

# Communication Systems

## EE-351

Lectures 17 and 18

# Frequency Modulation:

- FM wave is a nonlinear function of a modulating wave.
- Problem: This property makes **the spectral analysis of FM more complex** than AM wave.
- How then can we tackle the spectral analysis of FM wave:
- Two ways (two-stage spectral analysis) to answer this question:
  - First, simple case of single-tone modulation as we discussed in last lecture, the **narrow-band FM wave**.
  - Second is the more general case, also for single-tone modulation, but with **wide-band wave**.

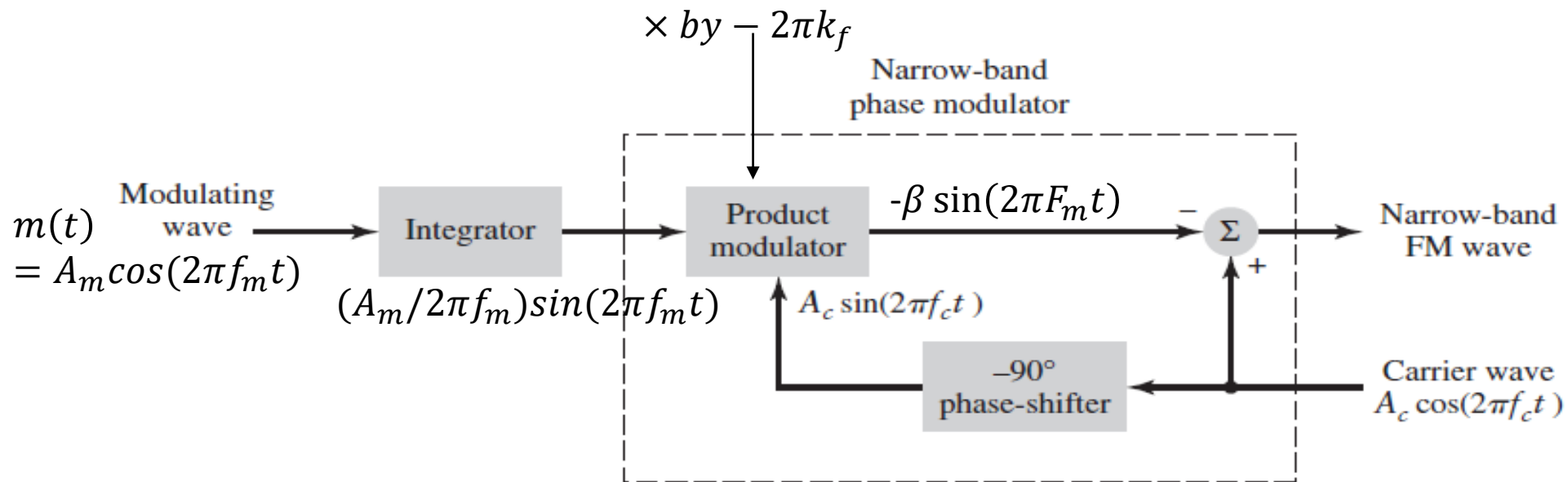
# Objective of this analysis:

- The objective of doing so is to establish a relationship between the transmission bandwidth of an FM wave and the message bandwidth.

- We will subsequently see, the **two-stage spectral analysis** provides us with enough insight to propose a useful solution to the problem.

# First Stage: Generating Narrowband FM:

This approximation ( $s(t) = A_c \cos(2\pi F_c t) - A_c \sin(2\pi F_c t) \beta \sin(2\pi F_m t)$ ) can be employed for narrowband FM generation.



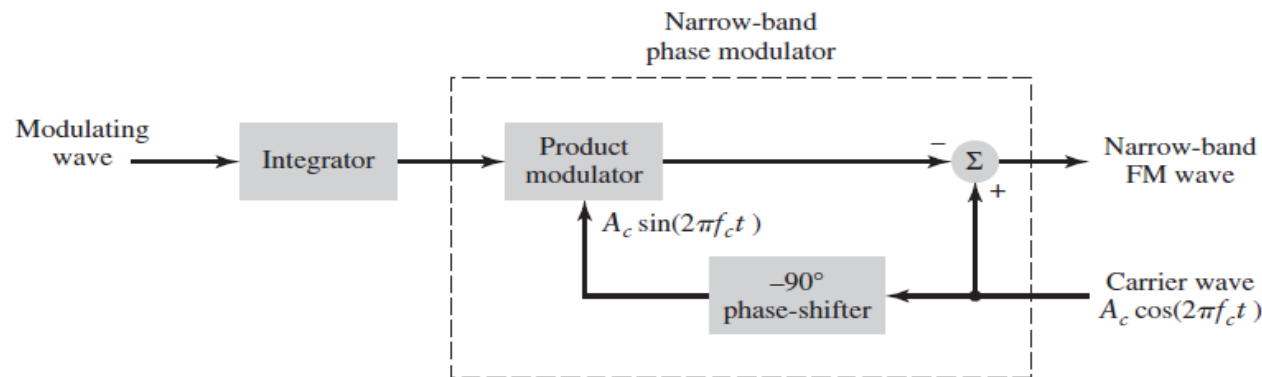
**FIGURE 4.4** Block diagram of an indirect method for generating a narrow-band FM wave.

# First Stage: Conclusion:

- Ideally, an **FM wave has a constant envelope** and, for the case of a sinusoidal modulating signal of frequency  $f_m$ , the angle  $\theta_i(t)$  is also sinusoidal with the same frequency.

# First Stage: Conclusion:

- But the modulated wave produced by the narrow-band modulator of Fig. 4.4 differs from this ideal condition in two fundamental respects:
  - The envelope contains a **residual** amplitude modulation that varies with time.
  - The angle  $\theta_i(t)$  contains **harmonic distortion** in the form of third- and higher order harmonics of the modulation frequency,  $f_m$ .



**FIGURE 4.4** Block diagram of an indirect method for generating a narrow-band FM wave.

# First Stage: Conclusion:

$$s(t) = A_c \cos(2\pi f_c t) - \beta A_c \sin(2\pi f_c t) \sin(2\pi f_m t)$$

- We may expand the modulated wave into three frequency components:

$$s(t) = A_c \cos(2\pi f_c t) + \frac{1}{2} \beta A_c \{\cos[2\pi(f_c + f_m)t] - \cos[2\pi(f_c - f_m)t]\}$$

This expression is somewhat similar to the corresponding one defining an AM wave, which is reproduced from Example 3.1 of Chapter 3 as follows:

$$s(t) = A_c \cos(2\pi f_c t) + \frac{1}{2} \mu A_c \{\cos[2\pi(f_c + f_m)t] + \cos[2\pi(f_c - f_m)t]\}$$

The basic difference between an AM wave and a narrow-band FM wave is that the algebraic sign of the lower side-frequency in the narrow-band FM is reversed.

Nevertheless, a narrow-band FM wave requires essentially the same transmission bandwidth (i.e.,  $2f_m$  for sinusoidal modulation) as the AM wave.



# Generation of Frequency Modulated Signal:

- Cartesian representation of band-pass signals (baseband representation/complex envelope) is well-suited for linear modulation.

$$s(t) = s_I(t) \cos(2\pi f_c t) - s_Q(t) \sin(2\pi f_c t)$$

- However, for nonlinear modulation, the polar representation is well-suited.

$$s(t) = a(t) \cos[2\pi f_c t + \phi(t)]$$

## Drill Problem 4.3:

- Show that the polar representation of  $s(t)$  is exactly equivalent to its cartesian representation:

$$a(t) = [s_I^2(t) + s_Q^2(t)]^{\frac{1}{2}}$$

$$\phi(t) = \tan^{-1} \left[ \frac{s_Q(t)}{s_I(t)} \right]$$

## Drill Problem 4.4:

- Consider the narrow-band FM wave approximately defined by Eq.

$$s(t) = A_c \cos(2\pi F_c t) - \beta A_c \sin(2\pi F_c t) \sin(2\pi F_m t)$$

- Building on Problem 4.3, do the following:
- Determine the envelope of this modulated wave. What is the ratio of the maximum to the minimum value of this envelope?

$$\frac{A_{\max}}{A_{\min}} \approx \left(1 + \frac{1}{2}\beta^2\right)$$

## Drill Problem 4.4:

- Determine the average power of the narrow-band FM wave, expressed as a percentage of the average power of the unmodulated carrier wave.

$$s(t)$$

$$= A_c \cos(2\pi f_c t) + \frac{1}{2} \beta A_c \{ \cos[2\pi(f_c + f_m)t] - \cos[2\pi(f_c - f_m)t] \}$$

$$\frac{P_{avg}}{P_c} = 1 + \beta^2$$

- Part (c) : Try yourself.

## Stage 2: Generating Wideband FM:

- We now determine the spectrum of the single-tone FM wave defined by the exact formula in Eq:

$$s(t)_{FM} = A_c \cos(2\pi f_c t + \beta \sin(2\pi f_m t))$$

(non periodic function of time)

For  $\beta > 1$

- In general, such an FM wave produced by a sinusoidal modulating wave is a **periodic function of time  $t$**  only when the carrier frequency,  $f_c$  is an integral multiple of the modulation frequency,  $f_m$ .
- How can we simplify the **spectral analysis of the wide-band** FM wave defined in the above Eq.
- The answer lies in using the **complex baseband representation** of a modulated (i.e., bandpass) signal.

# Generating Wideband FM:

- Assume that the carrier frequency,  $f_c$  is large enough (compared to the bandwidth of the FM wave).

$$s(t) = A_c \cos \theta$$
$$e^{j\theta} = \cos \theta + j \sin \theta$$

$\cos \theta = \text{real part of } e^{j\theta}$

$$s(t) = A_c \text{Re} \left| e^{j(2\pi f_c t + \beta \sin(2\pi f_m t))} \right|$$
$$= A_c \text{Re} \left| e^{j2\pi f_c t} e^{j\beta \sin(2\pi f_m t)} \right|$$

$\tilde{s}(t) = A_c e^{j\beta \sin(2\pi f_m t)}$  is the complex envelope of the FM wave  $s(t)$

# Generating Wideband FM:

- The important point to note from  $A_c e^{j\beta \sin(2\pi f_m t)}$  is that unlike the original FM wave  $s(t)$ , the complex envelope is a periodic function of time with a fundamental frequency equal to the modulation frequency,  $f_m$ .
- Check periodicity:

# Generating Wideband FM:

- We may therefore expand  $\tilde{s}(t)$  [ $\tilde{s}(t) = A_c e^{j\beta \sin(2\pi f_m t)}$ ] in the form of a complex Fourier series as follows:

$$\tilde{s}(t) = \sum_{n=-\infty}^{\infty} c_n e^{j2\pi n f_m t}$$

where the complex Fourier coefficient is

$$c_n = f_m \int_{-1/(2f_m)}^{1/(2f_m)} \tilde{s}(t) e^{-j2\pi n f_m t} dt$$
$$c_n = f_m A_c \int_{-1/(2f_m)}^{1/(2f_m)} e^{[j\beta \sin(2\pi f_m t) - j2\pi n f_m t]} dt$$



# Generating Wideband FM:

- Change variable  $t$  into  $\theta$ ,

$$2\pi f_m t = \theta$$

- Taking derivative,

$$2\pi f_m dt = d\theta$$
$$dt = \frac{d\theta}{2\pi f_m}$$

- Limits become,

$$t = -\frac{1}{2f_m} \Rightarrow \theta = -\pi$$

$$t = \frac{1}{2f_m} \Rightarrow \theta = \pi$$

$$c_n = f_m A_c \int_{-\pi}^{\pi} e^{[j\beta \sin\theta - jn\theta]} \frac{d\theta}{2\pi f_m}$$

# Generating Wideband FM:

$$c_n = \frac{A_c}{2\pi} \int_{-\pi}^{\pi} e^{j[\beta \sin \theta - n\theta]} d\theta$$

- The integral on the right-hand side of Eq except for the carrier amplitude  $A_c$ , is referred to as the **nth order Bessel function** of the first kind and argument  $\beta$ .
- This function is commonly denoted by the symbol  $J_n(\beta)$ , so we may write:

$$J_n(\beta) = \frac{1}{2\pi} \int_{-\pi}^{\pi} e^{j[\beta \sin \theta - n\theta]} d\theta$$
$$c_n = A_c J_n(\beta)$$

# Generating Wideband FM:

$$\tilde{s}(t) = \sum_{n=-\infty}^{\infty} c_n e^{j2\pi n f_m t}$$

Put  $c_n = A_c J_n(\beta)$

$$\tilde{s}(t) = A_c \sum_{n=-\infty}^{\infty} J_n(\beta) e^{j2\pi n f_m t}$$

# Generating Wideband FM:

- Also,

$$s(t) = A_c \operatorname{Re} \left| e^{j(2\pi f_c t + \beta \sin(2\pi f_m t))} \right|$$
$$\tilde{s}(t) = A_c e^{j\beta \sin(2\pi f_m t)}$$

Replace it with,

$$\tilde{s}(t) = A_c \sum_{n=-\infty}^{\infty} J_n(\beta) e^{j2\pi n f_m t}$$
$$s(t) = A_c \operatorname{Re} \left| \sum_{n=-\infty}^{\infty} J_n(\beta) e^{j2\pi(f_c + n f_m)t} \right|$$

# Generating Wideband FM:

$$s(t) = A_c \operatorname{Re} \left| \sum_{n=-\infty}^{\infty} J_n(\beta) e^{j2\pi(f_c + nf_m)t} \right|$$

The carrier amplitude is a constant and may therefore be taken outside the real-time operator  $\operatorname{Re}[\cdot]$ . Moreover, we may interchange the order of summation and real-part operation, as they are both linear operators. Accordingly, we may rewrite Eq in the simplified form:

$$s(t) = A_c \sum_{n=-\infty}^{\infty} J_n(\beta) \cos 2\pi(f_c + nf_m)t$$

The Fourier series expansion of the single-tone FM signal.

# Generating Wideband FM:

- The discrete spectrum is obtained by taking the Fourier transforms of both sides of  $s(t) = A_c \sum_{n=-\infty}^{\infty} J_n(\beta) \cos 2\pi(f_c + nf_m)t$

$$S(f) = \frac{A_c}{2} \sum_{n=-\infty}^{\infty} J_n(\beta) [\delta(f - f_c - nf_m) + \delta(f + f_c + nf_m)]$$

# Properties of Bessel Function:

1.  $J_n(x)$  decreases as  $n$  increases

$$J_0(x) > J_1(x) > J_2(x) \dots$$

2.  $J_{-n}(x) = (-1)^n J_n(x)$

$$J_{-1}(x) = (-1)^1 J_1(x) = -J_1(x)$$

$$J_{-2}(x) = (-1)^2 J_2(x) = J_2(x)$$

$$J_{-n}(x) = \begin{cases} J_n(x); n \text{ even} \\ -J_n(x); n \text{ odd} \end{cases}$$

3.  $\sum_{n=-\infty}^{\infty} J_n^2(x) = 1$

# Carson's Rule of Bandwidth:

- Consider significant amplitude only.

$\beta + 1$  sidebands are significant