University of Toronto Faculty of Applied Science and Engineering FINAL EXAMINATIONS -- APRIL 1999

SECOND YEAR -- ENGINEERING SCIENCE Program 5 AER 202S -- FLUID MECHANICS

Examiner: P.A. Sullivan

Instructions:

- (1) Closed book examination, no aids permitted.
- (2) The questions are NOT assigned equal marks. The marks for each part are indicated at the beginning of each part.
- (3) Attempt as many questions as you can. Parts of questions may be answered
- (4) Marks are given for careful reasoning according to the basic principles, with algebraic errors being penalized lightly.
- (5) The questions themselves contain formulae useful in other questions.
- (6) Bold face quantities represent vectors.
- (1a) [10 MARKS] Given two functions f(x,y) and g(x,y) which are continuous over a region R of the (x,y) plane bounded by a sectionally continuous convex closed curve C, show that

$$\oint_C [f(x,y)dx + g(x,y)dy] = \int_R \left[\frac{\partial g}{\partial x} - \frac{\partial f}{\partial y}\right] dR$$

- (1b) [3 MARKS] Describe how this result can be extended to a region bounded by a nonconvex curve.
- (2) [6 MARKS] Given a function $f(x_1, x_2, x_3)$ which is continuous over a region R of space, for a volume $V \in R$ enclosed by a surface, it can be shown that

$$\int_{V} \frac{\partial f}{\partial x_{j}} dV = \int_{S} f n_{j} dS \quad \text{for} \quad j = 1, 2, 3.$$

where n_j is the j-th component of the unit outward normal n on S. State the two vector field theorems that follow from this expression.

(3a) [8 MARKS] Given that, if

$$F(x) = \int_a^b f(x,y) dy$$
 then $\frac{dF}{dx} = \int_a^b \frac{\partial f}{\partial x} dy$

for a and b constant, show that

$$\frac{d}{dx} \int_{g_1(x)}^{g_2(x)} f(x, y) \, dy = \int_{g_1(x)}^{g_2(x)} \frac{\partial f}{\partial x} \, dy + f(x, g_2(x)) \frac{dg_2}{dx} - f(x, g_1(x)) \frac{dg_1}{dx}$$

(3b) [8 MARKS] Given the function F(t) defined by

$$F(t) = \int_0^{a(t)} \int_0^{b(t)} f(x,y) \, dy \, dx$$

find dF/dt.

[7 MARKS] Recall that, for a curve C in the (x,y)-plane enclosing a region R, if it is described parametrically by x = x(t) and y = y(t), the enclosed area A is given by the line integral

$$A = -\frac{1}{2} \oint_C [y(t) \frac{dx}{dt} - x(t) \frac{dy}{dt}] dt$$

Use this result to show that, for a transformation of co-ordinates x = x(u, v) and y = y(u, v),

$$A = \frac{1}{2} \oint_{C_{\bullet}} \left[x \frac{\partial y}{\partial u} - y \frac{\partial x}{\partial u} \right] du + \left[x \frac{\partial y}{\partial v} - y \frac{\partial x}{\partial v} \right] dv$$

where C^* is the curve bounding the image of R in the (u, v) plane, namely R^* .

(4b) [9 MARKS] Hence show that

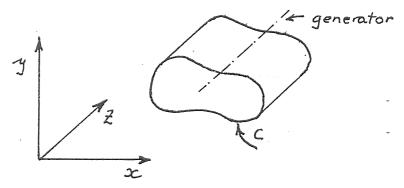
$$A = \iint_{R*} \frac{\partial(x,y)}{\partial(u,v)} du \, dv$$

(5) [14 MARKS] For the triangular region R having vertices at (x,y) = (0,0), (1,0), (0,1), evaluate

$$\int_{R} e^{g(x,y)} dR \quad \text{where} \quad g(x,y) = \frac{y-x}{y+x}$$

Hint: Use the transformation x + y = u and x - y = v.

(6a) [6 MARKS] A right cylinder having its generator parallel to the i_z axis intersects the (x,y) plane forming the curve C shown in the diagram below.



It is immersed in a fluid for which the pressure field has the form

$$p(x,y,z) = a + bx + cy$$

If the curve C is described parametrically in terms of the distance s along it, that is x = x(s) and y = y(s), by formulating the surface integral, show that the pressure force F_p per unit length in the i_z direction acting on the cylinder can be reduced to the line integral

$$F_p = -\oint_C [p(x,y)\frac{dy}{ds}i_x - p(x,y)\frac{dx}{ds}i_y]ds$$

(6b) [8 MARKS] If A is the area in the (x,y) plane enclosed by C, by completing the line integral show that this reduces to

$$F_p = -bAi_x - cAi_y$$

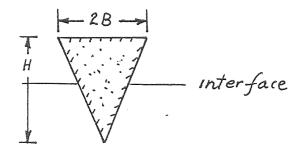
(6c) [6 MARKS] Show how this result may also be obtained by use of an appropriate form of Gauss' Theorem.

- (7a) [6 MARKS] Given a fluid at rest having density and pressure fields $\rho(r)$ and p(r) respectively, and given a body force field g(r), show that a necessary condition of hydrostatic equilibrium is $\nabla p = \rho g$.
- (7b) [6 MARKS] Hence show that the resultant pressure force F_p acting on a solid body immersed in a constant density fluid subject to terrestrial gravity is given by

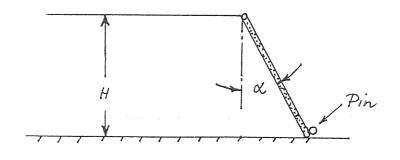
$$F_p = \rho g V i_z$$

where V is the volume of the body, and $g = -g i_z$.

(7c) [6 MARKS] A triangular beam having base width 2B, height H, and relative density 0.9 floats apex down at the interface of two immiscible liquids having relative densities 1.0 and 0.8 respectively; this is shown in the diagram below. Find the distance which the apex penetrates the lower liquid. Express your result as a fraction of H.



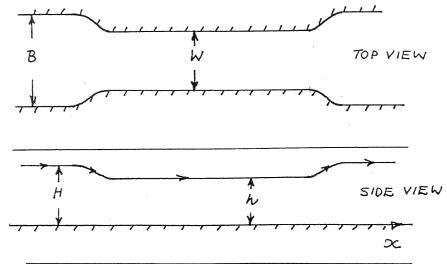
(8) [8 MARKS] A rectangular channel for conveying water has width B and depth H. It has a control gate depicted in the diagram below which is hinged at the top of the channel, inclined at an angle α to the vertical, and retained in place by a pin at the bottom. If water of density ρ can rise to the top of the channel, calculate the magnitude of the force acting on the pin. Ignore the weight of the gate.



- (9a) [8 MARKS] Apply Newton's law for the motion of a particle to steady frictionless flow in a fluid filament, and thus obtain an equation for the motion of a particle along the filament. Does this relationship apply to compressible or incompressible flow?
- (9b) [2 MARKS] Show how this may be integrated to obtain Bernoulli's Theorem for incompressible flow in the presence of terrestrial gravity; which is

$$\frac{p}{\rho} + gz + \frac{1}{2}q^2 = E_T$$

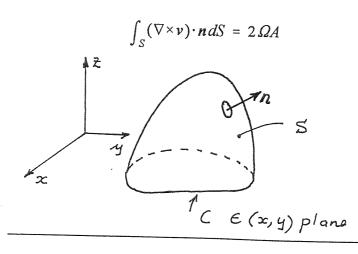
(10) [12 MARKS] Water flows in a horizontal rectangular channel of width B, and then passes through a measuring station in the form of a constriction which reduces the channel width to W as shown in the diagrams below. The height of the water level changes from H to h. By assuming that the flow is frictionless and steady and that, in both the upstream channel and the constriction, the streamlines are straight and parallel to the x-axis shown in the diagram below, find an expression for the volume flux Q through the channel as a function of B, W, H and h.



(11a) [4 MARKS] A fluid velocity field v(r) rotates about the i_z axis with angular speed Ω as if it were a solid body. Show that the velocity field takes the form

$$v(r,t) = -\Omega y i_x + \Omega x i_y$$

(11b) [8 MARKS] By carrying out the surface integral, for any surface S bounded by a curve C lying in the (x,y) plane as depicted in the diagram below. Show that, if A is the area of the planar region bounded by C,



(12a) [4 MARKS] Given a property of a fluid ϕ per unit mass, the Reynolds Transport Theorem gives the rate of change of the total amount of that property Φ for a moving body of fluid of mass M contained in a moving volume V_M :

$$\frac{d\Phi}{dt} = \frac{d}{dt} \int_{V_M} \phi \rho dV \doteq \frac{D}{Dt} \int_{V_c} \phi \rho dV = \int_{V_c} \frac{\partial}{\partial t} (\phi \rho) dV + \int_{S_c} \phi \rho v \cdot n dS$$

where $\rho(r,t)$ and v(r,t) are, respectively, the density and velocity fields. Explain the physical meaning of the two terms on the right-hand side of the above expression.

(12b) [7 MARKS] Use it to derive the differential form of the equation of continuity, which is

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho v) = 0$$

(12c) [7 MARKS] Show that, for steady flow in a fluid filament, the Reynolds Transport Theorem reduces to

$$\frac{d\Phi}{dt} = \dot{m}_f(\phi_2 - \phi_1)$$

and explain the meaning of the terms on the right hand side of this expression.

(13a) [6 MARKS] A one-dimensional unsteady flow field, such as that induced by a piston in a cylinder, has the functional form

$$v(r,t) = u(x,t)i_x$$

where the spatial co-ordinate x is aligned along the cylinder axis. Show that the acceleration a_x of a fluid particle is given by

$$a_x = \frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x}$$

(13b) [9 MARKS] By evaluating the fluxes out of a control volume V_C consisting of a section of the cylinder of length Δx , show directly that the equation of continuity takes the form

$$\frac{\partial \rho}{\partial t} + \frac{\partial}{\partial x}(\rho u) = 0$$

(14a) [8 MARKS] For surface waves propagating in a horizontal channel which are long compared with the depth *H* of the undisturbed water, vertical speeds and accelerations are very small, so that the velocity field has the approximate form

$$v(r,t) \approx u(x,t)i_x$$

where x is the distance along the channel. Show that the equation of motion takes the form

$$\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + g \frac{\partial h}{\partial x} = 0$$

(14b) [8 MARKS] If h = h(x,t) is the height of the water surface above the floor of the channel, given that the equation of continuity takes the form

$$\frac{\partial h}{\partial t} + \frac{\partial}{\partial x}(uh) = 0$$

Show that the speed c of propagation of small disturbances is given by $c = \sqrt{(gH)}$.

(15a) [8 MARKS] For a moving body of fluid contained within a volume $V_M(t)$ which coincides at some instant with a fixed control volume V_C , show that the rate dW_p/dt at which pressure forces acting at the boundary S of V_C do work on this body of fluid is

$$\frac{dW_p}{dt} = -\int_{S} p v \cdot n \, dS$$

where n is the unit outward normal on S.

(15b) [6 MARKS] Show that, in the case of incompressible flow, this reduces to

$$\frac{dW_p}{dt} = -\int_{V_C} v \cdot \nabla p \, dV$$

(16) [12 MARKS] For compressible inviscid adiabatic steady flow, use the principle of conservation of energy in the presence of terrestrial gravity to show that, with h being the enthalpy of the fluid, an equation having the form

$$h + gz + \frac{1}{2}q^2 = constant,$$

applies along streamlines.