

University Of Toronto: Unicycle PID Control Using Euler-Forward Numerical Method Simulation

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The Objective

Modeling a robot as a 'unicycle', we desire to create an iterative algorithm giving a feedback control in the form of PID, specifically using proportional gain, in order to regulate the unicycle to the origin pointing upwards starting from any pose restricted within a radius of 2m.

The Model

We first consider a 'unicycle' model for a robot. At any point in time, its rate of change in the translational and angular motion is given by the form:

$$\begin{bmatrix} \dot{x} \\ \dot{y} \\ \dot{\theta} \end{bmatrix} = \begin{bmatrix} \cos\theta & 0 \\ \sin\theta & 0 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} v \\ w \end{bmatrix}$$

We then apply the transformation of the form $(x, y, z) \rightarrow (\rho, \alpha, \beta)$ where,

$$\begin{aligned} \rho &= \sqrt{(x_d - x)^2 + (y_d - y)^2} \\ \beta &= -\tan^{-1} \frac{y_d - y}{x_d - x} \\ \alpha &= -\beta - \theta \end{aligned}$$

where ρ is the distance to the desired location, (x_d, y_d) , β is the desired angle (measured counter-clockwise) which will give the robot its proper orientation referenced from its initial pose, and hence leaves α to be the difference between θ and β , which indicates how far away we are to the desired pose angle wise.

Under proper substitution, one can then find the model becomes:

$$\begin{bmatrix} \dot{\rho} \\ \dot{\alpha} \\ \dot{\beta} \end{bmatrix} = \begin{bmatrix} -\cos\alpha & 0 \\ \rho^{-1}\sin\alpha & -1 \\ -\rho^{-1}\sin\alpha & 0 \end{bmatrix} \begin{bmatrix} v \\ w \end{bmatrix}$$

However, as the system is non-linear, we will then linearize the model using $(\rho, \alpha, \beta) = (0, 0, 0)$ as we desire the robot to be regulated to the origin with pointing upwards.

Now, given the feedback law:

$$v = -k_\rho \rho, \quad \omega = -k_\alpha \alpha - k_\beta \beta$$

we find that through using the Eigen equation, in order to ensure stability,

$$k_\rho < 0$$

$$k_\alpha - k_\rho < 0$$

$$k_\beta k_\rho < 0$$

Algorithm

To create the algorithm, the Euler-Forward method was utilized to approximate the values through an iterative method. So here, we use:

$$x_{k+1} = x_k + h\dot{x}_k$$

Using the model, we further have:

$$\dot{x} = -k_\rho \rho \cos\theta$$

$$\dot{y} = -k_\rho \rho \sin\theta$$

$$\dot{\theta} = -k_\alpha \alpha - k_\beta \beta$$

Using all the relationships, we then find:

$$\dot{x} = -k_\rho \sqrt{x^2 + y^2} \cos\theta$$

$$\dot{y} = -k_\rho \sqrt{x^2 + y^2} \sin\theta$$

$$\dot{\theta} = -k_\alpha \left(\tan^{-1} \frac{y}{x} - \theta \right) - k_\beta \left(\tan^{-1} \frac{y}{x} - \beta_d \right)$$

From all of the above, we substitute in order to formulate the final numerical equations that will regulate the unicycle to the origin pointing upwards:

$$x_{k+1} = x_k - k_\rho h \sqrt{x_k^2 + y_k^2} \cos\theta_k$$

$$y_{k+1} = y_k - k_\rho h \sqrt{x_k^2 + y_k^2} \sin\theta_k$$

$$\theta_{k+1} = \theta_k - h \left[k_\alpha \left(\tan^{-1} \frac{y_k}{x_k} - \theta_k \right) - k_\beta \left(\tan^{-1} \frac{y_k}{x_k} - \beta_d \right) \right]$$

where,

$$k_\rho < 0$$

$$k_\alpha - k_\rho < 0$$

$$k_\beta k_\rho < 0$$

$$\beta_d = -\frac{\pi}{2}$$

Simulation

The figure below shows the unicycle starting in different locations and orientation. The problem at hand required us to restrain the motion within a circle of radius 2m.

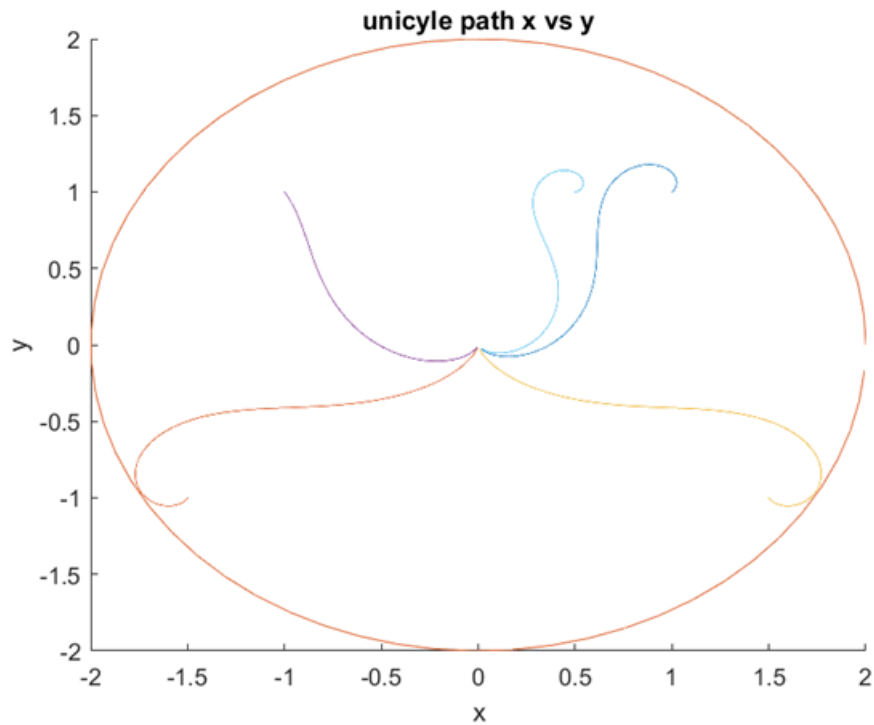


Figure 1: Unicycle starting in different poses converging to the origin pointing upwards

Modification: Following A Sinusoidal Path

In order to test the validity of the algorithm from the first part, the motivation is now to follow a sinusoidal path, the sine curve.

We first recognize the algorithm was established with static values, (x_d, y_d, β_d) . In order to make this a dynamic problem which will enable us to follow a curve, we will use Matlab's linspace function retrieving values from the function, $y = 0.5\sin x$. The model will now become:

$$\begin{aligned}x_{k+1} &= x_k - k_\rho h \sqrt{x_k^2 + (0.5\sin x_k)^2} \cos \theta_k \\y_{k+1} &= 0.5\sin x_k - k_\rho h \sqrt{x_k^2 + (0.5\sin x_k)^2} \sin \theta_k \\\theta_{k+1} &= \theta_k - h \left[k_\alpha \left(\tan^{-1} \frac{0.5\sin x_k}{x_k} - \theta_k \right) - k_\beta \left(\tan^{-1} \frac{0.5\sin x_k}{x_k} \right) \right]\end{aligned}$$

where in order to ensure convergence, we have the following restrictions for the feedback values again as:

$$\begin{aligned}k_\rho &< 0 \\k_\alpha - k_\rho &< 0 \\k_\beta k_\rho &< 0 \\\beta_d &= 0\end{aligned}$$

Simulation

The figure below shows the unicycle with different step-size values. The problem at hand required us to follow the sinusoidal path, $y = 0.5\sin x$, which is red curve starting at point, $(0, 0)$.

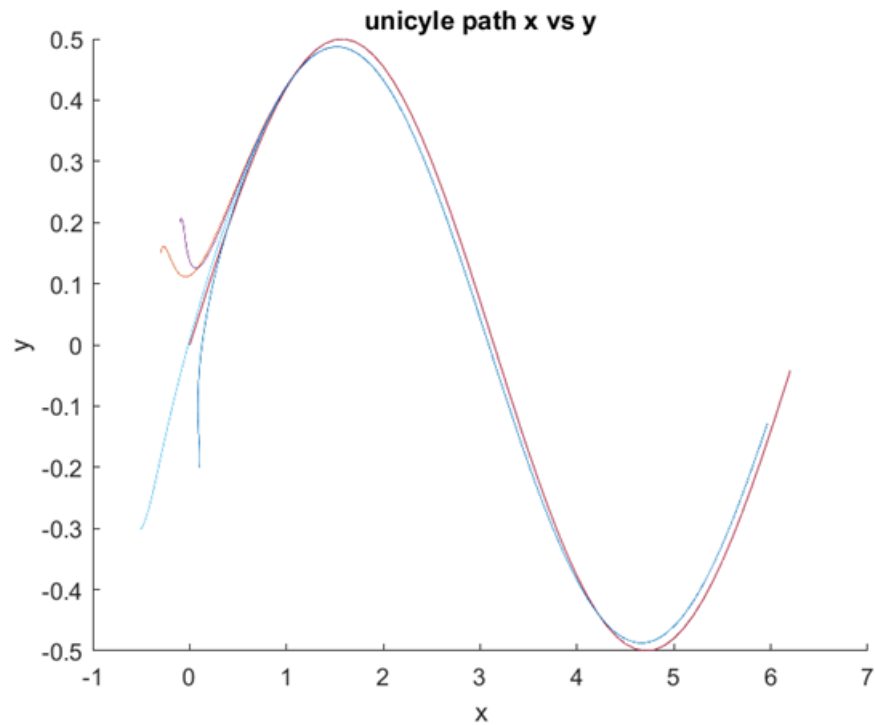


Figure 2: Unicycle following sinusoidal path

Appendix (a): The Variable Transformation Derivation

We first recognize the problem at hand, wherein:

$$\rho = \rho(x(t), y(t))$$

$$\beta = \beta(x(t), y(t))$$

$$\alpha = \alpha(x(t), y(t))$$

Under such circumstances, owing to multivariate calculus, differentiating with respect to time yields the results:

$$\dot{\rho} = \frac{\partial \rho}{\partial x} \frac{dx}{dt} + \frac{\partial \rho}{\partial y} \frac{dy}{dt} \quad eq.1$$

$$\dot{\beta} = \frac{\partial \beta}{\partial x} \frac{dx}{dt} + \frac{\partial \beta}{\partial y} \frac{dy}{dt} \quad eq.2$$

$$\dot{\alpha} = -\dot{\beta} - \dot{\theta} \quad eq.3$$

We then go through differentiating one by one. For *eq.1*, we obtain:

$$-\rho\dot{\rho} = (x_d - x)\dot{x} + (y_d - y)\dot{y}$$

Manipulating the equation and using the relationship, $-\tan(\beta) = \frac{y_d - y}{x_d - x}$, $\dot{x} = v\cos(\theta)$, $\dot{y} = v\sin(\theta)$, the equation boils down to:

$$\dot{\rho} \left(\frac{\rho}{x_d - x} \right) = -v\cos(\alpha)\sec(\alpha + \theta)$$

Owing to trigonometry, we can further deduce:

$$\sec(\alpha + \theta) = \sec(\beta) = \frac{\rho}{x_d - x}$$

Hence, the final refined equation becomes:

$$\dot{\rho} = -v\cos\alpha$$

Similar procedures follow for obtaining $\dot{\alpha}$. We first give the terms associated with the differential terms:

$$\frac{\partial \beta}{\partial x} \frac{dx}{dt} = \frac{-(y_d - y)\dot{x}}{(x_d - x)^2 + (y_d - y)^2} = -\rho^{-2}(y_d - y)\dot{x}$$

$$\frac{\partial \beta}{\partial y} \frac{dy}{dt} = \frac{(x_d - x)\dot{y}}{(x_d - x)^2 + (y_d - y)^2} = \rho^{-2}(x_d - x)\dot{y}$$

We then have the equation, using $\dot{x} = v \cos \theta$, $\dot{y} = v \sin \theta$, $\beta = -(\alpha + \theta)$, $-\tan \beta = \frac{y_d - y}{x_d - x}$,

$$\rho \dot{\beta} \left(\frac{\rho}{x_d - x} \right) = v \left(\sin \theta - \tan(\alpha + \theta) \cos \theta \right)$$

$$\rho \dot{\beta} \left(\frac{\rho}{x_d - x} \right) = -v \left(\sin \alpha (\sec \beta) \right)$$

Owing to trigonometry, we again have:

$$\rho \dot{\beta} \sec \beta = -v \sin \alpha (\sec \beta)$$

Hence, the final relationship then becomes the desired equation without neglecting the angular term:

$$\dot{\beta} = -\rho^{-1} v \sin \alpha$$

Using the derived relationships above, we then have for α :

$$\dot{\alpha} = \rho^{-1} v \sin \alpha - \omega$$

Putting all the above into matrix form, we finally obtain:

$$\begin{bmatrix} \dot{\rho} \\ \dot{\alpha} \\ \dot{\beta} \end{bmatrix} = \begin{bmatrix} -\cos \alpha & 0 \\ \rho^{-1} \sin \alpha & -1 \\ -\rho^{-1} \sin \alpha & 0 \end{bmatrix} \begin{bmatrix} v \\ w \end{bmatrix}$$

Appendix (b): Feedback Stability Derivation

The feedback we give to the system is:

$$v = -k_\rho \rho, \quad \omega = -k_\alpha \alpha - k_\beta \beta$$

Upon substitution using the transformed variables, we obtain:

$$\begin{bmatrix} \dot{\rho} \\ \dot{\alpha} \\ \dot{\beta} \end{bmatrix} = \begin{bmatrix} -\cos\alpha & 0 \\ \rho^{-1}\sin\alpha & -1 \\ -\rho^{-1}\sin\alpha & 0 \end{bmatrix} \begin{bmatrix} -k_\rho \rho \\ -k_\alpha \alpha - k_\beta \beta \end{bmatrix}$$

To figure out stability, we will linearize the equations above and use the Eigen-value problem. The linearization equation is given as follows:

$$\dot{\rho} \approx f(\rho_o, \alpha_o) + \rho \frac{\partial f}{\partial \rho}(\rho_o, \beta_o) + \alpha \frac{\partial f}{\partial \alpha}(\rho_o, \beta_o)$$

where, $f(\rho, \alpha) = k_\rho \rho \cos\alpha$, $(\rho_o, \beta_o) = (0, 0)$

Hence we obtain the following approximation near the origin:

$$\dot{\rho} = k_\rho \rho$$

Under similar procedures, the other approximations become:

$$\dot{\beta} = (k_\alpha - k_\rho)\alpha + k_\beta \beta$$

$$\dot{\alpha} = k_\rho \alpha$$

Putting all the above into matrix form, we obtain:

$$\begin{bmatrix} \dot{\rho} \\ \dot{\alpha} \\ \dot{\beta} \end{bmatrix} = \begin{bmatrix} k_\rho & 0 & 0 \\ 0 & k_\alpha - k_\rho & k_\beta \\ 0 & k_\rho & 0 \end{bmatrix} \begin{bmatrix} \rho \\ \alpha \\ \beta \end{bmatrix}$$

Hence, this becomes an Eigen-value problem. As we have a 3x3 matrix, we use Cramer's rule in finding the determinant for the following matrix:

$$\begin{bmatrix} k_\rho - \lambda & 0 & 0 \\ 0 & k_\alpha - k_\rho - \lambda & k_\beta \\ 0 & k_\rho & -\lambda \end{bmatrix}$$

In order to ensure stability, all Eigen-values must be negative. Hence,

$$k_\rho < 0$$

$$k_\alpha - k_\rho < 0$$

$$k_\beta k_\rho < 0$$