

Last Time we Found  $T \in \mathbb{R}^{2 \times 2}$  Such That

$$\begin{bmatrix} x \\ \dot{x} \end{bmatrix} = T \begin{bmatrix} \alpha \\ g \end{bmatrix} \quad \text{where } \ddot{x} = v$$

$x^*(t)$  Is Compute By Solving Some OCP  
Or More Generally Given Any  $x_d(t)$

$$\begin{bmatrix} \alpha_d(t) \\ g_d(t) \end{bmatrix} = T^{-1} \begin{bmatrix} x_d(t) \\ \dot{x}_d(t) \end{bmatrix}$$

$\alpha_d(t)$  &  $g_d(t)$  Uniquely Described By  $x_d(t)$   
& Its Derivatives

### Differential Flatness

Property That Allows One To Parameterize The  
System's State By Set of Indep Variables

& Their Derivatives

Flat Variables

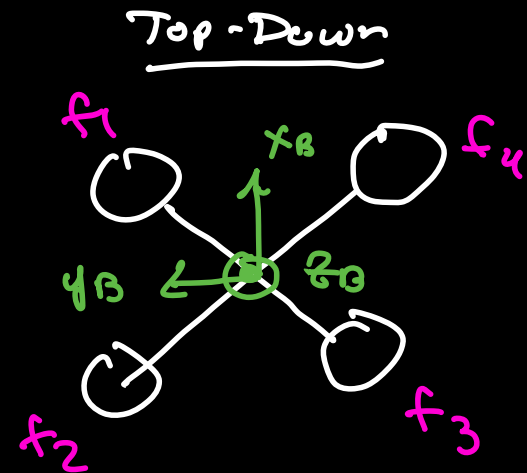
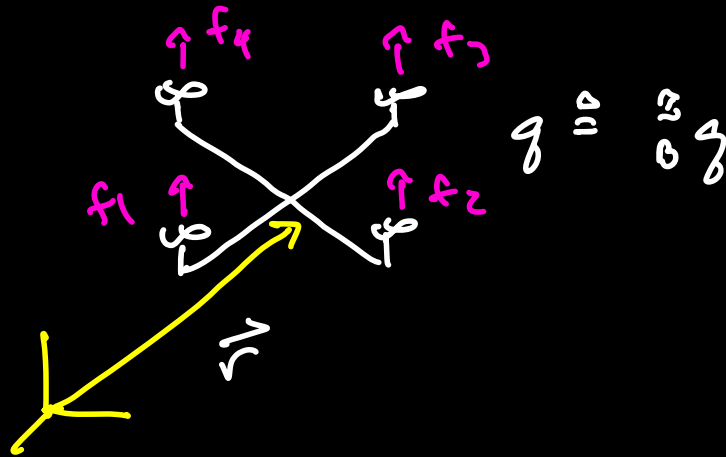
$$\dot{\vec{x}} = A\vec{x} + Bu \quad \begin{array}{c} \xrightarrow{T} \\ \xleftarrow{T^{-1}} \end{array} \quad \vec{z}^{(n)} = v \quad z: \text{Flat Variable}$$

$$\text{where } \begin{bmatrix} z \\ \dot{z} \\ \vdots \end{bmatrix} = T \vec{x} \quad \vec{x} \in \mathbb{R}^n$$

Differential Flatness Bypasses The Dynamics  
Of Original System

Fact: # of Flat Variables = # of Control Inputs

# Ex. 3D Quadrotor



States:  $\vec{r}, \dot{\vec{r}}, g, \vec{\omega}$

Inputs:  $f_1, f_2, f_3, f_4 \Rightarrow \vec{T} = \begin{bmatrix} 0 \\ 0 \\ \sum f_i \end{bmatrix}, \vec{M}_B = \Gamma \begin{pmatrix} f_1 \\ \vdots \\ f_4 \end{pmatrix}$

Depends On  
veh. Geom.

Objective: Smooth Point-To-Point Trajectory +  
Some BC

Dynamics:  $m \ddot{\vec{r}} = g \otimes \vec{T} \otimes g^* - \vec{g}$

$$\dot{g} = \frac{1}{2} g \otimes \begin{bmatrix} 0 \\ \vec{v} \end{bmatrix}$$

$$J \dot{\vec{\omega}} = - \vec{\omega} \times J \vec{\omega} + \vec{M}_B$$

Min  
 $\vec{F}, \vec{M}_B$

$J$

Sub To

Dynamics  
+ BC

}

Non-Convex Optimization

B/C Nonlinear Dynamics

$\Rightarrow$  Hard...

Non-Convex  $\Rightarrow$  Trajectory Design with Original States  
Is very Challenging

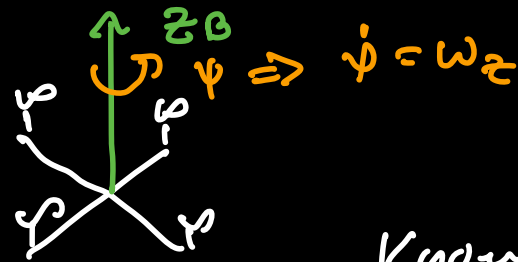
Key Insight: System Is Differentially Flat

$$\Rightarrow \vec{r}, \vec{v}, g, \vec{\omega} \iff z_1, z_2, \dots \text{ s.t. } z_i^{(m)} = v_i$$

Nonlinear  
System

Linear  
System

Fact:  $\vec{r}$  &  $\psi$  (Yaw Angle) Are Flat variables



Known

Let  $\vec{r}_d(t) \in \mathcal{R}^3$  Be sufficiently smooth Trajectory

Differentiating  $r_d(t)$  Twice

$$m \ddot{\vec{r}}_d = \mathcal{F}_d \otimes \vec{T}_d \otimes \mathcal{F}_d^* - m \vec{g}$$

Let's solve for  $\vec{T}_d$

Recall That Rotations Preserve Length

$$m \|\ddot{\vec{r}}_d + \vec{g}\| = \|\mathcal{F}_d \otimes \vec{T}_d \otimes \mathcal{F}_d^*\| = \|\vec{T}_d\| = \sum f_{i,d} = T_d$$

$$\Rightarrow \boxed{\tau_d = m \|\ddot{r}_d + g\|} \Rightarrow \vec{\tau}_d = \begin{bmatrix} 0 \\ 0 \\ m \|\ddot{r}_d + g\| \end{bmatrix}$$

$$g_d \otimes \vec{\tau}_d \otimes g_d^* = m (\ddot{r}_d + \vec{g})$$

Formula: Given  $\hat{v}_B$  &  $\hat{v}_x$   $\|\hat{v}_B\| = \|\hat{v}_x\| = 1$  Then  
The Quaternion That Aligns  $\hat{v}_B$  &  $\hat{v}_x$  Is

$$q = \frac{1}{\sqrt{2(1 + \hat{v}_B^T \hat{v}_x)}} \begin{bmatrix} 1 + \hat{v}_B^T \hat{v}_x \\ \hat{v}_B \times \hat{v}_x \end{bmatrix}$$

Recall That  $\vec{\tau}_d = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} \Rightarrow \hat{\tau}_d = \frac{\vec{\tau}_d}{\|\tau_d\|}$

$$q_d = \frac{1}{\sqrt{2(1 + \hat{\tau}_d^T \hat{F}_x)}} \begin{bmatrix} 1 + \hat{\tau}_d^T \hat{F}_x \\ \hat{\tau}_d \times \hat{F}_x \end{bmatrix} \quad \text{Where } \hat{F}_x = m(\ddot{r}_d + g)$$

$$m \ddot{\vec{r}}_d = \vec{g}_d \otimes \vec{T}_d \otimes \vec{g}_d^* - \vec{g}$$

$$\Downarrow \frac{d}{dt}(\cdot)$$

$$m \vec{r}_d^{(3)} = \dot{\vec{g}}_d \otimes \vec{T}_d \otimes \vec{g}_d^* + \vec{g}_d \otimes \dot{\vec{T}}_d \otimes \vec{g}_d^* + \vec{g}_d \otimes \vec{T}_d \otimes \dot{\vec{g}}_d^*$$

$$\dot{\vec{g}}_d = \frac{1}{2} \vec{g}_d \otimes \begin{bmatrix} 0 \\ \dot{\vec{\omega}}_d \end{bmatrix} \quad \dot{\vec{g}}_d^* = -\frac{1}{2} \begin{bmatrix} 0 \\ \dot{\vec{\omega}}_d \end{bmatrix} \otimes \vec{g}_d^*$$

$$m \vec{r}_d^{(3)} = \vec{g}_d \otimes \left\{ \frac{1}{2} \begin{bmatrix} 0 \\ \dot{\vec{\omega}}_d \end{bmatrix} \otimes \begin{bmatrix} 0 \\ \dot{\vec{T}}_d \end{bmatrix} - \frac{1}{2} \begin{bmatrix} 0 \\ \dot{\vec{T}}_d \end{bmatrix} \otimes \begin{bmatrix} 0 \\ \dot{\vec{\omega}}_d \end{bmatrix} + \begin{bmatrix} 0 \\ \dot{\vec{T}}_d \end{bmatrix} \right\} \otimes \vec{g}_d^*$$

Can show  $\begin{bmatrix} 0 \\ \dot{\vec{\omega}}_d \end{bmatrix} \otimes \begin{bmatrix} 0 \\ \dot{\vec{T}}_d \end{bmatrix} - \begin{bmatrix} 0 \\ \dot{\vec{T}}_d \end{bmatrix} \otimes \begin{bmatrix} 0 \\ \dot{\vec{\omega}}_d \end{bmatrix} = \begin{bmatrix} 0 \\ 2 \dot{\vec{\omega}}_d \times \dot{\vec{T}}_d \end{bmatrix}$

$$m \vec{r}_d^{(3)} = \vec{g}_d \otimes \left\{ \begin{bmatrix} 0 \\ \dot{\vec{\omega}}_d \times \dot{\vec{T}}_d \end{bmatrix} + \begin{bmatrix} 0 \\ \dot{\vec{T}}_d \end{bmatrix} \right\} \otimes \vec{g}_d^*$$

Want  $\vec{\omega}_d$

$$\vec{T}_d = \begin{bmatrix} 0 \\ 0 \\ T_d \end{bmatrix} \quad \& \quad \vec{\omega}_d = \begin{bmatrix} \omega_{xd} \\ \omega_{yd} \\ \omega_{zd} \end{bmatrix}$$

$$\vec{\omega}_d \times \vec{T}_d = \begin{bmatrix} \omega_{yd} T_d \\ -\omega_{xd} T_d \\ 0 \end{bmatrix} = T_d \begin{bmatrix} \omega_{yd} \\ -\omega_{xd} \\ 0 \end{bmatrix}$$

Rearranging, we get

$$\begin{bmatrix} \omega_{yd} \\ -\omega_{xd} \\ 0 \end{bmatrix} = \frac{m}{T_d} \vec{r}_d^* \otimes \vec{r}_d^{(3)} \otimes \vec{g}_d - \frac{\dot{\vec{T}}_d}{T_d}$$

$\omega_{zd}$  is absent  $\Rightarrow \omega_{zd}$  can be freely picked!  
 $\Rightarrow \psi_d$  where  $\dot{\psi}_d = \omega_{zd}$  is



Indeed Flat variable

Yaw Angle  $\psi_d(t)$  Can Be Arbitrarily Picked  
 $\Rightarrow g_d$  Doesn't Restrict what  $\psi_d(t)$  should Be

Given Some  $\psi_d(t)$  Then

$$\bar{g}_d = g_d \otimes \underbrace{(c(\psi_d/2), 0, 0, s(\psi_d/2))}_{\text{Body Frame Rotation}}$$

Body Frame Rotation  
About  $(0, 0, 1)$  Through  $\psi_d$

Observe  $\ddot{\vec{r}}_d \rightarrow g_d$  &  $\vec{T}_d$  (Up To Yaw Angle)

$$\vec{r}_d^{(3)}, \ddot{\vec{r}}_d, \dot{\psi}_d \rightarrow \vec{\omega}_d$$

$$\vec{r}_d^{(u)}, \dots, \ddot{\psi}_d \rightarrow \dot{\vec{\omega}}_d = \vec{\alpha}_d \rightarrow \vec{M}_{B_d}$$



$$J \dot{\vec{\omega}}_d = -\vec{\omega}_d \times J \vec{\omega}_d + \vec{M}_{B_d}$$

So Given  $\vec{r}_d(t), \dots, \vec{r}_d^{(k)}(t) + \psi_d(t), \dots, \psi_d^{(k)}(t)$

Then we know  $\vec{r}_d, \dot{\vec{r}}_d, g_d, \vec{\omega}_d + f_{1d}, f_{2d}, f_{3d}, f_{4d}$   
 $(\vec{T}_d, \vec{M}_{B_d})$

For Instance If  $\vec{r}_d(t) = \begin{bmatrix} \sum a_i t^i \\ \sum b_i t^i \\ \sum c_i t^i \end{bmatrix}$   $\psi_d(t) = \sum d_i t^i$

Then we know  $\vec{r}_d, \dot{\vec{r}}_d, g_d, \vec{\omega}_d + \vec{T}_d, \vec{M}_{B_d}$