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## Stationary Liquid Method:

⑥ Clean & Dry

① Sat. with W phase (100%)  
→  $k_{abs}$

② Inject NW → Displace W until  $S_{w,irr}$

→ Calculate  $S_{w,irr}$  &  $S_{nw}$

→  $\Delta P_{steady\ state}$  &  $q_{nw}$

$$\rightarrow k_{rnw} = \frac{M_{nw} q_{nw} L}{K A \Delta P} \text{ at } S_{w,irr}$$

③ Inject a mixture  $\frac{q_w}{q_{nw}}$  at low values

→  $\Delta P, q$  →  $k_{rw}$  &  $k_{rnw}$   
 $S_w, S_{nw}$

①

## Unsteady-State Method:

- ① sat. sample with nw phase at  $S_{w,irr}$
- ② Inject w phase  $\rightarrow$  Displace nw
- ③ w phase breaks through at outlet

$$\underbrace{f_w, f_{nw}, \Delta P}_{K_r}$$

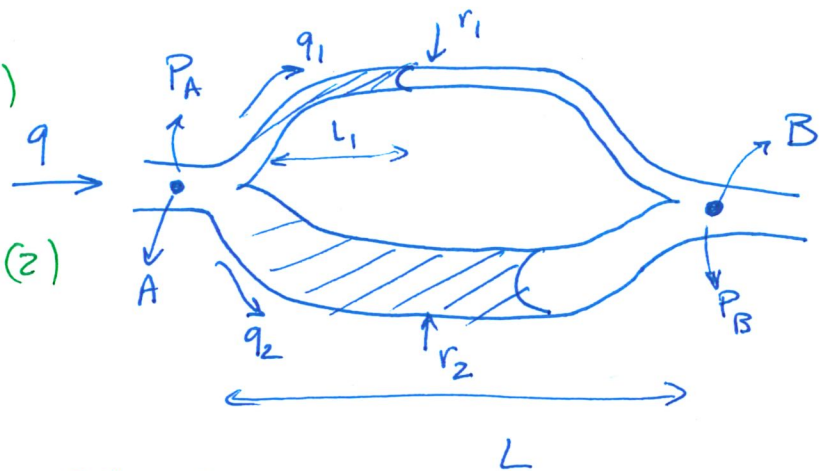
# Capillary Trapping in Porous Media :

$$P_A - P_B = P_A - P_w + P_w - P_{nw} + P_{nw} - P_B \quad (*)$$

H-P's Law:

$$q_1 = \frac{\pi r_1^4}{8\mu} \frac{P_A - P_w}{L_1} \quad (1)$$

$$q_2 = \frac{\pi r_2^4}{8\mu} \frac{P_{nw} - P_B}{(L - L_1)} \quad (2)$$



\*  
→  
(1), (2)

$$P_A - P_B = \frac{8q_1\mu L}{\pi r_1^4} - P_c1$$

$$P_A - P_B = \frac{8q_2\mu L}{\pi r_2^4} - P_c2$$

$$\Rightarrow -\left(\frac{8\mu L}{\pi r_1^4}\right)q_1 + \left(\frac{8\mu L}{\pi r_2^4}\right)q_2 = (P_{c2} - P_{c1}) \quad (**)$$

$$= 2\sigma \cos\theta \left(\frac{1}{r_2} - \frac{1}{r_1}\right)$$

From Laplace's eq.

$$q_1 + q_2 = q \quad (**)$$

$$q_1 = \frac{\left(\frac{8\mu L}{\pi r_2^4}\right)q - 2\sigma \cos\theta \left(\frac{1}{r_2} - \frac{1}{r_1}\right)}{\left(\frac{8\mu L}{\pi r_1^4}\right) + \left(\frac{8\mu L}{\pi r_2^4}\right)}$$

$$q_2 = \frac{\left(\frac{8\mu L}{\pi r_1^4}\right)q + 2\sigma \cos\theta \left(\frac{1}{r_2} - \frac{1}{r_1}\right)}{\left(\frac{8\mu L}{\pi r_1^4}\right) + \left(\frac{8\mu L}{\pi r_2^4}\right)}$$

$$\Rightarrow \frac{q_2}{q_1} = \frac{\left(\frac{r_2}{r_1}\right)^4 q + \frac{\pi r_2^4 \epsilon \cos \theta}{4\mu L} \left(\frac{1}{r_2} - \frac{1}{r_1}\right)}{q - \frac{\pi r_2^4 \epsilon \cos \theta}{4\mu L} \left(\frac{1}{r_2} - \frac{1}{r_1}\right)}$$

let  $\left\{ \begin{array}{l} v_1 = \frac{q_1}{\pi r_1^2} \quad , \quad v_2 = \frac{q_2}{\pi r_2^2} \\ B = \left( \frac{r_2}{r_1} \right) \quad , \quad N_{\text{v cap}} = \frac{qML}{\pi r_1^3 \epsilon \cos \theta} \end{array} \right.$   $\rightarrow$  viscous force

$\rightarrow$  capillary force

$$\Rightarrow \frac{v_2}{v_1} = \frac{4N_{\text{vcap}} + \left(\frac{1}{\beta} - 1\right)}{\frac{4N_{\text{vcap}}}{\beta^2} - \beta^2 \left(\frac{1}{\beta} - 1\right)}$$

$$\frac{v_2}{v_1} > 1 \Rightarrow \text{Trap in smaller pores}$$

$$\equiv N_{\text{rcap}} > \frac{\beta(\beta^2 + 1)}{4(\beta + 1)}$$

$$\frac{v_2}{v_1} < 1 \Rightarrow \text{Trap in larger pore}$$

$$\equiv N_{\text{vcap}} < \frac{\beta(\beta^2 + 1)}{4(\beta + 1)}$$

low  $q \rightarrow$  displacement will be dominated by cap. force

→ Trap in large pore  $\Rightarrow$  low displacement efficiency

high  $q \rightarrow$   $\hookrightarrow \hookrightarrow \hookrightarrow \hookrightarrow$   $\hookrightarrow$  Viscous force  
little less off

→ Trap in small pores  $\Rightarrow$  high disp. eff.