

Q1

b) Find  $v_b$  first by applying voltage divider rule given that  $R_3$  and  $R_4$  are in series.

c)  $I_3$  can be found by considering the voltage across  $R_1$ .  $I_3 = I_F$  because  $I_1 = 0$ . Last,  $v_o$  can be found by considering the voltage drop across  $R_2$ .

Q2

a) Applying nodal analysis at non-inverting input:

$$\frac{10mV - V^+}{4k} = \frac{V^+}{6k} + \frac{V^+}{12k} \quad (\text{Bear in mind there is no current going into the op amp})$$

b) Applying nodal analysis at inverting input:

$$\frac{10mV - V^-}{6k} + \frac{v_o - V^-}{12k} = \frac{V^-}{4k} \quad (\text{Bear in mind there is no current going into the op amp})$$

And the value of  $V^-$  is already known from the previous part.

Q3

b) Note that  $i_4$  is the sum of the  $i_3$  and the current in the  $100\text{ k}\Omega$  resistor.

c)  $i_5$  can be found by considering the voltage drop across the  $50\text{ k}\Omega$  resistor, which equals  $v_{o2}$ . Note that the  $100\text{ k}\Omega$  and  $50\text{ k}\Omega$  resistors are in series, allowing us to apply voltage divider rule to find  $v_o$ .

Q4

Note that first stage is a summing amplifier with  $v_i$  and  $v_o$  as inputs:

If we define  $V_1$  as the output of this stage, then:

$$V_1 = -10/5 * v_i - 10/4 * v_o$$

The second stage is a non-inverting amplifier with  $V_1$  as input:

$$\text{Therefore, } v_o = (1 + 10/2) * V_1$$

Q5

a) With  $V_S = 1.2\text{ V}$ , the corresponding output (a negative voltage) would be over the saturation limit. So it will be limited by  $V_S^-$ .

b) Two features of the graph that should be highlighted:

- The line around the origin (where  $V_S$  is small) has a slope equal to the gain. As implied by the negative sign of the closed loop gain, the slope of the line should be negative.
- Once the curve reaches  $+5\text{V}$  or  $-5\text{V}$ , it should be horizontal to represent saturation.