I be reversed to disassemble the product for recycling?	Generally,
	why or why not? [3]	

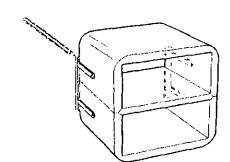
2.	Generally, for a give	en assembly step	, are the insertion	code and time ider	ntical for the correspo	onding
	disassembly time?	Why or why not	? [3]			

3. Generally, would the Alpha and Beta for disassembly be the same as for assembly? If so, why? If not, how would you determine Alpha and Beta? [3]

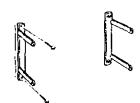
Description of Operation	Alpha	Beta	Handle	Handle	Insert	Insert	Handle	# times	Total
	{		Code	Time	Code	Time	+ Insert	per-	Time
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- V. Product Liability [20] circle choice partial credit may be awarded for less-clueless choices
 In a post-exam senioritis (a burnout phenomenon commonly observed where fourth-year students are referred to as seniors) stupor, you use the Rulla in a manner for which it is clearly not intended, and you injure yourself.
 While you contemplate suing Rulla's manufacturer, you review the relevant concepts and cases.
- 1. Most likely, your case would be based on:
 - a. tort
 - b. strict liability
 - c. common law
 - d. b and c
- 2. Using as precedence the Lambert vs. Lastoplex Chemicals Co, Ltd. et al case (1971, Supreme Court of Canada), involving a mechanical engineer and some lacquer sealer,
 - a. Your engineering license will be revoked because of your ill-advised actions on the Rulla
 - b. Rulla's manufacturer would not be found at fault, because you as an engineer, should have known better
 - c. All of the above
 - d. None of the above
- 3. Tort
 - i. is a fruity dessert
 - ii. involves default on a contract
 - iii. is intended to punish a wrong-doer
 - iv. is intended to compensate victims
 - v. requires demonstration of negligence
 - a) ii and iii
 - b) iii and iv
 - c) iii, iv and v
 - d) iv and v
 - e) None of the above combinations
- 4. Strict liability means
 - i. A strict and objective standard must be used to determine whether a manufacturer is negligent
 - ii. A manufacturer does not have to be negligent to be liable
 - iii. The damages incurred to a consumer must be severe
 - iv. The engineer is found so negligent that the manufacturer is released from liability
 - v. Manufacturers may be found liable when consumers injure themselves using product in manner not intended
 - a) i and iii
 - b) i and iv
 - c) ii and v
 - d) ii. jii and v
 - c) i, iii, iv
- 5. Common law means
 - a. Laws are based on the results of previous cases
 - b. Laws should be simple enough that the common person can understand them
 - c. Commoners should be have the right to a jury of their peers, i.e., other commoners
 - d. Engineers are not common and therefore an engineer suffering from misuse of a product releases the manufacturer from liability
 - e. Placing warning labels on dangerous products releases manufacturers from liability because this is just common sense.

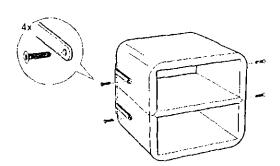
Use of mounting brackets for Rulla, now renamed Hänga



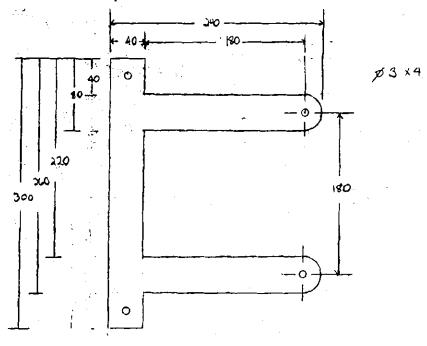




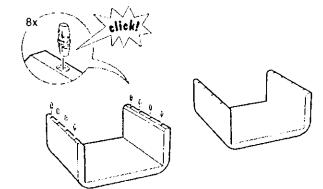
3.

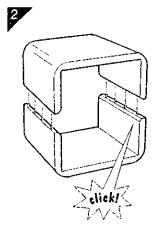


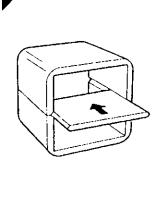
Assume that the positions of 2 holes are critical. Material is medium stainless, sheet thickness = 1.5mm

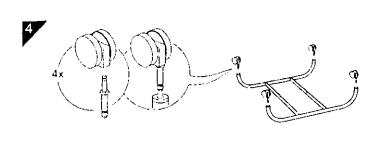


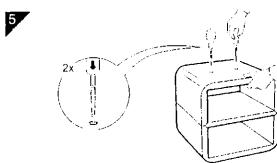


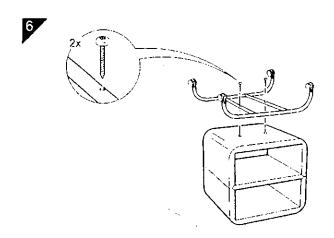












Completed Assembly:



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Other processes

Other processes

Other processes

chemical processes (e.g. adhesine busding.

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non-mechanical lastening processes (pards) already in place but not secured immediately after insertion)

metallurgical processes

additional material

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not easy to align or position during assembly

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Figure 3.15 Classification, coding and database for part features affecting manual handling time (in seconds). (Copyright Boothroyd Dewhurst, Inc., reproduced with permission.)

and fastening (in seconds). (Copyright Boothroyd Dewhurst, Inc., reproduced with per-Figure 3.16 Classification, coding and database for part features affecting insertion ASSEMULY mission.)

25.4 mm; 100 mm = 3.94 m

Flat Parts 7	DARLO GOUDIEU	. ~		F	Humb	250 :	nn (4)	25 An	Hueb	er of	18 Bnm	Hu	eber	0 mm
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			,_	0	1	2	3	•	5	_6_	7	Θ	9	10
	Parts whose peripheral height from a planar dividing sufface	Part in one hatf(3)	0	1.69			2.15	//		/		/		1/
Parts Without F Internal Undercuts	is constant (2)	Part not in one half(3)	1	1.19	1.37	1.52	1 65/ 2 30	1.61	1.09	1.99/	2.13/	2.09	2.32/	2.5%
R S	Parts whose peripheral height from a Dividing Surface is not constant - parts with a non-planar Dividing Surf	Planar or -	2	12	1.59	100	1.60 2.44	1.81	2.04	2.19/	2.33	2.39	2.58	2.83
	Parts whose DMLY Dividing Surface(2) planar, or parts whose peripheral he from a planar dividing surface is con-	ight	3	2.33	2.57	2.71	2.85/	2.75	2.99	3.13	3.27	3 17	3 49	3.65
I r or the G s n Part	Parts whose peripheral height from a Dividing Surface is not constant - parts with a non-planar Dividing Surf	OT -	4	2.99	3.27	3.36/	3.50 9.26	3.52	3.75/	3.83	4.09	۰.99	4 28	4.59
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	Parts whose peripheral height from a Dividing Surface is not constant - c parts with a non-planar Dividing Surf	or -	6	\$.37	\$.69	5.79	5.89 5.89	5.99	6.13	6.29	8.27	6.43	5.67	6.93

Figure 11.1 Classification System for Basic Tool Complexity, Cb Notes (1)-(5) are found in Appendix 11A.

Feat	ure	Number of Features (n)	Ponalty per Cealures	Penalty	SMALL PARTS (L < 250 mm) Total Penalty < (10 => 10m cover detail
Holes	Circular		2n		10 C Total Penalty (20 => Moderato cavily detail 20 C Total Penalty (40 => High cavity detail Total Penalty >40 => Very high cavily detail
or Depressions	Rectangular	 	<u>4n</u>		MEDIUM PARTS (250 CL .C 480 mm)
Depressions	Irregular		7 n		Total Penalty ((15 -> Low cavity dotail 15 (Total Penalty ((30 -> Moderato cavity detail
Basses	Solid (9)		n		30 cTotal Penalty (60 => High cavity defail Intal Penalty >60 => Very high cavity detail
50,,,,	Hollow (8)		3n		TARGE BARYS (1) AND A
	ral ribs and/or rib_clusters:@		3n		Total Penalty (C20 -) Low cavity detail
Side	Simple (9)		2.5n		20 (Total Penalty (C40 => Moderate cavity detail 40 (Total Penalty (C60 => High cavity detail
Shutoffs	Complex (9)		4.5n		Total Penalty > 80 -> Very high cavity detail
Lett	tering (10)		n		(lin = 25 (mm; 100 mm = 3 9 (in)

Figure 11.16 Determination of Cavity Detail. Notes (8)-(10) can be found in Appendix 11A.

				FOURTH	DIGIT
		SUBSIDIAR	Y	UHDE	RNAL RCUT EXITY
		COMPLEXIT	¥	Without Extensive (7) External Undercuts (5)	With Extensive (7) External Undercuts (5)
		.			1
TD	CP	Low	0	1.00	1.25
H I I G	V T	Hoderate	1	1.25	1.45
ŘΪ	Y L	High	2	1.60	1.75
DŦ	(၈	Yery High	3	2.05	2.15

Table 11.1 Subsidiary Complexity Rating, C_S for Injection Molding. Notes (5) - (7) can be found in Appendix 11A on page 11-26.

					SIXTH I	
					Connercial	Tight
. ,					0	1
s	F	SPI	5-6	0	-	-
SURF	ĭ	SPI	3-4	1	1.00	1.05
A CE	Š	TEXT	URE	2	1.05	1.10
Ě	R.	SPI	1-2	3	1.10	1.15

Table 11.2 Tolerance and Surface Finish Rating, C_b for Injection Molding.

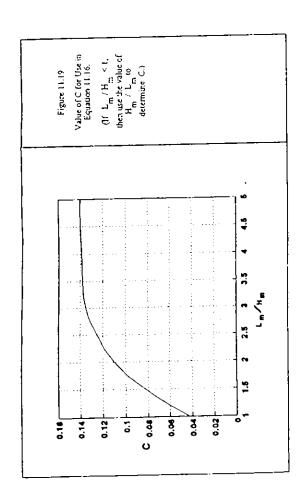


Table 15.1 Data for	Data for the Reference Part
Material	Polystyreno
Material Cost (Kp)	1.46 x 10 ⁻⁴
	cents/ mm ³⁽¹⁾
Part Volume (K _p)	1244 mm ³
Die Mat Cost (K _{dmo})	(2)086\$
Die Construction Time (Includes design and build hours)	200 hours
Labor Rate (Die Construction)	\$30/h ⁽²⁾
Cycle Time (t _o)	16 seconds (2)
Mold Machine Hourly Rate (C _{ho})	(5)
(1) Planic Techn (2) Data from collabor (3) Planic Techn	(1) Plastic Technology, June 1989. (2) Data from collaborating companies, 1989. (3) Plastic Technology, July 1989.

Car	123	2.92	1.54	2.79	3.96	0.74	0.62	1.00 (Reference)	2.33	0.62
Material	A85	Acetal	Acrylic	Nylon 6	Polycarbonate	Polyethylene	Polypropylene	Polystyrene	PPO	PVC

Material A88 Acetal Acetylic Nylon 6 Polycazbonate Polyctylene	2.92 2.92 1.54 2.79 2.79 2.79
Polystyrene Polystyrene	0.62 1.30 (Reference)
PPO PVC	2.33

Relative Die Material Cost, Com

E 8

80 100 160 200 260 300 380 400 480 800 880 600 Projected Area of Mode Bear, Mg (x 10³ mm²)

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Mt = 11to (378 mm)

Not. Die Material Cost. Cam

Figure 11.20

01 0 20 30 %	in (percent)	<u> </u>	8.0	۰,	9.0	.\ .\.	0	<u>:</u>	2	0	٦	8 8
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	•		ġ	7		1	:	1	_			2
	8 5	110	8 8	<u></u>	- <u>:</u>	8	<u>3</u>	3	: B 8	5 5	ڲٳ	•

Figure 15.23 Variation of fo, fo, and fm With Production Volume in Injection Molding.

Table 15.5 Machine Founage and Relative Hourly Rate (Data published in Plastic Technology, June, 1589.) Injection Molding.	Relative Hourly Rate	00'1	61.1	#	1.83	2.87	2.93
Table 15.5 Machine Fours (Data published in Plastic Injection	Machine Tormage	< 100	100 - 259	300 - 499	\$00 - 699	700 - 999	> 1000

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Classification System for Shearing and Local Features

7. Figure

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	_	serve prescholate of serve colores (f))	~	~	~	~	**	~	
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. —		Parts will soon thee east type of costary operand pro- trucked feature (I), will or without closely operand cor- protrucing features, sames calous or easter projections		3	5	=	204	2.70	69 0	· ~ •
		. OR Purts with only see type of dously spaced protecting sectors with cosety spaced exerging the sectors protected exerging the sectors source corrections.	7	<u>ب</u>	~	~	~	۰	~	• • -
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oecoe(ou	-	Parle without dotally spaced leadure (f), narrow projections or narrow catowie (f).	e T	<u>~</u>	•	•	٠.	^	•	0 >
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		Parts with oak one from or closely against projections	ις.	~	^			^-	·.	·
1		leature and dosely spaced see-protecting features and/or serror cetairs and/or serror projections								0.0
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- 4	die des lin	Pears with closely spicoed sor-providing leaenres and/or sering projections (7).		•	۲	^	^	<u> </u>		
		Parts well soins these one type of closely special pro- tryclady testare (), with or without closely special soin procedure searce colours of service projections.		154	7.0		•	ž.		······································
		Parts with only one type of dosely spaced probading learns and dosely spaced on-protecting beautie deduct a service eddion surver protections.	0	-	-	<u>-</u>	-	-		<u> </u>
200	v (f) stand b	biological party () without safety shickses, or unfolded parts with western safety safety and the safety safety of the safety safety of the safety sa	0		1/2	s We	ie sių	Parts like this are not usually	nensn	
9	3 C	nor-people at features (f) whose direction read pyralist to be sheet.	<u> </u>		S	tamped and/or can no penerally he stemped	1 and	slamped and/or can not	200	

Stanpins 34

Feeture	Neaber Peobres (a)	Opposite Ourchosen Penalty (Y/N)		
Standard		•	Sand Paris (Let 100 am)	
Non-standard Hole		24 20	4 C Total Panelty At 1-3 Low Local 4 C Total Panelty A 3 -3 Local Detail Total Panelty 3 -3 -3 Foh Die Detail	Figure 12.24
Cola		30 30	Medium Paris (160 mm c.L. of 206 mm)	Determination of Die Detail
Standard		(1:-1)	Total Peachy of 8 -> Low Oie Detail 8 - Total Peachy 12-> Median Die Detail	
Non-standerd Embose	<u> </u>	2(10.1) 20	Tord Penalty 212-2 Kigh Ole Detail	
Hole		2(n-1) 2n	Total Peesly -(10-) Low Die Deteal	
Form		3(n-1) 3a	Total Pasalty 417-5 Hearth De Detail	
S.		3(0-1) 30		
Se d		3(4-1) 30		
Ę		4(0-1)		
Semi-Perl		0 (1.0)		
Teb		3(0-1) 30		
Lettering		2(n-1) 2n		
		Total Penalty		

Bottom Plate of Die Set Table 12.3 Determination of Number of Stations Required [2] fumber of Active Stations, NA . Nat + Nat + Nat + lumber of Icle Stations, N_I = N_{II} + N_D + N_B =

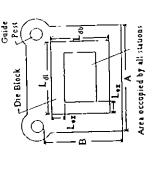
(a) For $L_{UW} \le 25$ mm $N_{Ij} = 1.5 (N_{2j} - 1)$, j = 1, 2, 3

(b) For 25 mm < L_{0м} < 125 mm

 $N_{II} = 0$ (part without curls) $N_{II} = 2$ (part with curls) $N_{IJ} = (N_{IJ} - 1)$ $N_{IJ} = (N_{IJ} - 1)$

(c) For $L_{cw} \ge 125 \text{ mm}$, $N_{II} - N_{II} - N_{II}$ ocal Number of Stations, NS • NA + NI

Table 12.4 Die Block and Die Set Stze [2]



where L_{CK}=25 if N₂L_{LW} ≤75 L_{CK}=37 if 75 < N₂L_W <250 L_{CK}=50 if N₂L_{GW} ≥ 250 $L_d = N_5 L_{LW} + 2 L_{cc} = L_{cd} + 2 L_{$ Die Block Size (mm)

Die Set Size:

A = L_d +25 = B = L_d +25 = S_d = AB =

Sufficient data not

Paris At o this are not considered here | | | Four stide form (pack used | | |

0 - U - H

Figure 12.3 Classification System for Contour Forming, Notes (11) - (27) can be found in Appendix 12.A

-—Ţ			ige .	_				_]	
Comments	1008-1012 tempered rolled or amealed last	C23060 (red brass) annealed; C26000 (carnidge trass) annealed	C23006 (red brass) cold roiled; C26000 (cartidge brass) cold rolled	1100-0; 5052-0	1100-H18; 5052-H18	1008-1012 half-hard (Rockwell 70-85; tensile strength 380-520 Mpa	302 annealed	304 cold rolled	
Fut	0.1	0:1	2	91	1.2	1.2	1.2	1.2	
Fmb	0.1	0.1		97	11	=	111	Ξ	
Fm	00:1	86.0	66:0	09:1	1.00	10:1	1.02	8.	
Digit 7	0		2	-	7	~	9	7	
Material	Soft CRS, Low C	Soft Red Metal	Hard Red Metal	Soft Al Alloy	Hard Al Attoy	Hard CRS, Low C	Medium Stainless	Hard Stainless	

Table 12.2 - Classification System for Sheet Thickness	ation System	n for Sheet 1	hickness
t (mm)	Digit 8	Ft	Fdm
0.125-3	0	0.1	1.0
< 0.125	-	<u>1'1</u>	1.0
^]	2	0.1	5 1

Stempton St