

Lecture 16: Special Surfaces

God hath chosen thee to be ... special

Deuteronomy 7:6

1. Simple Surfaces

Some surfaces are easy to describe without equations. A sphere is the locus of points at a fixed distance from a given point; a cylinder is the locus of points at a fixed distance from a given line. Thus a sphere can be represented simply by a center point and a radius; a cylinder by an axis line and a radius. For these simple surfaces, we can compute surface normals and ray-surface intersections directly from their geometry, without resorting to implicit or parametric equations. Thus ray tracing these surfaces is particularly easy.

In this lecture we shall investigate ray tracing strategies for surfaces defined geometrically rather than algebraically. These surfaces include the plane and the natural quadrics -- the sphere, the right circular cylinder, and the right circular cone. We shall also explore ray tracing for general quadric (second degree) surfaces as well as for the torus, which is a surface of degree four. These surfaces are among the simplest and most common surfaces in computer graphics, so they deserve some special attention.

2. Intersection Strategies

Special strategies exist for ray tracing simple surfaces. One of the most common tactics is to apply a transformation to reduce the ray-surface intersection problem to a simpler problem either by projecting to a lower dimension, or by repositioning to a canonical location, or by rescaling to a more symmetric shape.

Consider intersecting a curve C and a surface S . If a point P lies on the intersection of the curve C and the surface S , then for any affine or projective transformation M the point $P * M$ lies on the intersection of the curve $C * M$ and the surface $S * M$. If the transformation M is cleverly chosen, in many cases it is easier to intersect the curve $C * M$ with the surface $S * M$ rather than the original curve C with the original surface S . Moreover, if the transformation M is invertible, then

$$P \in C \cap S \Leftrightarrow P * M \in C * M \cap S * M.$$

Therefore when M is invertible, we can find the intersection points of the original curve C and the original surface S by computing the intersection points of the transformed curve $C * M$ with the transformed surface $S * M$ and then mapping back by M^{-1} . This method is essentially the deformation technique discussed in the previous lecture, though M may also be a rigid motion as well as a shear or a scale.

But what if the transformation M is not invertible? For example, what if M is an orthogonal or perspective projection? Remarkably, for parametric curves and surfaces the same strategy can still work.

Consider intersecting a parametric curve $C = C(t)$ and a parametric surface $S = S(u, v)$. The curve C and the surface S intersect whenever there are parameter values t^*, u^*, v^* for which

$$C(t^*) = S(u^*, v^*).$$

Applying an affine or projective transformation M yields

$$C(t^*) * M = S(u^*, v^*) * M.$$

Thus if the original curve and surface intersect at the parameters t^*, u^*, v^* , so will the transformed curve and surface. The intersection points may change, but the parameter values are unaffected. This observation is the key to our intersection strategy.

If no new intersection points are introduced by applying the transformation M , then we can find the intersection points of the original curve and surface by solving for the parameters t^* or (u^*, v^*) of the intersection points of the transformed curve and surface and then substituting these parameter values back into the original equations $C = C(t^*)$ or $S = S(u^*, v^*)$ to find the intersection points of the original curve and surface.

Moreover, even if we do introduce some new spurious intersection points by applying a singular transformation, we never lose any of the old intersection points. So, at worst, we would need to check whether the parameters representing intersection points on the transformed curve and surface represent actual intersection points on the original curve and surface. But we can always verify potential intersections by substituting the intersection parameters back into the parametric equations of the original curve and surface and checking whether or not we get the same point on the curve and the surface -- that is, by verifying that $C(t^*) = S(u^*, v^*)$.

We shall see many examples of this general transformation strategy for computing intersections throughout this lecture.

3. Planes

A plane can be described by a single point Q on the plane and a unit vector N normal to the plane. A point P lies on the plane if and only if the vector $P - Q$ is perpendicular to the normal vector N or equivalently if and only if $N \cdot (P - Q) = 0$.

A line $L(t) = P + t v$ intersects the plane determined by the point Q and the normal vector N at

the parameter value t^* where

$$N \cdot (L(t^*) - Q) = N \cdot (P + t^*v - Q) = 0.$$

Solving for t^* yields

$$t^* = \frac{N \cdot (Q - P)}{N \cdot v}.$$

Substituting the parameter t^* back into the equation of the line yields the intersection point

$$R = L(t^*) = P + t^*v.$$

Thus we have a simple algorithm to intersect a line with an infinite plane.

Often, however, we want to find the intersection of a line with a finite polygon, rather than with an infinite plane. For example, when we ray trace a cube, the faces of the cube are squares, not infinite planes. Even if a line intersects the plane containing the polygon, the line might not intersect the plane at a point inside the polygon.

There are two standard tests for determining if a point on a plane lies inside a polygon. Consider first a convex polygon with vertices P_i , $i = 1, \dots, m$. Let $N_{i,i+1}$ be vectors normal to the edges P_iP_{i+1} and pointing into the polygon (see Figure 1). Then a point R lies inside the polygon if and only if

$$(R - P_i) \cdot N_{i,i+1} \geq 0 \quad i = 1, \dots, m.$$

To find the normal vectors $N_{i,i+1}$, observe that if the vertices of the polygon are oriented counterclockwise with respect to the normal N to the plane, then

$$N_{i,i+1} = N \times (P_{i+1} - P_i);$$

if the vertices are oriented clockwise, then

$$N_{i,i+1} = N \times (P_i - P_{i+1}).$$

This test works only for convex polygons.

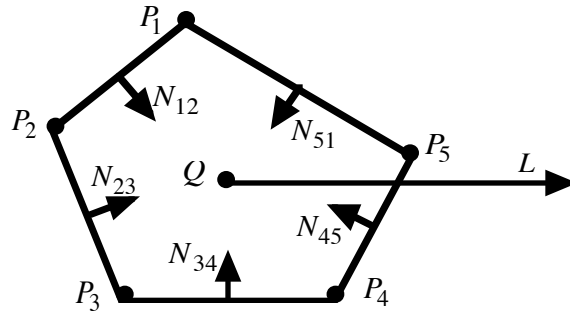


Figure 1: A point R lies inside the polygon if and only if R lies on the positive side of the normal vector to each bounding line. Alternatively, a point R lies inside the polygon if and only if an arbitrary ray L through the point R intersects the polygon in an odd number of points.

For arbitrary, possibly non-convex, polygons there is a more general parity test. A point R lies inside a polygon if and only if an arbitrary ray L through the point R intersects the edges of the polygon in an odd number of points (see Figure 1). Rays through points outside the polygon will intersect the polygon in an even (possibly zero) number of points. Note that this test may fail if the ray intersects the polygon at one of the vertices of the polygon. Nevertheless, if the ray is chosen in a random direction, this problem will almost never arise.

4. Natural Quadrics

The natural quadrics consist of the sphere, the right circular cylinder, and the right circular cone. These three surfaces are among the most common surfaces in computer graphics, so we shall develop special ray tracing algorithms for each of these surfaces. Moreover, for these three surfaces, we shall reduce the ray-surface intersection computation to a single algorithm for computing the intersection of a line and a circle.

4.1 Spheres. Next to planes, spheres are the simplest and most common surfaces in computer graphics. Therefore we would like to have a simple way to represent spheres as well as a fast, robust ray-sphere intersection algorithm.

A sphere can be represented simply by a center point C and a scalar radius R . The vector N from the center point C to a point P on the surface of the sphere is normal to the surface of the sphere at the point P . Therefore the normal vector N at the point P is given by

$$N = P - C.$$

To simplify the ray-sphere intersection calculation, we shall reduce the 3-dimensional ray-sphere intersection problem to a 2-dimensional ray-circle intersection problem. Suppose we want to intersect the line L with the sphere. Consider the plane containing the center point C and the line L (see Figure 2). This plane intersects the sphere in a circle with center C and radius R , and the line L intersects this circle in the same points that the line L intersects the sphere.

To find the intersection points of a line and a circle, we can take a simple geometric approach. Let the line L be determined by a point P and a direction vector v . First we check the distance from the center point C to the line L . If this distance is greater than the radius R , then there is no intersection between the line and the circle. Thus we have a fast test for rejection. Otherwise, we proceed by first finding the point Q on the line L closest to the center point C . We then use the Pythagorean theorem to calculate the distance from Q to the intersection points A, B of the line and the circle. Below is pseudocode for this Line-Circle intersection algorithm.

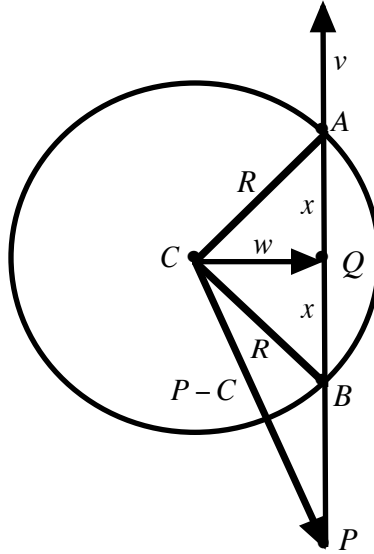


Figure 2: A line intersecting a circle.

Line-Circle Intersection Algorithm

Input

C = Circle Center

R = Circle Radius

P = Point on the Line

v = Vector in the Direction of the Line

Algorithm

If $\text{Dist}(C, L) > R$, there are no intersection points (fast reject)

Otherwise

Normalize the direction vector v to a unit vector

$$v \rightarrow \frac{v}{|v|}$$

Find the orthogonal projection w of the vector $P - C$ on the line vector v

$$w = (P - C)_{\perp} = (P - C) - ((P - C) \cdot v)v$$

Find the point Q on the line L closest to the center point C

$$Q = C + w$$

Using the Pythagorean theorem, find the distance x from the point Q to the intersection points A, B .

$$x^2 = R^2 - |w|^2$$

Compute the intersection points A, B

$$A = Q + xv$$

$$B = Q - xv$$

4.1.1 Inversion Formulas for the Line. The preceding algorithm finds the intersection points of a line and circle or equivalently a line and a sphere. But in ray tracing we also need to know the parameter values along the line corresponding to these intersection points. A formula for finding the parameter value corresponding to a point on the line is called an *inversion formula* for the line. The exact form of the inversion formula depends on the particular form of the parametric equation of the line.

Consider, for example, a line L determined by a point P and a vector v ; then $L(t) = P + tv$. If Q is a point on the line $L(t)$, then for some value t

$$Q = P + tv.$$

Subtracting P from both sides, dotting with v , and solving for t yields

$$t = \frac{(Q - P) \cdot v}{v \cdot v}. \quad (\text{inversion formula 1})$$

If v is a unit vector, then $v \cdot v = 1$ and the inversion formula simplifies to

$$t = (Q - P) \cdot v. \quad (\text{inversion formula 2})$$

If the line L is determined by two points P_0, P_1 , then

$$L(t) = (1 - t)P_0 + tP_1 = P_0 + t(P_1 - P_0).$$

Therefor to find the parameter value corresponding to a point Q on the line $L(t)$, we can use inversion formula 1 with $v = P_1 - P_0$.

Suppose, however, that L is the image under perspective projection of a line in 3-space. Perspective projection maps points and vectors into mass-points. Therefore if the original line is represented either by a point and a vector or by two points, then the image L is represented by two mass-points (X_0, m_0) and (X_1, m_1) . Here if $m_k \neq 0$, then $X_k = m_k P_k$, where P_k is a point in affine space, whereas if $m_k = 0$, then $X_k = v_k$, where v_k is a vector. In either case, since L is determined by mass-points, to find the affine points on the projected line $P + tv \rightarrow (X_0, m_0) + t(X_1, m_1)$, we must divide by the mass. Thus L has a rational linear parameterization

$$L(t) = \frac{X_0 + tX_1}{m_0 + tm_1}.$$

If Q is a point on the line $L(t)$, then for some value of t

$$Q = \frac{X_0 + tX_1}{m_0 + tm_1}.$$

Multiplying both sides by $m_0 + tm_1$ yields

$$(m_0 + tm_1)Q = X_0 + tX_1$$

or equivalently

$$(m_0Q - X_0) = t(X_1 - m_1Q).$$

Dotting both sides with $X_1 - m_1Q$, and solving for t , we arrive at

$$t = \frac{(m_0Q - X_0) \cdot (X_1 - m_1Q)}{(X_1 - m_1Q) \cdot (X_1 - m_1Q)}. \quad (\text{inversion formula 3})$$

If $m_1, m_2 \neq 0$, then $(X_k, m_k) = (m_k P_k, m_k)$ and this formula reduces to

$$t = \frac{m_0(Q - P_0) \cdot (P_1 - Q)}{m_1(P_1 - Q) \cdot (P_1 - Q)} \quad (\text{inversion formula 4})$$

We shall have occasion to apply these inversion formulas for rational linear parameterizations of the line in Section 4.3 when we ray trace the cone.

4.2 Cylinders. A sphere is the locus of points equidistant from a given point; a cylinder is the locus of points equidistant from a given line. Thus a cylinder can be represented simply by an axis line L and a scalar radius R . Typically the axis line L is itself represented by a point Q on the line and a unit direction vector A (see Figure 3).

The normal N to the cylinder at a point P on the surface is just the orthogonal projection of the vector $P - Q$ onto the axis vector A (see Figure 3). Therefore,

$$N = (P - Q)_\perp = (P - Q) - ((P - Q) \cdot A)A.$$

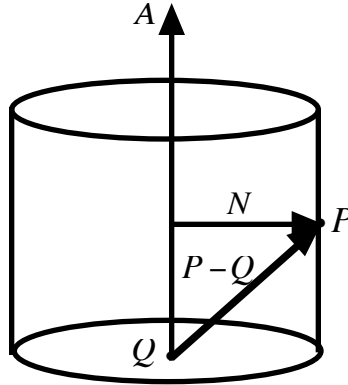


Figure 3: A right circular cylinder with an axis line L determined by a point Q and a unit direction vector A . The normal vector N to the surface of the cylinder at the point P is the orthogonal projection of the vector $P - Q$ onto the axis vector A .

As with the sphere, we can reduce the ray-cylinder intersection problem to a ray-circle intersection problem. The strategy here is to project both the cylinder and the line orthogonally onto the plane determined by the point Q and the axis vector A . The cylinder projects to the circle with center Q and radius R ; the line projects to another line. Now we can use the algorithm in the previous section to intersect the projected line with the circle. However, orthogonal projection is not an invertible map, so we cannot use the inverse map to recover the actual intersection points of the line and the cylinder.

What saves us here is our observation in Section 2 that the parameters of the intersection points of the projected line and the projected cylinder (the circle) are the same as the parameters of the intersection points of the unprojected line and the unprojected cylinder.

Thus to intersect a line and a cylinder we can proceed in the following manner. Let the line L be determined by a point P and a unit direction vector v . If the distance from the point Q on the cylinder axis to the line L is greater than the cylinder radius R or if $v \parallel A$, then there is no intersection between the line and the cylinder. Thus, once again, we have fast tests for rejection. If the line and the cylinder do intersect, then we project the line L orthogonally into the plane determined by the point Q and the axis vector A , and we intersect the projected line with the projection of the cylinder, the circle with center Q and radius R . We then apply the inversion formula for the projected line to find the corresponding parameter values. Finally, we substitute these parameters values into the equation of the original line L to find the intersection points of the line and the cylinder. Below is pseudocode for this Line-Cylinder intersection algorithm. Notice that this algorithm computes both the intersection points and the parameter values along the line corresponding to these intersection points.

Line-Cylinder Intersection Algorithm

Input

Q = Point on the Cylinder Axis
 A = Unit Direction Vector of the Cylinder Axis
 R = Cylinder Radius
 P = Point on the Line L
 v = Unit Vector in the Direction of the Line L

Algorithm

If $\text{Dist}(Q, L) > R$ or $v \parallel A$, there are no intersection points (fast reject).

Otherwise

Project the line L into the plane determined by the point Q and the axis vector A , and find the equation of the projected line L_{\perp} .

$$\begin{aligned} L_{\perp}(t) &= P_{\perp} + t v_{\perp} \\ v_{\perp} &= v - (v \cdot A) A \\ P_{\perp} &= P - ((P - Q) \cdot A) A \end{aligned}$$

Intersect the projected line L_{\perp} with the circle with center Q and radius R .

Apply the line-circle intersection algorithm of the previous section to find the intersection points D_1, D_2 .

Use the inversion formula for the line $L_{\perp}(t) = P_{\perp} + t v_{\perp}$ to find the corresponding parameter values $t = t_1, t_2$.

$$t_i = \frac{(P_{\perp} - D_i) \cdot v_{\perp}}{v_{\perp} \cdot v_{\perp}} = \frac{(P - D_i) \cdot v_{\perp}}{v \cdot v_{\perp}} \quad i = 1, 2$$

Substitute the parameters values $t = t_1, t_2$ into the equation of the line L to find the intersection points R_1, R_2 of the line and the cylinder.

$$R_i = L(t_i) = P + t_i v \quad i = 1, 2.$$

This algorithm intersects a line with an infinite cylinder. To intersect a line with a finite cylinder, first intersect the line with the infinite cylinder and then test whether the distance from the intersection point to the plane of the point Q and the normal vector A is less than the height of the cylinder. If the cylinder is closed, then additional computations will be needed to find the intersection of the ray with the planes at the top and the bottom of the cylinder.

4.3 Cones. A cone can be represented simply by a vertex V , a unit axis vector A , and a cone angle α (see Figure 4). Notice that a cylinder is a special case of a cone, where the vertex V is located at infinity.

The normal N to the cone at a point P on the surface is the sum of a component along the cone axis A and a component along the vector $P - V$ from the cone vertex V to the point P (see Figure 4).

4). By straightforward trigonometry, the length of component of N along A is $\frac{|P - V|}{\cos(\alpha)}$. Therefore,

$$N = (P - V) + \left\{ \frac{|P - V|}{\cos(\alpha)} \right\} A.$$

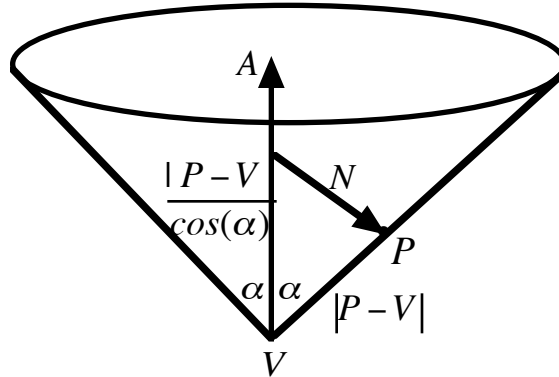


Figure 4: A right circular cone with a vertex V , an axis vector A , and a cone angle α . The normal vector N to the surface of the cone at the point P can be decomposed into the sum of two components: one along the axis of the cone and the other along the vector from the cone vertex V to the point P . By trigonometry, the length of component of N along A is $|P - V| / \cos(\alpha)$.

As with the cylinder, we can reduce the ray-cone intersection problem to a ray-circle intersection problem by projecting both the cone and the line onto the plane determined by the point $Q = V + A$ and the axis vector A . Here, however, instead of using orthogonal projection, we use perspective projection from the vertex of the cone. Under perspective projection, the cone projects to the circle with center Q and since $Dist(V, Q) = 1$, the radius $R = Tan(\alpha)$. The line projects to another line, but since perspective projection introduces mass, the projected line has a rational linear parameterization. Nevertheless, we can now proceed much as we did in the ray-cylinder intersection algorithm. We intersect the projected line with the circle to find the parameter values corresponding to the intersection points, and we substitute these parameter values back into the equation of the original line to find the intersection points of the line with the cone. Below is pseudocode for this Line-Cone intersection algorithm. As usual this algorithm computes both the intersection points and the parameter values along the line corresponding to these intersection points.

Line-Cone Intersection Algorithm

Input

V = Cone Vertex
 A = Unit Direction Vector of the Cone Axis
 α = Cone Angle
 P = Point on the Line L
 u = Unit Vector in the Direction of the Line L

Algorithm

Project the line L into the plane determined by the point $Q = V + A$ and the normal vector A , and find the rational parameterization of the projected line $\tilde{L}^*(t)$.

$$\tilde{L}^*(t) = \frac{X_0 + t X_1}{m_0 + t m_1}$$

$$X_0 = ((V - Q) \cdot A)P + ((Q - P) \cdot A)V = -P + ((Q - P) \cdot A)V$$

$$m_0 = (V - P) \cdot A = (Q - P) \cdot A - 1$$

$$X_1 = ((V - Q) \cdot A)u - (u \cdot A)V = -(u + (u \cdot A)V)$$

$$m_1 = -u \cdot A$$

Intersect the projected line \tilde{L}^* with the circle with center $Q = V + A$ and radius $R = Tan(\alpha)$.

Apply the line-circle intersection algorithm to find the intersection points D_1, D_2 .

There are four cases to consider, depending on the masses m_0, m_1 :

Case 1: $m_0 = m_1 = 0$. The line L projects to the line at infinity, so there are no intersection points between the circle and the line $\tilde{L}^*(t)$.

Case 2: $m_0, m_1 \neq 0$. The line $\tilde{L}^*(t)$ is determined by the two affine points

$\frac{X_0}{m_0}, \frac{X_1}{m_1}$ or equivalently by the point $P = \frac{X_0}{m_0}$ and the vector $v = \frac{X_0}{m_0} - \frac{X_1}{m_1}$.

Case 3: $m_0 \neq 0, m_1 = 0$. The line $L^*(t)$ is determined by the affine point $P = \frac{X_0}{m_0}$ and the vector $v = X_1$.

Case 4: $m_0 = 0, m_1 \neq 0$. The line $L^*(t)$ is determined by the affine point $P = \frac{X_1}{m_1}$ and the vector $v = X_0$.

Use the inversion formula for the rational linear parameterization of the line $L^*(t)$ to find the corresponding parameter values $t = t_1, t_2$.

$$t = \frac{(m_0 D_i - X_0) \cdot (X_1 - m_1 D_i)}{(X_1 - m_1 D_i) \cdot (X_1 - m_1 D_i)} \quad i = 1, 2$$

Substitute the parameters values $t = t_1, t_2$ into the equation of the line L to find the intersection points R_1, R_2 of the line and the cone.

$$R_i = L(t_i) = P + t_i v \quad i = 1, 2.$$

This algorithm intersects a line with a double infinite cone. To intersect a line with a finite cone, first intersect the line with the infinite cone and then test whether the distance from each intersection point to the plane of the vertex point V and the normal vector A is less than the height of the cone. If the cone is closed, then additional computations will be needed to find the intersection of the ray with the planes at the top and the bottom of the cone.

4.4 Ellipsoids, Elliptical Cylinders, and Elliptical Cones. The ellipsoid is a scaled sphere; the elliptical cylinder and the elliptical cone are scaled variants of the right circular cylinder and right circular cone. One simple strategy for ray tracing these elliptical surfaces is to apply non-uniform scaling to transform these surfaces to the corresponding natural quadrics, perform the surface normal and ray-surface intersection calculations on these natural quadrics, and then map the normal vectors and the ray-surface intersection points back to the elliptical quadrics.

For example, the ellipsoid can be represented by a center point C , three orthogonal unit axis vectors u, v, w , and three scalar lengths a, b, c . Scaling non-uniformly about the center point C by a in the u direction, b in the v direction, and c in the w direction maps the sphere with center C and unit radius to the ellipsoid (see Figure 5). The inverse transformation that maps the ellipsoid to the unit sphere scales non-uniformly about the center point C by $1/a$ in the u direction, $1/b$ in the v direction, and $1/c$ in the w direction.

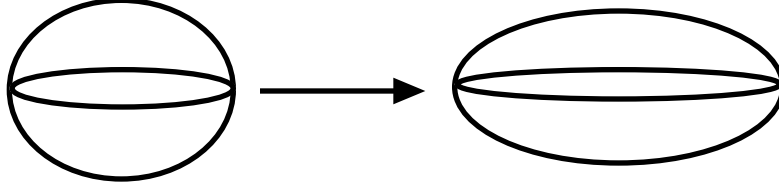


Figure 5: The ellipsoid is the image of the sphere under non-uniform scaling.

To find the normal vector to the ellipsoid at an arbitrary point, let M be the non-uniform scaling transformation that maps the sphere to the ellipsoid, and let N_E, N_S denote the normal vectors to the ellipsoid and the sphere at corresponding points. We know for any point P on the sphere how to compute $N_S = P - C$. Now we can easily compute N_E , since by the results in the previous lecture,

$$N_E = N_S * M_u^{-T},$$

where M_u is the upper 3×3 submatrix of M .

Intersection points between a ray L and an ellipsoid E are similarly easy to compute. Simply intersect the ray $L \cdot M^{-1}$ with the unit sphere centered at C using the algorithm in Section 4.1. If R_1, R_2 are the intersection points of $L \cdot M^{-1}$ with the unit sphere, then $R_1 * M, R_2 * M$ are the intersection points of L with the ellipsoid.

Analogous strategies can be applied to find the normal vectors and the ray-surface intersection points for the elliptical cylinder and the elliptical cone by applying non-uniform scaling transformations to the right circular cylinder and right circular cone. We leave the details as simple exercises for the reader (see Exercises 1,2)..

5. General Quadric Surfaces

A general quadric surface is the collection of points satisfying a second degree equation in x, y, z -- that is, an implicit equation of the form

$$Q(x, y, z) \equiv Ax^2 + By^2 + Cz^2 + 2Dxy + 2Eyz + 2Fxz + 2Gx + 2Hy + 2Iz + J = 0.$$

We can rewrite this equation in matrix notation. Let

$$P = (x, y, z, 1)$$

$$Q = \begin{pmatrix} A & D & F & G \\ D & B & E & H \\ F & E & C & I \\ G & H & I & J \end{pmatrix}.$$

Then

$$P * Q * P^T = Ax^2 + By^2 + Cz^2 + 2Dxy + 2Eyz + 2Fxz + 2Gx + 2Hy + 2Iz + J.$$

Thus in matrix notation, the equation of a quadric surface is

$$P * Q * P^T = 0.$$

For this reason, we will typically represent quadric surfaces by symmetric 4×4 matrices Q .

The normal vector to an implicit surface is parallel to the gradient. For a quadric surface

$$Q(x, y, z) = A x^2 + B y^2 + C z^2 + 2 D x y + 2 E y z + 2 F x z + 2 G x + 2 H y + 2 I z + J$$

the gradient

$$\nabla Q(x, y, z) = 2(A x + D y + F z + G, D x + B y + E z + H, F x + E y + C z + I).$$

Therefore the normal vector

$$N(x, y, z) \parallel (A x + D y + F z + G, D x + B y + E z + H, F x + E y + C z + I).$$

Equivalently in matrix notation,

$$N(x, y, z) \parallel P * Q_{4 \times 3}. \quad (5.1)$$

where $Q_{4 \times 3}$ consists of the first three columns of Q .

To intersect a line $L(t) = P + t v$ with a quadric surface Q , we can use the quadratic formula to solve the second degree equation

$$L(t) * Q * L(t)^T = 0.$$

The real roots of this equation represent the parameter values along the line of the intersection points. The actual intersection points can be computed by substituting these parameter values into the parametric equation $L(t) = P + t v$ for the line.

Affine and projective transformations map quadric surfaces to quadric surfaces. To find the image of a quadric surface Q under an nonsingular transformation matrix M , recall that for any implicit surface $F(P) = 0$, the equation of the transformed surface is

$$F_{new}(P) = F(P * M^{-1})$$

For a quadric surface represented by a symmetric 4×4 matrix Q , this result means that

$$P * Q_{new} * P^T = (P * M^{-1}) * Q * (P * M^{-1})^T = P * (M^{-1} * Q * M^{-T}) * P.$$

Therefore

$$Q_{new} = M^{-1} * Q * M^{-T} \quad (5.2)$$

is the matrix representation of the transformed surface.

There are many different types of quadric surfaces. In addition the the natural quadrics -- the sphere, the right circular cylinder and the right circular cone -- and their elliptical variants, there are also parabolic and hyperbolic cylinders, elliptical and hyperbolic paraboloids, and hyperboloids of one or two sheets. In Table 1, we list the equations of the different types of quadric surfaces in canonical position -- that is, with center at the origin and axes along the coordinate axes.

<i>Sphere</i> $x^2 + y^2 + z^2 - R^2 = 0$	<i>Right Circular Cylinder</i> $x^2 + y^2 - R^2 = 0$	<i>Right Circular Cone</i> $x^2 + y^2 - c^2 z^2 = 0$
<i>Ellipsoid</i> $\frac{x^2}{a^2} + \frac{y^2}{b^2} + \frac{z^2}{c^2} - 1 = 0$	<i>Elliptical Cylinder</i> $\frac{x^2}{a^2} + \frac{y^2}{b^2} - 1 = 0$	<i>Elliptical Cone</i> $\frac{x^2}{a^2} + \frac{y^2}{b^2} - z^2 = 0$
<i>Parabolic Cylinder</i> $x^2 - 4py = 0$	<i>Hyperbolic Cylinder</i> $\frac{x^2}{a^2} - \frac{y^2}{b^2} - 1 = 0$	<i>Elliptical Paraboloid</i> $\frac{x^2}{a^2} + \frac{y^2}{b^2} - z = 0$
<i>Hyperbolic Paraboloid</i> $\frac{x^2}{a^2} - \frac{y^2}{b^2} - z = 0$	<i>Hyperboloid of One Sheet</i> $\frac{x^2}{a^2} - \frac{y^2}{b^2} - \frac{z^2}{c^2} - 1 = 0$	<i>Hyperboloid of Two Sheets</i> $\frac{x^2}{a^2} + \frac{y^2}{b^2} - \frac{z^2}{c^2} - 1 = 0$

Table 1: Equations of quadric surfaces in canonical position.

Special ray tracing algorithms for the natural quadrics and their elliptical variants are presented in Section 4. The reason that these special ray tracing techniques are effective is that it is easy to represent the natural quadrics in arbitrary positions geometrically without resorting to equations. But it is not so natural to represent general quadric surfaces such as paraboloids and hyperboloids in arbitrary positions geometrically without resorting to equations, and even if such geometric representations were feasible, straightforward intersection algorithms are not readily available. Rather than start with a quadric surface in general position, typically one starts with a quadric surface in canonical position and then repositions the surface by applying a rigid motion M .

Now there are two ways we can proceed to ray trace a quadric surface in general position. We can compute the equation of the surface and the surface normal in general position from the equation of the surface in canonical position using Equations (5.1) and (5.2). We can then solve the general second degree equation to find the intersection of the ray and the quadric surface. Alternatively, if we store the transformation matrix M along with the equation of the surface in canonical position, then we can compute the normal to the surface in arbitrary position from the normal to the surface in canonical position from the formula

$$N_{new} = N_{old} * M_u^{-T}.$$

The normal N_{old} to the surface in canonical position is parallel to the gradient, and this gradient is easy to compute because the canonical equation is simple. Similarly, to intersect a line L with a quadric surface in general position, we can intersect the line $L * M^{-1}$ with the quadric surface in canonical position and then map these intersection points back to the desired intersection points by the transformation M . Again since the equation of a quadric in canonical position is simple, the quadratic equation for the intersection of a line and a quadric in canonical position is also simple.

6. Tori

The torus is the next most common surface in computer graphics, after the plane and the natural quadrics. A torus can be represented geometrically by a center point C , an axis vector A , and two scalar radii d, a (see Figure 6). Cutting the torus by the plane through C orthogonal to A generates two concentric circles with center C on the surface of the torus. The scalar d represents the radius of a third concentric circle midway between these two circles -- that is, a circle inside the torus. We call this circle the *generator* of the torus. The surface of the torus consist of all points at a fixed distance a from this generator. Thus the scalar a is the radius of the toroidal tube.

To find the implicit equation of the torus, project an arbitrary point P on the torus orthogonally into the plane of the generator. Then the point P , the image point Q , and the point R lying on the generator between Q and C form a right triangle whose hypotenuse has length a . Thus by the Pythagorean theorem

$$|P - Q|^2 + |Q - R|^2 = a^2. \quad (6.1)$$

But $|P - Q|$ is just the distance from the point P to the plane determined by the center point C and the axis vector A , which in turn is just the length of the parallel projection of the vector $P - C$ on A . Therefore

$$|P - Q| = |(P - C) \cdot A|. \quad (6.2)$$

Moreover,

$$|Q - R| = |Q - C| - d, \quad (6.3)$$

and $|Q - C|$ is just the length of the perpendicular projection of the vector $P - C$ on A . Therefore

$$|Q - C| = |(P - C)_\perp| = \sqrt{|P - C|^2 - ((P - C) \cdot A)^2}. \quad (6.4)$$

Substituting Equations 6.2-6.4 into Equation 6.1, we arrive at the following implicit equation for the torus in general position:

$$\left(\underbrace{(P - C) \cdot A}_{\text{Dist. to Plane}} \right)^2 + \left(\underbrace{\sqrt{|P - C|^2 - ((P - C) \cdot A)^2}}_{\text{Dist. of Projection to Center}} - \underbrace{d}_{\text{Radius of Generator}} \right)^2 = a^2. \quad (6.5)$$

Because of the square root, this equation is actually degree four in the coordinates (x, y, z) of the point P , since to clear the square root we must square the equation.

We can also find the normal N to the surface of the torus at the point P by a geometric argument. Cut the torus by the plane determined by the point P and the axis of the torus. The intersection of this plane and the torus consists of two circle; one of these circles passes through the point P . The center of this circle is the point R on the generator of the torus, and the vector $P - R$ from R to P is orthogonal to the surface of the torus. Thus we need to find the point R .

Now R is on the line from Q to C , and

$$Q = P - ((P - C) \cdot A)A.$$

Let q be the distance from Q to C . Then

$$q = |Q - C| = \sqrt{|P - C|^2 - ((P - C) \cdot A)^2}.$$

Thus

$$R = C + (d/q)(Q - C),$$

so

$$N \parallel P - R = (P - C) - (d/q)(Q - C).$$

To intersect a line $L(t) = P + tv$ with a torus, we simply substitute the parametric equations of the line into the implicit equation for the torus and solve the fourth degree equation

$$((L(t) - C) \cdot A)^2 + \left(\sqrt{|L(t) - C|^2 - ((L(t) - C) \cdot A)^2} - d \right)^2 = a^2.$$

The real roots of this equation represent the parameter values along the line of the intersection points. As usual, the actual intersection points can be computed by substituting these parameter values into the parametric equation $L(t) = P + tv$ for the line.

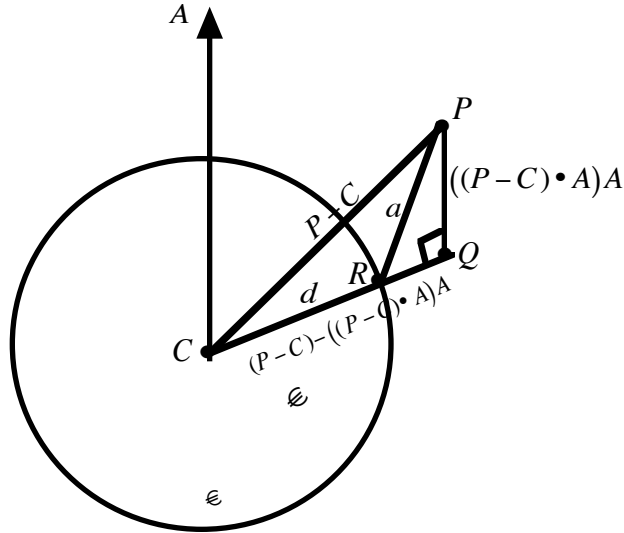


Figure 6: The torus. The circle is a generator for the torus at a distance d from the center of the torus. The radius of the inner tube is a .

The implicit equation for the torus in general position is somewhat complicated. Often, as with general quadric surfaces, it is easier to begin with a torus in canonical position -- with center at the origin and axis along the z -axis -- and then apply a rigid motion to relocate the torus to an arbitrary

position and orientation. This approach also works for an elliptical torus, since we can include a non-uniform scaling along with the rigid motion.

To find the implicit equation of the torus in canonical position, substitute $C = (0,0,0)$ and $A = (0,0,1)$ into Equation (6.5), the implicit equation of the torus in general position. Squaring to eliminate the square root and simplifying the algebra, we arrive at the fourth degree implicit equation for the torus in canonical position

$$T(x,y,z) \equiv \left(x^2 + y^2 + z^2 - d^2 - a^2\right)^2 + 4d^2z^2 - 4a^2d^2 = 0.$$

The normal vector $N(x,y,z)$ to the surface $T(x,y,z)$ is given by the gradient. Therefore

$$N(x,y,z) = \left(\frac{\partial T}{\partial x}, \frac{\partial T}{\partial y}, \frac{\partial T}{\partial z}\right) = \left(4xG(x,y,z), 4yG(x,y,z), 4z(G(x,y,z) + 2d^2)\right)$$

$$G(x,y,z) = x^2 + y^2 + z^2 - d^2 - a^2.$$

To reposition the torus so that the center is at C and the axis is oriented along the direction A , rotate the z -axis to A and then translate the origin to C . These transformations are given explicitly by the matrices

$$trans(C) = \begin{pmatrix} I & 0 \\ C & 1 \end{pmatrix}$$

$$rot(u, \theta) = \cos(\theta)I + (1 - \cos(\theta))(u \otimes u) + \sin(\theta)(u \times _)$$

where $u = \frac{k \times A}{|k \times A|}$ and $\cos(\theta) = k \cdot A$.

Now we can find normal vectors on the surface of the torus in general position simply by transforming the corresponding normal vectors from canonical position. Thus

$$N_{general \ position} = N_{canonical \ position} * rot(u, \theta).$$

(Notice that $rot(u, \theta)^{-T} = rot(u, \theta)$, so we do not have to take the inverse transpose.) Similarly, we can intersect lines with the torus in general position by transforming the lines to canonical position via the inverse transformation

$$M^{-1} = trans(-C) * rot(u, -\theta),$$

intersecting the transformed lines with the torus in canonical position, and then transforming the intersection points back to general position using the forward transformation matrix

$$M = \begin{pmatrix} rot(u, \theta) & 0 \\ trans(C) & 1 \end{pmatrix}.$$

7. Surfaces of Revolution

A surface of revolution is a surface generated by rotating a planar curve called the *directrix* about an axis line. Thus the cross sections of a surface of revolution by planes orthogonal to the axis of revolution are circles. Spheres, right circular cylinders, right circular cones, and tori are all examples of surfaces of revolution.

So far we have studied special surfaces using either a geometric approach or implicit equations. Surfaces of revolution, however, are modeled most easily using parametric equations.

Consider a parametric curve

$$D(u) = (f(u), 0, g(u))$$

in the xz -plane. Rotating this curve about the z -axis generates the parametric surface

$$R(u, v) = (f(u)\cos(v), f(u)\sin(v), g(u)) \quad (7.1)$$

(see Figure 7). If we fix a parameter $u = u^*$, then the plane $z = g(u^*)$ intersects the surface $R(u, v)$ in the circle

$$C(v) = (f(u^*)\cos(v), f(u^*)\sin(v), g(u^*))$$

with center $(0, 0, g(u^*))$ and radius $f(u^*)$, since $x^2 + y^2 = f^2(u^*)$. Thus cross sections of the surface $R(u, v)$ by planes perpendicular to the z -axis are indeed circles, so the parametric surface $R(u, v)$ truly is a surface of revolution. Table 2 provides some examples of simple directrix curves and the corresponding surfaces of revolution. Using this table together with Equation (7.1) allows us to generate simple parametric equations for cylinders, cones, spheres, and tori.

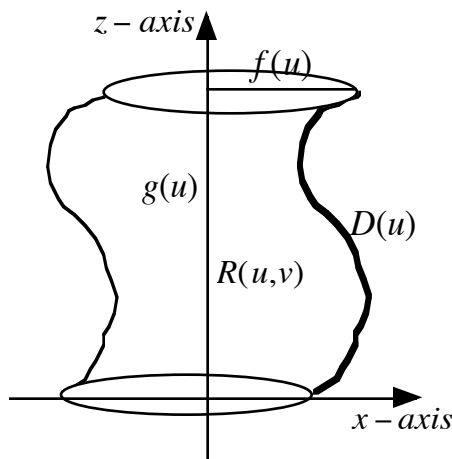


Figure 7: Surface of revolution $R(u, v)$ with directrix $D(u)$.

Directrix

Line: $D(u) = (1, 0, u)$

Line: $D(u) = (u, 0, u)$

Circle: $D(u) = (\cos(u), 0, \sin(u))$

Circle $D(u) = (d + a \cos(u), 0, a \sin(u))$

Surface of Revolution

Cylinder: $R(u, v) = (\cos(v), \sin(v), u)$

Cone: $R(u, v) = (u \cos(v), u \sin(v), u)$

Sphere: $R(u, v) = (\cos(u) \cos(v), \cos(u) \sin(v), \sin(u))$

Torus: $R(u, v) = \begin{pmatrix} (d + a \cos(u)) \cos(v) \\ (d + a \cos(u)) \sin(v) \\ a \sin(u) \end{pmatrix}$

Table 2: Directrix curves that are lines and circles together with the corresponding surfaces of revolution. The axis of revolution is the z -axis.

We are not restricted to surfaces of revolution whose axes of revolution are the z -axis. To extend our parametric equations to general position, we first rewrite the parametric equations of the directrix and the surface of revolution in vector notation

$$D(u) = \text{Origin} + f(u)i + g(u)k$$

$$R(u, v) = \text{Origin} + f(u) \cos(v)i + f(u) \sin(v)j + g(u)k.$$

Rotating the axis vectors i, j, k to three arbitrary orthogonal unit vectors C, B, A and then translating the origin to an arbitrary point E , we arrive at the parametric equations of the directrix and the surface of revolution in general position

$$D(u) = E + f(u)C + g(u)A$$

$$R(u, v) = E + f(u) \cos(v)C + f(u) \sin(v)B + g(u)A.$$

Notice that here the axis of revolution is parallel to the vector A ; the vectors B and C are orthogonal unit vectors perpendicular to A .

There is not much difference between working in canonical position and working in general position for surfaces of revolution, since we can always transform from canonical position to general position by the rigid motion

$$M = \begin{pmatrix} C & 0 \\ B & 0 \\ A & 0 \\ E & 1 \end{pmatrix}.$$

Therefore, for the remainder of this discussion, we will consider surfaces of revolution in canonical position, where the axis of revolution is the z -axis.

The normal vector to a parametric surface is parallel to the cross product of the partial derivatives. For the surface of revolution in Equation (7.1),

$$R(u, v) = (f(u) \cos(v), f(u) \sin(v), g(u))$$

so

$$\frac{\partial R}{\partial u} = (f'(u)\cos(v), f'(u)\sin(v), g'(u))$$

$$\frac{\partial R}{\partial v} = (-f(u)\sin(v), f(u)\cos(v), 0).$$

Therefore,

$$N(u, v) \parallel \frac{\partial R}{\partial u} \times \frac{\partial R}{\partial v} = (-f(u)g'(u)\cos(v), -f(u)g'(u)\sin(v), f(u)f'(u))$$

A surface of revolution

$$R(u, v) = (f(u)\cos(v), f(u)\sin(v), g(u))$$

intersects a line

$$L(t) = At + B = (A_x t + B_x, A_y t + B_y, A_z t + B_z),$$

at parameters where

$$R(u, v) = L(t) \Leftrightarrow (f(u)\cos(v), f(u)\sin(v), g(u)) = (A_x t + B_x, A_y t + B_y, A_z t + B_z)$$

Thus to find the intersection of a line and a surface of revolution, we need to solve three simultaneous nonlinear equations with three unknown t, u, v . The simplest of these three equations is the z -equation, since only two parameters u, t appear in this equation. Solving $A_z t + B_z = g(u)$ for t yields

$$t = \frac{g(u) - B_z}{A_z}, \quad (7.2)$$

so we can eliminate one of the variables. {If $L(t)$ is horizontal, then $A_z = 0$ and we can solve $g(u) = B_z$ directly for u .} Next, summing the squares of the x, y equations and invoking the trigonometric identity

$$\cos^2(v) + \sin^2(v) = 1$$

yields

$$f^2(u) = (A_x t + B_x)^2 + (A_y t + B_y)^2 \quad (7.3)$$

Since we already know t as a function of u , we can reduce this equation to one unknown. We then solve Equation (7.3) for u , usually by numerical methods. The corresponding t parameters can now be computed from Equation (7.2). Finally taking the ratio of the x and y equations yields

$$\tan(v) = \frac{A_y t + B_y}{A_x t + B_x} \Rightarrow v = \tan^{-1}\left(\frac{A_y t + B_y}{A_x t + B_x}\right).$$

The only bottleneck in this intersection algorithm is solving Equation 7.2. If $f(u), g(u)$ are trigonometric functions, as is the case for the sphere and the torus in Table 2, then this equation contains transcendental functions and may be difficult to solve.

Fortunately, there is a trick for replacing sines and cosines by rational functions. Let

$s = \tan(u/2)$. Then

$$\cos(u) = \cos^2(u/2) - \sin^2(u/2) = 2\cos^2(u/2) - 1 \Rightarrow \cos^2(u/2) = \frac{1 + \cos(u)}{2}$$

so

$$s^2 + 1 = \tan^2(u/2) + 1 = \sec^2(u/2) = \frac{1}{\cos^2(u/2)} = \frac{2}{1 + \cos(u)}.$$

Solving for $\cos(u)$, we find that

$$\cos(u) = \frac{1 - s^2}{1 + s^2} \quad \text{and} \quad \sin(u) = \frac{2s}{1 + s^2}$$

Replacing sine and cosine with rational functions often leads to faster computations. Moreover, it is generally easier to solve polynomial equations than to solve trigonometric equations.

Exercises

1. Explain in detail how to ray trace an elliptical cylinder. In particular, explain how you would
 - i. model the elliptical cylinder;
 - ii. compute the surface normals to the elliptical cylinder;
 - iii. find ray-surface intersections for the elliptical cylinder.
2. Explain in detail how to ray trace an elliptical cone. In particular, explain how you would
 - i. model the elliptical cone;
 - ii. compute the surface normals to the elliptical cone;
 - iii. find ray-surface intersections for the elliptical cone.
3. Let $D(s) = (x(s), y(s), z(s))$ be a parametrized curve lying in a plane in 3-space, and let $v = (v_1, v_2, v_3)$ be a fixed vector in 3-space not in the plane of $D(s)$. The parametric surface:

$$C(s, t) = D(s) + tv$$

is called the *generalized cylinder* over the curve $D(s)$. Suppose that you already have an algorithm to compute the intersection points of any line in the plane of $D(s)$ with the curve $D(s)$. Based on this algorithm, develop a procedure to find the intersection points of an arbitrary line in 3-space with the surface $C(s, t)$.

4. Let $D(s) = (x(s), y(s), z(s))$ be a parametrized curve lying in a plane in 3-space, and let $Q = (q_1, q_2, q_3)$ be a fixed point in 3-space not in the plane of $D(s)$. The parametric surface:

$$C(s, t) = (1 - t)D(s) + tQ$$

is called the *generalized cone* over the curve $D(s)$. Suppose that you already have an algorithm to compute the intersection points of any line in the plane of $D(s)$ with the curve $D(s)$. Based on

this algorithm, develop a procedure to find the intersection points of an arbitrary line in 3-space with the surface $C(s,t)$.

5. Let $U_1(s), U_2(s)$ be two curves in 3-space. The parametric surface

$$R(s,t) = (1-t)U_1(s) + tU_2(s)$$

is called the *ruled surface* generated by the curves $U_1(s), U_2(s)$. Explain how you would find the intersection points of a ruled surface $R(s,t)$ with an arbitrary straight line $L(t)$.

6. Let $R(s) = R + su$ and $P(t) = P + tv$ be two intersecting lines in 3-space. Let v_{\perp} be the component of v perpendicular to u .

a. Show that the lines $R(s)$ and $P(t)$ intersect at the parameter value

$$t = \frac{(R - P) \cdot v_{\perp}}{v \cdot v_{\perp}}$$

b. Use the result of part a to find the parameter value where the line and the cylinder intersect without resorting to the inversion formula for the line $L_{\perp}(t)$.

c. Use the result of part a to find the parameter value where the line and the cone intersect without resorting to the inversion formula for the rational linear parameterization of the line $L^*(t)$

7. Let $R = (x_0, y_0, z_0, 1)$ be a point on a quadric surface represented by a symmetric 4×4 matrix Q . Show that the equation of the plane tangent to the quadric Q at the point R is given by $R * Q * P^T = 0$.

8. Find the symmetric 4×4 matrices representing each of the quadrics in Table 1.

9. Compute the mean and Gaussian curvature for each of the quadrics in Table 1.

10. Compute the mean and Gaussian curvature for a torus in canonical position in two ways:

- from the implicit equation
- from the parametric equation

11. A *cyclide* is a surface whose lines of constant curvature are all either circles or straight lines. (The torus is a special case of a cyclide.) The equation of a cyclide in canonical position -- centered at the origin with axes aligned along the coordinate axes -- is

$$F(x, y, z) = \left(x^2 + y^2 + z^2 - d^2 + b^2 \right)^2 - 4(ax - cd)^2 - 4b^2y^2 = 0$$

where a, b, c, d are constants such that $c, d \geq 0$, $b > 0$, and $a^2 = b^2 + c^2$.

- a. For the cyclide in canonical position, explain how you would:
 - i. compute the normal vector at the point (x, y, z) ,
 - ii. find the intersection with an arbitrary straight line.
 - b. For a cyclide in arbitrary position -- a cyclide with center at the point C and axes aligned along three mutually orthogonal unit vectors u, v, w -- explain how you would:
 - i. model the cyclide,
 - ii. compute the normal to the cyclide at the point (x, y, z) ,
 - iii. find the intersection of the cyclide with an arbitrary straight line.
12. Consider a surface whose cross sections by planes perpendicular to a fixed line L are ellipses whose centers lie on the line L and whose major axes are all parallel to each other. Explain how you would:
- a. model this surface,
 - b. compute the normal to this surface at an arbitrary point on the surface,
 - c. find the intersection of this surface with an arbitrary straight line.
13. Consider a surface of revolution
- $$R(u, v) = (f(u)\cos(v), f(u)\sin(v), g(u)).$$
- Suppose that there is a function $F(u)$ such that
- $$F(g(u)) = f^2(u).$$
- a. Show that the implicit equation of $R(u, v)$ is given by

$$x^2 + y^2 = F(z).$$
 - b. Find the function $F(u)$ for each of the surfaces of revolution in Table 2.
 - c. Using the results of part b, find the implicit equation for each of the surfaces of revolution in Table 2.
14. Consider the parameterizations in Table 2 of the cylinder, the cone, the sphere, and the torus.
- a. using the substitution $t = \tan(v/2)$ find parameterizations for the cylinder and the cone that do not involve trigonometric functions.
 - b. using in addition the substitution $s = \tan(u/2)$ find parameterizations for the sphere and the torus that do not involve trigonometric functions.