



Robotics 2

Robots with kinematic redundancy

Part 2: Extensions

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A general task priority formulation

- consider a large number p of tasks to be executed at best and with strict priorities by a robotic system having many dofs
- everything should run efficiently in real time, with possible addition, deletion, swap, or reordering of tasks
- a recursive formulation that reduces computations is convenient

$$\dot{q} \in \mathbb{R}^n \quad \dot{r}_k \in \mathbb{R}^{m_k} \quad \dot{r}_k = J_k(q)\dot{q} \quad k = 1, \dots, p$$

k -th task

$$P_k(q) = I - J_k^\#(q)J_k(q)$$

projector in the null-space of k -th task

$i < j \Rightarrow$ task i has higher priority than task j

$$\sum_{k=1}^p m_k = m (\leq n)$$

even larger!

$$\dot{r}_{A,k} = \begin{pmatrix} \dot{r}_1 \\ \dot{r}_2 \\ \vdots \\ \dot{r}_k \end{pmatrix} \quad J_{A,k} = \begin{pmatrix} J_1 \\ J_2 \\ \vdots \\ J_k \end{pmatrix}$$

stack of first k tasks

augmented Jacobian
of first k tasks

$$P_{A,k} = I - J_{A,k}^\# J_{A,k}$$

projector in the null-space of the augmented Jacobian of the first k tasks

$$J_i P_{A,k} = O \quad \forall i \leq k$$

$\iff J_{A,k} P_{A,k} = O$



Recursive solution with priorities - 1

- start with the first task and **reformulate** the problem so as to provide **always** a “solution”, at least in terms of **minimum error norm**

for $k = 1$

$$\begin{cases} \dot{\mathbf{q}}_1 = \arg \min_{\dot{\mathbf{q}} \in \mathbb{R}^n} \frac{1}{2} \|\dot{\mathbf{q}}\|^2 \\ \text{s.t. } J_1 \dot{\mathbf{q}} = \dot{\mathbf{r}}_1 \end{cases} \xrightarrow{\quad} \begin{cases} \dot{\mathbf{q}}_1 = \arg \min_{\dot{\mathbf{q}} \in \mathcal{S}_1} \frac{1}{2} \|\dot{\mathbf{q}}\|^2 \\ \mathcal{S}_1 = \left\{ \arg \min_{\dot{\mathbf{q}} \in \mathbb{R}^n} \frac{1}{2} \|J_1 \dot{\mathbf{q}} - \dot{\mathbf{r}}_1\|^2 \right\} \end{cases}$$

$$\xrightarrow{\quad} \dot{\mathbf{q}}_1 = J_1^\# \dot{\mathbf{r}}_1 \quad \xrightarrow{\quad} \mathcal{S}_1 = \{\dot{\mathbf{q}}_1 + \mathbf{P}_1 v_1, v_1 \in \mathbb{R}^n\}$$

for $k = 2$

$$\begin{cases} \dot{\mathbf{q}}_2 = \arg \min_{\dot{\mathbf{q}} \in \mathcal{S}_2} \frac{1}{2} \|\dot{\mathbf{q}}\|^2 \\ \mathcal{S}_2 = \left\{ \arg \min_{\dot{\mathbf{q}} \in \mathcal{S}_1} \frac{1}{2} \|J_2 \dot{\mathbf{q}} - \dot{\mathbf{r}}_2\|^2 \right\} \end{cases} \xrightarrow{\quad} \begin{aligned} \dot{\mathbf{q}}_2 &= \dot{\mathbf{q}}_1 + (J_2 \mathbf{P}_1)^\# (\dot{\mathbf{r}}_2 - J_2 \dot{\mathbf{q}}_1) \\ \mathcal{S}_2 &= \{\dot{\mathbf{q}}_2 + \mathbf{P}_{A,2} v_2, v_2 \in \mathbb{R}^n\} \end{aligned}$$



Recursive solution with priorities - 2

generalizing to step k

\dot{q}_{k-1}
prioritized solution
up to task $k - 1$

LQ problem
for k -th task

recursive formula
(Siciliano, Slotine:
ICAR 1991)

$$\dot{q}_k = \dot{q}_{k-1} + (J_k P_{A,k-1})^\# (r_k - J_k \dot{q}_{k-1})$$

prioritized
solution
up to task k

over the steps, the search set
is progressively reduced

$$\mathcal{S}_{k-1} = \{\dot{q}_{k-1} + P_{A,k-1} v_{k-1}, v_{k-1} \in \mathbb{R}^n\}$$

set of all solutions up to task $k - 1$

$$\left\{ \begin{array}{l} \dot{q}_k = \arg \min_{\dot{q} \in \mathcal{S}_k} \frac{1}{2} \|\dot{q}\|^2 \\ \mathcal{S}_k = \left\{ \arg \min_{\dot{q} \in \mathcal{S}_{k-1}} \frac{1}{2} \|J_k \dot{q} - r_k\|^2 \right\} \end{array} \right.$$

initialization

$$\begin{aligned} \dot{q}_0 &= 0 \\ P_{A,0} &= I \end{aligned}$$

correction needed when
the solution up to task $k - 1$
is not satisfying also task k

$$\Leftrightarrow \mathbb{R}^n = \mathcal{S}_0 \supseteq \mathcal{S}_1 \supseteq \dots \supseteq \mathcal{S}_{p-1} \supseteq \mathcal{S}_p$$



Recursive solution with priorities

properties and implementation

- the solution considering the first k tasks with their priority

$$\dot{\mathbf{q}}_k = \dot{\mathbf{q}}_{k-1} + (\mathbf{J}_k \mathbf{P}_{A,k-1})^\# (\dot{\mathbf{r}}_k - \mathbf{J}_k \dot{\mathbf{q}}_{k-1})$$

satisfies also ("does not perturb") the previous $k - 1$ tasks

$$\mathbf{J}_{A,k-1} \dot{\mathbf{q}}_k = \mathbf{J}_{A,k-1} \dot{\mathbf{q}}_{k-1}$$

since

$$\mathbf{J}_{A,k-1} (\mathbf{J}_k \mathbf{P}_{A,k-1})^\# = \underbrace{\mathbf{J}_{A,k-1} \mathbf{P}_{A,k-1}}_{=} \underbrace{(\mathbf{J}_k \mathbf{P}_{A,k-1})^\#}_{= \circ} = \mathbf{O}$$

(Maciejewski, Klein: IJRR 1985): check the four defining properties of a pseudoinverse

- recursive expression also for the null-space projector

$$\boxed{\mathbf{P}_{A,k} = \mathbf{P}_{A,k-1} - (\mathbf{J}_k \mathbf{P}_{A,k-1})^\# \mathbf{J}_k \mathbf{P}_{A,k-1}}$$

$$\mathbf{P}_{A,0} = \mathbf{I}$$

(Baerlocher, Boulic: IROS 1998): for the proof, see Appendix A

- when the k -th task is (*close to be*) incompatible with the previous ones (**algorithmic singularity**), use "DLS" instead of "#" in k -th solution...



A list of extensions

(some still on-going research)

- up to now, only “basic” redundancy resolution schemes
 - defined at **first-order** differential level (velocity)
 - it is possible to work in **acceleration**
 - useful for obtaining **smoother** motion
 - allows including the consideration of **dynamics**
 - seen within a **planning**, not a **control** perspective
 - take into account and recover errors in task execution by using **kinematic control** schemes
 - applied to robot manipulators with **fixed base**
 - extend to **wheeled mobile manipulators**
 - tasks specified only by **equality constraints**
 - add also **linear inequalities** in a complete QP formulation
 - very common also for **humanoid robots** in multiple tasks
 - consider **hard limits** in joint/command space



Resolution at acceleration level

$$r = f(q) \rightarrow \dot{r} = J(q)\dot{q} \rightarrow \ddot{r} = J(q)\ddot{q} + \dot{J}(q)\dot{q}$$

- rewritten in the form

$$J(q)\ddot{q} = \ddot{r} - \dot{J}(q)\dot{q} \triangleq \ddot{x}$$

to be chosen given
 (at time t) known q, \dot{q}
 (at time t)

$$\begin{aligned} & \min_{\ddot{q}} \frac{1}{2} \|\ddot{q} - \ddot{q}_0\|^2 = \frac{1}{2} (\ddot{q} - \ddot{q}_0)^T (\ddot{q} - \ddot{q}_0) \\ & \text{s.t. } J\ddot{q} = \ddot{x} \quad (= \ddot{r} - \dot{J}\dot{q}) \\ & \ddot{q}_0 = -K_D \dot{q} \quad K_D \text{ diag } > 0 \\ & \ddot{q} = -K_D \dot{q} + J^*(\ddot{x} + J K_D \dot{q}) \end{aligned}$$

the problem is formally equivalent to the previous one,
with **acceleration** in place of velocity commands

- for instance, in the null-space method

$$\ddot{q} = J^*(q)\ddot{x} + (I - J^*(q)J(q))\ddot{q}_0$$

solution with **minimum acceleration** norm $\|\ddot{q}\|^2$

needed
to **damp/stabilize**
self-motions
in the null space
($K_D > 0$)



Dynamic redundancy resolution

- dynamic model of a robot manipulator (more later!)

$$M(q)\ddot{q} + n(q, \dot{q}) = \tau$$

\uparrow

$N \times N$ symmetric
inertia matrix,
positive definite for all q

\uparrow

input torque vector
(provided by the motors)

\uparrow

Coriolis/centrifugal vector $c(q, \dot{q})$
+ gravity vector $g(q)$

$$J(q)\ddot{q} = \ddot{x} (= \ddot{r} - j(q)\dot{q})$$

\uparrow

M -dimensional acceleration task

- we can formulate and solve interesting dynamic problems in the general framework of LQ optimization^(o)
 - closed-form expressions can be obtained by the solution formula^(o) (assuming a full rank Jacobian J)

^(o) in block *Kinematic redundancy - Part 1*, slide #28



Dynamic redundancy resolution

as Linear-Quadratic optimization problems

min $\quad 2:07:00$

- typical **dynamic** objectives to be **locally minimized** at (q, \dot{q})

torque norm

$$H_1(\ddot{q}) = \frac{1}{2} \|\tau\|^2 = \frac{1}{2} \ddot{q}^T M^2(q) \ddot{q} + n^T(q, \dot{q}) M(q) \ddot{q} + \frac{1}{2} n^T(q, \dot{q}) n(q, \dot{q})$$

(squared inverse inertia weighted) torque norm

$$\begin{aligned} H_2(\ddot{q}) &= \frac{1}{2} \|\tau\|_{M^{-2}}^2 = \frac{1}{2} \tau^T M^{-2}(q) \tau \\ &= \frac{1}{2} \ddot{q}^T \ddot{q} + n^T(q, \dot{q}) M^{-1}(q) \ddot{q} + \frac{1}{2} n^T(q, \dot{q}) M^{-2}(q) n(q, \dot{q}) \end{aligned}$$

(inverse inertia weighted) torque norm

$$\begin{aligned} H_3(\ddot{q}) &= \frac{1}{2} \|\tau\|_{M^{-1}}^2 = \frac{1}{2} \tau^T M^{-1}(q) \tau \\ &= \frac{1}{2} \ddot{q}^T M(q) \ddot{q} + n^T(q, \dot{q}) \ddot{q} + \frac{1}{2} n^T(q, \dot{q}) M^{-1}(q) n(q, \dot{q}) \end{aligned}$$



Closed-form solutions

minimum torque norm solution

$$\frac{1}{2} \|\tau\|^2 \rightarrow \tau_1 = (J(q)M^{-1}(q))^{\#}(\ddot{r} - \dot{j}(q)\dot{q} + J(q)M^{-1}(q)n(q, \dot{q}))$$

- good for **short** trajectories (in fact, it is still only a “local” solution!)
- for **longer** trajectories it leads to torque “oscillation/explosion” (**whipping** effect)

minimum (squared inverse inertia weighted) torque norm solution

$$\frac{1}{2} \|\tau\|_{M^{-2}}^2 \rightarrow \tau_2 = M(q)J^{\#}(q)(\ddot{r} - \dot{j}(q)\dot{q} + J(q)M^{-1}(q)n(q, \dot{q}))$$

- good performance in general, to be **preferred**

minimum (inverse inertia weighted) torque norm solution

$$\frac{1}{2} \|\tau\|_{M^{-1}}^2 \rightarrow \tau_3 = J^T(q)(J(q)M^{-1}(q)J^T(q))^{-1}(\ddot{r} - \dot{j}(q)\dot{q} + J(q)M^{-1}(q)n(q, \dot{q}))$$

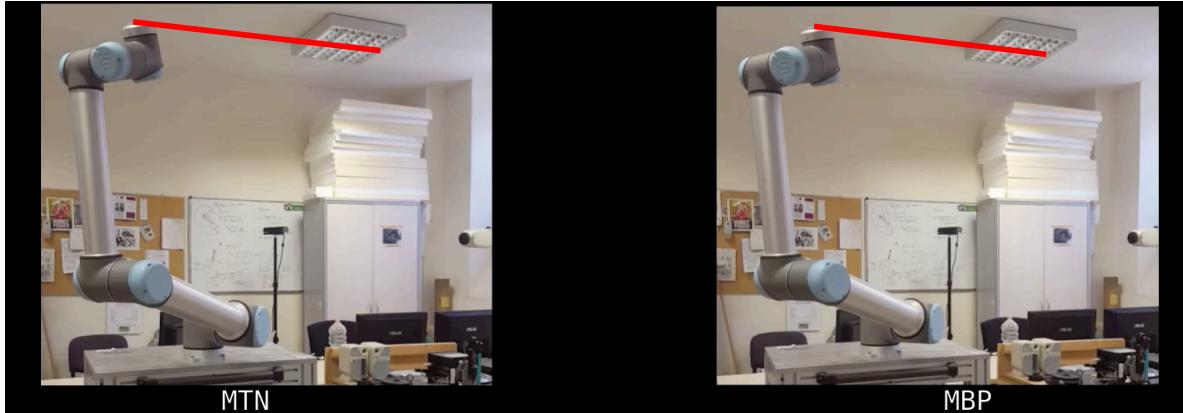
- a solution with a **leading $J^T(q)$** term: what is its nice physical interpretation?

May we add terms in a (dynamic) null space? Easy to do in the LQ framework!



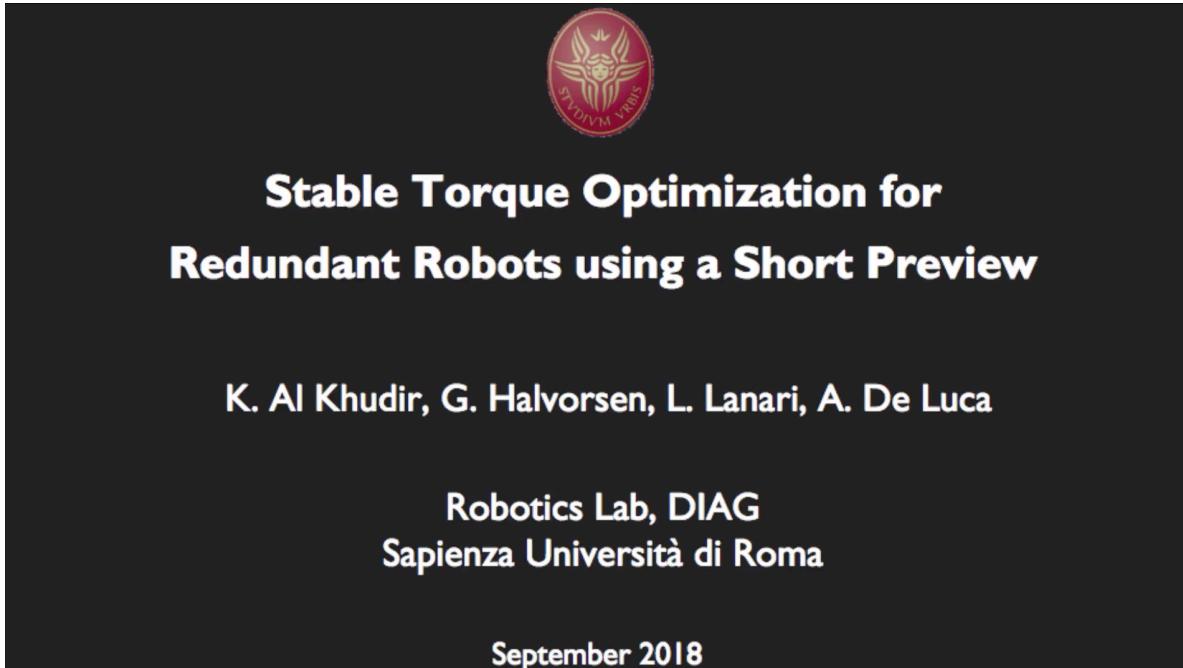
Stabilizing the minimum torque solution

Universal
Robots
UR-10
(6-dof)



video

KUKA
LRW 4
(7-dof,
last joint
not used)



video

$$\min \frac{1}{2} \|\tau\|^2 = \text{MTN}$$

versus

- MBP = minimizing torque also at a short preview instant
- MTND = damping joint velocity in the null space
- MBPD = ... do both

IEEE Robotics and
Automation Lett. 2019



Kinematic control

- given a desired M -dimensional task $r_d(t)$, in order to recover a task error $e = r_d - r$ due to initial mismatch or due to
 - disturbances
 - inherent linearization error in using the Jacobian (first-order motion)
 - discrete-time implementation

we need to “close” a **feedback loop on task execution**, by replacing (with diagonal matrix gains $K > 0$ or $K_P, K_D > 0$)

$$\dot{r} \rightarrow \dot{r}_d + K(r_d - r) \quad \text{in velocity-based...}$$

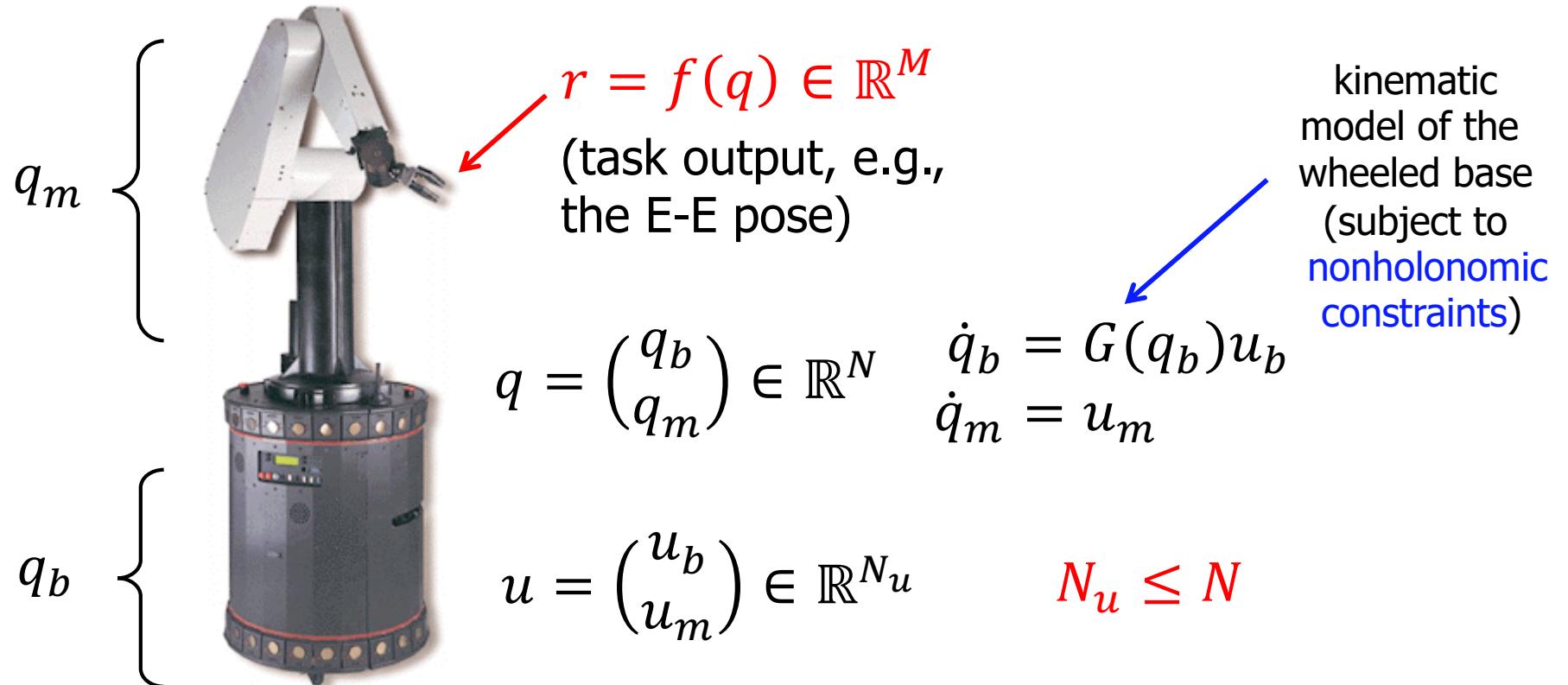
$$\ddot{r} \rightarrow \ddot{r}_d + K_D(\dot{r}_d - \dot{r}) + K_P(r_d - r) \quad \dots \text{in acceleration-based methods}$$

where $r = f(q)$, $\dot{r} = J(q)\dot{q}$



Mobile manipulators

- coordinates: q_b of the base and q_m of the manipulator
- differential map: from available commands u_b on the mobile base and u_m on the manipulator to task output velocity





Mobile manipulator Jacobian

$$r = f(q) = f(q_b, q_m)$$

$$\dot{r} = \frac{\partial f(q)}{\partial q_b} \dot{q}_b + \frac{\partial f(q)}{\partial q_m} \dot{q}_m = J_b(q)\dot{q}_b + J_m(q)\dot{q}_m$$

$$= J_b(q)G(q_b)u_b + J_m(q)u_m = (J_b(q)G(q_b) \quad J_m(q)) \begin{pmatrix} u_b \\ u_m \end{pmatrix}$$

$$= \boxed{J_{NMM}(q)u}$$

Nonholonomic Mobile Manipulator (NMM)
Jacobian ($M \times N_u$)

- ... most previous results follow by just replacing

$$J \Rightarrow J_{NMM} \quad \dot{q} \Rightarrow u \quad (\text{redundancy if } N_u - M > 0)$$

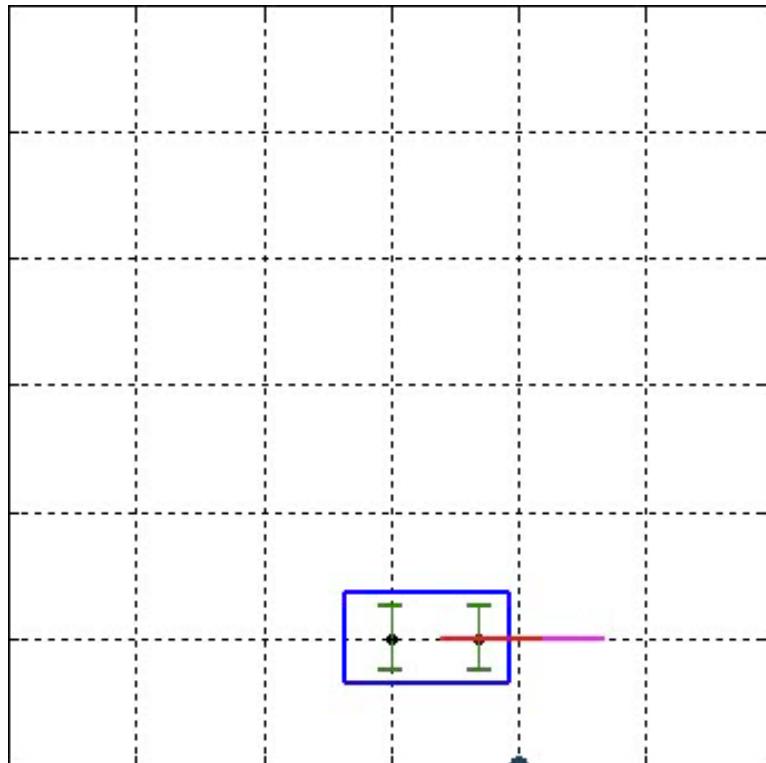


namely, the
available velocity commands



Mobile manipulators

video



car-like+2R planar arm

($N = 6, N_u = 4$):

E-E trajectory control on a line ($N_u - M = 2$)
with maximization of J_{NMM} manipulability

Automatica Fair 2008



video

wheeled Justin with centered
steering wheels

($N = 3 + 4 \times 2, N_u = 8$)
“dancing” in controlled
but otherwise passive mode



Quadratic Programming (QP)

with equality and inequality constraints

- minimize a **quadratic** objective function (typically positive definite, like when using norms of vectors) subject to **linear** equality and inequality constraints, all expressed in terms of **joint velocity** commands

$$J\dot{q} = \dot{r} \quad C\dot{q} \leq d \quad \dot{q} \in \Omega \subseteq \mathbb{R}^n$$

within a given **convex** set

solution set, with **only equality** constraints

$$\mathcal{S}_{eq} = \arg \min_{\dot{q} \in \Omega} \frac{1}{2} \|J\dot{q} - \dot{r}\|^2$$

given $\dot{q}^* \in \mathcal{S}_{eq}$ $\Rightarrow \mathcal{S}_{eq} = \{\dot{q} \in \Omega : J\dot{q} = J\dot{q}^*\}$

solution set, with **only inequality** constraints

$$\mathcal{S}_{ineq} = \arg \min_{\dot{q} \in \Omega} \frac{1}{2} \|w\|^2$$

s.t. $C\dot{q} - d \leq w \quad w \in \mathbb{R}_+^m$
(non-negative) **slack** variables

given $\dot{q}^* \in \mathcal{S}_{ineq}$ $\Rightarrow \mathcal{S}_{ineq} = \Omega \cap \begin{cases} c_j^T \dot{q} \leq d_j, & \text{if } c_j^T \dot{q}^* \leq d_j \\ c_j^T \dot{q} = c_j^T \dot{q}^*, & \text{if } c_j^T \dot{q}^* > d_j \end{cases}$

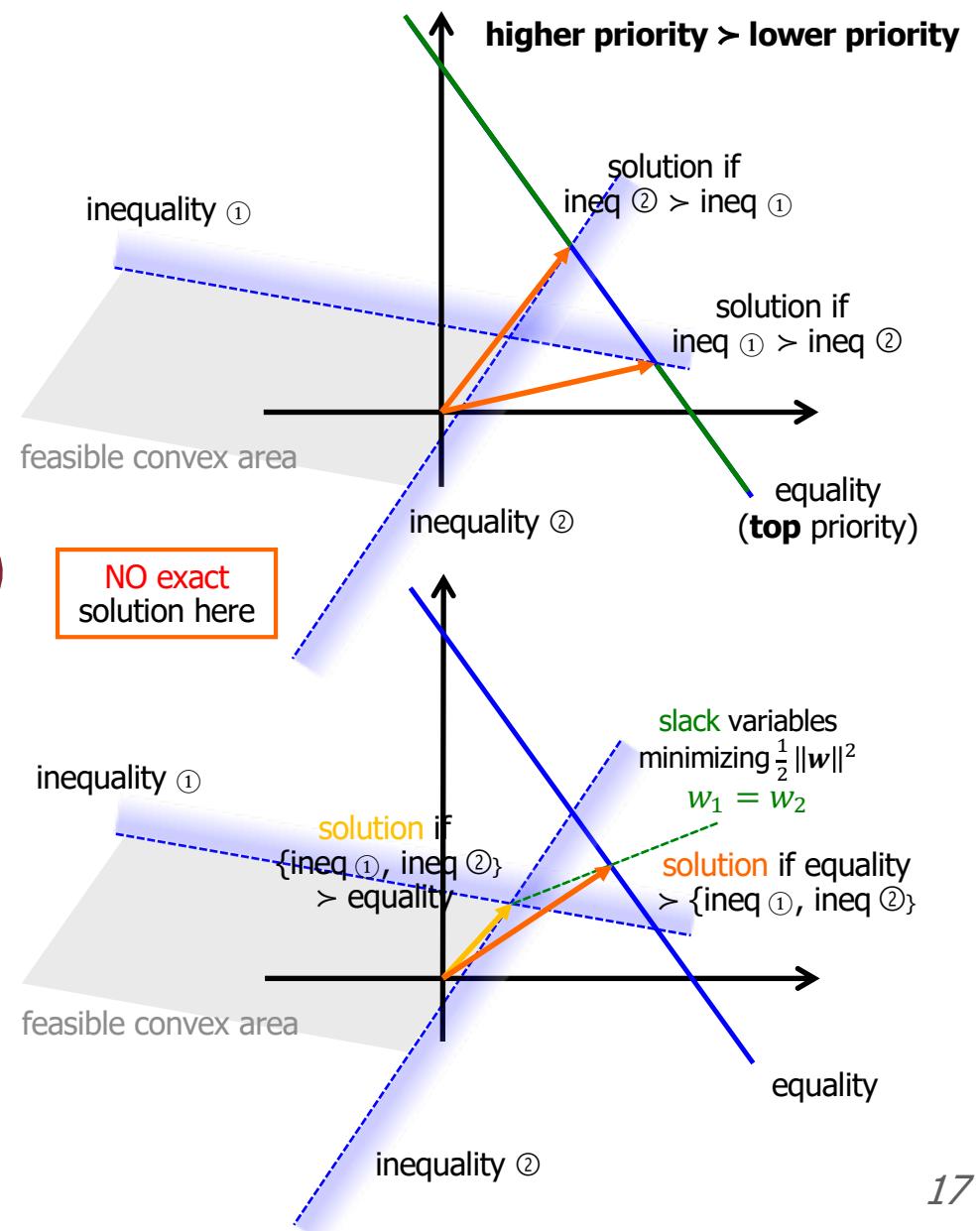
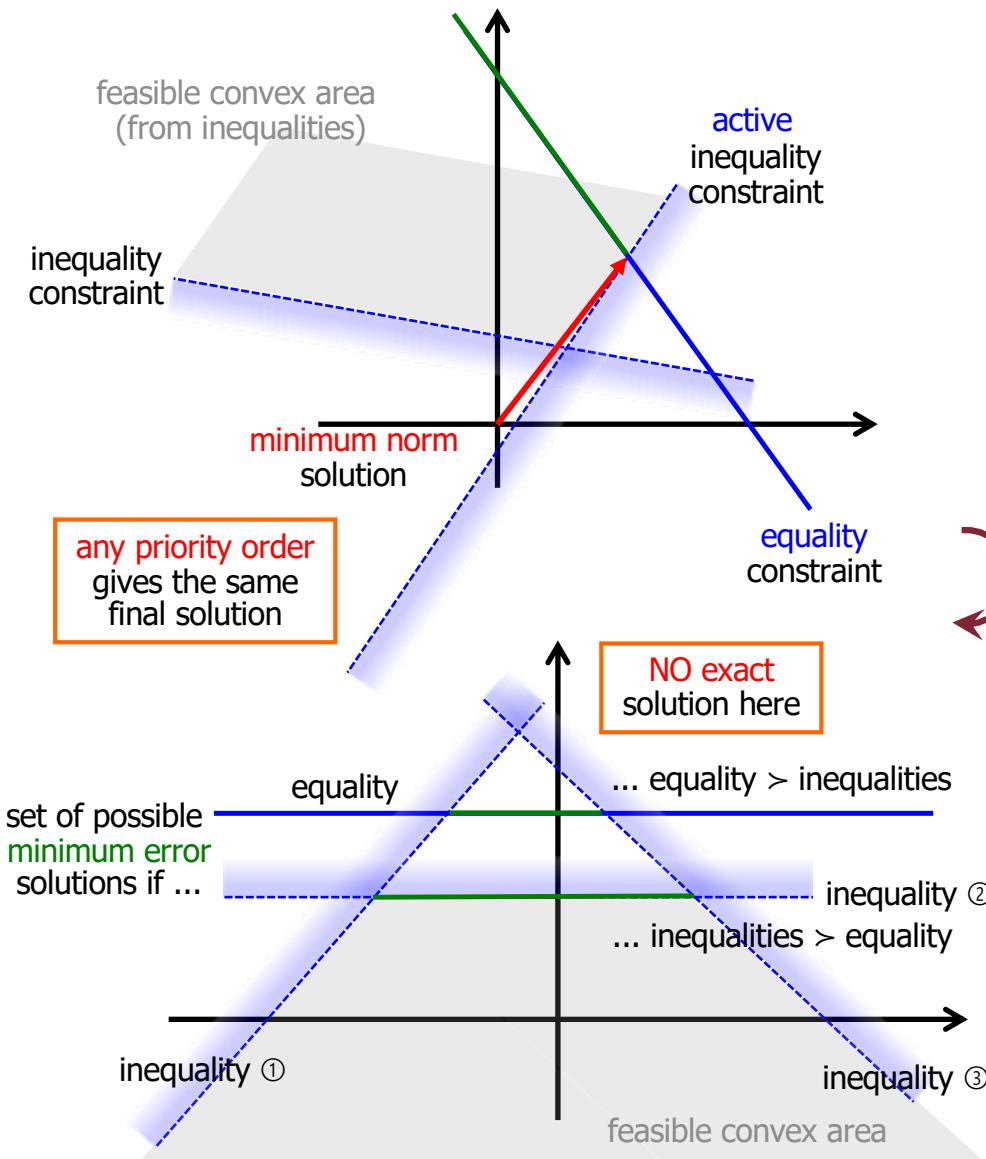
QP complete formulation

$$\begin{aligned} & \min_{\dot{q} \in \Omega} \frac{1}{2} \|J\dot{q} - \dot{r}\|^2 + \frac{1}{2} \|w\|^2 \\ \text{s.t. } & C\dot{q} - w \leq d \quad w \in \mathbb{R}_+^m \end{aligned}$$

(possibly with prioritization
of constraints)



Equality and inequality linear constraints



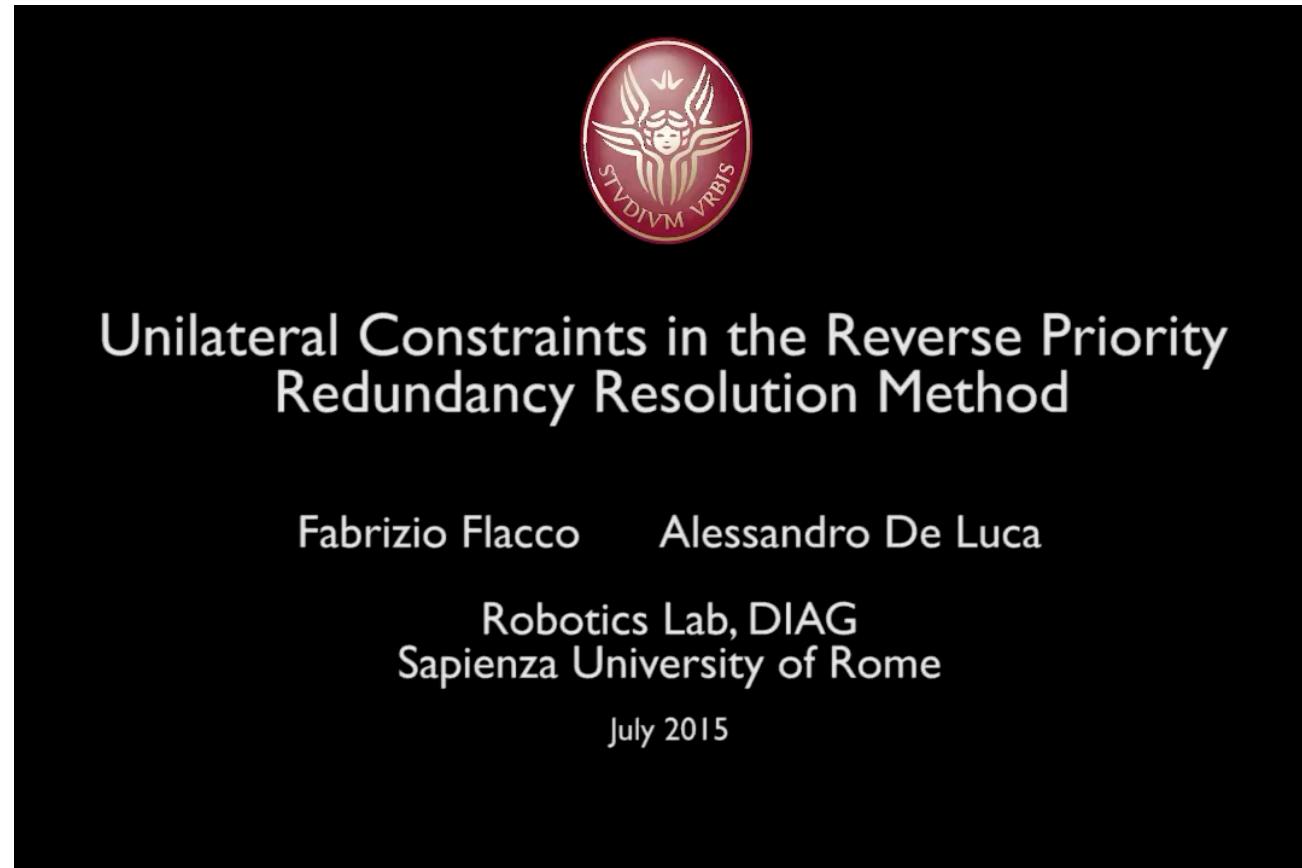


Equality and Inequality Tasks

6R planar robot (simulations) and 7R KUKA LWR (experiment)

- an efficient **task priority** approach, with simultaneous inequality tasks handled as **hard** (cannot be violated) or **soft** (can be relaxed) constraints

[video](#)



IEEE/RSJ Int. Conf. on Intelligent Robots and Systems (IROS) 2015



Equality and Inequality Tasks

for the high-dof humanoid robot HRP2

- a systematic **task priority** approach, with several simultaneous tasks

video

Prioritizing linear equality and
inequality systems: application to local
motion planning for redundant robots.

*Oussama Kanoun, Florent Lamiraux,
Pierre-Brice Wieber, Fumio Kanehiro,
Eiichi Yoshida and Jean-Paul Laumond*

in **any order** of priority

- avoid the obstacle
 - gaze at the object
 - reach the object
 - ...
- while **keeping balance!**



all subtasks are **locally**
expressed by linear
equalities or **inequalities**
(possibly relaxed
when needed)
on **joint velocities**

IEEE Int. Conf. on Robotics and Automation (ICRA) 2009

Inclusion of hard limits in joint space

Saturation in the Null Space (SNS) method



- robot has “limited” capabilities: **hard limits** on joint ranges and/or on joint motion or commands (max velocity, acceleration, torque)
 - represented as **box inequalities** that can **never** be violated (at most, **active** constraints or **saturated** commands) – kept separated from “stack” of tasks
 - (equality) tasks are usually executed in full (with priorities, if desired), but can be relaxed (**scaled**) in case of need (i.e., when robot capabilities are used at their limits)
- $\begin{matrix} (-\dot{q}_{\min}, \dot{q}_{\max}) \\ \dot{q}_{\min} \leq \dot{q} \leq \dot{q}_{\max} \end{matrix}$ Joint at absolute limit
 $\begin{matrix} q_{\min} \leq q \leq q_{\max} \\ q_{\min} < q < q_{\max} \end{matrix}$ Joint is not saturated
- $\ddot{q}_S = \ddot{r}_S \text{ with } s \in [0,1]$
 \downarrow
 The direction of motion is being preserved, only the intensity is being scaled
 Only valid when there's no solution at all
- $\Rightarrow \ddot{q} = J^T S \dot{x}$
- ↓
- saturate **one overdriven joint command at a time**, until a feasible and better performing solution is found \Rightarrow **Saturation in the Null Space = SNS**
 - on-line decision:** which joint commands to saturate and **how**, so that this does not affect task execution
 - for tasks that are (certainly) not feasible, SNS **embeds** the selection of a task scaling factor **preserving execution of the task direction** with **minimal scaling**

$$\dot{q}_{SNS} = (JW)^{\#} s \dot{x} + \left(I - (JW)^{\#} J \right) \dot{q}_N$$

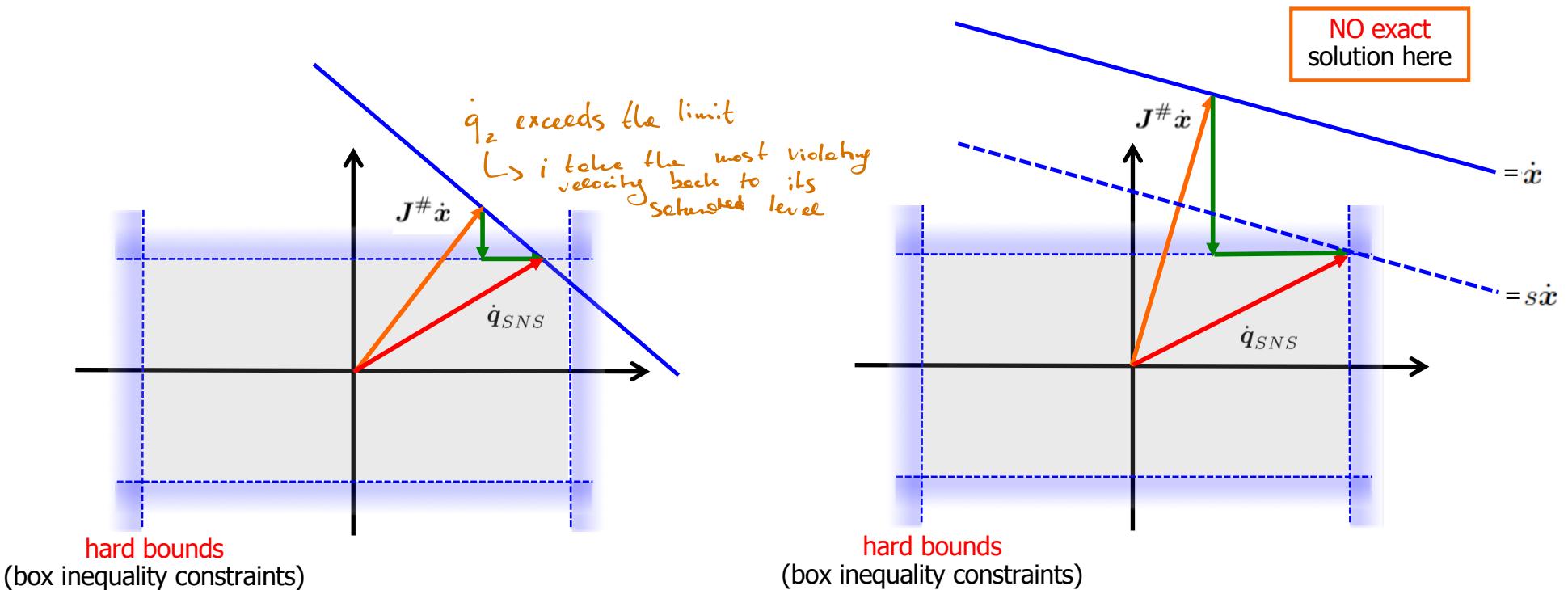
\uparrow scaling factor \uparrow diagonal 0/1 matrix \leftarrow contains saturated joint velocities

Task scaling means preserving geometry of the task, but the execution will be slower



Geometric view on SNS operation

in the space of joint velocity commands

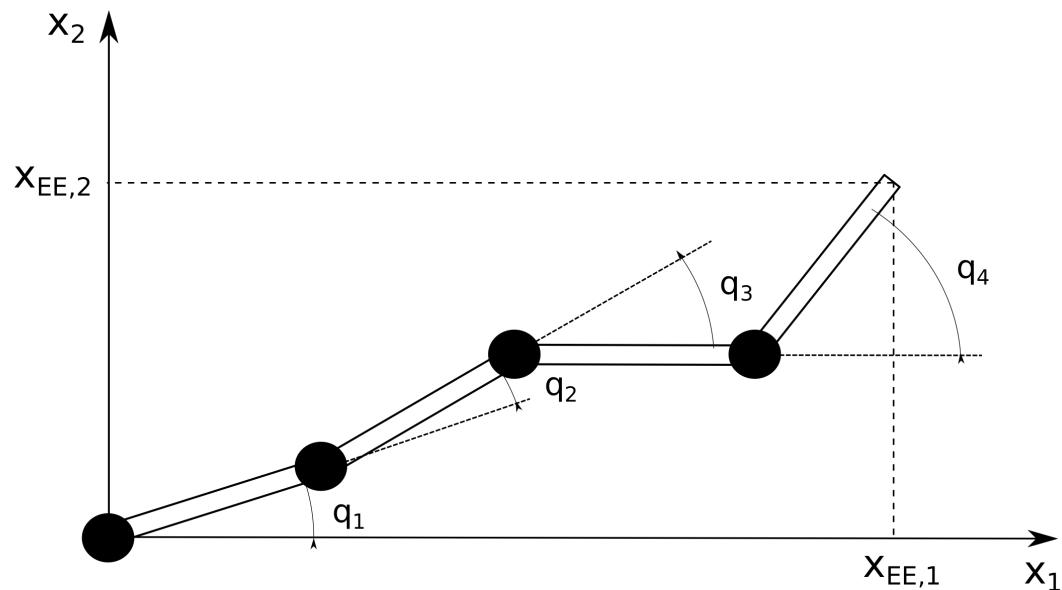


the total correction to the original pseudoinverse solution
is always in the **null space** of the Jacobian (up to task scaling, if present)



Illustrative example - 1

consider a 4R robot with equal links of unitary length



task: end-effector Cartesian position

$$\boldsymbol{x} = (x_{EE,1} \ x_{EE,2})$$

manipulator configuration

$$\boldsymbol{q} = (q_1 \ q_2 \ q_3 \ q_4)$$

differential map

$$\dot{\boldsymbol{x}} = \boldsymbol{J}(\boldsymbol{q})\dot{\boldsymbol{q}}$$

desired Cartesian velocity $\dot{\boldsymbol{x}} \in \mathcal{R}^2$

commanded joint velocity $\dot{\boldsymbol{q}} \in \mathcal{R}^4$

task Jacobian

$$\boldsymbol{J}(\boldsymbol{q}) = \begin{pmatrix} -lS_1 - lS_{12} - lS_{123} - lS_{1234} & -lS_{12} - lS_{123} - lS_{1234} & -lS_{123} - lS_{1234} & -lS_{1234} \\ lC_1 + lC_{12} + lC_{123} + lC_{1234} & lC_{12} + lC_{123} + lC_{1234} & lC_{123} + lC_{1234} & lC_{1234} \end{pmatrix}$$

velocity limits $|\dot{q}_i| \leq V_i, i = 1 \dots 4$

$V_1 = V_2 = 2 \quad V_3 = V_4 = 4 \text{ [rad/s]}$

$$\dot{q}_{sus} =$$

$$= \dot{q}_v + (\Im\omega)^\# (s^x -) \dot{q}_v$$



Schuntet

$$s = 1$$



$$\dot{q}_v$$



$$\Im\ddot{q}_v = \Im\omega v_1$$

$$W = \begin{pmatrix} 0 & & & \\ & 1 & & \\ & & 1 & \\ & & & 1 \end{pmatrix}$$

$$\dot{q}_v = \begin{pmatrix} v_1 \\ 0 \\ 0 \\ 0 \end{pmatrix}$$

$$\Im\omega = \begin{pmatrix} 0 & \vdots & \Im_2 & \Im_3 & \Im_4 \\ \vdots & & & & \end{pmatrix}$$

$$(\Im\omega)^\# = \begin{pmatrix} 0 \\ (\Im_2 \Im_3 \Im_4)^\# \end{pmatrix}$$

Suppose that we discover that
actually V_4 has bound 3.5 and not 4

$$|\dot{q}_4| \leq 3.5 \Rightarrow \text{let } \ddot{q}_4 = -3.5$$

$$\dot{x}_{sns} = \dot{x} - J_1 V_1 + J_4 V_4 = \begin{bmatrix} -4 \\ -1.5 \end{bmatrix} - \begin{bmatrix} -2 \\ 2 \end{bmatrix} 2 + \begin{bmatrix} 0 \\ 1 \end{bmatrix} 3.5 = \begin{bmatrix} 0 \\ -2 \end{bmatrix}$$

The rest becomes

$$\hookrightarrow w = \begin{pmatrix} 0 & 1 & 1 & 0 \end{pmatrix}$$

$$\ddot{q}_{sns} = (2 \ -2 \ 2 \ -3.5) \leq \begin{pmatrix} \dot{q}_2 \\ \dot{q}_3 \end{pmatrix} = \begin{pmatrix} -2 \\ 2 \end{pmatrix}.$$

$$\dot{x}_{sns} = (J_2 \ J_3) \begin{pmatrix} \dot{q}_2 \\ \dot{q}_3 \end{pmatrix} = \begin{pmatrix} -1 & -1 \\ 2 & 1 \end{pmatrix} \begin{pmatrix} \dot{q}_2 \\ \dot{q}_3 \end{pmatrix}$$

By chance, this unique final solution is feasible for all joints. If that were not the case, we would have had to scale the task. That's because in that particular case we have a 4dof robot for a 2dim task, which means the null space is 2dim, which means we can freely "modify" the task velocity vector with max other two vectors.



Illustrative example - 2

current configuration $\mathbf{q} = (\pi/2 \quad -\pi/2 \quad \pi/2 \quad -\pi/2)^T$

associated Jacobian $\mathbf{J} = (J_1 \quad J_2 \quad J_3 \quad J_4) = \begin{pmatrix} -2 & -1 & -1 & 0 \\ 2 & 2 & 1 & 1 \end{pmatrix}$

desired end-effector velocity $\dot{\mathbf{x}} = (-4 \quad -1.5)^T$

The columns of the jacobian are related to each joint velocity, so if i saturate joint i vel, J_i will be affected

$$\dot{\mathbf{q}}_{PS} = \mathbf{J}^\# \dot{\mathbf{x}} = (2.4545 \quad 2.0 \quad -2.0 \quad 1.2273 \quad -3.3636)^T$$

direct (velocity =) task scaling? $s = 0.8148$

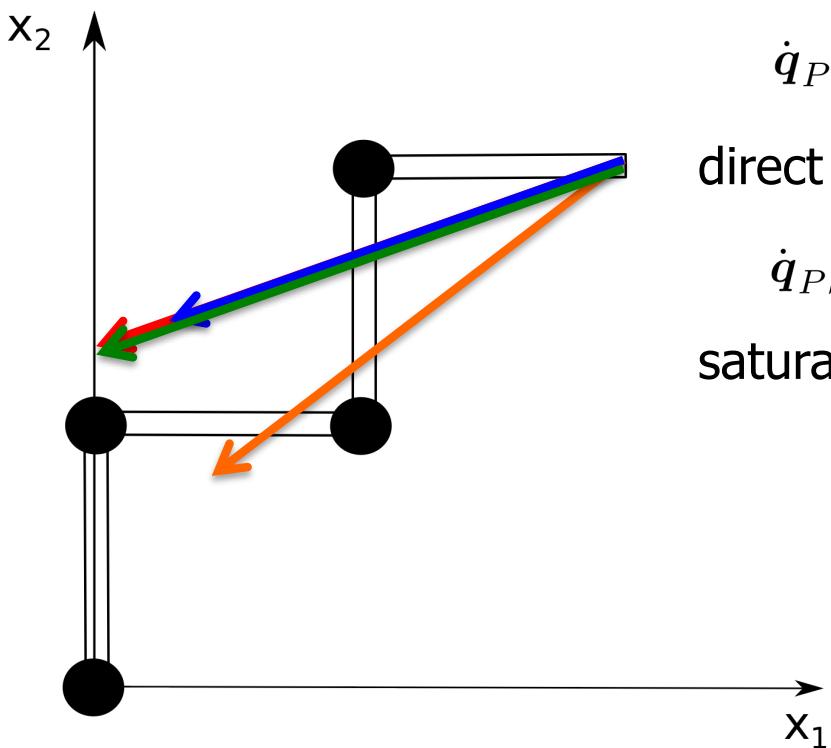
$$\dot{\mathbf{q}}_{PS} = s \mathbf{J}^\# \dot{\mathbf{x}} = (2.0 \quad -1.74 \quad 1.0 \quad -2.74)^T$$

saturating **only** the **most violating** velocity? $\dot{q}_1 = V_1 = 2$

$$\dot{\mathbf{x}}_{SNS} = \dot{\mathbf{x}} - J_1 V_1 = (J_2 \quad J_3 \quad J_4) \begin{pmatrix} \dot{q}_2 \\ \dot{q}_3 \\ \dot{q}_4 \end{pmatrix}$$

$$\dot{\mathbf{q}}_{SNS} = \left(V_1 \quad [(J_2 \quad J_3 \quad J_4)^\# \dot{\mathbf{x}}_{SNS}]^T \right)^T$$

$$= (2 \quad -1.8333 \quad 1.8333 \quad -3.6667)^T$$





Joint velocity bounds

joint space
limits

$$\begin{aligned} Q_{min,i} &\leq q_i \leq Q_{max,i} \\ -V_{max,i} &\leq \dot{q}_i \leq V_{max,i} \quad i = 1, \dots, n \\ -A_{max,i} &\leq \ddot{q}_i \leq A_{max,i} \end{aligned}$$

joint velocity bounds

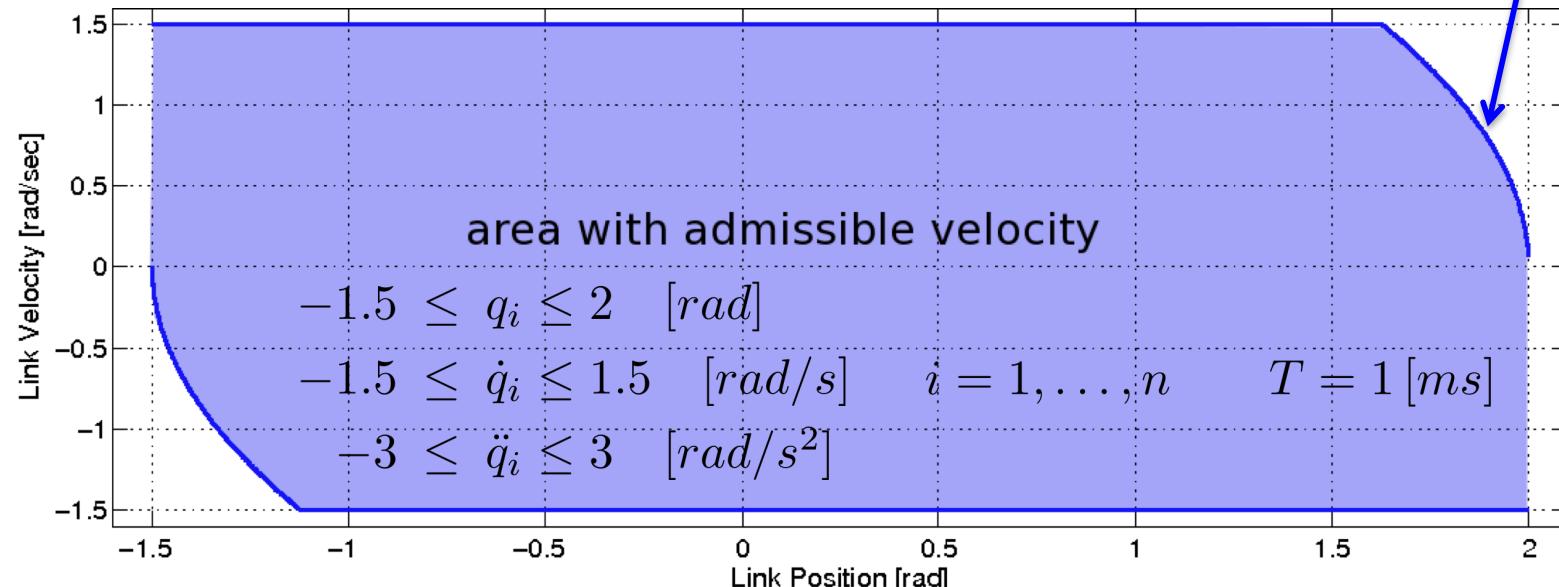
$$\dot{\mathbf{Q}}_{min}(t_k) \leq \dot{\mathbf{q}} \leq \dot{\mathbf{Q}}_{max}(t_k)$$

conversion: control sampling (piece-wise constant velocity commands) + max feasible velocities and decelerations to stay/stop within the joint range

$$\begin{aligned} \dot{Q}_{min,i} &= \max \left\{ \frac{Q_{min,i} - q_{k,i}}{T}, -V_{max,i}, -\sqrt{2A_{max,i}(q_{k,i} - Q_{min,i})} \right\} \\ \dot{Q}_{max,i} &= \min \left\{ \frac{Q_{max,i} - q_{k,i}}{T}, V_{max,i}, \sqrt{2A_{max,i}(Q_{max,i} - q_{k,i})} \right\} \end{aligned}$$

min 1.09.50

smooth velocity bound “anticipates” the reaching of a hard limit





SNS at velocity level

Algorithm 1

$W = I$, $\dot{q}_N = \mathbf{0}$, $s = 1$, $s^* = 0$

repeat

 limit_exceeded = FALSE

$\bar{q} = \dot{q}_N + (JW)^\# (\dot{x} - J\dot{q}_N)$

 if $\left\{ \begin{array}{l} \exists i \in [1:n] : \\ \dot{\bar{q}}_i < \dot{Q}_{min,i} \text{ OR } \dot{\bar{q}}_i > \dot{Q}_{max,i} \end{array} \right\}$ then

 limit_exceeded = TRUE

$a = (JW)^\# \dot{x}$

$b = \bar{q} - a$

 getTaskScalingFactor(a , b) (*call Algorithm 2*)

 if {task scaling factor} $> s^*$ then

$s^* = \{\text{task scaling factor}\}$

$W^* = W$, $\dot{q}_N^* = \dot{q}_N$

 end if

$j = \{\text{the most critical joint}\}$

$W_{jj} = 0$

$\dot{q}_{N,j} = \begin{cases} \dot{Q}_{max,j} & \text{if } \dot{\bar{q}}_j > \dot{Q}_{max,j} \\ \dot{Q}_{min,j} & \text{if } \dot{\bar{q}}_j < \dot{Q}_{min,j} \end{cases}$

 if $\text{rank}(JW) < m$ then

$s = s^*$, $W = W^*$, $\dot{q}_N = \dot{q}_N^*$

$\dot{\bar{q}} = \dot{q}_N + (JW)^\# (s\dot{x} - J\dot{q}_N)$

 limit_exceeded = FALSE (*outputs solution*)

 end if

end if

until limit_exceeded = TRUE

$\dot{q}_{SNS} = \dot{\bar{q}}$

initialization

W : diagonal matrix with (j, j) element
= 1 if joint j is enabled
= 0 if joint j is disabled

\dot{q}_N : vector with saturated velocities in correspondence of disabled joints

s : current task scale factor

s^* : largest task scale factor so far



SNS at velocity level

Algorithm 1

$W = I$, $\dot{q}_N = 0$, $s = 1$, $s^* = 0$

repeat

 limit_exceeded = FALSE

$$\dot{\bar{q}} = \dot{q}_N + (JW)^\# (\dot{x} - J\dot{q}_N)$$

 if $\left\{ \exists i \in [1:n] : \dot{\bar{q}}_i < \dot{Q}_{min,i} \text{ OR } \dot{\bar{q}}_i > \dot{Q}_{max,i} \right\}$ then
 limit_exceeded = TRUE

$$a = (JW)^\# \dot{x}$$

$$b = \dot{\bar{q}} - a$$

 getTaskScalingFactor(a, b) (*call Algorithm 2*)

 if {task scaling factor} $> s^*$ then
 $s^* = \{\text{task scaling factor}\}$
 $W^* = W$, $\dot{q}_N^* = \dot{q}_N$
 end if

$j = \{\text{the most critical joint}\}$

$$W_{jj} = 0$$

$$\dot{q}_{N,j} = \begin{cases} \dot{Q}_{max,j} & \text{if } \dot{\bar{q}}_j > \dot{Q}_{max,j} \\ \dot{Q}_{min,j} & \text{if } \dot{\bar{q}}_j < \dot{Q}_{min,j} \end{cases}$$

 if $\text{rank}(JW) < m$ then
 $s = s^*$, $W = W^*$, $\dot{q}_N = \dot{q}_N^*$
 $\dot{\bar{q}} = \dot{q}_N + (JW)^\# (s\dot{x} - J\dot{q}_N)$
 limit_exceeded = FALSE (*outputs solution*)
 end if

end if

until limit_exceeded = TRUE

$$\dot{q}_{SNS} = \dot{\bar{q}}$$

compute the **joint velocity** with initialized values

$$\dot{\bar{q}} = J^\# \dot{x}$$

check the **joint velocity bounds**

compute the **task scaling factor** and the **most critical joint**

if a larger task scaling factor is obtained, **save** the current solution

disable the **most critical joint** by forcing it at its saturated velocity



SNS at velocity level

Algorithm 1

$\mathbf{W} = \mathbf{I}$, $\dot{\mathbf{q}}_N = \mathbf{0}$, $s = 1$, $s^* = 0$

repeat

 limit_exceeded = FALSE

$$\dot{\bar{\mathbf{q}}} = \dot{\mathbf{q}}_N + (\mathbf{J}\mathbf{W})^\# (\dot{\mathbf{x}} - \mathbf{J}\dot{\mathbf{q}}_N)$$

if $\left\{ \begin{array}{l} \exists i \in [1:n] : \\ \dot{\bar{q}}_i < \dot{Q}_{min,i} \text{ OR } \dot{\bar{q}}_i > \dot{Q}_{max,i} \end{array} \right\}$ **then**

 limit_exceeded = TRUE

$$\mathbf{a} = (\mathbf{J}\mathbf{W})^\# \dot{\mathbf{x}}$$

$$\mathbf{b} = \dot{\bar{\mathbf{q}}} - \mathbf{a}$$

 getTaskScalingFactor(\mathbf{a} , \mathbf{b}) (*call Algorithm 2*)

if {task scaling factor} $> s^*$ **then**

$s^* = \{\text{task scaling factor}\}$

$$\mathbf{W}^* = \mathbf{W}, \dot{\mathbf{q}}_N^* = \dot{\mathbf{q}}_N$$

end if

$j = \{\text{the most critical joint}\}$

$$W_{jj} = 0$$

$$\dot{q}_{N,j} = \begin{cases} \dot{Q}_{max,j} & \text{if } \dot{\bar{q}}_j > \dot{Q}_{max,j} \\ \dot{Q}_{min,j} & \text{if } \dot{\bar{q}}_j < \dot{Q}_{min,j} \end{cases}$$

if $\text{rank}(\mathbf{J}\mathbf{W}) < m$ **then**

$$s = s^*, \mathbf{W} = \mathbf{W}^*, \dot{\mathbf{q}}_N = \dot{\mathbf{q}}_N^*$$

$$\dot{\bar{\mathbf{q}}} = \dot{\mathbf{q}}_N + (\mathbf{J}\mathbf{W})^\# (s\dot{\mathbf{x}} - \mathbf{J}\dot{\mathbf{q}}_N)$$

 limit_exceeded = FALSE (*outputs solution*)

end if

end if

until limit_exceeded = TRUE

$$\dot{\mathbf{q}}_{SNS} = \dot{\bar{\mathbf{q}}}$$

check if task can be accomplished with the remaining **enabled** joints

if NOT, use the parameters that allow the **largest** task scaling factor and **exit**

repeat until no joint limit is exceeded



Task scaling factor

Algorithm 2

```
function getTaskScalingFactor( $a$ ,  $b$ )
for  $i = 1 \rightarrow n$  do
     $S_{min,i} = (\dot{Q}_{min,i} - b_i) / a_i$ 
     $S_{max,i} = (\dot{Q}_{max,i} - b_i) / a_i$ 
    if  $S_{min,i} > S_{max,i}$  then
        {switch  $S_{min,i}$  and  $S_{max,i}$ }
    end if
end for
 $s_{max} = \min_i \{S_{max,i}\}$ 
 $s_{min} = \max_i \{S_{min,i}\}$ 
the most critical joint =  $\operatorname{argmin}_i \{S_{max,i}\}$ 
if  $s_{min} > s_{max}$  .OR.  $s_{max} < 0$  .OR.  $s_{min} > 1$  then
    task scaling factor = 0
else
    task scaling factor =  $s_{max}$ 
end if
```

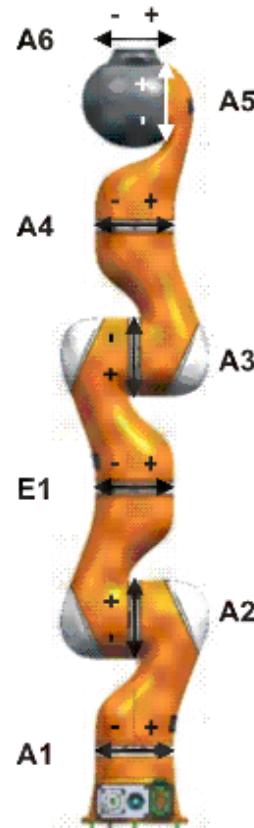
yields the best **task scaling factor**
(i.e., closest to the ideal value = 1)
for the **most critical joint** in the
current joint velocity solution



Simulation results

Axis	Range of motion, software-limited	Velocity without payload
A1 (J1)	+/-170°	100°/s
A2 (J2)	+/-120°	110°/s
E1 (J3)	+/-170°	100°/s
A3 (J4)	+/-120°	130°/s
A4 (J5)	+/-170°	130°/s
A5 (J6)	+/-120°	180°/s
A6 (J7)	+/-170°	180°/s

7-dof KUKA LWR IV



$$Q_{max} = (170, 120, 170, 120, 170, 120, 170) \text{ [deg]}$$

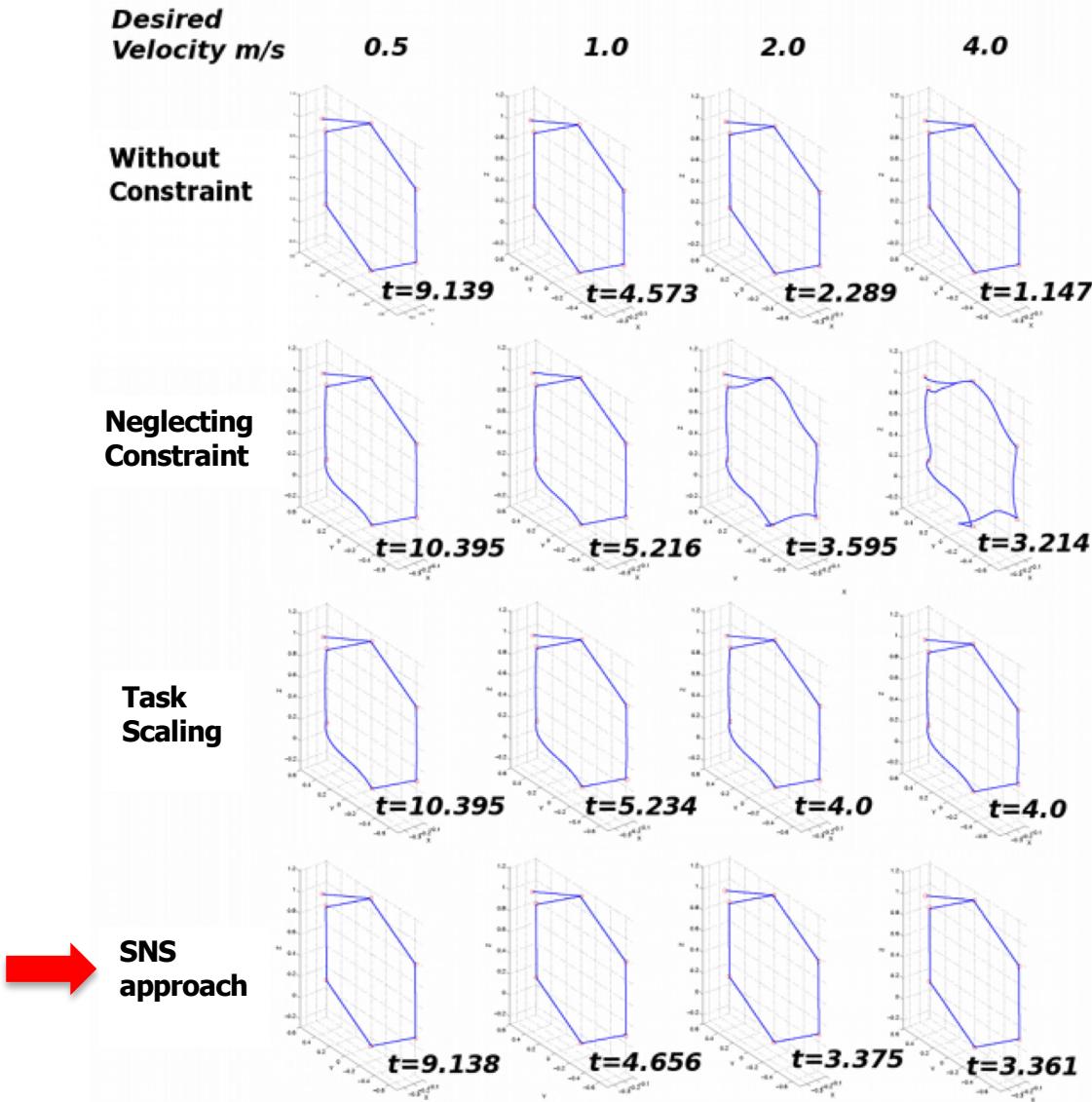
$$V_{max} = (100, 110, 100, 130, 130, 180, 180) \text{ [deg/s]}$$

$$A_{max,i} = 300 \text{ [deg/s}^2\text{]} \quad \forall i = 1 \dots n$$

$$T = 1 \text{ [ms]}$$



Simulation results



← for increasing V

requested task

move the end-effector through **six** desired Cartesian positions along linear paths with constant speed V

$$\dot{x} = V \frac{\mathbf{x}_r - \mathbf{x}}{\|\mathbf{x}_r - \mathbf{x}\|}$$

task **redundancy** degree = $7 - 3 = 4$

robot starts at the configuration

$$\mathbf{q}(0) = (0, 45, 45, 45, 0, 0, 0) [\text{deg}]$$

(with a small initial approaching phase)



Experimental results

KUKA LWR IV with hard joint-space limits

[video](#)



Control of Redundant Robots under Hard Joint Constraints: Saturation in the Null Space

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Robotics Lab, DIAG
Sapienza Università di Roma

Artificial Intelligence Lab
Stanford University

July 2014

IEEE Transactions on Robotics 2015



Variations of the SNS method

SNS at the acceleration command level + consideration of multiple tasks with priority
video



Prioritized Multi-Task Motion Control of Redundant Robots under Hard Joint Constraints



Attached video to IROS 2012

* F. Flacco *A. De Luca

** O Khatib

*Robotics Laboratory, Università di Roma "La Sapienza"

**Artificial Intelligence Laboratory , Stanford University

IEEE/RSJ Int. Conf. on Intelligent Robots and Systems (IROS) 2012



Inclusion of hard Cartesian bounds

- SNS at the **velocity command** level, with hard bounds on joint position, velocity, and acceleration and task scaling factor (just **one task** is considered here)
- additional** (possibly, time-varying) Cartesian box inequalities on position, velocity, and acceleration of ***r* control points** along the structure (including end effector)
- generalized** treatment of all bounds in a **unified** way (conversions like in **slide #24**)

$$Q_j^{\min} \leq q_j \leq Q_j^{\max}$$

$$V_j^{\min} \leq \dot{q}_j \leq V_j^{\max}$$

$$\Lambda_j^{\min} \leq \ddot{q}_j \leq \Lambda_j^{\max}$$

$$j = 1, \dots, n$$

generalized vector

$$P_{cp,i}^{\min} \leq p_{cp,i} \leq P_{cp,i}^{\max}$$

$$V_{cp,i}^{\min} \leq \dot{p}_{cp,i} \leq V_{cp,i}^{\max}$$

$$\Lambda_{cp,i}^{\min} \leq \ddot{p}_{cp,i} \leq \Lambda_{cp,i}^{\max}$$

$$i = 1, \dots, r$$

$$p_{cp,i} \in \mathbb{R}^{d_i}$$

$$d_i \in \{1, 2, 3\}$$

$$\mathbf{a} = (\mathbf{q}^T \quad \mathbf{p}_{cp,1}^T \quad \mathbf{p}_{cp,2}^T \quad \dots \quad \mathbf{p}_{cp,r}^T)^T$$

additional processing of \dot{q} in
Algorithm 1 (rather than by I only) $\longrightarrow A = (I \quad J_{cp,1}^T \quad J_{cp,2}^T \quad \dots \quad J_{cp,r}^T)^T$

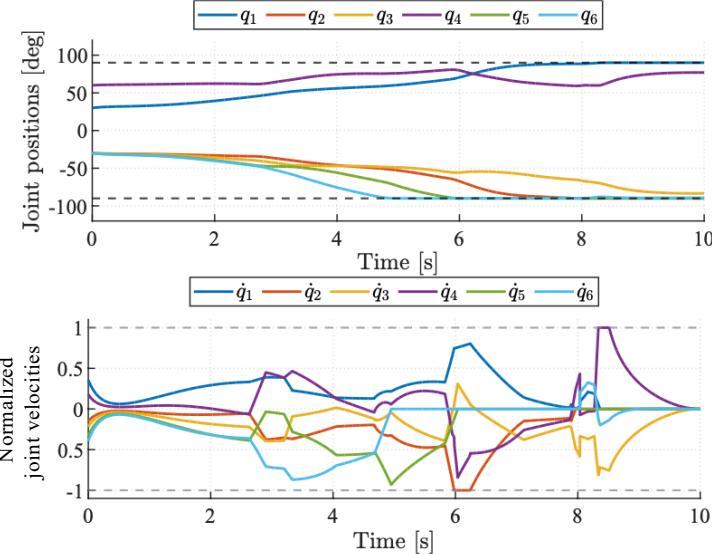
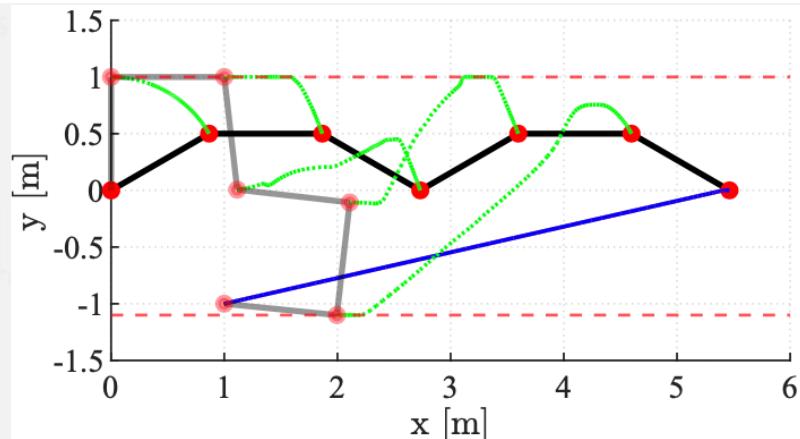
$$\Rightarrow B_{\min}(t_k) \leq \dot{a}(\mathbf{q}, \dot{\mathbf{q}}) \leq B_{\max}(t_k) \quad \text{unified joint/Cartesian bounds}$$



Inclusion of hard Cartesian bounds

simulation on a **6R planar manipulator** with $r = 5$ control points (at joints 2 to 6)

video



$$Q_j^{\max} = -Q_j^{\min} = 90 \text{ [deg]}$$

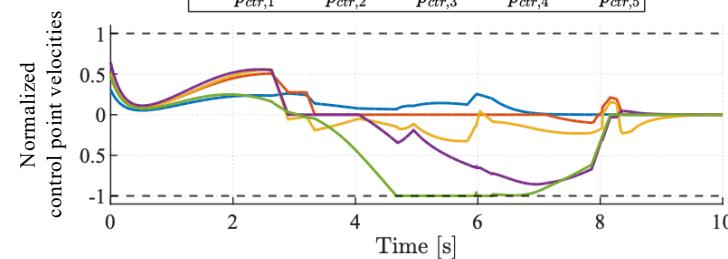
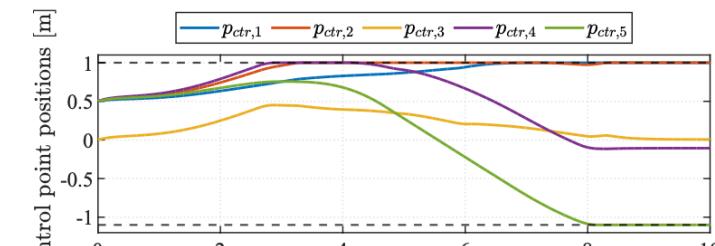
$$V_j^{\max} = -V_j^{\min} = \frac{90}{\pi} \text{ [deg/s]}$$

joint limits on position and velocity
($j = 1, \dots, 6$)

$$P_{cp,i}^{\max,y} = 1, \quad P_{cp,i}^{\min,y} = -1.1 \text{ [m]}$$

$$V_{cp,i}^{\max,y} = 0.5, \quad V_{cp,i}^{\min,y} = -0.5 \text{ [m/s]}$$

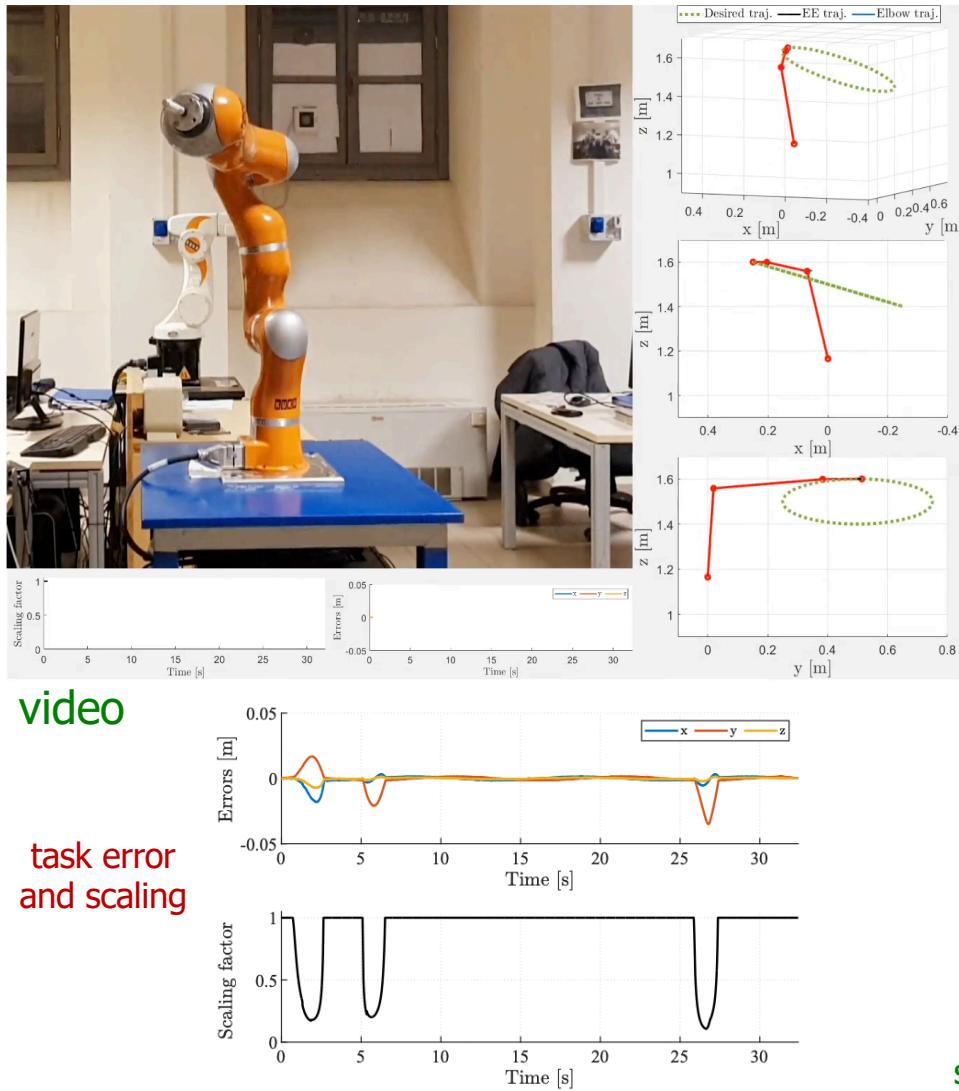
control point limits on position and velocity
($i = 1, \dots, 5$)





Inclusion of hard Cartesian bounds

experiment #1 on KUKA LWR IV robot with $r = 1$ control point at the robot elbow (with $d_1 = 2$)



Robotics 2

joint limits on position, velocity and acceleration

$$\mathbf{Q}^{max} = -\mathbf{Q}^{min} = (170 \ 105 \ 170 \ 120 \ 170 \ 85 \ 170)^T \text{ [deg]}$$

$$\mathbf{V}^{max} = -\mathbf{V}^{min} = (20 \ 22 \ 20 \ 26 \ 26 \ 36 \ 36)^T \text{ [deg/s]}$$

$$\mathbf{\Lambda}^{max} = -\mathbf{\Lambda}^{min} = (30 \ 30 \ 30 \ 30 \ 30 \ 30 \ 30)^T \text{ [deg/s}^2]$$

control point limits on position, velocity and acceleration

$$-0.1 \leq \dot{\mathbf{p}}_{cp_x,1} \leq 0.1, \quad -0.1 \leq \dot{\mathbf{p}}_{cp_y,1} \leq 0.1 \text{ [m/s].}$$

permanent

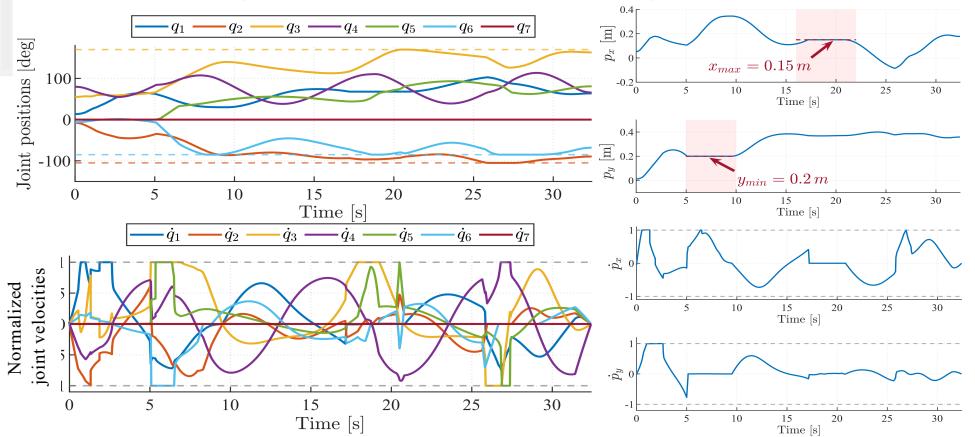
$$-0.5 \leq \ddot{\mathbf{p}}_{cp_x,1} \leq 0.5, \quad -0.5 \leq \ddot{\mathbf{p}}_{cp_y,1} \leq 0.5 \text{ [m/s}^2]$$

$$\mathbf{p}_{cp_x,1} \leq 0.15 \text{ [m]}, \quad 16 \leq t \leq 22 \text{ [s]}$$

(online) time-varying

$$\mathbf{p}_{cp_y,1} \leq 0.2 \text{ [m]}, \quad 5 \leq t \leq 10 \text{ [s]}$$

joint-space and Cartesian control point behaviors

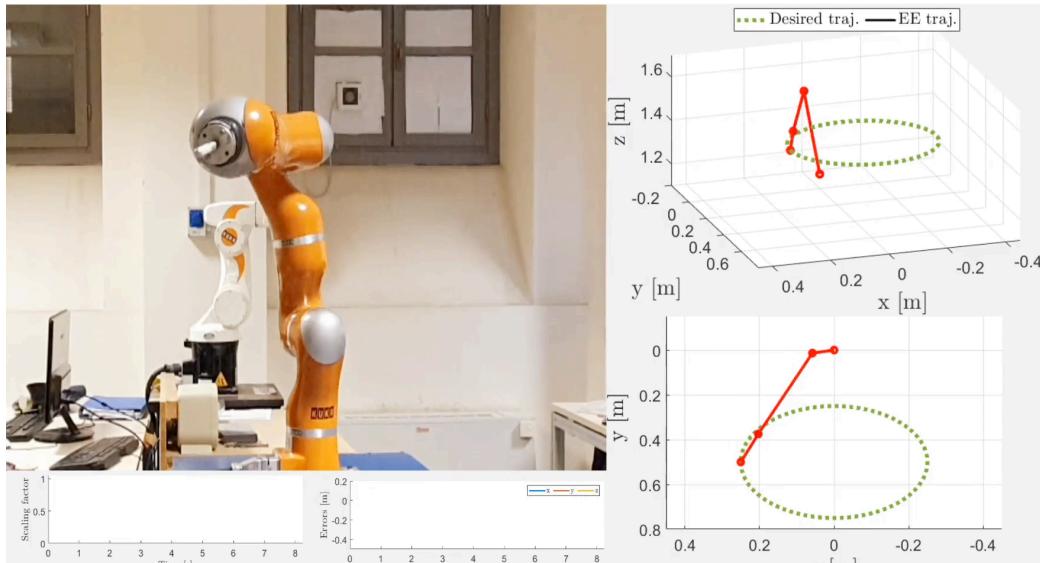


submitted to IEEE Robotics and Automation Letters, Feb 2022

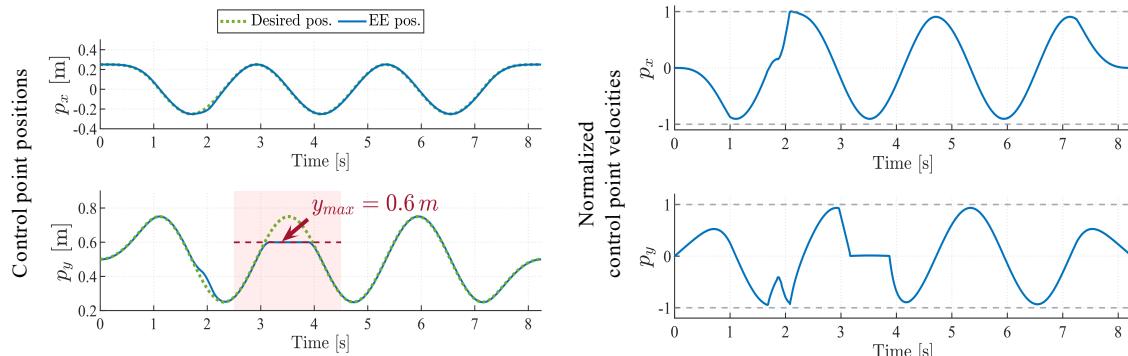


Inclusion of hard Cartesian bounds

experiment #2 on KUKA LWR IV robot with $r = 1$ control point at the robot elbow (with $d_1 = 2$)



video



circle will be "cut" during second turn!

joint limits on position, velocity and acceleration

$$Q^{max} = -Q^{min} = (170 \ 120 \ 170 \ 120 \ 170 \ 120 \ 170)^T \text{ [deg]}$$

$$V^{max} = -V^{min} = (100 \ 110 \ 100 \ 130 \ 130 \ 180 \ 180)^T \text{ [deg/s]}$$

$$\Lambda^{max} = -\Lambda^{min} = (300 \ 300 \ 300 \ 300 \ 300 \ 300 \ 300)^T \text{ [deg/s}^2]$$

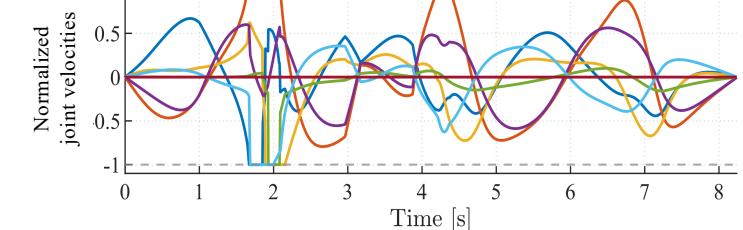
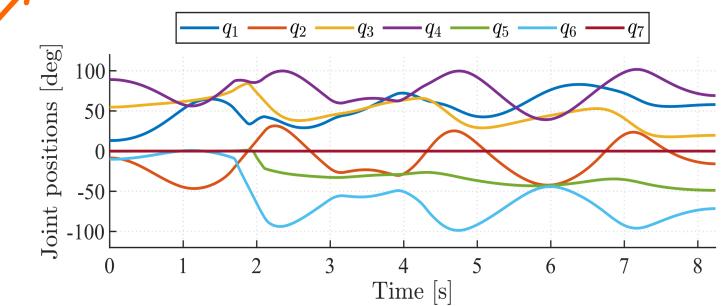
much higher than before \Rightarrow faster motion!

control point limits on position, velocity and acceleration

$$-0.7 \leq \dot{p}_{cp_x,1} \leq 0.7, \quad -0.7 \leq \dot{p}_{cp_y,1} \leq 0.7 \text{ [m/s]} \quad \text{permanent}$$

$$-1.5 \leq \ddot{p}_{cp_x,1} \leq 1.5, \quad -1.5 \leq \ddot{p}_{cp_y,1} \leq 1.5 \text{ [m/s}^2]$$

$$p_{cp_y,1} \leq 0.6 \text{ [m]}, \quad 2.5 \leq t \leq 4.5 \text{ [s]} \quad \text{(online) time-varying}$$





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Appendix A - Recursive Task Priority

proof of recursive expression for null-space projector

$$P_{A,k} = P_{A,k-1} - (J_k P_{A,k-1})^\# J_k P_{A,k-1}$$

- proof based on a result on pseudoinversion of **partitioned** matrices (Cline: J. SIAM 1964)

$$\begin{pmatrix} A \\ B \end{pmatrix}^\# = \begin{pmatrix} A^\# - TBA^\# & T \end{pmatrix} \quad \begin{aligned} T &= E^\# + X(I - EE^\#) && X \text{ is irrelevant here} \\ E &= B(I - A^\# A) \end{aligned}$$

- (i) $P_{A,k} = I - J_{A,k}^\# J_{A,k} = I - \begin{pmatrix} J_{A,k-1} \\ J_k \end{pmatrix}^\# \begin{pmatrix} J_{A,k-1} \\ J_k \end{pmatrix}$
 - (ii) $T = (J_k P_{A,k-1})^\# + X(I - (J_k P_{A,k-1})(J_k P_{A,k-1})^\#)$
- $$\begin{aligned} &= I - \left(J_{A,k-1}^\# - TJ_k J_{A,k-1}^\# \quad T \right) \begin{pmatrix} J_{A,k-1} \\ J_k \end{pmatrix} && \blacksquare \text{ (i) + (ii)} \Rightarrow \text{Q.E.D.} \\ &= I - J_{A,k-1}^\# J_{A,k-1} + TJ_k J_{A,k-1}^\# J_{A,k-1} - TJ_k \\ &= P_{A,k-1} - TJ_k P_{A,k-1} && \blacksquare \text{ if } k\text{-th task is scalar} \\ &\Rightarrow TJ_k P_{A,k-1} = (J_k P_{A,k-1})^\# J_k P_{A,k-1} && \begin{aligned} J_k &= \text{single row } j_k^T \\ P_{A,k} &= P_{A,k-1} - \frac{P_{A,k-1} j_k j_k^T P_{A,k-1}}{\|P_{A,k-1} j_k\|^2} \end{aligned} \quad \text{(Greville formula)}$$