

## EXERCISE 3

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# SC Circuit

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## 1. OBJECTIVE

### 1 Objective

The main target of this laboratory exercise is to make certain that we understand the way that switching capacitors works, better understand them and know how to solve exercises about them. Also we will work on switching between Z and S domain and see differences between them.

### 2 Exercise 1: Low pass filter and its SC circuit analysis

Design a low pass passive first order filter with  $f_c = 1\text{kHz}$  and write a transfer function  $H(s)$ . Same structure must be realized in discrete z-domain (resistor must be replaced with SC circuit) where transfer function  $H(z)$  must be plotted and compared with continuous time  $H(s)$  transfer function. Draw the SC schematic. Use `freqs()` and `freqz()` functions.

For the design of the low pass filter we will use a RC circuit like this:

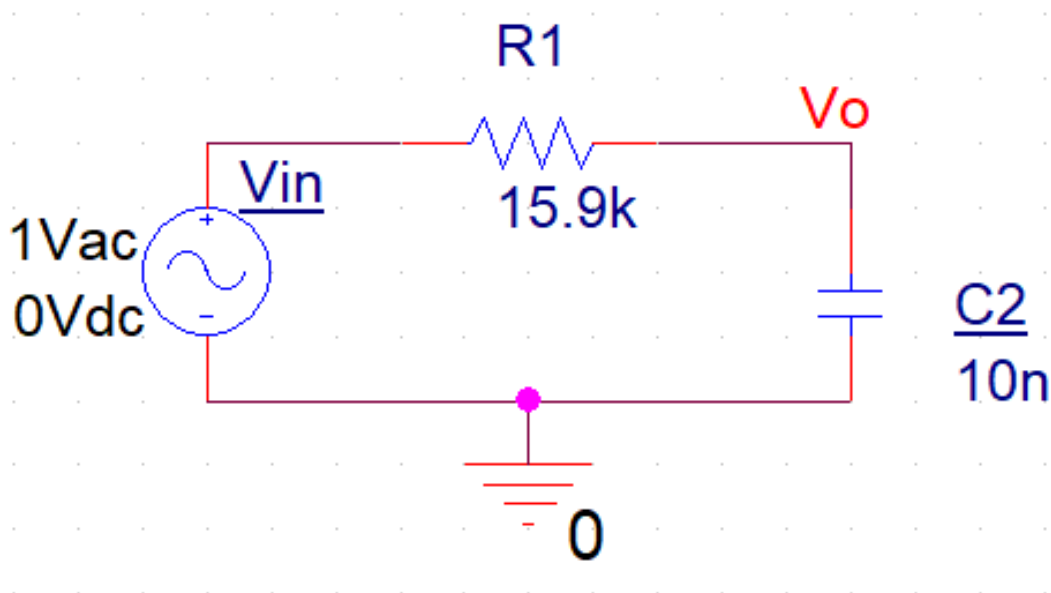


Figure 1: Schematic of the low pass filter

We need a  $f_c$  of  $1\text{kHz}$ , so we will calculate the components of such filter and confirm that

## 2. EXERCISE 1: LOW PASS FILTER AND ITS SC CIRCUIT ANALYSIS

we have a LPF. We know that a LPF transfer function looks like this:

$$H(s) = \frac{w_c}{s+w_c} = \frac{1}{1+s/w_c}$$

So now, we will get the transfer function of our schematic and obtain the value of the components.

$$Vo(s) = Vin(s) \cdot \frac{1/C_2s}{1/C_2s+R}$$

$$H(s) = \frac{Vo(s)}{Vin(s)} = \frac{1/C_2s}{1/C_2s+R} = \frac{1}{1+RC_2s}$$

Comparing the obtained transfer function with the theoretical one and fixing a value to the capacitor (we will choose 10pF) we will get the value of the resistor

$$H(s) = \frac{w_c}{s+w_c} = \frac{1}{1+s/w_c} = \frac{1}{1+RC_2s}$$

$$RC = \frac{1}{w_c} \rightarrow R = \frac{1}{2\pi \cdot f_c \cdot 10pF} = 15.9k\Omega$$

We will simulate the schematic doing an AC sweep from 10Hz to 500kHz in OrCAD to see the result:

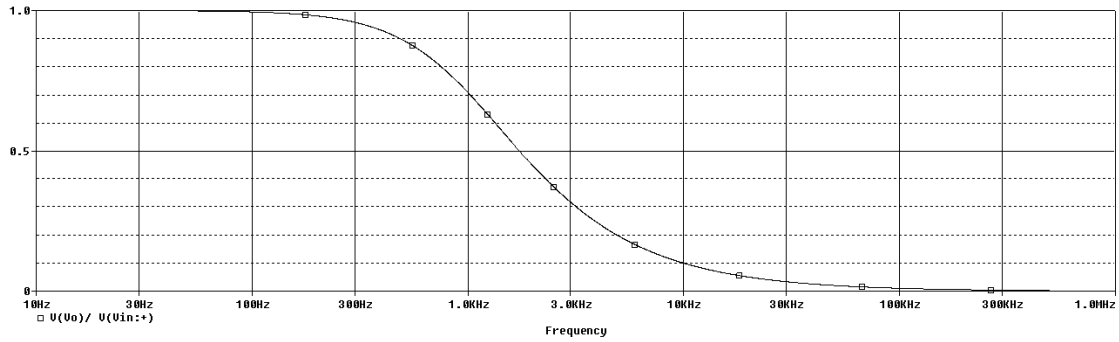


Figure 2: Bode diagram of the designed schematic

Now we will draw the corresponding SC schematic that will look like this:

## 2. EXERCISE 1: LOW PASS FILTER AND ITS SC CIRCUIT ANALYSIS

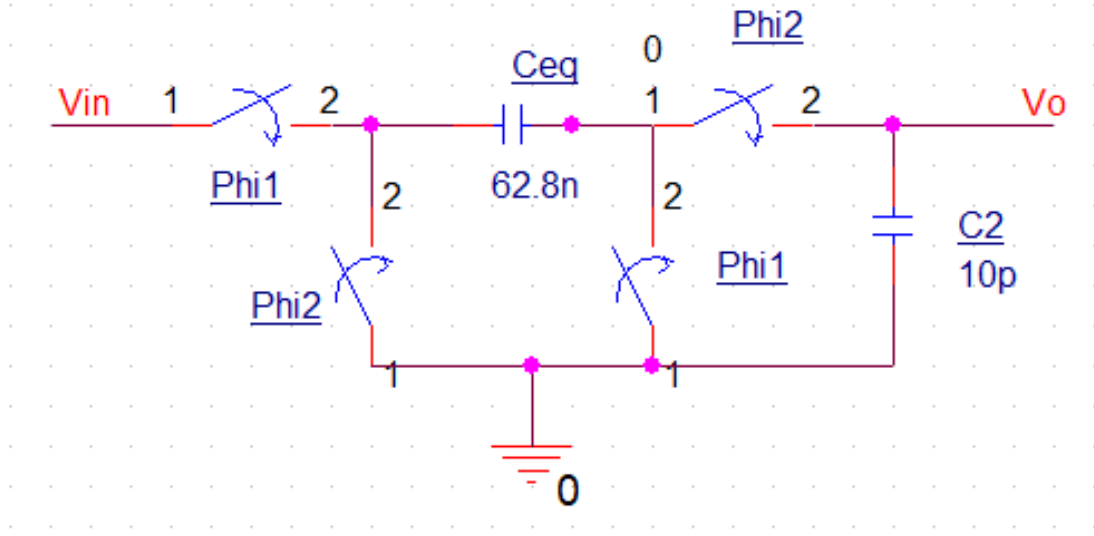


Figure 3: SC shematic

Where  $Ceq = \frac{1}{R \cdot f_s}$ . In order to study the SC schematic we will use the balance of charge theorem:

In (n-1)  $\phi_1$  will be closed and  $\phi_2$  open so we will have:

$$Vin(n-1) \cdot Ceq + Vo(n-1) \cdot C_2$$

In (n)  $\phi_1$  will be open and  $\phi_2$  closed so we will have:

$$Vo(n) \cdot (C_2 + Ceq)$$

Since the charge has to remain the same, we will equal the two equations and work in the Z domain to obtain the transfer function

$$Vin(n-1) \cdot Ceq + Vo(n-1) \cdot C_2 = Vo(n) \cdot (C_2 + Ceq)$$

$$Vin \cdot z^{-1} \cdot Ceq + Vo \cdot z^{-1} \cdot C_2 = Vo \cdot z \cdot (C_2 + Ceq)$$

$$Vo[-z^{-1} + (C_2 + Ceq)] = Vin \cdot z^{-1} \cdot Ceq$$

$$H(z) = \frac{Vo}{Vin} = \frac{z^{-1} \cdot Ceq}{-z^{-1} + (C_2 + Ceq)}$$

To conclude exercise 1 we will use MatLab in order to compare results and we will plot magnitude and phase diagrams of Bode both in Z and S domain using the functions *freqs* and *freqz*. The code will be explained in the appendix via comments:

## 2. EXERCISE 1: LOW PASS FILTER AND ITS SC CIRCUIT ANALYSIS

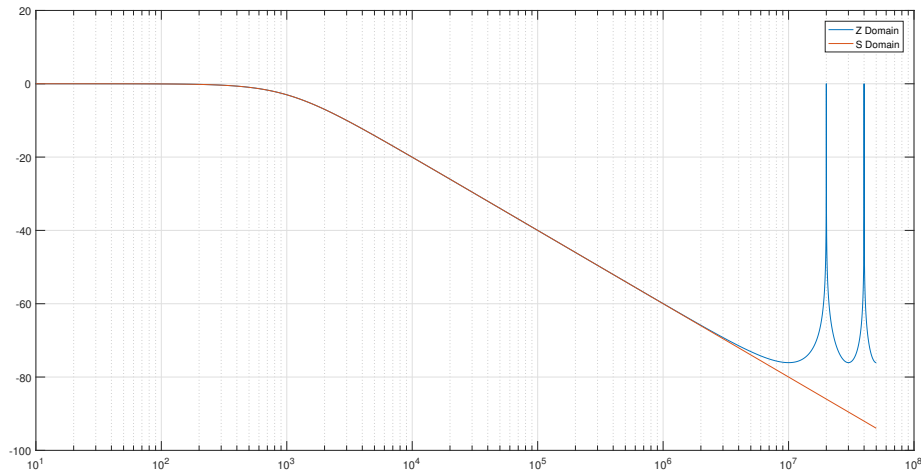


Figure 4: Magnitude diagram in S and Z Domain

Looking at the magnitude diagram we see how it decreases -20dB per decade, it is a first order filter, and we can also appreciate that the pole frequency is the expected one

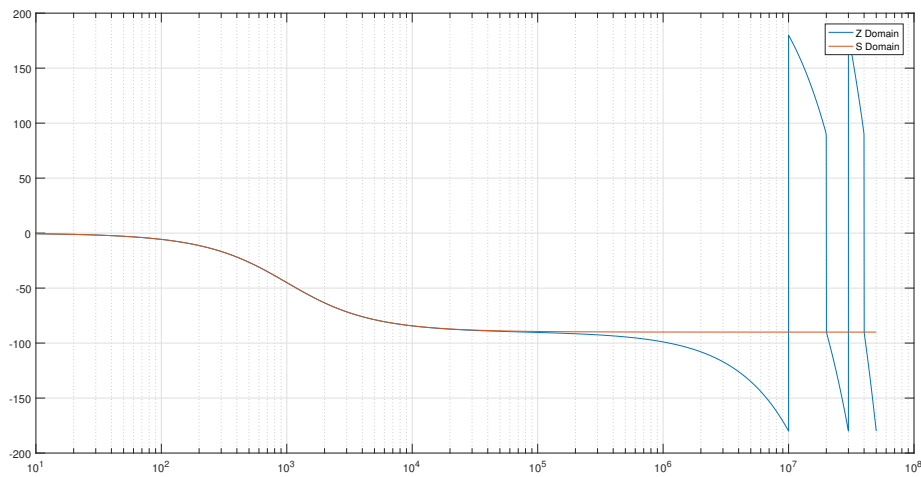


Figure 5: Phase diagram in S and Z Domain

The phase diagram is also the expected one, it decreases  $90^\circ$  ( $\frac{\pi}{2}$  rad) and the pole frequency is 1kHz

The spikes that we are getting in both graphics are due to the digital filter, but since we

### 3. EXERCISE 2: ANALYSIS OF INVERTING AND NON-INVERTING SC AMPLIFIER

are using a high sampling frequency they are out of the filter and its not a problem.(If we would use lower  $F_s$  they may be in the middle of the filter)

## 3 Exercise 2: Analysis of inverting and non-inverting SC amplifier

Determine transfer function of the circuits in the Figure 6 and 7. Capacitors must be calculated from the switching frequency  $F_s=1$  MHz and its value should not exceed 1 pF. The gain at low frequencies is 40 dB. The characteristics of the opamp and the switches are ideal.

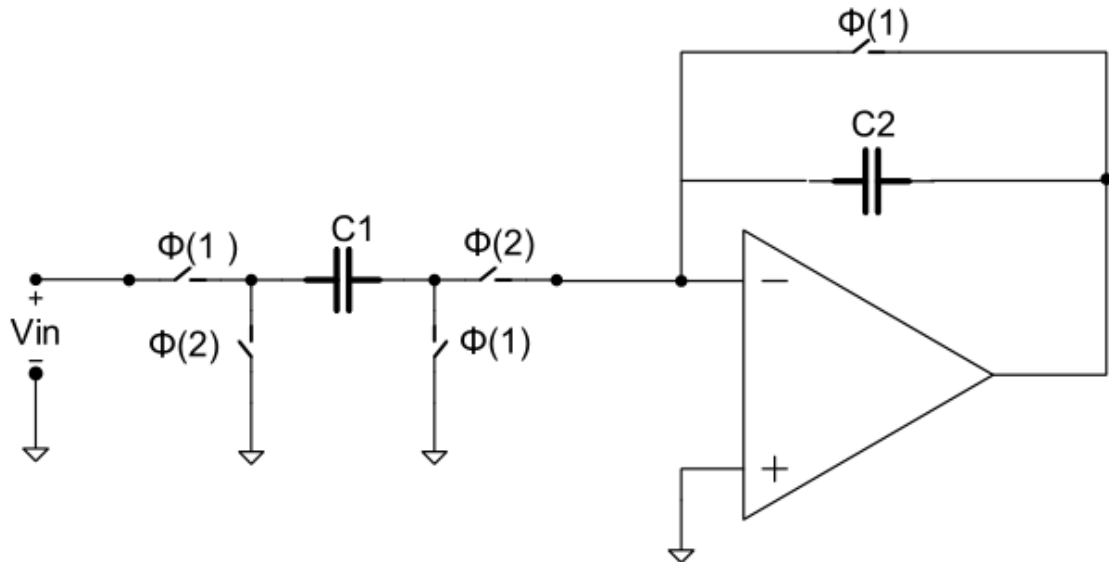


Figure 6: Non-inverting SC amplifier.

We will now obtain the transfer function of the first schematic:

In  $(n-1)$   $\phi_1$  will be closed and  $\phi_2$  open so we will have:

$$V_{in}(n-1) \cdot C_1$$

In  $(n)$   $\phi_1$  will be open and  $\phi_2$  closed so we will have:

$$V_o(n) \cdot C_2$$

### 3. EXERCISE 2: ANALYSIS OF INVERTING AND NON-INVERTING SC AMPLIFIER

We will transfer the equations to Z domain and equal them:

$$Vin(n-1) \cdot C_1 = Vo(n) \cdot C_2$$

$$Vin \cdot z^{-1} \cdot C_1 = Vo \cdot C_2$$

$$H(z) = \frac{Vo}{Vin} = \frac{C_1}{C_2} z^{-1}$$

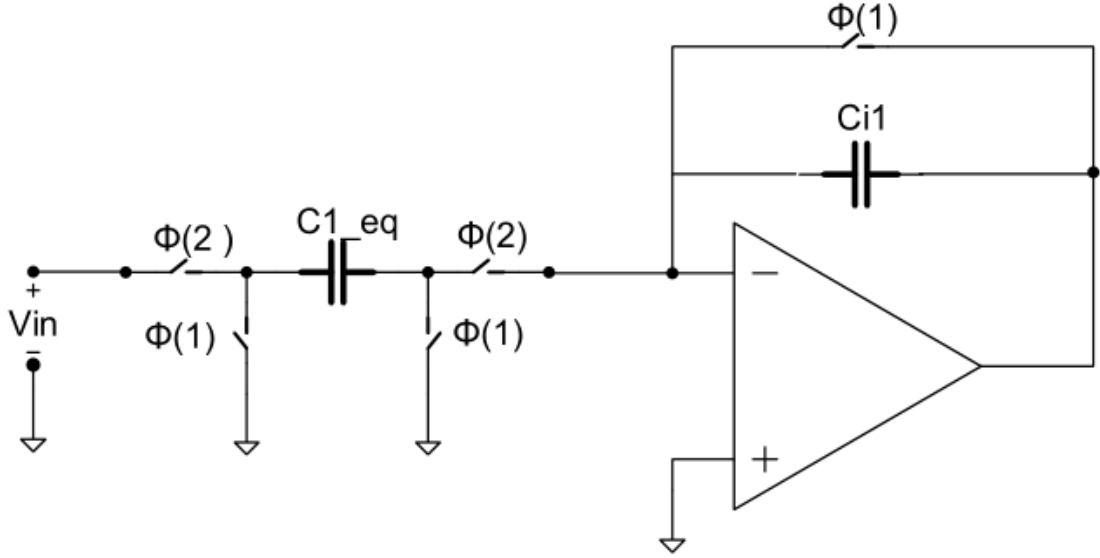


Figure 7: Inverting SC amplifier.

For the second schematic we will do pretty much the same:

In (n-1)  $\phi_1$  will be closed and  $\phi_2$  open so we won't have any equation

In (n)  $\phi_1$  will be open and  $\phi_2$  closed so we will have:

$$Vi(n) \cdot C1_{eq} + Vo(n) \cdot Ci_1$$

We will transfer the equations to Z domain and equal them:

$$0 = Vi(n) \cdot C1_{eq} + Vo(n) \cdot Ci_1$$

$$Vi \cdot C1_{eq} + Vo \cdot Ci_1 = 0$$

$$H(z) = \frac{Vo}{Vin} = -\frac{C1_{eq}}{Ci_1}$$

In both we have the same scenario, the gain is the division of both and since we want a gain of 40dB (100 in linear) we will need  $C1$  and  $C1_{eq}$  100 times higher than  $C2$  and  $Ci_1$



#### 4. EXERCISE 3: COMPARISON OF CT AND SC INTEGRATORS

.Since they need to be lower than 1pF We will take  $C_1$  and  $C_{1eq}$  1pF and  $C_2$  and  $C_{i1}$  will be 100 times lower, that means 10fF.

### 4 Exercise 3: Comparison of CT and SC integrators

Calculate transfer function of the integrator in Figure 3. Determine the value of  $R_1$ ,  $R_f$  and  $C_f$  in a way, to achieve low frequency gain of  $A_{DC} = 10$  with corner frequency  $f_c = 1$  kHz. Realize SC integrator and replace  $R_1$  and  $R_f$  with circuit shown in the Figure 4. For proper inverting operation, it is essential to pay attention to the phases on each switch driven with 1 MHz. Prepare .m file to analyse and compare CT and SC transfer functions. Use `freqs()` and `freqz()` functions.

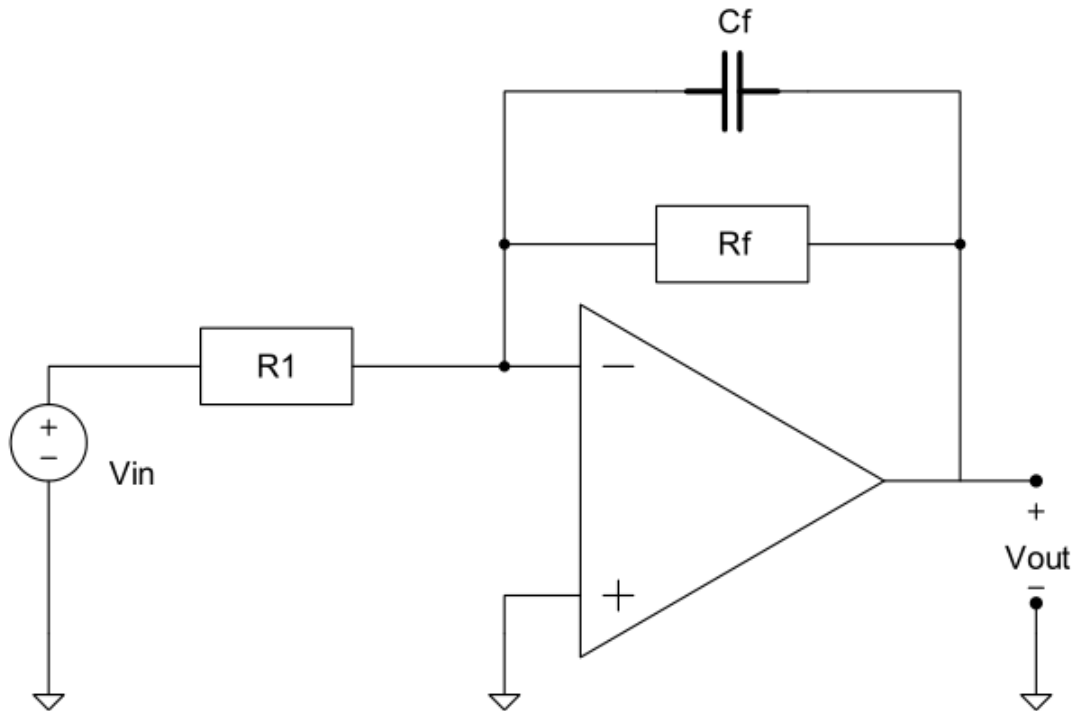


Figure 8: CT integrator.

#### 4. EXERCISE 3: COMPARISON OF CT AND SC INTEGRATORS

First we will his transfer function on S domain. We will start obtaining the parallel between  $R_f$  and  $C_f$ :

$$Z_f = \frac{R_f C_f}{R_f + C_f} = \frac{\frac{R_f}{sC_f}}{R_f + \frac{1}{sC_f}}$$

$$\text{Transfer function } H(s) = \frac{V_o}{V_i} = -\frac{Z_f}{R_1} = -\frac{R_f}{R_1} \frac{1}{1 + \frac{s}{\omega_c}}$$

We can see by the transfer function that it will behave like a low pass filter with a gain of  $-\frac{R_f}{R_1}$  and since we want a  $A_{DC}$  gain of 10  $R_f$  will be 10 times higher than  $R_1$ , we will take  $R_1 = 1k\Omega$  and  $R_f = 10k\Omega$ , we can also  $C_f = \frac{1}{2 \cdot \pi \cdot R_f \cdot f_c} = 15.915pF$

So the equivalent circuit in SC will be like this:

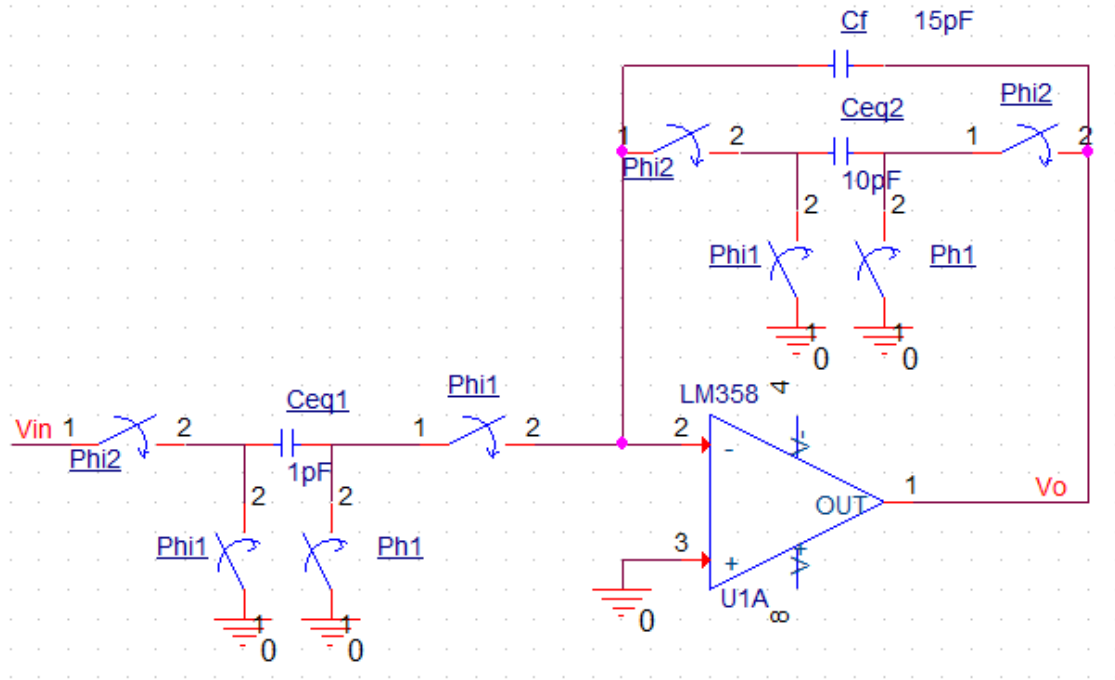


Figure 9: Equivalent SC schematic

In (n-1)  $\phi_1$  will be closed and  $\phi_2$  open so we will have:

$$V_o(n-1) \cdot C_f$$

In (n)  $\phi_1$  will be open and  $\phi_2$  closed so we will have:

$$V_{in}(n) \cdot C_{eq1} + V_o(n)(C_{eq2} + C_f)$$

#### 4. EXERCISE 3: COMPARISON OF CT AND SC INTEGRATORS

We will transfer the equations to Z domain and equal them:

$$Vo(n-1) \cdot C_f = Vin(n) \cdot C_{eq1} + Vo(n)(C_{eq2} + C_f)$$

$$Vo \cdot z^{-1} \cdot C_f = Vin \cdot C_{eq1} + Vo(C_{eq2} + C_f)$$

$$H(z) = \frac{Vo}{Vin} = \frac{\frac{-C_{eq1}}{C_f}}{1 + \frac{C_{eq2}}{C_f}} \cdot \frac{1}{1 - \frac{1}{1 + \frac{C_{eq2}}{C_f}} \cdot z^{-1}}$$

Finally we will prepare the MatLab code in order to plot the transfer functions. The code explanation will be in the appendix

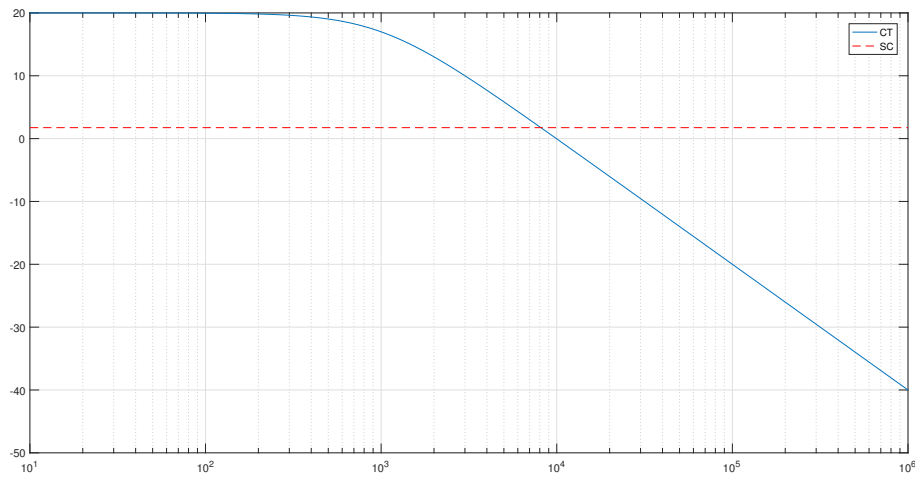


Figure 10: Comparison of CT and SC transfer function

We can see how the CT behaves as a LPF while the SC is constant through all the frequencies.

## 5 Appendix

### 5.1 Exercise 1

```

1 % We define the frequency vector and sampling frequency
2 freq= 0:10:50e6;
3 Fs = 20e6;
4 % We define the calculated elements R and C2
5 R=15.9e3;
6 C2=10e-9;
7
8 % For S Domain
9 % We define numerator and denominator of the transfer function
10 Bs=[1];
11 As=[R*C2 1];
12 % We define angular frequency
13 w=2*pi*freq;
14 % We calculate the transfer function
15 [Hs,Ws] = freqs(Bs,As,w);
16 % We transform from angular freq to freq
17 fs=Ws/(2*pi);
18 % We calculate the phase and transform it to degrees
19 phase = angle(Hs);
20 degPhaseS = phase*180/(pi);
21
22
23 % For Z Domain
24 Ceq=1/(R*Fs);
25 Bz=[0 Ceq];
26 Az=[Ceq+C2 -C2];
27
28 [Hz,Wz] = freqz(Bz,Az,freq,Fs);
29 fz=Wz/2*pi;
30

```

## 5. APPENDIX

```
31 phase = angle(Hz);
32 degPhaseZ = phase*180/(pi);
33
34 % Finally we plot the results
35 figure(1)
36 semilogx(fs,20*log10(Hz))
37 grid on
38 hold on
39 semilogx(fs,20*log10(Hs))
40 legend('Z Domain','S Domain')
41 % The spikes are due to the digital filter, but since we are using
    a higher
42 % sampling freq they are out of the filter and its not a problem
    .(If we use
43 % lower Fs they may be in the middle of the filter)
44
45 figure(2)
46 semilogx(fs,degPhaseZ)
47 grid on
48 hold on
49 semilogx(fs,degPhaseS)
50 legend('Z Domain','S Domain')
51 % Spikes also appear in phase but we can see that the phase is
    pretty much
52 % the same as in continuous time
```

### 5.2 Exercise 3

```
1 clear all;
2 close all;
3
4 % We define the data provided in the statement
5 fc=1e3;           % Pole freq
6 Fs=1e6;           % Sampling freq
7 R1=1e3;
```

## 5. APPENDIX

```

8  Rf=10e3 ;
9  Cf=1/(2*pi*Rf*fc)
10 f=0:10:1e6 ;           % Array of frequenciess
11 w=2*pi.*f ;           % Array of anguar frequencies
12
13 % In S Domain
14 num=-Rf/R1 ;
15 den=[(Rf*Cf)  1] ;
16
17 % We calculate the value of Ceq1 and Ceq2
18 Ceq2=1/(Rf*Fs)          % We get the formula from the equivalency of
    a resistor in SC
19 Ceq1=1/(R1*Fs)
20
21 % In S domain
22 num1=-(Ceq1/Ceq2)/(1-Ceq1/Ceq2) ;
23 den1=[1  -1/(1+Ceq1/Ceq2)] ;
24
25 % We use both fuction to get H and W
26 [h, w_plot]=freqs (num, den ,w) ;
27
28 [h1 , w_plot1]=freqz (num1, den1 ,w) ;
29
30 % We plot the results
31 semilogx(w_plot/(2*pi) ,20*log10(abs(h))) ;
32 grid ;
33 hold on
34 semilogx(w_plot1/(2*pi) ,20*log10(abs(h1)) , '—r') ;

```