Due: Monday, March 10, 2003

- 1. An abrupt Si p-n junction is formed by alloying a uniformly doped n-type silicon bar where $N_d = 8x10^{16}/\text{cm}^3$ in the beginning. During the alloying process, a uniform counter doping of acceptors of $N_a = 1.4x10^{17}/\text{cm}^3$ is introduced in the region for x<0. Basically, x<0 is the p-side and x>0 is the n-side.
 - (a) Calculate the Fermi level positions at 300 K in the p and n regions.
 - (b) Draw an equilibrium band diagram for the junction and determine the contact potential V_o from the diagram.
 - (c) Compare the results of part (b) with V_o as calculated from Eq. (5-8).
 - (d) Using Eq. (5-8), calculate and plot V_O versus temperature ranging from 250 K to 500 K.

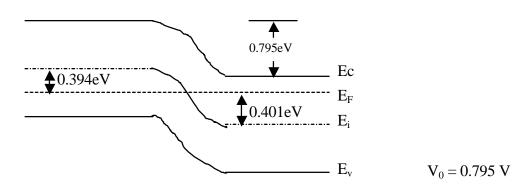
Solutions:

(a), At x<0,
$$p_p = N_a - N_d = 6 \times 10^{16} cm^{-3}$$

In p region,
$$E_{ip} - E_{Fp} = \frac{kT}{q} \ln \frac{p}{n_i} = 0.0259 \times \ln \frac{6 \times 10^{16}}{1.5 \times 10^{10}} = 0.394 eV$$

In n region,
$$E_{Fn} - E_{in} = \frac{kT}{q} \ln \frac{n}{n_i} = 0.0259 \times \ln \frac{8 \times 10^{16}}{1.5 \times 10^{10}} = 0.401 eV$$

(b),



(c), Equations 5-8:

$$V_0 = 0.0259 \ln \frac{N_a N_d}{n_i^2} = 0.0259 \ln \frac{6 \times 10^{16} \times 8 \times 10^{16}}{n_i^2} = 0.795 V$$

Result is same as (b)

(d), Notice that the n_i is related to temperature through Eq. 3-26

Method 1:

Read n_i from Figure 3-17, plug into Eqn 5-8 to obtain the plot.

For example: at T=400K, $n_i = 8*10^{12} \text{ cm}^{-3}$.

$$V_0 = \frac{kT}{q} \ln \frac{N_a N_d}{n_i^2} = \frac{1.38 \times 10^{-23} \times 400}{1.6 \times 10^{-19}} \ln \frac{6 \times 10^{16} \times 8 \times 10^{16}}{(8 \times 10^{12})^2} = 0.626V$$

At least 5 points must be correctly read and calculated.

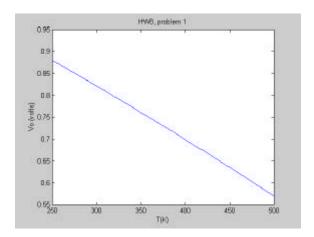
Method 2

$$n_i(T) = 2\left(\frac{2\mathbf{p}kT}{h^2}\right)^{3/2} (m_n^* m_p^*)^{3/4} e^{-E_g/2kT}, \text{ therefore, if we assume } m_n^*, m_p^*, E_g \text{ is independent of T, we have:}$$

$$\frac{n_i(T)}{n_i(300K)} = \left(\frac{T}{300}\right)^{3/2} e^{\left[-\frac{E_g}{2k}\left(\frac{1}{T} - \frac{1}{300}\right)\right]}, \text{ i.e., } n_i(T) = n_i(300K) \left(\frac{T}{300}\right)^{3/2} e^{\left[-\frac{E_g}{2k}\left(\frac{1}{T} - \frac{1}{300}\right)\right]}$$

$$\begin{split} V_0 &= \frac{kT}{q} \ln \frac{N_a N_d}{n_i^2} = \frac{kT}{q} \ln \frac{N_a N_d}{\left(n_i (300K) \left(\frac{T}{300}\right)^{3/2} e^{\left[\frac{E_g}{2k} \left(\frac{1}{T} - \frac{1}{300}\right)\right]}\right)^2} \\ &= \frac{kT}{q} \left[\ln \frac{N_a N_d}{n_i^2 (300K)} - 3 \left(\ln T - \ln 300 \right) + \frac{E_g}{k} \left(\frac{1}{T} - \frac{1}{300}\right) \right] \\ &= \frac{1.38 \times 10^{-23} \times T}{1.6 \times 10^{-19}} \left[30.69 - 3 \ln T + 3 \times \ln 300 + \frac{1.1 \times 1.6 \times 10^{-19}}{1.38 \times 10^{-23}} \left(\frac{1}{T} - \frac{1}{300}\right) \right] \\ &= 8.625 \times 10^{-5} \times T \times \left(47.8 - 3 \ln T + 1.275 \times 10^4 \times \left(\frac{1}{T} - \frac{1}{300}\right) \right) (volts) \end{split}$$

Plot:

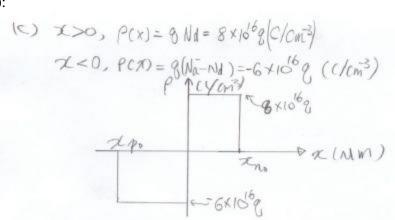


2. Refer to problem 1, the silicon bar has a cross section with diameter 20 μ m. Assume that the depletion approximation holds. (a) Calculate W, X_{no} and X_{po} at 300 K. (b) Determine the total positive ion charge in the depletion region. (c) Sketch to scale the charge density $\rho(x)$, electrical field E(x), and electrostatic potential V(x) in the depletion region. Assume that the electrostatic potential is zero at x=0. (d) Draw the energy band diagram for the device.

(a):
$$W = \left[\frac{2eV_0}{q}\left(\frac{1}{N_a} + \frac{1}{N_a}\right)\right]^{1/2} = \left[\frac{2(11.8 \times 8.85 \times 10^{-14})(0.795)}{1.6 \times 10^{-19}}\left(\frac{1}{6 \times 10^{16}} + \frac{1}{8 \times 10^{16}}\right)\right]^{1/2} = 0.174 \, \text{mm}$$

$$x_{n0} = \frac{W}{1 + N_d / N_a} = 0.0746 mn$$
$$x_{p0} = \frac{W}{1 + N_a / N_d} = 0.0994 mn$$

(b): $Q_+ = qAx_{n0}N_d = (1.6 \times 10^{-19})[\mathbf{p} \times (10 \times 10^{-4})^2](7.46 \times 10^{-6})(8 \times 10^{16}) = 3.00 \times 10^{-13}C$ (c):



E = - 8 Nd Zno = - 116×1519 11.8 ×8 85×1514 ×8×106× 0,0746 ×154 = -9.14×104 v/cm

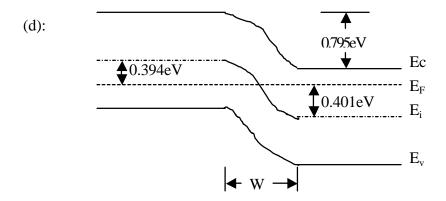
E(x) TS linear E(x) (v/cm)

Loo (um)

-9.14 x104 v/cm

When X < 0. $V(0X) = -\int_0^X \mathcal{E}(X) dX = -\int_0^X \frac{X+Xp}{Xp_0} \mathcal{E}_0 dX = \int_0^X \frac{X}{2p_0} \mathcal{E}_0 dX - \mathcal{E}_0 X$ $= -\frac{\mathcal{E}_0}{22p_0} \mathcal{I}^2 - \mathcal{I}\mathcal{E}_0 \simeq 4.6 \times 10^9 \mathcal{I}^2 + 9.14 \times 10^4 \mathcal{I}$ (Xincm)

When x>0 $V(x) = -S_0^x E(x) dx = - = -6.13 \times 10^9 x^2 + 9.14 \times 10^9 x^2$ $-xp_6$



3. Refer to problem 1 again. In reality, the alloying process will introduce a much higher concentration of acceptor. Assume that the uniform counter doping is $N_a = 3x10^{19}/cm^3$ instead. Determine and plot the contact potential V_0 and depletion widths W, X_{n0} and X_{n0} versus temperature ranging from 250 K to 500 K.

$$\begin{split} V_0 &= \frac{kT}{q} \ln \frac{N_a N_d}{n_i^2} \;, \qquad \left| \mathbf{E}_0 \right| = \frac{q N_d x_{n0}}{\mathbf{e}} = \sqrt{\frac{2q V_0}{\mathbf{e}} \left(\frac{N_a N_d}{N_a + N_d} \right)}, \quad W = \sqrt{\frac{2\mathbf{e} V_0}{q} \left(\frac{1}{N_a} + \frac{1}{N_d} \right)}, \\ x_{n0} &= \frac{W}{1 + N_d / N_a} \;, \qquad x_{p0} = \frac{W}{1 + N_a / N_d} \end{split}$$

Notice that n_i is a function of temperature. You can either use equation 3-26 or figure 3-17 Both are ok. If you use figure 3-17, at least 5 points need to be correctly read. Below I use eqn 3-26.

$$V_0 = \frac{kT}{q} \left[\ln \frac{N_a N_d}{n_i^2 (300K)} - 3(\ln T - \ln 300) + \frac{E_g}{k} \left(\frac{1}{T} - \frac{1}{300} \right) \right]$$

Using a computer program can greatly speed up calculation.

