

# Consistency of <sup>1</sup>Fanbeam Projections of a Translating Object Along an Arc of a Circle

Thomas Boulier, Rolf Clackdoyle, Jérôme Lesaint, Laurent Desbat

**Abstract**—In this article, we compute data consistency conditions (DCCs) in <sup>2</sup>in beam geometry in <sup>4</sup>the case of a translating object illuminated <sup>6</sup>by source moving along an arc of a circle. The DCCs are thus a generalization of those computed in [2], where the object remained still. In a second part, we use the DCCs in order to retrieve parameters of the object velocity. These results are illustrated by numerical examples.

## I. INTRODUCTION

In the field of CT-imaging, data consistency conditions (DCCs) use the redundancy of the data in order to establish relations that must be fulfilled between projections. These conditions are called *full* when they are not only necessary but also sufficient. One of the best known DCCs are the Helgason-Ludwig (H-L) conditions [3], [4], which are full for parallel projections. Full DCCs are also known for the case of fan-beam projections with source position taken along a straight

9line [1].

In [2], the <sup>10</sup>beam DCCs were modified to handle the case of a source moving along an arc of a circle. Briefly, all rays passing through the same point along a "virtual" <sup>11</sup>between the two extreme positions of the source are gathered to form a <sup>12</sup>beam projection. The DCCs for fanbeam projections along a line from [1] could then be applied; numerical examples showed a situation where an artificial detector attenuation was added, and the DCCs were invoked to recover the unknown attenuation coefficient. The case of a moving object has been tackled in [8], [7], where the authors used parallel <sup>13</sup>H-L conditions in <sup>14</sup>case of an object undergoing rigid body motion while illuminated <sup>15</sup>a fan-beam source along a line <sup>16</sup>. Those conditions allowed the authors to recover the parameters of the movement <sup>17</sup>in order to suppress the artifacts caused by such movement. However, using the parallel-beam H-L conditions means that the fan-beam projections had to cover all rays in the plane so that a fan-to-parallel rebinning could be achieved. The rebinning was achieved mathematically; however, the requirement of at least a standard fan-beam shortscan of  $180^\circ$  plus fan-angle is <sup>18</sup>required. In our work, we are concerned with the opposite extreme of a short arc of fan-beam measurements.

In this article, we <sup>19</sup>be interested in these two situations. We will suppose that an object is translating while illuminated <sup>22</sup>by a fan-beam source which is moving along an arc of a circle.

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The authors would like to thank Simon Rit for his help using RTK.

This work is partially supported by the Agence Nationale de la Recherche (France), project "DROITE", number ANR-12-BS01-0018.

Using a change of reference frame, we will use the same idea as in [2] <sup>5</sup>a change of variables. Then, in a second part, we will use the DCCs <sup>7</sup>in order to identify the translation velocity so that motion artifacts in the reconstructed images can be avoided <sup>8</sup>.

## II. THEORY

### A. Problem under consideration

Let us begin with some notation and definitions. We will consider an object in  $\mathbb{R}^2$  to be imaged in a fanbeam geometry with sources on an arc of circle with center  $O$  and radius  $R_0$  (see Figure 1, top). The object is identified with its density function  $\mathbf{x} \mapsto \mu(\mathbf{x}) \in C_c^\infty(\mathbb{R}^2)$ . The angular velocity of the

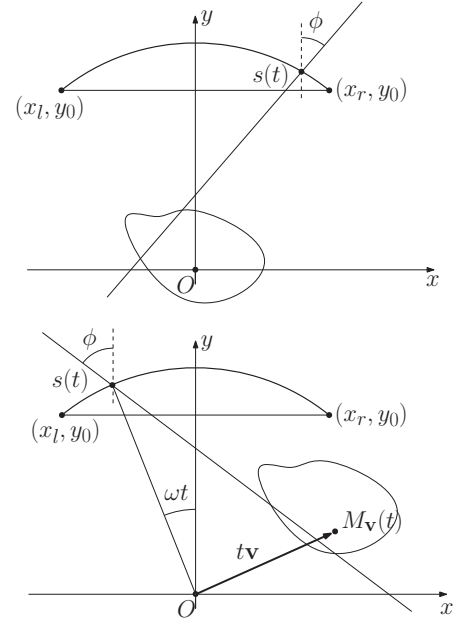


Fig. 1. Problem under consideration. The source point  $s(t)$  follows the arc of circle depicted in bold. The circle has center  $O$  and radius  $R_0$ . The object is continually undergoing a translation during the movement of the source.
























source will be denoted  $\omega$ , and the time  $t$  will range from  $-T/2$  to  $T/2$ , where  $T > 0$ . Hence, if we denote <sup>20</sup> <sup>21</sup> position of the source at time  $t$ , we have

$$s(t) = (-R_0 \sin(\omega t), R_0 \cos(\omega t)). \quad (1)$$

Furthermore, we will let  $s(T/2) = (x_l, y_l)$  (resp.  $s(-T/2) = (x_r, y_r)$ ) denote the extreme left (resp. right) position of the source. Since  $y_l = y_r = R_0 \cos(\omega T/2)$ , we will call  $y_0$  <sup>23</sup> common value. In the following, we will suppose <sup>24</sup> that  $\text{supp}(\mu)$

# Résumé des commentaires sur DCC\_translation\_CT\_meeting\_2018\_Boulier.RC.pdf

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# Consistency of Fanbeam Projections of a Translating Object Along an Arc of a Circle

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**Abstract**—In this article, we compute data consistency conditions (DCCs) in fan beam geometry in the case of a translating object illuminated by source moving along an arc of a circle. The DCCs are thus a generalization of those computed in [2], where the object remained still. In a second part, we use the DCCs in order to retrieve parameters of the object velocity. These results are illustrated by numerical examples.

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Let us begin with some notation and definitions. We will consider an object in  $\mathbb{R}^2$  to be imaged in a fanbeam geometry with sources on an arc of circle with center  $O$  and radius  $R_0$  (see Figure 1, top). The object is identified with its density function  $\mathbf{x} \mapsto \mu(\mathbf{x}) \in C_c^\infty(\mathbb{R}^2)$ . The angular velocity of the

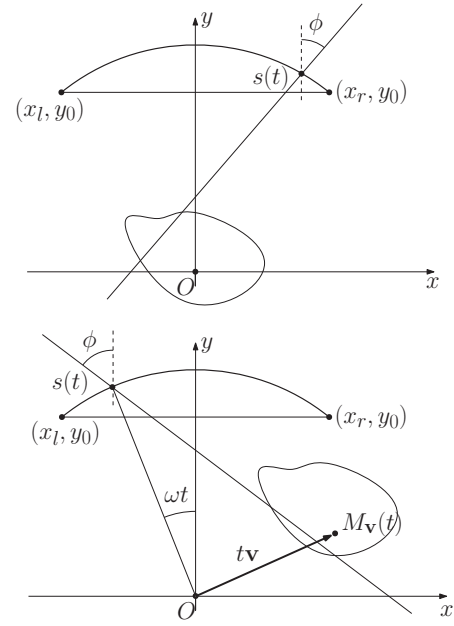


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source will be denoted  $\omega$ , and the time  $t$  will range from  $-T/2$  to  $T/2$ , where  $T > 0$ . Hence, if we denote  $s(t)$  the position of the source at time  $t$ , we have

$$s(t) = (-R_0 \sin(\omega t), R_0 \cos(\omega t)). \quad (1)$$

Furthermore, we will let  $s(T/2) = (x_l, y_l)$  (resp.  $s(-T/2) = (x_r, y_r)$ ) denote the extreme left (resp. right) position of the source. Since  $y_l = y_r = R_0 \cos(\omega T/2)$ , we will call this common value. In the following, we will suppose  $\text{supp}(\mu)$

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lies in the half-space  $\{y < y_0\}$ , and that  $y_0 > 0$  ( $-e_1 \cdot \mathbf{v} < \omega T < \pi/2$ ).

We will suppose that at any time  $t$ , rays are simultaneously emitted from the source  $s(t)$  with angle  $\phi$  ranging from  $-\pi/2$  to  $\pi/2$ . With this setup in mind, we can define the operator modeling the acquired data from the object.

**Definition 1.** The fanbeam projection data of an object with density function  $\mu$  is a function  $(t, \phi) \mapsto \mathcal{F}\mu(t, \phi)$  defined by

$$(\mathcal{F}\mu)(t, \phi) = \int_0^{+\infty} \mu(s(t) + l[\sin \phi, -\cos \phi]) dl, \quad (2)$$

where  $t \in [-T/2, T/2]$ ,  $\phi \in [-\pi/2, \pi/2]$  and  $s(t)$  is given by (1). The operator  $\mu \mapsto \mathcal{F}\mu$  is called the fanbeam projection operator.

Now let us suppose that the object is translating along a line with a constant velocity vector  $\mathbf{v} = (v_1, v_2) \in \mathbb{R}^2$  (see Figure 1, bottom). In other words, if we let  $M_{\mathbf{v}}(t)$  denote its center of mass at any time  $t$ , we have

$$M_{\mathbf{v}}(t) = (t + T/2) \mathbf{v} \quad (3)$$

The density function of the object now depends on both the spatial variable  $\mathbf{x} \in \mathbb{R}^2$  and the time  $t$ . If we denote the time varying object by  $\mu_{\mathbf{v}}$ , we have

$$\mu_{\mathbf{v}}(t, \mathbf{x}) = \mu(\mathbf{x} - M_{\mathbf{v}}(t)). \quad (4)$$

In this regard, the fanbeam projection data will be modified in the following way.

**Definition 2.** The fanbeam projection data of a translating object with density function  $\mu$  and velocity vector  $\mathbf{v}$  is given by

$$(\mathcal{F}_{\mathbf{v}}\mu)(t, \phi) = (\mathcal{F}\mu_{\mathbf{v}})(t, \phi). \quad (5)$$

The aim of this note is to derive data consistency conditions (DCCs) from (5), in order to retrieve the velocity vector  $\mathbf{v}$  from the knowledge of a single element of the range of  $\mathcal{F}_{\mathbf{v}}$ .

### B. Derivation of DCCs

In order to derive DCCs, we will first change our reference frame, from  $(O, x, y)$  to  $(M(t), x', y')$ , so that the origin is the center of mass of the object at any time  $t$ . The line between the start point and the end point of the source is still parallel to the  $x'$ -axis (see Figure 2). In other words, we are performing the following change of variables

$$(x, y) \leftrightarrow (x', y') = \mathcal{R}_{\beta}((x, y) - M_{\mathbf{v}}(t)), \quad (6)$$

where  $\mathcal{R}_{\beta}$  rotation by  $\beta$  angle  $\beta$  depicted in Figure 2 (top) and is given by

$$\beta = \arctan\left(\frac{Tv_2}{2R_0 \sin(\omega T/2) + Tv_1}\right). \quad (7)$$

Note that in this equation, the denominator can be equal to zero. Such situation occurs particularly when  $v_1 < 0$ . We studied those particular cases, both in terms of physical meaning and numerical implications. For the sake of simplicity, we will assume this abstract that  $v_1$  is not too negative (e.g.,  $v_1 > -2R_0/T$ ) to ensure that the denominator is non-zero.

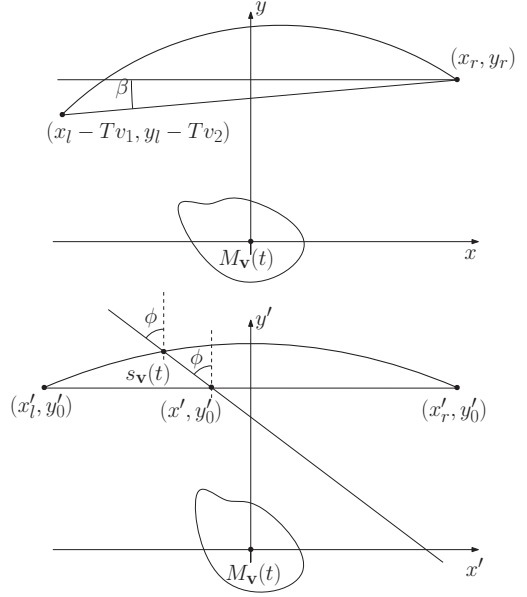


Fig. 2. Change of frame: the object is now at center of the coordinates system. Top: only translation of the center of frame; bottom: after rotation of angle  $\beta$ . Note that the angle  $\phi$  is the same as in Figure 1, bottom. The virtual source position  $(x', y'_0)$  is defined in terms of  $s_{\mathbf{v}}(t)$  and  $\phi$ ; see equation (10).

In this frame, the coordinates of the source position is given by  $s_{\mathbf{v}}(t) = \mathcal{R}_{\beta}(s(t) - M_{\mathbf{v}}(t))$ . With this in mind, the data are given by the following formula

$$(\mathcal{F}_{\mathbf{v}}\mu)(t, \phi) = \int_0^{+\infty} \mu \circ \mathcal{R}_{\beta}(s_{\mathbf{v}}(t) + l[\sin \phi, -\cos \phi]) dl. \quad (8)$$

In other words, we are now dealing with a fixed object whose density function is given by  $\mu \circ \mathcal{R}_{\beta}$ , illuminated a source following an arc of a cycloid in the frame  $(M(t), x', y')$  (see Figure 2, bottom).

Here, the extreme points  $s_{\mathbf{v}}(-T/2)$  and  $s_{\mathbf{v}}(T/2)$  have the same  $y'$ -coordinate,  $y'_0$ . We will call  $x'_l$  (resp.  $x'_r$ ) the  $x'$ -coordinates of  $s_{\mathbf{v}}(T/2)$  (resp.  $s_{\mathbf{v}}(-T/2)$ ).

Now we define what we call the *virtual fanbeam projection* from a point  $(x', y'_0)$ .

**Definition 3.** For any point  $x'$  between  $x'_l$  and  $x'_r$ , and for any angle  $\phi \in [-\pi/2, \pi/2]$ , the virtual fanbeam projection of the object  $\mu$  is defined by

$$(\tilde{\mathcal{F}}\mu)(x', \phi) = \int_0^{+\infty} \mu((x', y'_0) + l[\sin \phi, -\cos \phi]) dl. \quad (9)$$

























This is called *virtual* since it does not correspond to an actual position of the source.

In the following lemma, we will make the connection between the virtual fanbeam projection and the fanbeam projection of the translating object.

**Lemma 1.** Let us fix a time  $t \in [-T/2, T/2]$  and an angle  $\phi \in [-\pi/2, \pi/2]$ . Let us define

$$x' = s_{1,\mathbf{v}}(t) + \tan \phi (s_{2,\mathbf{v}}(t) - y'_0), \quad (10)$$

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