

Spring 2011

信號與系統
Signals and Systems

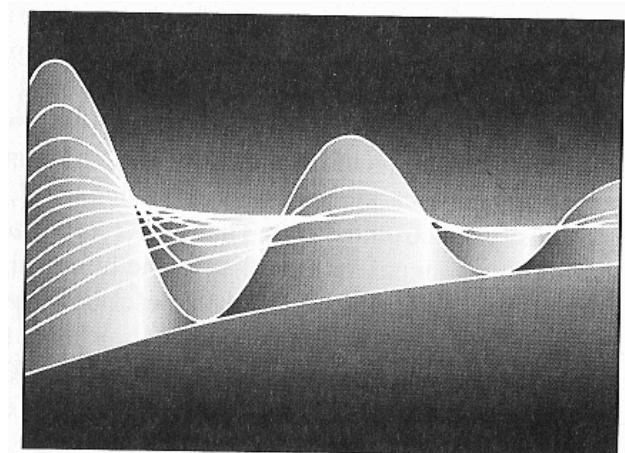
Chapter SS-6
Time & Frequency Characterization of
Signals and Systems

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NTU-EE

Feb11 – Jun11

Figures and images used in these lecture notes are adopted from
“Signals & Systems” by Alan V. Oppenheim and Alan S. Willsky, 1997



Introduction

[\(Chap 1\)](#)

LTI & Convolution

[\(Chap 2\)](#)Bounded/ConvergentPeriodic**FS**[\(Chap 3\)](#)– CT
– DTAperiodic**FT**– CT [\(Chap 4\)](#)
– DT [\(Chap 5\)](#)Unbounded/Non-convergent**LT**– CT [\(Chap 9\)](#)**zT**– DT [\(Chap 10\)](#)Time-Frequency [\(Chap 6\)](#)

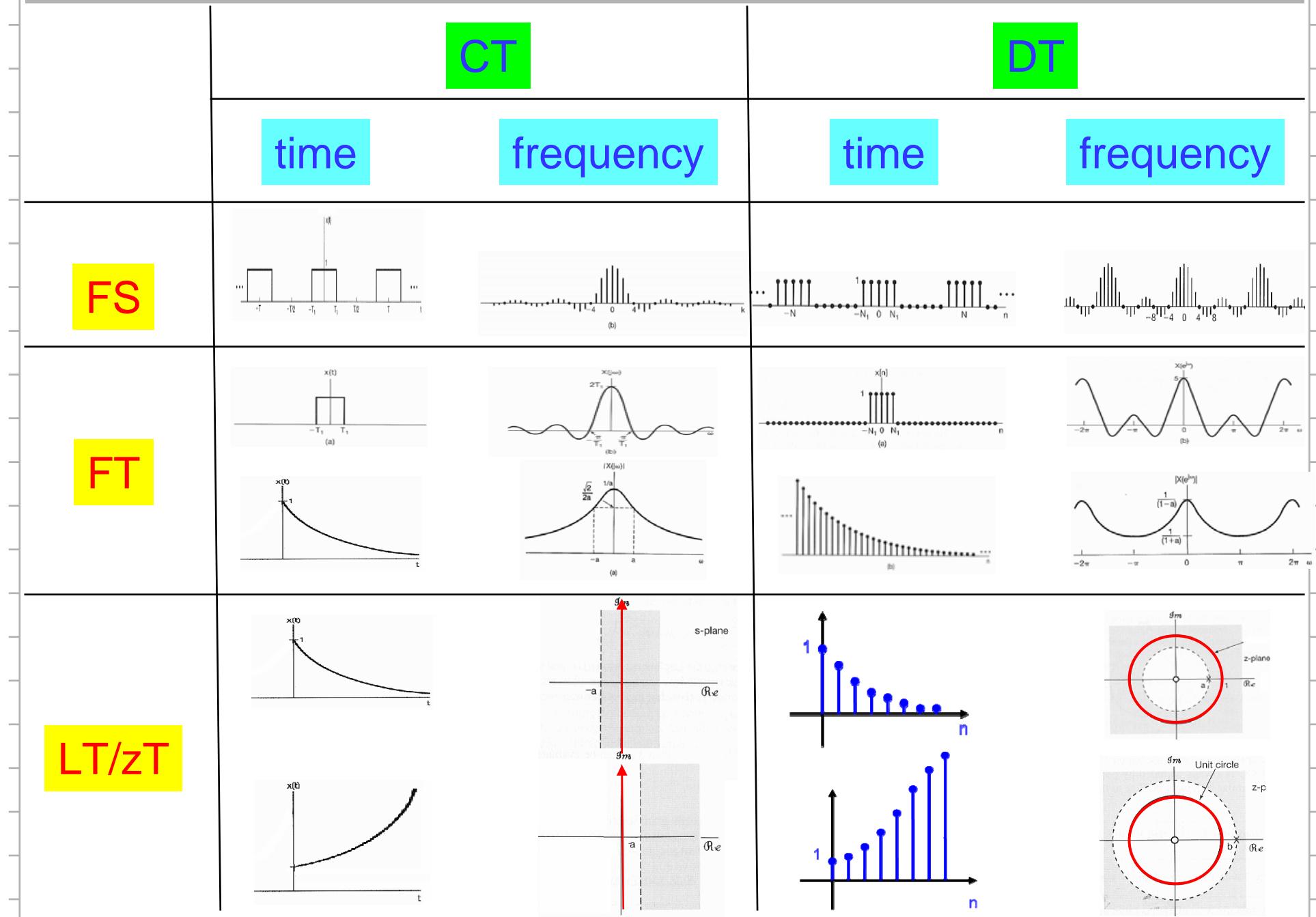
CT-DT

[\(Chap 7\)](#)Communication [\(Chap 8\)](#)

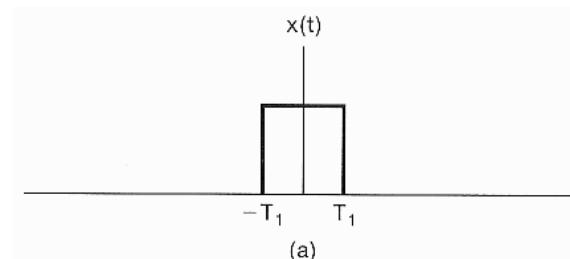
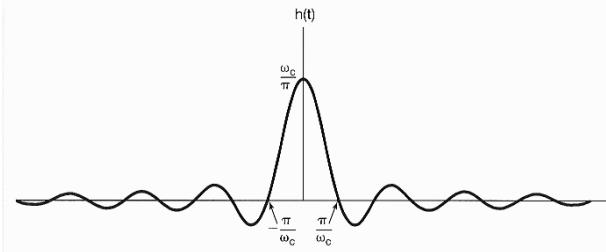
Control

Digital
Signal
Processing
[\(dsp-8\)](#)

Fourier Series, Fourier Transform, Laplace Transform, z-Transform

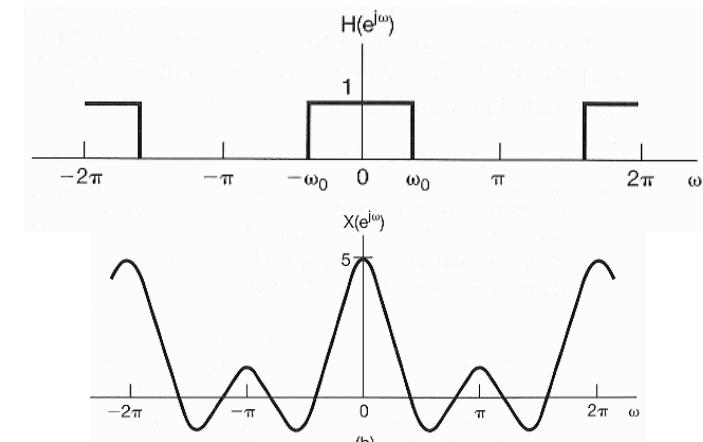
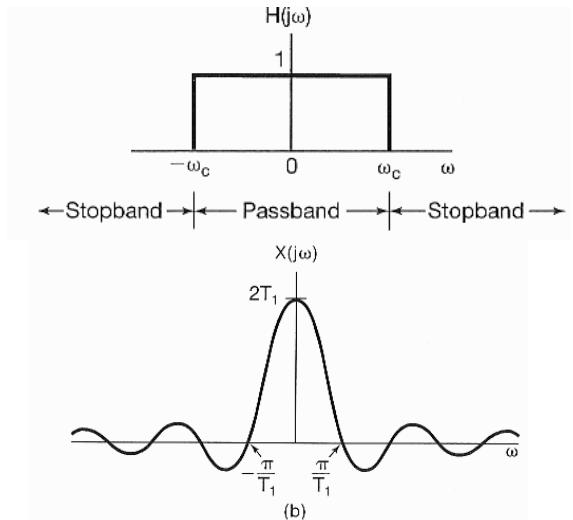
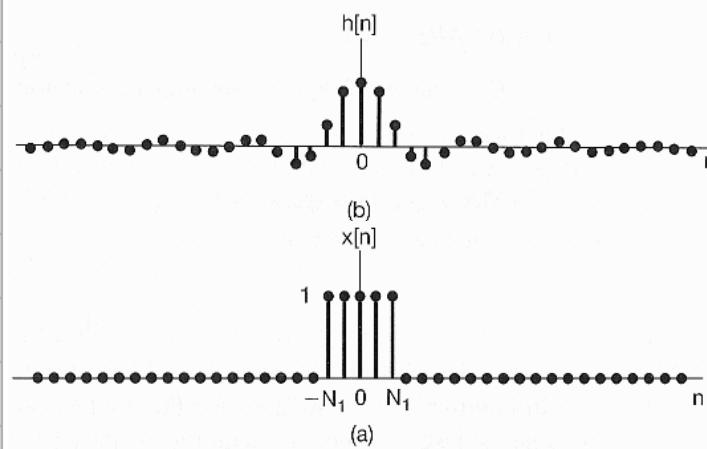


■ Time- & Frequency-Domain Characterization:



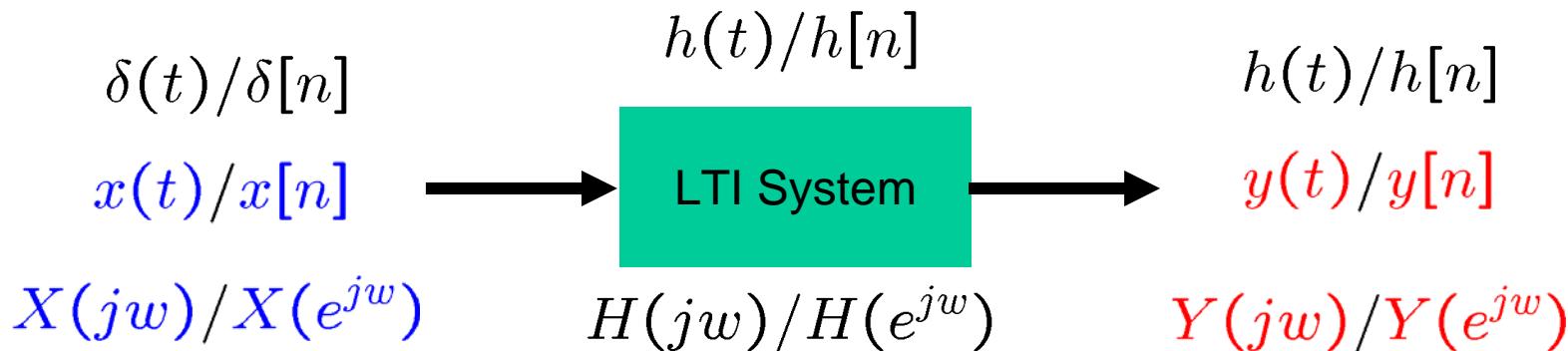
$$h(t) \xleftrightarrow{\mathcal{F}} H(jw)$$

$$h[n] \xleftrightarrow{\mathcal{F}} H(e^{jw})$$



■ Time- & Frequency-Domain Characterization:

$$H(jw) = \int_{-\infty}^{\infty} h(t)e^{-jwt}dt \quad H(e^{jw}) = \sum_{n=-\infty}^{+\infty} h[n]e^{-jwn}$$



$$\begin{array}{lll} x(t) \xleftrightarrow{\mathcal{F}} X(jw) & h(t) \xleftrightarrow{\mathcal{F}} H(jw) & y(t) \xleftrightarrow{\mathcal{F}} Y(jw) \\ x[n] \xleftrightarrow{\mathcal{F}} X(e^{jw}) & h[n] \xleftrightarrow{\mathcal{F}} H(e^{jw}) & y[n] \xleftrightarrow{\mathcal{F}} Y(e^{jw}) \end{array}$$

$$y(t) = x(t) * h(t) \xleftrightarrow{\mathcal{F}} Y(jw) = X(jw)H(jw)$$

$$y[n] = x[n] * h[n] \xleftrightarrow{\mathcal{F}} Y(e^{jw}) = X(e^{jw})H(e^{jw})$$

Time-Domain

Frequency-Domain

Convolution
Transformation

Differential or
Difference
Equations

System
Model
& Operations

Algebraic
Equations

Convolution
Multiplication

Techniques

Multiplication
Convolution

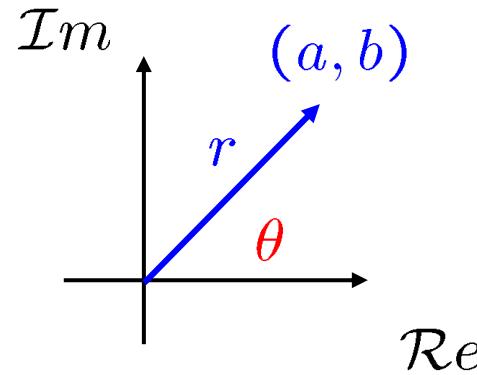
Time-Domain
Considerations

System
Design

Frequency-Domain
Considerations

- The Magnitude-Phase Representation of the Fourier Transform
- The Magnitude-Phase Representation of Frequency Response of LTI Systems (p. 427)
- Time-Domain Properties of Ideal Frequency-Selective Filters
- Time-Domain and Frequency-Domain Aspects of Non-ideal Filters
- 1st-Order & 2nd-Order Continuous-Time Systems
- 1st-Order & 2nd-Order Discrete-Time Systems
- Time- & Frequency-Domain Analysis of Systems

■ Magnitude & Phase Representation:



$$a + jb \Rightarrow \begin{cases} r = \sqrt{a^2 + b^2} \\ \tan(\theta) = \frac{b}{a} \end{cases} \Rightarrow a + jb = re^{j\theta}$$

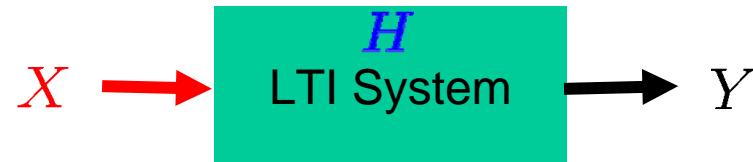
$$X(jw) = \mathcal{R}e\{X(jw)\} + j \mathcal{I}m\{X(jw)\} = |X(jw)| e^{j\angle X(jw)}$$

$$X(e^{jw}) = \mathcal{R}e\{X(e^{jw})\} + j \mathcal{I}m\{X(e^{jw})\} = |X(e^{jw})| e^{j\angle X(e^{jw})}$$

$|X(jw)|$ or $|X(e^{jw})|$: magnitude

$\angle X(jw)$ or $\angle X(e^{jw})$: phase angle

■ Magnitude Distortion & Phase Distortion: (p. 428)



$$Y(jw) = X(jw) H(jw)$$

$$Y(e^{jw}) = X(e^{jw}) H(e^{jw})$$

$$\Rightarrow |Y(jw)| e^{j\angle Y(jw)} = |X(jw)| e^{j\angle X(jw)} |H(jw)| e^{j\angle H(jw)}$$

$$= |X(jw)| |H(jw)| e^{j(\angle X(jw) + \angle H(jw))}$$

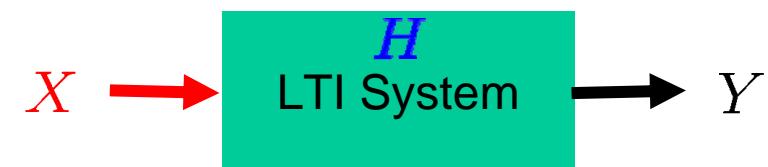
$$\Rightarrow \begin{cases} |Y(jw)| &= |X(jw)| |H(jw)| & \text{magnitude distortion} \\ \angle Y(jw) &= \angle X(jw) + \angle H(jw) & \text{phase distortion} \end{cases}$$

$$\Rightarrow \begin{cases} |Y(e^{jw})| &= |X(e^{jw})| |H(e^{jw})| \\ \angle Y(e^{jw}) &= \angle X(e^{jw}) + \angle H(e^{jw}) \end{cases}$$

$|H(jw)|$ or $|H(e^{jw})|$: gain of the system

$\angle H(jw)$ or $\angle H(e^{jw})$: phase shift of the system

- Log-Magnitude & Bode Plots: (p. 436)



$$Y(jw) = X(jw) H(jw)$$

$$\Rightarrow \begin{cases} |Y(jw)| = |X(jw)| |H(jw)| \\ \angle Y(jw) = \angle X(jw) + \angle H(jw) \end{cases}$$

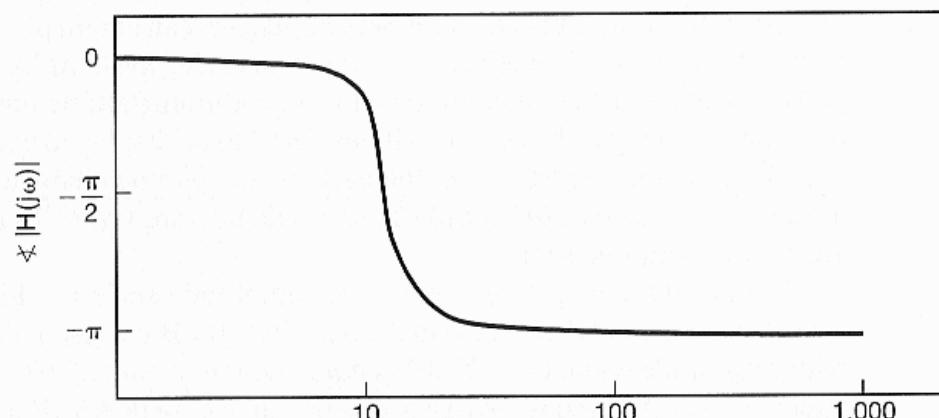
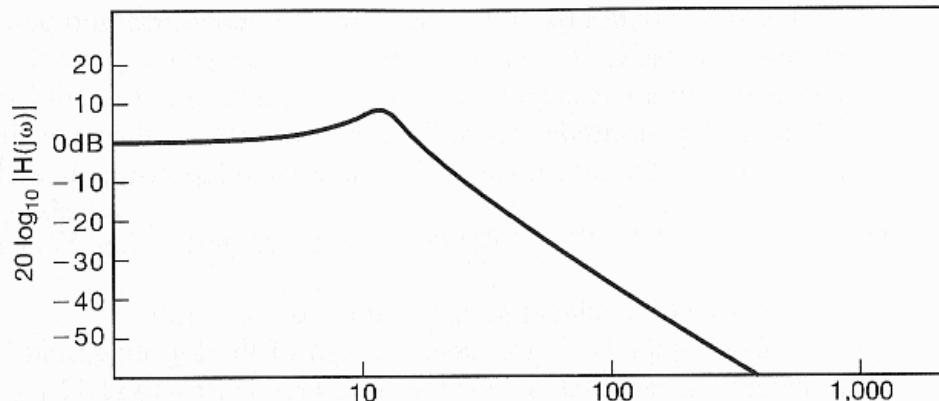
$$\Rightarrow \log |Y(jw)| = \log |X(jw)| + \log |H(jw)|$$

$$\Rightarrow 20 \log_{10} |Y(jw)| = 20 \log_{10} |X(jw)| + 20 \log_{10} |H(jw)|$$

$$\Rightarrow \begin{cases} 20 \log_{10} (1) = 0 \text{ dB} \\ 20 \log_{10} (10) = 20 \text{ dB} \\ 20 \log_{10} (0.1) = -20 \text{ dB} \end{cases}$$

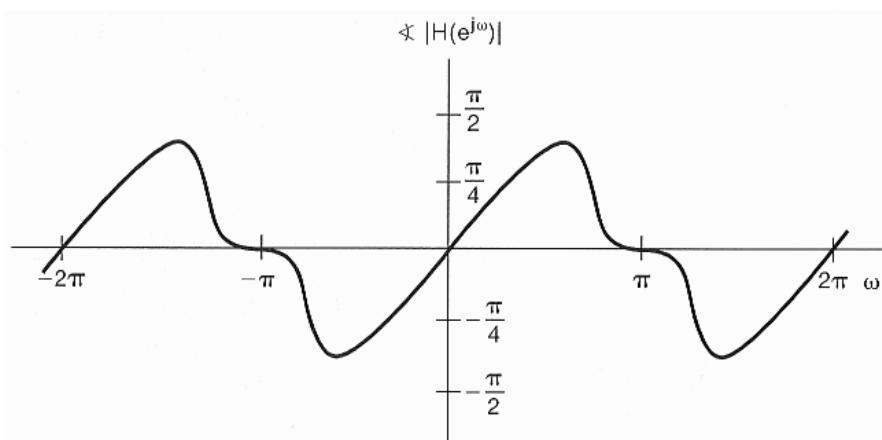
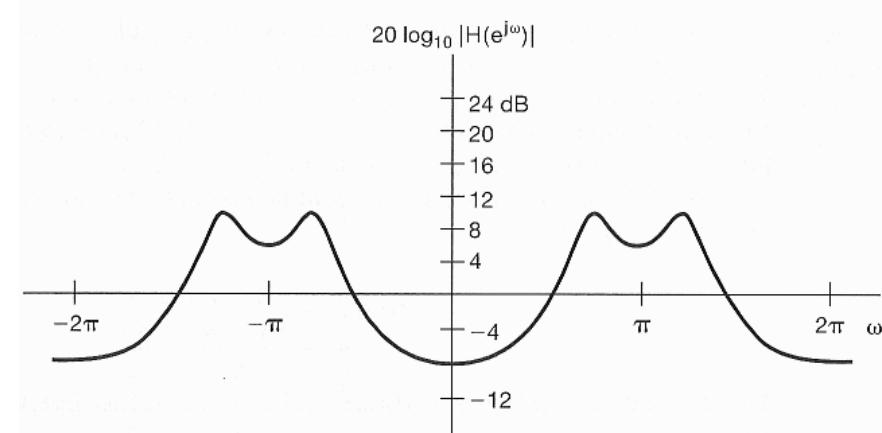
- Log-Magnitude & Bode Plots: (p. 436)

Continuous-Time Bode plot



$\log(\omega), \quad \omega : 0 \leftrightarrow \infty$

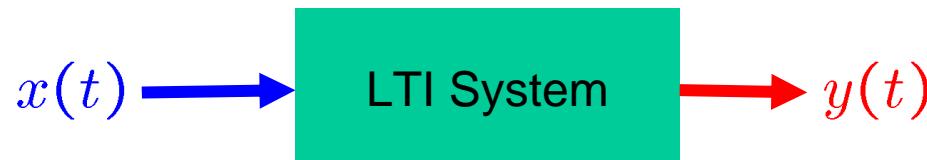
Discrete-Time Bode plot



$(\omega), \quad \omega : -\pi \leftrightarrow \pi$

- The Magnitude-Phase Representation of the Fourier Transform
- The Magnitude-Phase Representation of Frequency Response of LTI Systems
- Time-Domain Properties of Ideal Frequency-Selective Filters
- Time-Domain and Frequency-Domain Aspects of Non-ideal Filters (p. 436)
- 1st-Order & 2nd-Order Continuous-Time Systems
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■ First-Order CT Systems: (p. 448)



$$Y(jw) = X(jw)H(jw)$$

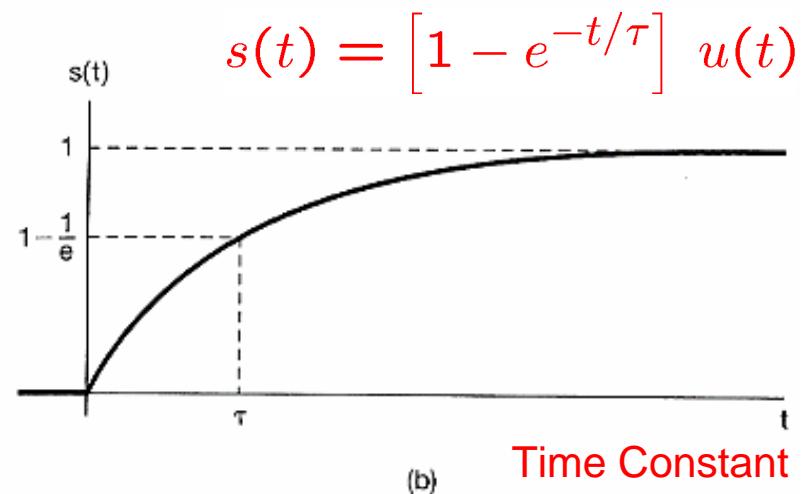
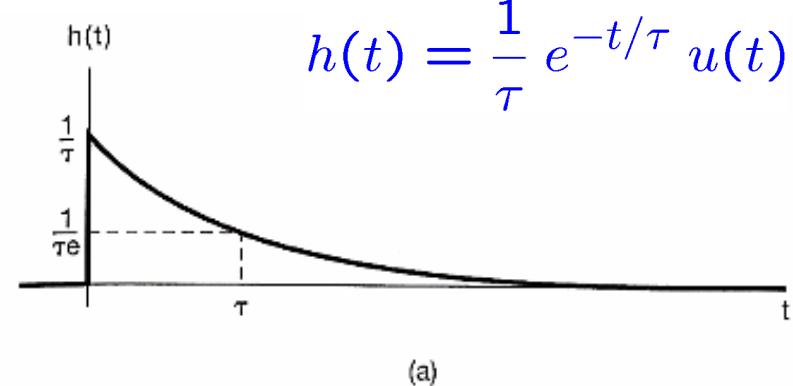
$$\tau \frac{d}{dt}y(t) + y(t) = x(t)$$

$$\Rightarrow H(jw) = \frac{1}{jw\tau + 1}$$

$$\Rightarrow h(t) = \frac{1}{\tau} e^{-t/\tau} u(t)$$

$$\Rightarrow s(t) = h(t) * u(t)$$

$$= [1 - e^{-t/\tau}] u(t)$$



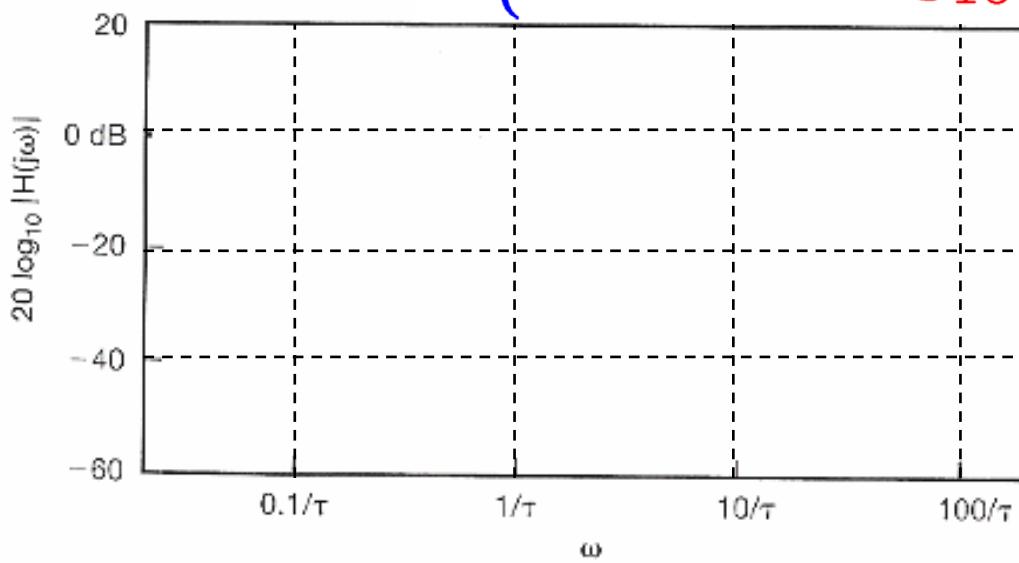
■ First-Order CT Systems:

$$H(jw) = \frac{1}{jw\tau + 1}$$

$$|H(jw)| = \frac{1}{\sqrt{(w\tau)^2 + 1}}$$

$$20 \log_{10} |H(jw)| = -10 \log_{10} [(w\tau)^2 + 1]$$

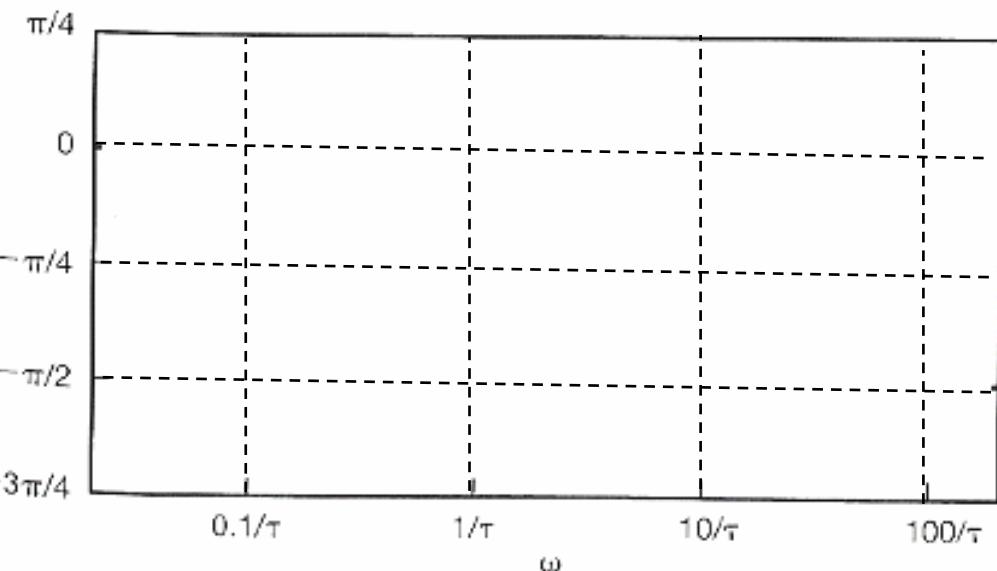
$$\approx \begin{cases} 0 & w \ll 1/\tau \\ -10 \log_{10}(2) \approx -3dB & w = 1/\tau \\ -20 \log_{10}(w\tau) & w \gg 1/\tau \\ = -20 \log_{10}(w) - 20 \log_{10}(\tau) \end{cases}$$



■ First-Order CT Systems:

$$\nexists H(jw) = -\tan^{-1}(w\tau)$$

$$\approx \begin{cases} 0 & w \leq 0.1/\tau \\ -\pi/4 & w = 1/\tau \\ -\pi/2 & w \geq 10/\tau \\ -(\pi/4)[\log_{10}(w\tau) + 1] & 0.1/\tau \leq w \leq 10/\tau \\ = -(\pi/4) [\log_{10}(w) + \log_{10}(\tau) + 1] & \end{cases}$$



$$H(jw) = \frac{1}{jw\tau + 1}$$

$$w \leq 0.1/\tau$$

$$w = 1/\tau$$

$$w \geq 10/\tau$$

$$0.1/\tau \leq w \leq 10/\tau$$

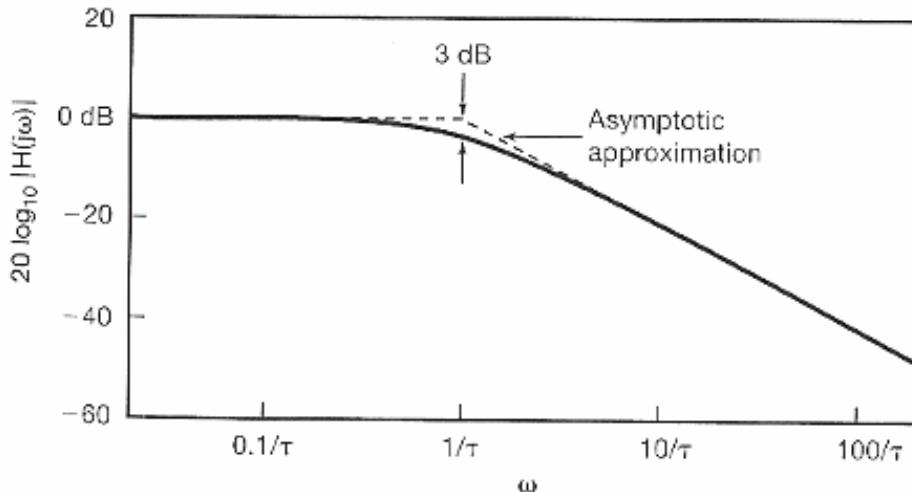
$$\tan^{-1}(x) = x - \frac{x^3}{3} + \frac{x^5}{5} - \dots$$

■ First-Order CT Systems:

$$20 \log_{10} |H(jw)| =$$

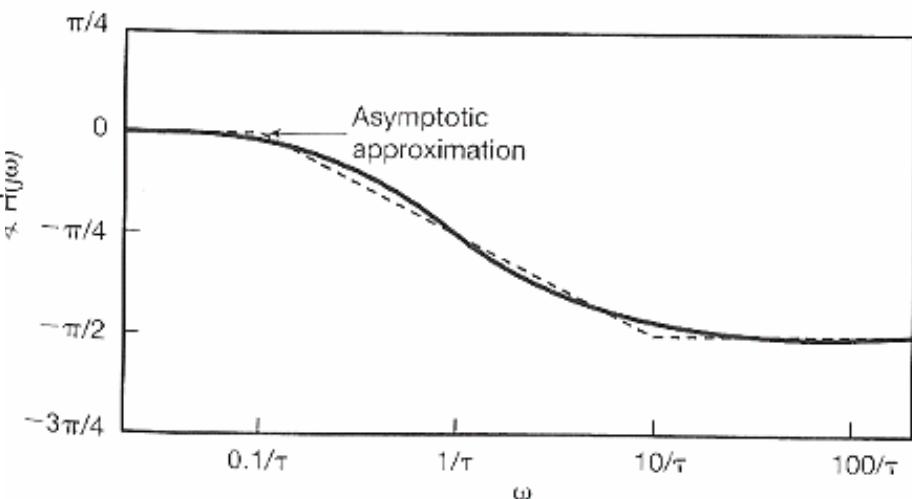
$$\begin{cases} 0 & w \ll 1/\tau \\ -10 \log_{10}(2) \approx -3 \text{dB} & w = 1/\tau \\ -20 \log_{10}(w\tau) & w \gg 1/\tau \\ = -20 \log_{10}(w) - 20 \log_{10}(\tau) \end{cases}$$

$$H(jw) = \frac{1}{jw\tau + 1}$$



$$\angle H(jw) =$$

$$\begin{cases} 0 & w \leq 0.1/\tau \\ -(\pi/4)[\log_{10}(w\tau) + 1] & 0.1/\tau \leq w \leq 10/\tau \\ = -(\pi/4) [\log_{10}(w) + \log_{10}(\tau) + 1] & \\ -\pi/4 & w = 1/\tau \\ -\pi/2 & w \geq 10/\tau \end{cases}$$



■ Second-Order CT Systems: (p. 451)

$$\frac{d^2}{dt^2}y(t) + 2\zeta w_n \frac{d}{dt}y(t) + w_n^2 y(t) = w_n^2 x(t)$$

$$\Rightarrow H(jw) = \frac{w_n^2}{(jw)^2 + 2\zeta w_n(jw) + w_n^2}$$
$$= \frac{1}{(jw/w_n)^2 + 2\zeta(jw/w_n) + 1}$$

$$\Rightarrow H(jw) = \frac{w_n^2}{(jw - c_1)(jw - c_2)}$$

$$\begin{cases} c_1 = -\zeta w_n + w_n \sqrt{\zeta^2 - 1} \\ c_2 = -\zeta w_n - w_n \sqrt{\zeta^2 - 1} \end{cases}$$

- Second-Order CT Systems:

$$H(jw) = \frac{1}{(jw/w_n)^2 + 2\zeta(jw/w_n) + 1}$$

ζ : damping ratio

w_n : undamped natural frequency

$$\left\{ \begin{array}{ll} 0 < \zeta < 1 & \text{: underdamped} \\ \zeta = 1 & \text{: critically damped} \\ \zeta > 1 & \text{: overdamped} \end{array} \right.$$

■ Second-Order CT Systems:

- For $\zeta \neq 1$, $\Rightarrow c_1, c_2$: unequal:

$$\Rightarrow H(jw) = \frac{M}{jw - c_1} - \frac{M}{jw - c_2}$$

$$M = \frac{w_n}{2\sqrt{\zeta^2 - 1}}$$

$$\Rightarrow h(t) = M [e^{c_1 t} - e^{c_2 t}] u(t)$$

- For $\zeta = 1$, $\Rightarrow c_1 = c_2 = -w_n$:

$$\Rightarrow H(jw) = \frac{w_n^2}{(jw + w_n)^2}$$

$$\Rightarrow h(t) = w_n^2 t e^{-w_n t} u(t)$$

■ Second-Order CT Systems:

- For $0 < \zeta < 1$, c_1, c_2 : complex:

$$H(jw) = \frac{1}{(jw/w_n)^2 + 2\zeta(jw/w_n) + 1} = \frac{w_n^2}{(jw - c_1)(jw - c_2)}$$

$$\Rightarrow h(t) = M [e^{c_1 t} - e^{c_2 t}] u(t) \quad \left\{ \begin{array}{l} c_1 = -\zeta w_n + j w_n \sqrt{1 - \zeta^2} \\ c_2 = -\zeta w_n - j w_n \sqrt{1 - \zeta^2} \end{array} \right.$$

$$= \frac{w_n e^{-\zeta w_n t}}{2j \sqrt{1 - \zeta^2}} \left\{ e^{j(w_n \sqrt{1 - \zeta^2})t} - e^{-j(w_n \sqrt{1 - \zeta^2})t} \right\} u(t)$$

$$= \frac{w_n e^{-\zeta w_n t}}{\sqrt{1 - \zeta^2}} \left[\sin \left((w_n \sqrt{1 - \zeta^2})t \right) \right] u(t)$$

$$\Rightarrow s(t) = h(t) * u(t) = \left\{ 1 + M \left[\frac{e^{c_1 t}}{c_1} - \frac{e^{c_2 t}}{c_2} \right] \right\} u(t) \quad \zeta \neq 1$$

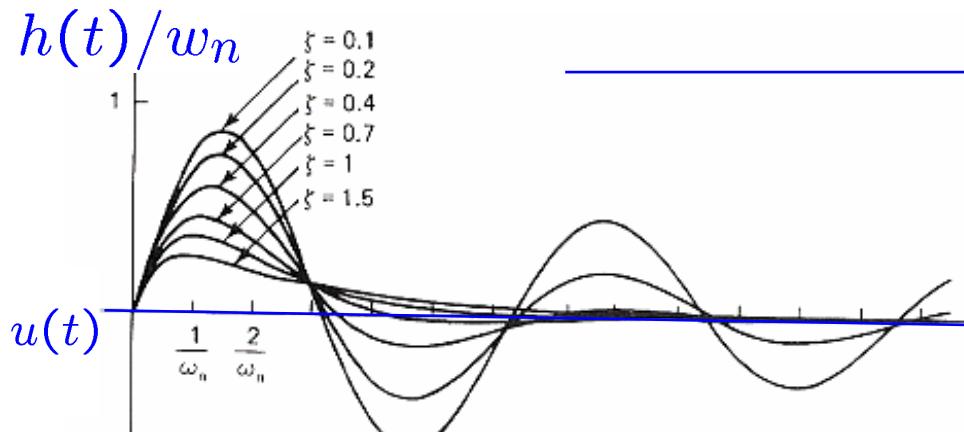
$$M = \frac{w_n}{2\sqrt{\zeta^2 - 1}}$$

■ Second-Order CT Systems:

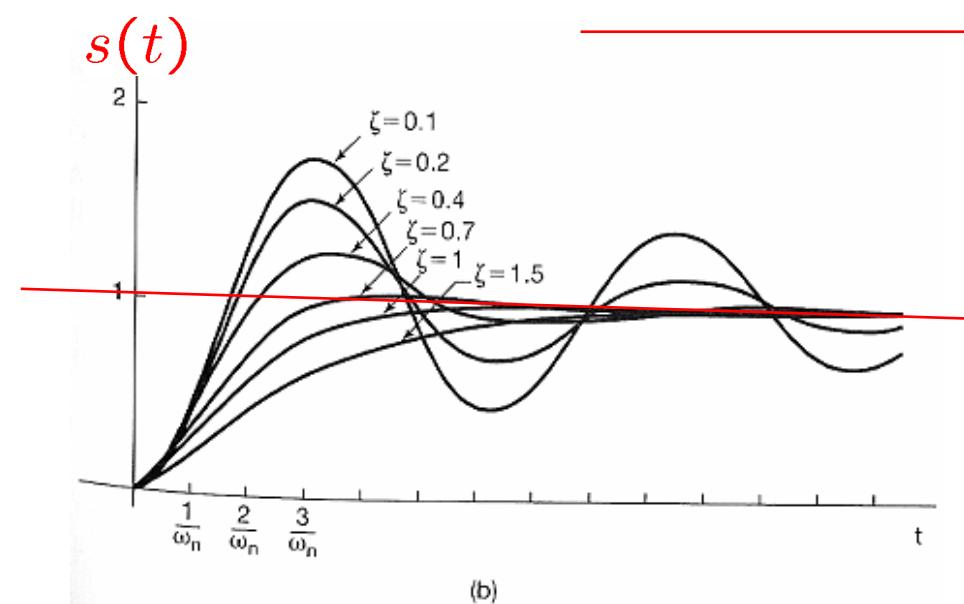
$$h(t) = \frac{w_n e^{-\zeta w_n t}}{\sqrt{1 - \zeta^2}} \left[\sin \left((w_n \sqrt{1 - \zeta^2}) t \right) \right] u(t)$$

$$\frac{h(t)}{w_n} = \frac{e^{-\zeta w_n t}}{\sqrt{1 - \zeta^2}} \left[\sin \left((w_n \sqrt{1 - \zeta^2}) t \right) \right] u(t)$$

$$s(t) = \left\{ 1 + M \left[\frac{e^{c_1 t}}{c_1} - \frac{e^{c_2 t}}{c_2} \right] \right\} u(t)$$



(a)



(b)

■ Second-Order CT Systems:

$$H(jw) = \frac{1}{(jw/w_n)^2 + 2\zeta(jw/w_n) + 1}$$

$$|H(jw)| = \frac{1}{\sqrt{\left[1 - \left(\frac{w}{w_n}\right)^2\right]^2 + 4\zeta^2\left(\frac{w}{w_n}\right)^2}}$$

$$20 \log_{10} |H(jw)| = -10 \log_{10} \left\{ \left[1 - \left(\frac{w}{w_n}\right)^2\right]^2 + 4\zeta^2\left(\frac{w}{w_n}\right)^2 \right\}$$

$$Q = \frac{1}{2\zeta}$$

$$\approx \begin{cases} 0 & w \ll w_n \\ -20 \log_{10}(2\zeta) & w = w_n \\ -40 \log_{10}(w) + 40 \log_{10}(w_n) & w \gg w_n \end{cases}$$

$$|H(jw)| = \frac{1}{\sqrt{\left[1 - \left(\frac{w}{w_n}\right)^2\right]^2 + 4\zeta^2\left(\frac{w}{w_n}\right)^2}}$$

$$\Rightarrow \left(\frac{w}{w_n}\right)^4 - 2\left(\frac{w}{w_n}\right)^2 + 1 + 4\zeta^2\left(\frac{w}{w_n}\right)^2 = \left(\frac{w}{w_n}\right)^4 + (4\zeta^2 - 2)\left(\frac{w}{w_n}\right)^2 + 1$$

$$\Rightarrow \frac{d}{dw} \left\{ \left(\frac{w}{w_n}\right)^4 + (4\zeta^2 - 2)\left(\frac{w}{w_n}\right)^2 + 1 \right\} = 0$$

$$\Rightarrow \left(\frac{4w^3}{w_n^4}\right) + (4\zeta^2 - 2)\left(\frac{2w}{w_n^2}\right) = 0 \quad \Rightarrow w(w^2 + (2\zeta^2 - 1)w_n^2) = 0$$

$$\Rightarrow w = 0, \pm\sqrt{1 - 2\zeta^2} w_n$$

- For $\zeta < \sqrt{2}/2$

$$\Rightarrow \max \{|H(jw)|\} \text{ at } w_{\max} = w_n \sqrt{1 - 2\zeta^2}$$

$$|H(jw_{\max})| = \frac{1}{2\zeta\sqrt{1 - \zeta^2}}$$

■ Second-Order CT Systems:

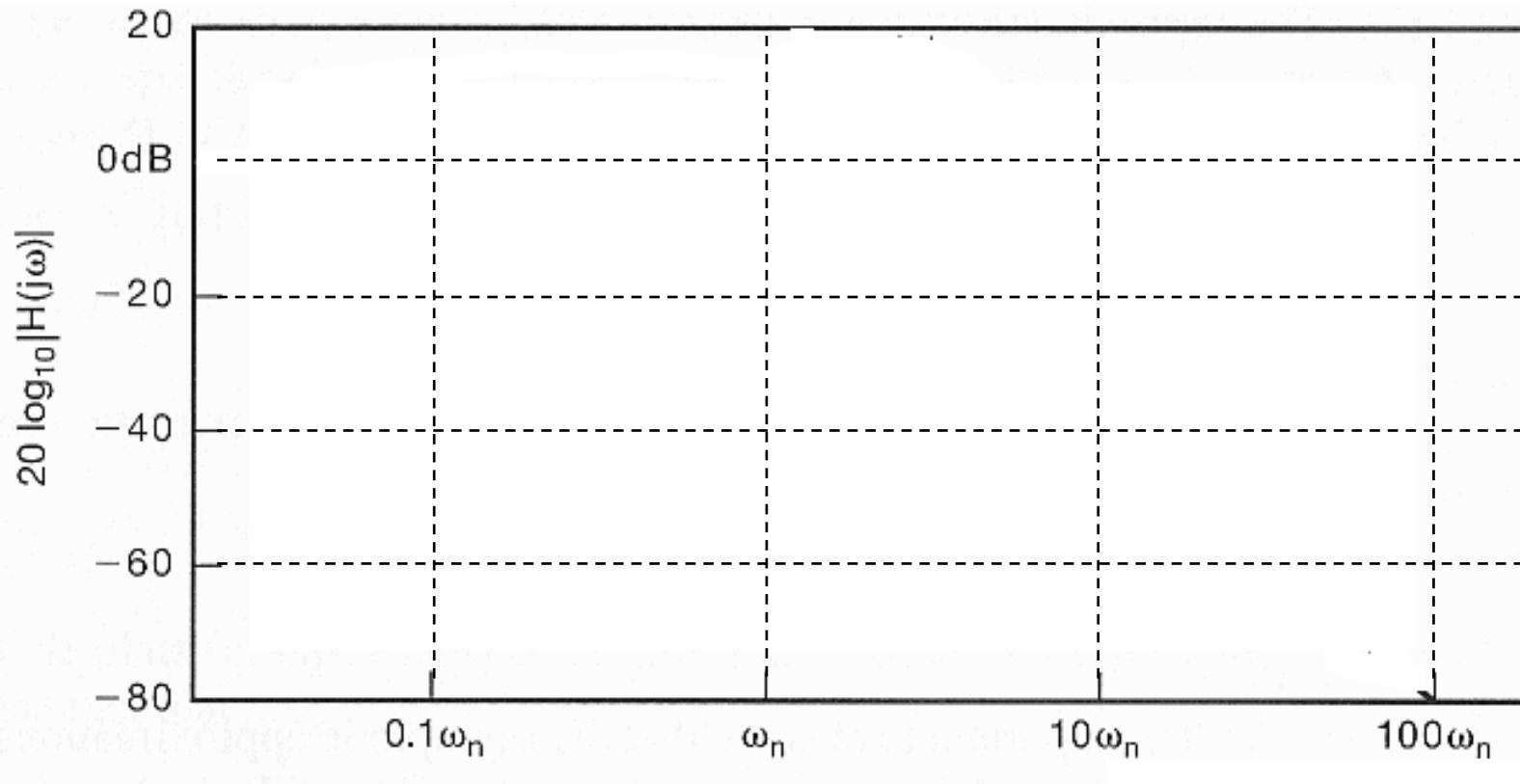
$$\left\{ \begin{array}{ll} 0 & \\ -20 \log_{10}(2\zeta) & \\ -40 \log_{10}(w) + 40 \log_{10}(w_n) & w >> w_n \end{array} \right.$$

$$H(jw) = \frac{1}{(jw/w_n)^2 + 2\zeta(jw/w_n) + 1}$$

$$w << w_n$$

$$w = w_n$$

$$Q = \frac{1}{2\zeta}$$



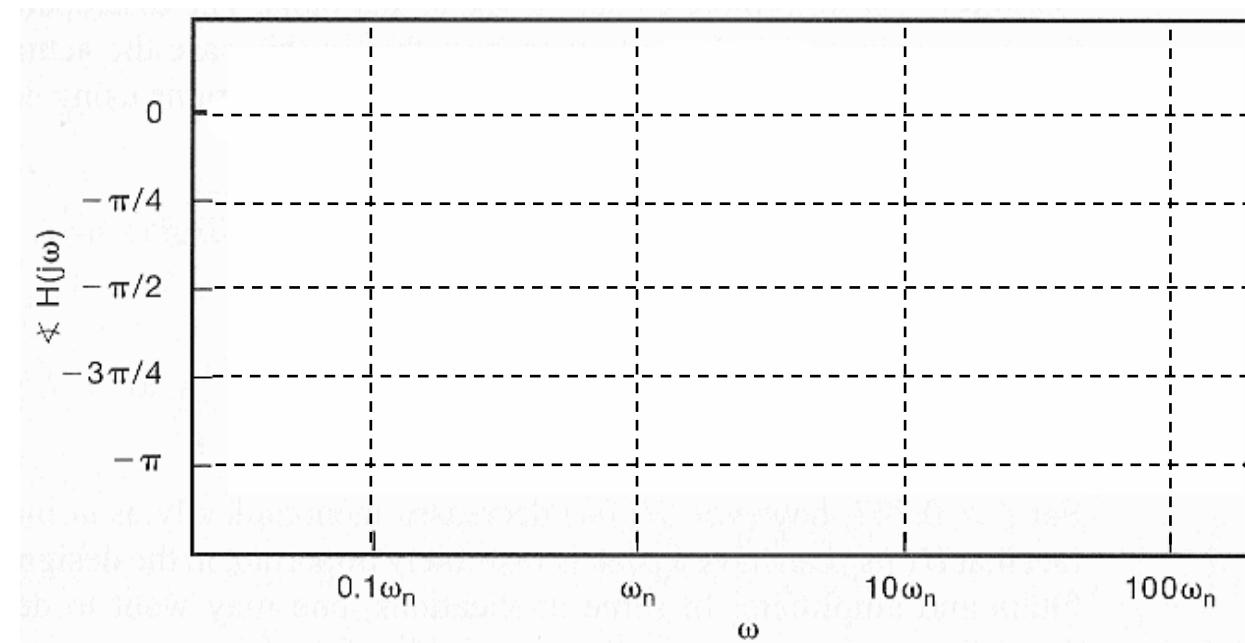
$$w_{max} = w_n \sqrt{1 - 2\zeta^2}$$

$$|H(jw_{max})| = \frac{1}{2\zeta\sqrt{1 - \zeta^2}}$$

- Second-Order CT Systems: $H(jw) = \frac{1}{(jw/w_n)^2 + 2\zeta(jw/w_n) + 1}$

$$\Im H(jw) = -\tan^{-1} \left(\frac{2\zeta(w/w_n)}{1 - (w/w_n)^2} \right)$$

$$\approx \begin{cases} 0 & w \leq 0.1w_n \\ -\pi/2 & w = w_n \\ -(\pi/2)[\log_{10}(w/w_n) + 1] & 0.1w_n \leq w \leq 10w_n \\ -\pi & w \geq 10w_n \end{cases}$$



■ Second-Order CT Systems:

$$H(jw) = \frac{1}{(jw/w_n)^2 + 2\zeta(jw/w_n) + 1}$$

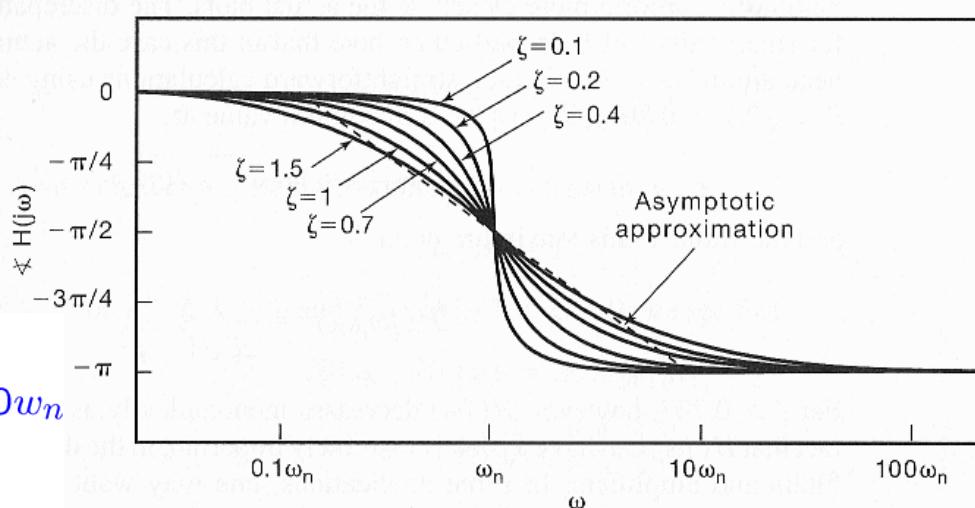
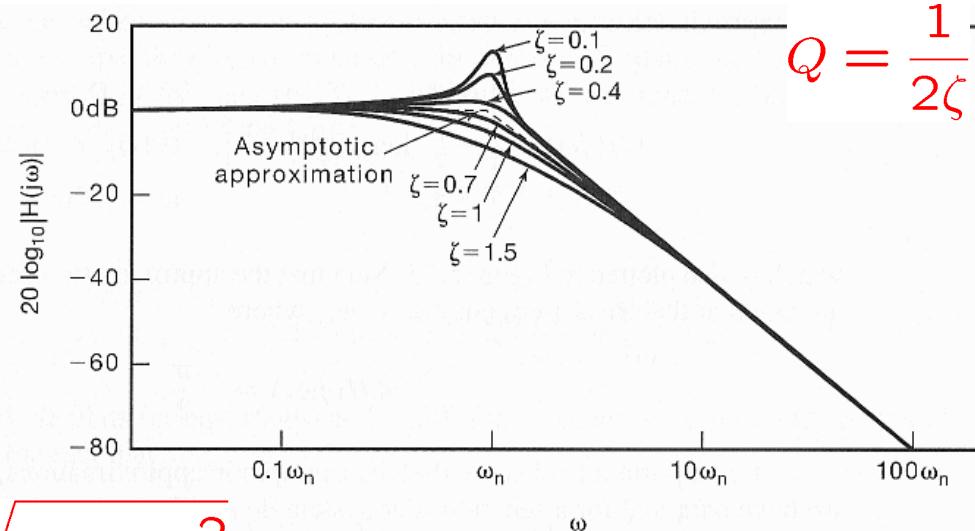
$$20 \log_{10} |H(jw)| =$$

$$\begin{cases} 0 & w \ll w_n \\ -20 \log_{10}(2\zeta) & w = w_n \\ -40 \log_{10}(w) + 40 \log_{10}(w_n) & w \gg w_n \end{cases}$$

- For $\zeta < \sqrt{2}/2$ $w_{\max} = w_n \sqrt{1 - 2\zeta^2}$

$$\angle H(jw) =$$

$$\begin{cases} 0 & w \leq 0.1w_n \\ -(\pi/2)[\log_{10}(w/w_n) + 1] & 0.1w_n \leq w \leq 10w_n \\ -\pi/2 & w = w_n \\ -\pi & w \geq 10w_n \end{cases}$$



■ Example 6.4: (p.457)

$$H(jw) = \frac{2 \times 10^4}{(jw)^2 + 100(jw) + 10^4}$$

$$H(jw) = 2 \times \hat{H}(jw)$$

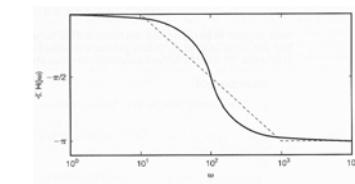
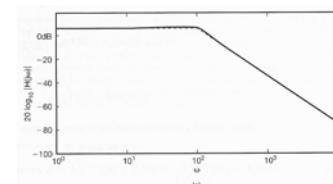
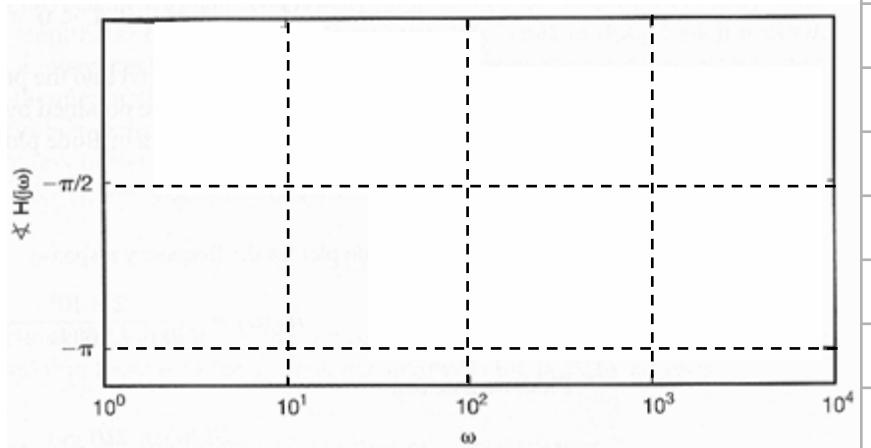
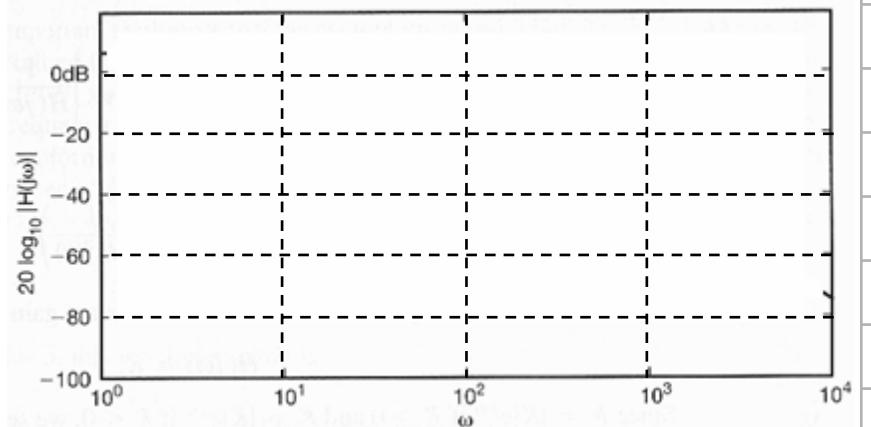
$$\Im H(jw) = \Im \hat{H}(jw)$$

$$\Rightarrow \begin{cases} w_n = 100 \\ \zeta = 1/2 \end{cases}$$

$$\Rightarrow 20 \log_{10} |H(jw)| =$$

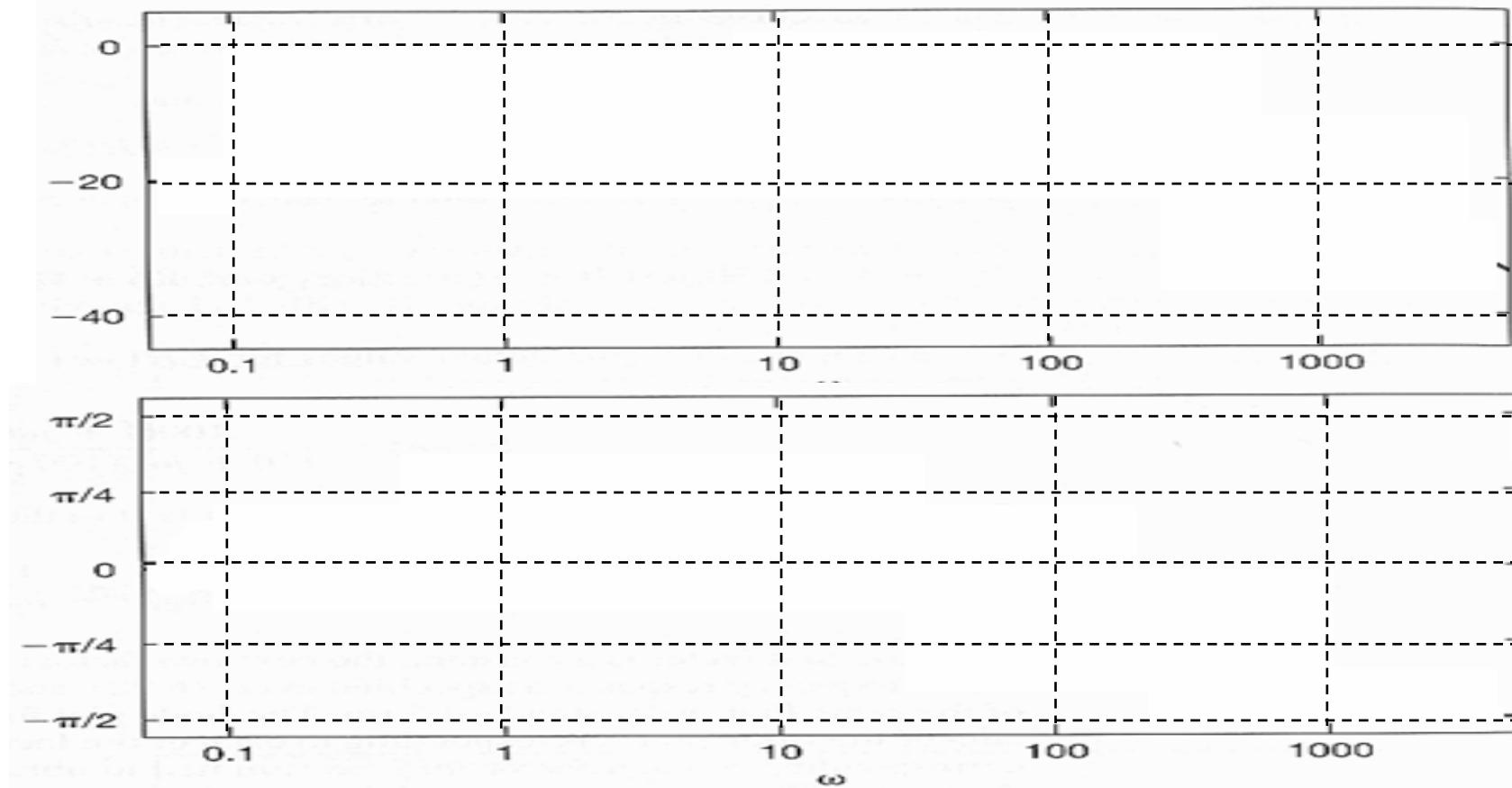
$$20 \log_{10}(2) + 20 \log_{10} |\hat{H}(jw)|$$

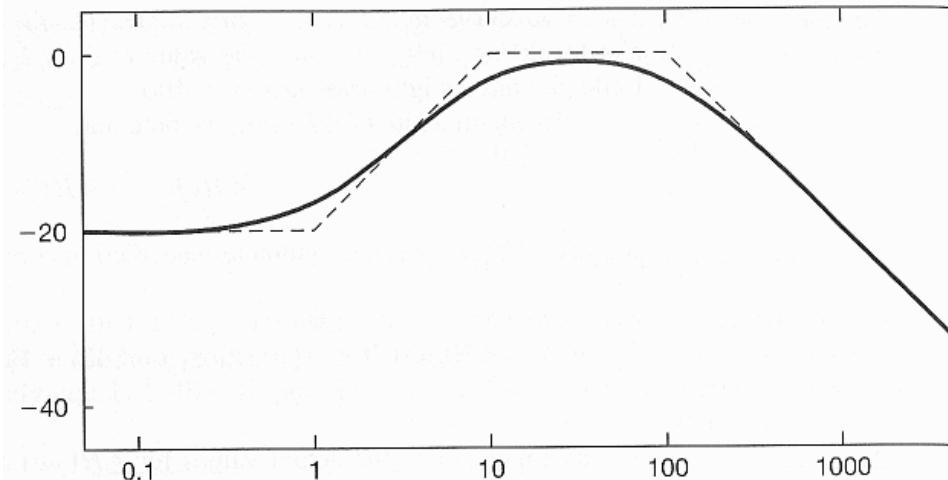
$$\hat{H}(jw) = \frac{w_n^2}{(jw)^2 + 2\zeta w_n(jw) + w_n^2}$$



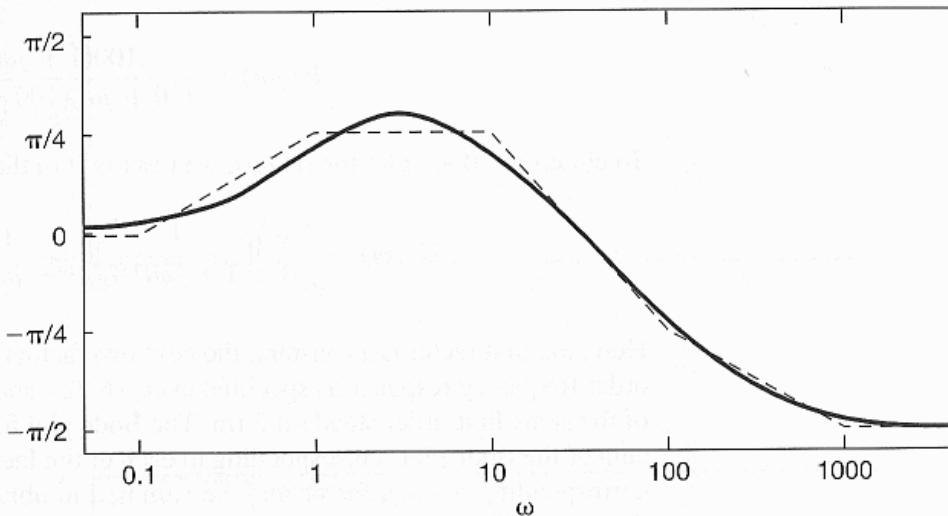
■ Example 6.5: $H(jw) = \frac{100(1 + jw)}{(10 + jw)(100 + jw)}$

$$= \left(\frac{1}{10}\right) (1 + jw) \left(\frac{1}{1 + jw/10}\right) \left(\frac{1}{1 + jw/100}\right)$$



■ Example 6.5:

(a)



(b)

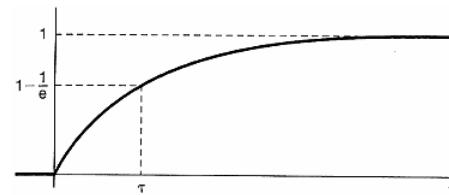
First-Order & Second-Order CT Systems

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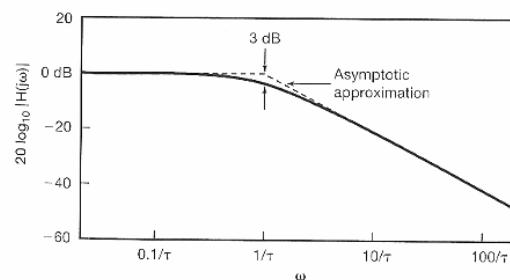
$h(t)$



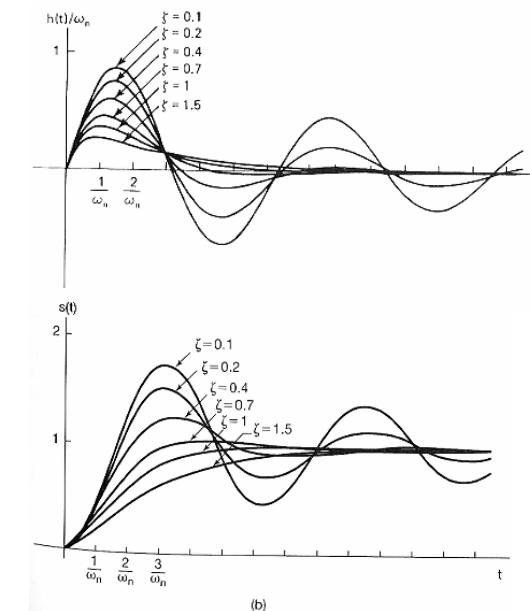
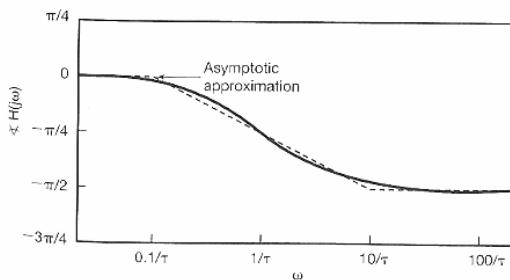
$s(t)$



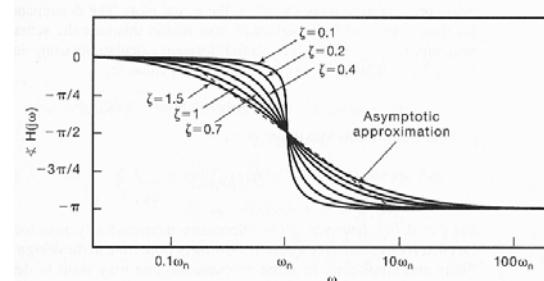
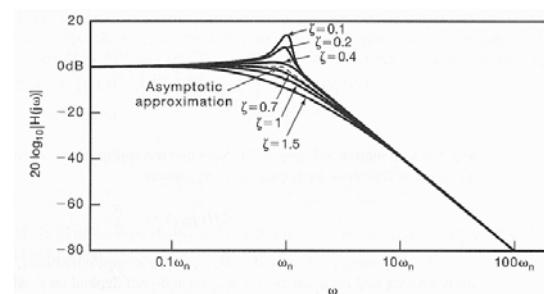
$20 \log_{10} |H(j\omega)|$



$\angle H(j\omega)$



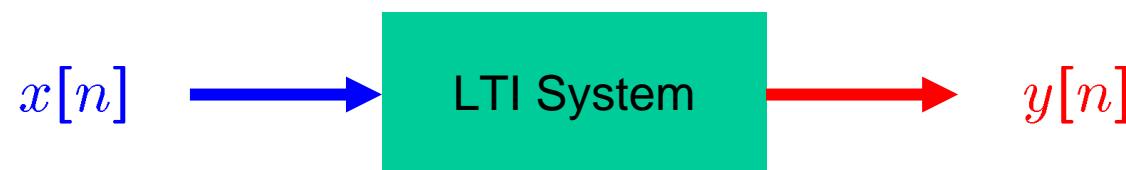
(b)



- The Magnitude-Phase Representation of the Fourier Transform
- The Magnitude-Phase Representation of Frequency Response of LTI Systems
- Time-Domain Properties of Ideal Frequency-Selective Filters
- Time-Domain and Frequency-Domain Aspects of Non-ideal Filters
- 1st-Order & 2nd-Order Continuous-Time Systems
- p.461 ■ 1st-Order & 2nd-Order Discrete-Time Systems
- Time- & Frequency-Domain Analysis of Systems

- First-Order DT Systems: (p.461)

$$Y(e^{jw}) = X(e^{jw}) H(e^{jw})$$

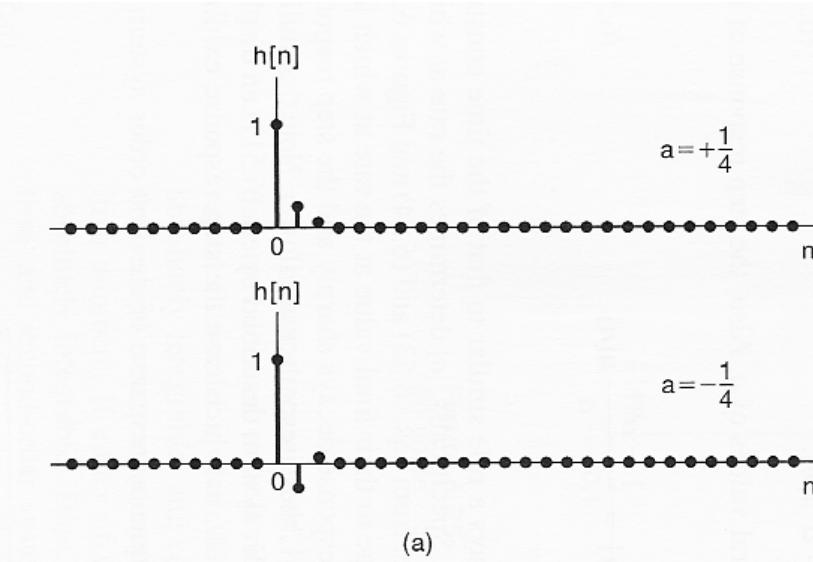


$$y[n] - a y[n - 1] = x[n] \quad |a| < 1$$

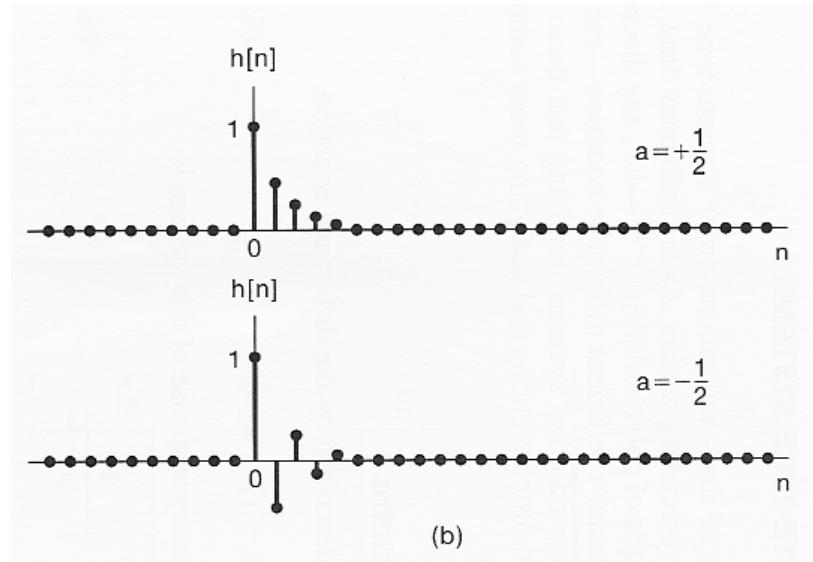
$$\Rightarrow H(e^{jw}) = \frac{1}{1 - ae^{-jw}}$$

$$\Rightarrow h[n] = a^n u[n]$$

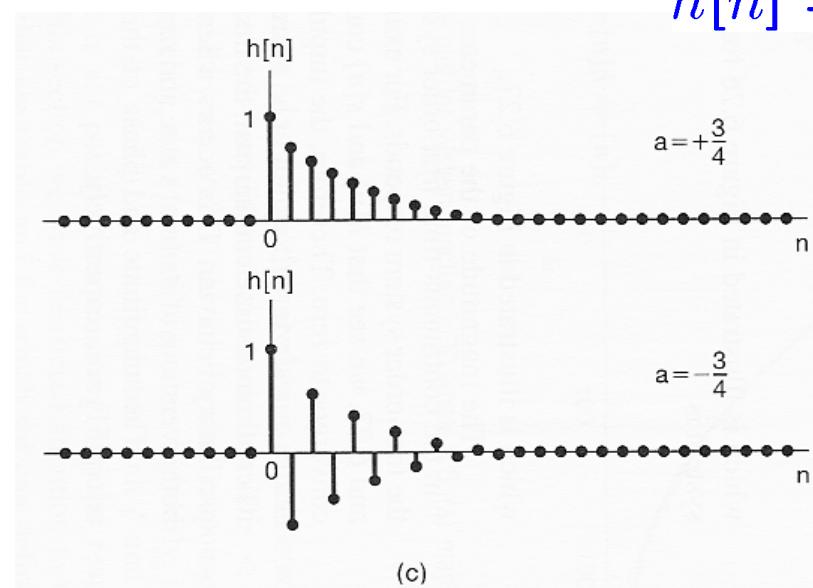
$$\Rightarrow s[n] = h[n] * u[n] = \frac{1 - a^{n+1}}{1 - a} u[n]$$

■ Impulse Response of First-Order DT Systems:

(a)

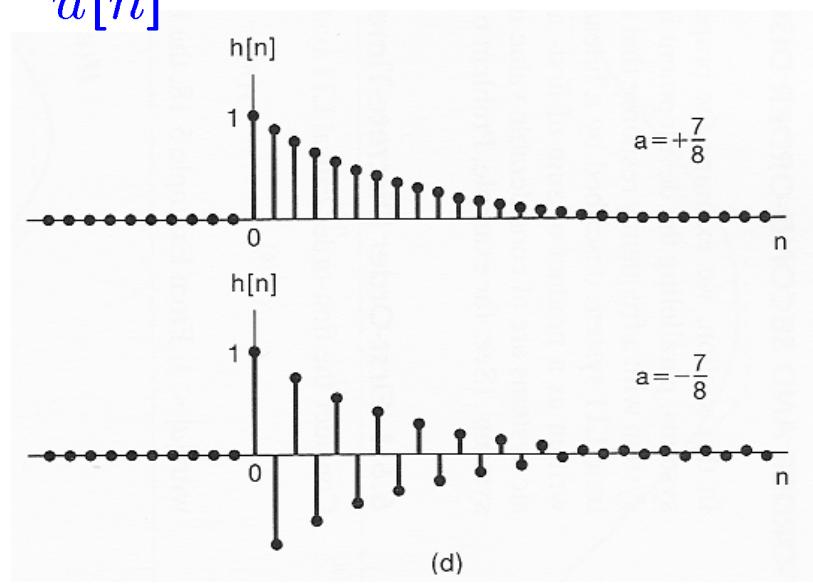


(b)



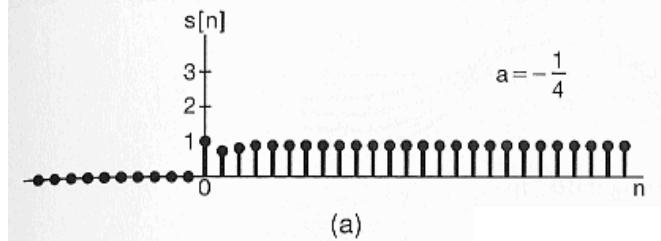
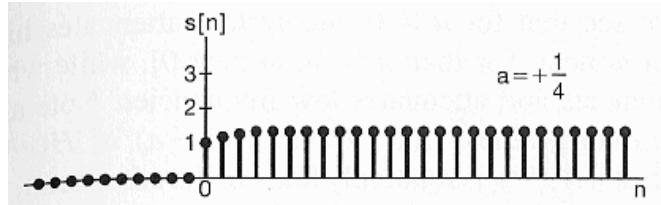
(c)

$$h[n] = a^n u[n]$$

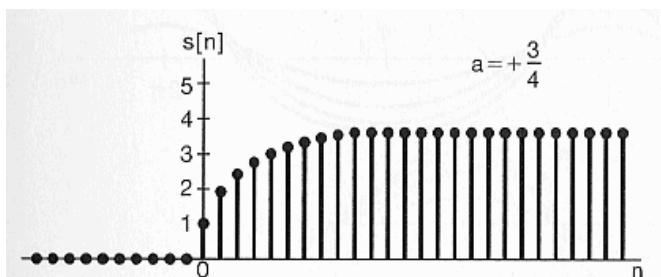


(d)

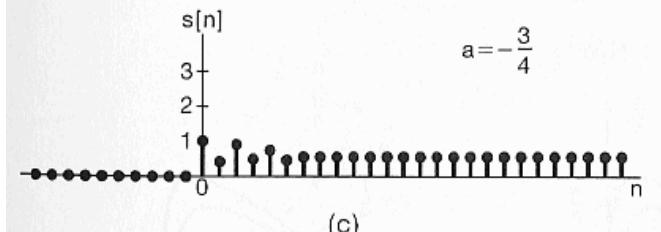
■ Step Response of First-Order DT Systems:



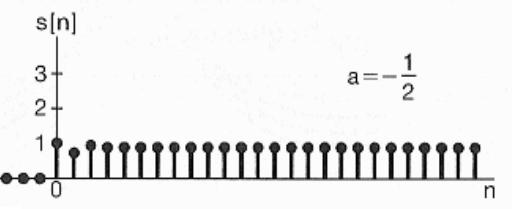
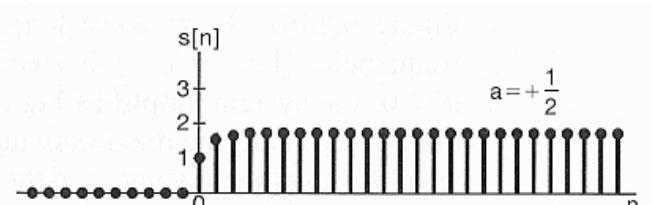
(a)



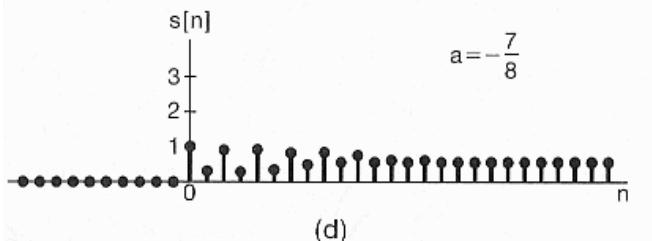
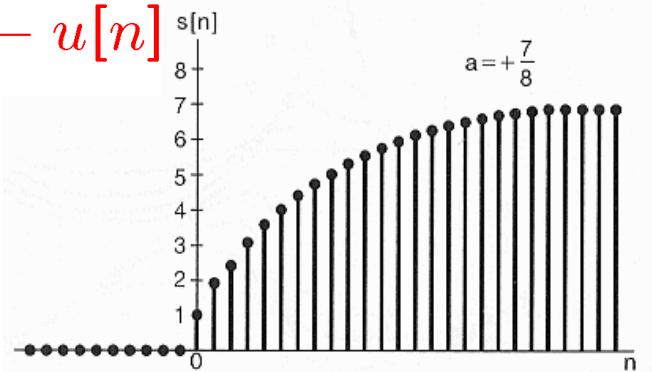
s[n]

 $a = -\frac{3}{4}$ 

(c)



(b)



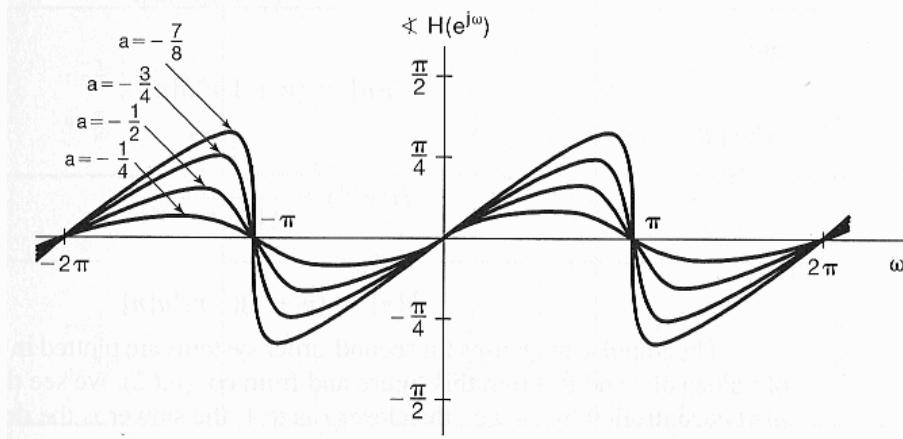
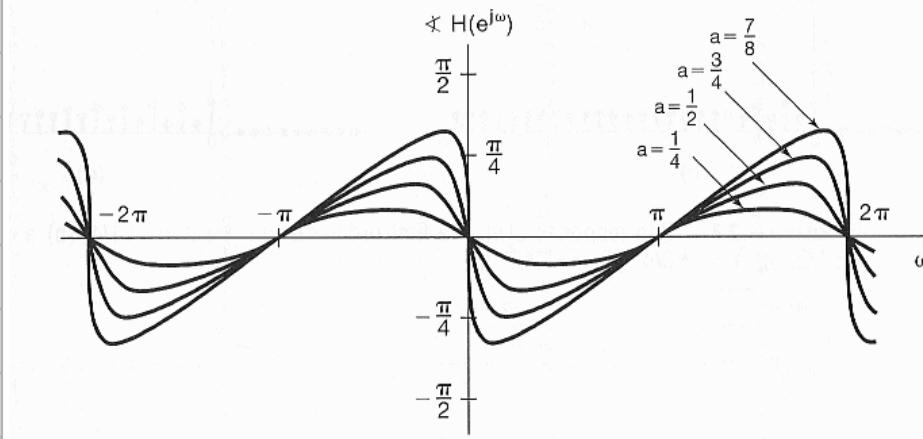
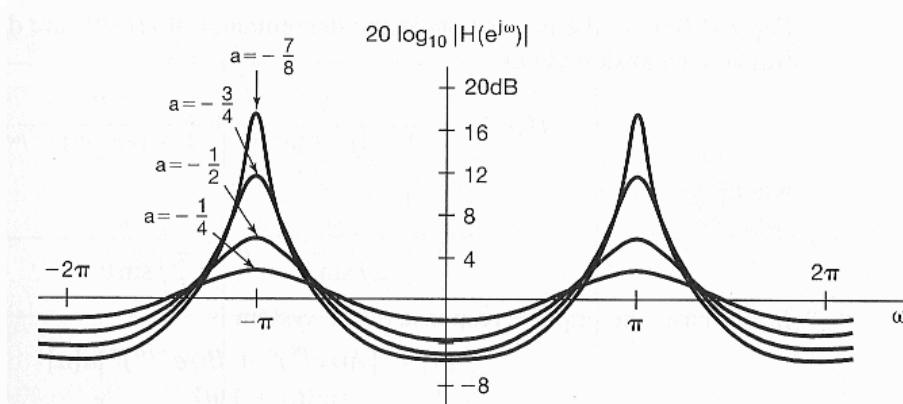
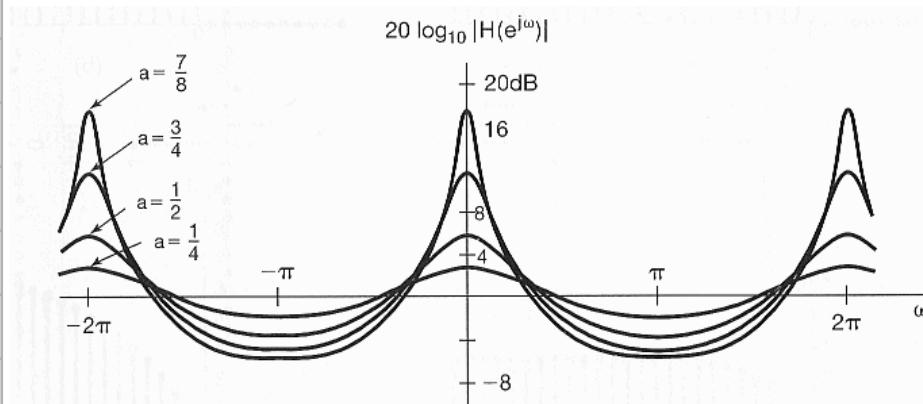
(d)

- Magnitude & Phase of Frequency Response:

$$H(e^{jw}) = \frac{1}{1 - ae^{-jw}} = \frac{1}{1 - a \cos w + ja \sin w}$$

$$|H(e^{jw})| = \frac{1}{\sqrt{1 + a^2 - 2a \cos w}}$$

$$\angle H(e^{jw}) = -\tan^{-1} \left[\frac{a \sin w}{1 - a \cos w} \right]$$

Magnitude & Phase of Frequency Response:

- Second-Order DT Systems: (p.465)

$$0 < r < 1 \text{ and } 0 \leq \theta \leq \pi$$

$$y[n] - 2r \cos(\theta) y[n-1] + r^2 y[n-2] = x[n]$$

$$\Rightarrow H(e^{jw}) = \frac{1}{1 - 2r \cos(\theta) e^{-jw} + r^2 e^{-j2w}}$$

$$= \frac{1}{[1 - (re^{j\theta})e^{-jw}] [1 - (re^{-j\theta})e^{-jw}]}$$

■ Impulse Response of 2nd-Order DT Systems:

- For $\theta = 0$:

$$\Rightarrow H(e^{jw}) = \frac{1}{(1 - r e^{-jw})^2} \Rightarrow h[n] = (n+1) (r)^n u[n]$$

- For $\theta = \pi$:

$$\Rightarrow H(e^{jw}) = \frac{1}{(1 + r e^{-jw})^2} \Rightarrow h[n] = (n+1) (-r)^n u[n]$$

- For $\theta \neq 0$ or π :

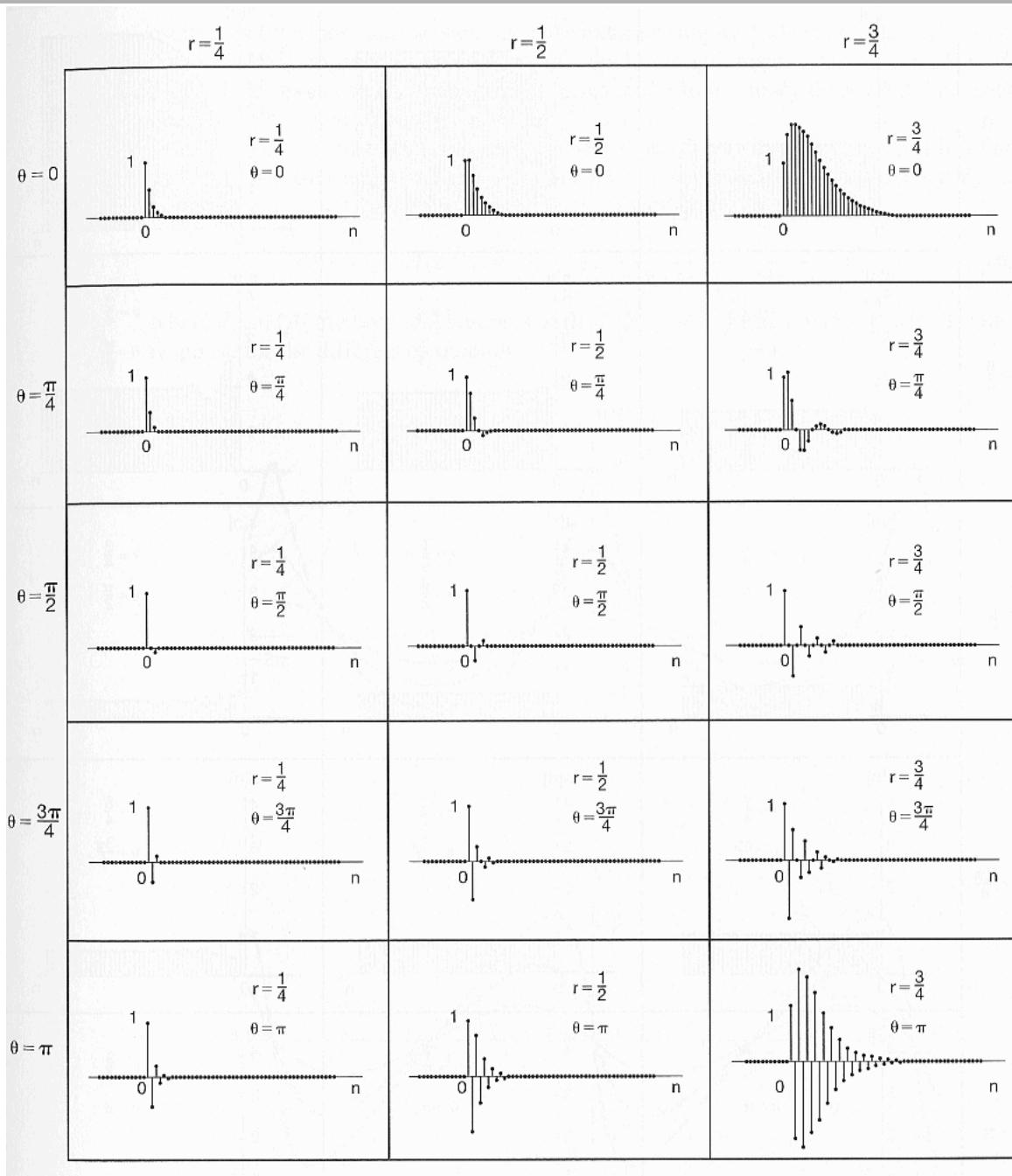
$$A = \frac{e^{j\theta}}{2j \sin(\theta)} \quad B = -\frac{e^{-j\theta}}{2j \sin(\theta)}$$

$$\Rightarrow H(e^{jw}) = \frac{A}{1 - (r e^{j\theta}) e^{-jw}} + \frac{B}{1 - (r e^{-j\theta}) e^{-jw}}$$

$$\Rightarrow h[n] = [A(r e^{j\theta})^n + B(r e^{-j\theta})^n] u[n]$$

$$= r^n \frac{\sin[(n+1)\theta]}{\sin(\theta)} u[n]$$

First-Order & Second-Order DT Systems



$$h[n] = (n+1) (r)^n u[n]$$

$$r^n \frac{\sin[(n+1)\theta]}{\sin(\theta)} u[n]$$

$$h[n] = (n+1) (-r)^n u[n]$$

■ Step Response of 2nd-Order DT Systems:

- For $\theta = 0$:

$$s[n] = \left[\frac{1}{(r-1)^2} - \frac{r}{(r-1)^2} r^n + \frac{r}{r-1} (n+1) r^n \right] u[n]$$

- For $\theta = \pi$:

$$s[n] = \left[\frac{1}{(r+1)^2} + \frac{r}{(r+1)^2} (-r)^n + \frac{r}{r+1} (n+1) (-r)^n \right] u[n]$$

- For $\theta \neq 0$ or π :

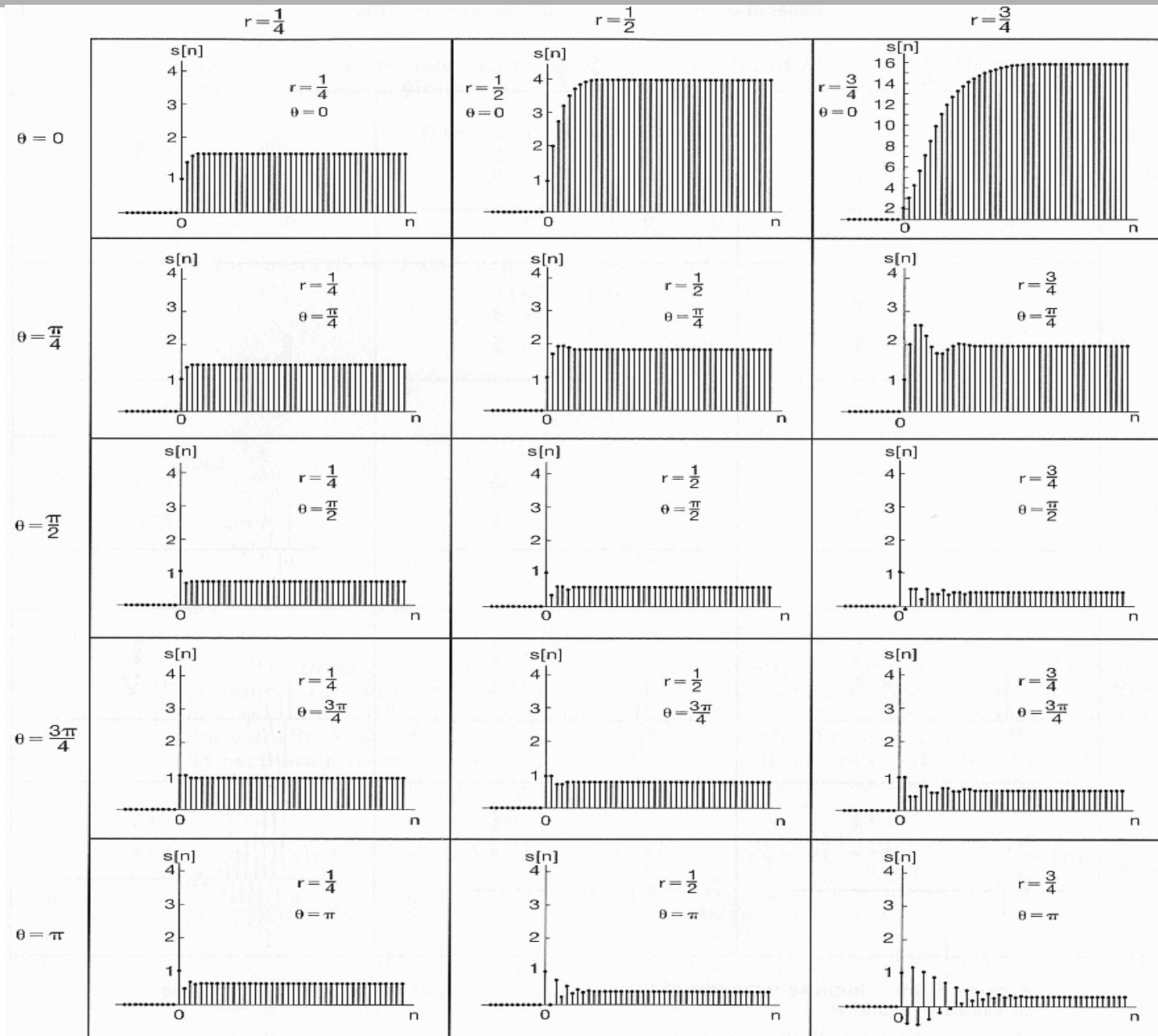
$$s[n] = h[n] * u[n]$$

$$A = \frac{e^{j\theta}}{2j \sin(\theta)}$$

$$B = -\frac{e^{-j\theta}}{2j \sin(\theta)}$$

$$= \left[A \left(\frac{1 - (re^{j\theta})^{n+1}}{1 - re^{j\theta}} \right) + B \left(\frac{1 - (re^{-j\theta})^{n+1}}{1 - re^{-j\theta}} \right) \right] u[n]$$

First-Order & Second-Order DT Systems

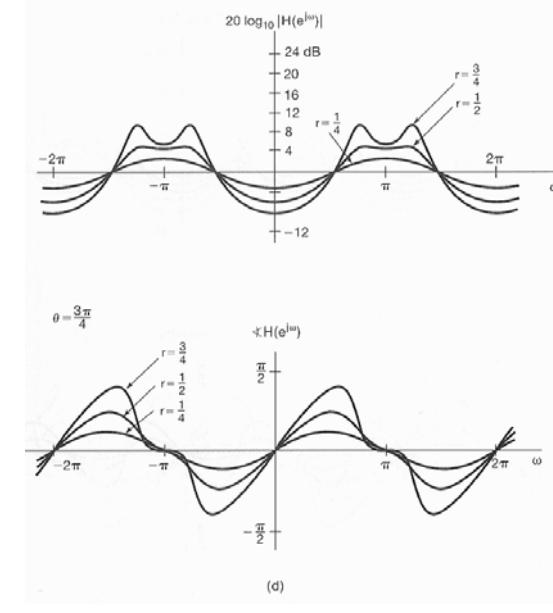
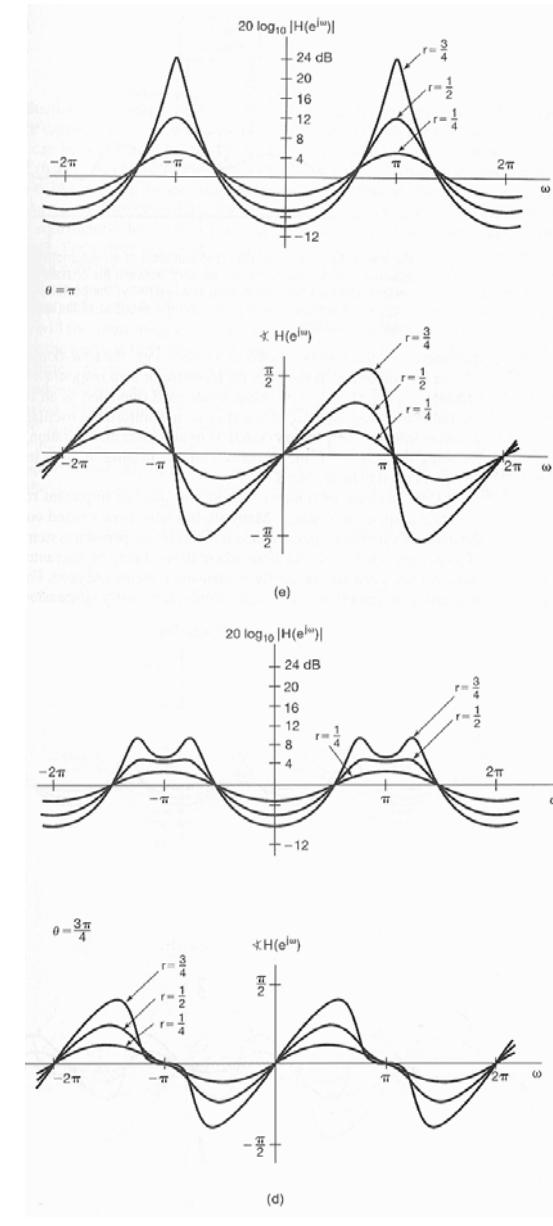
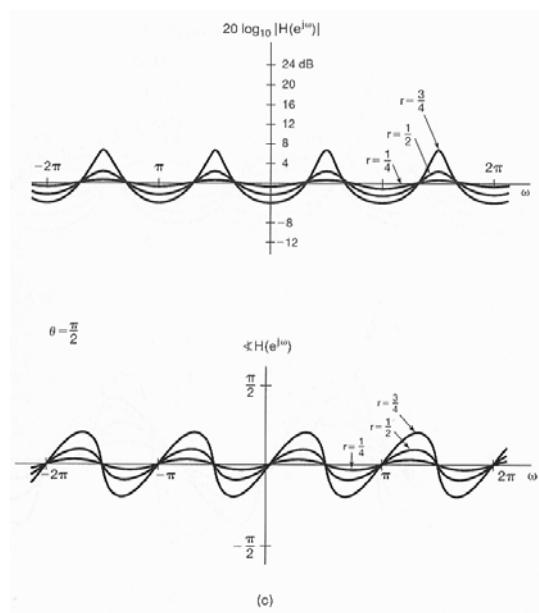
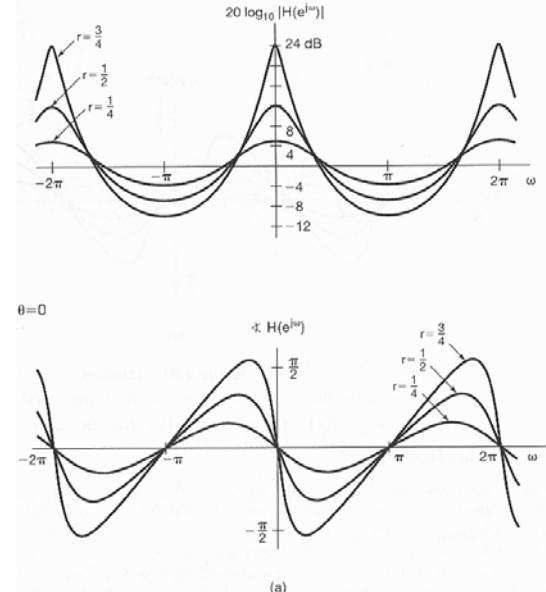
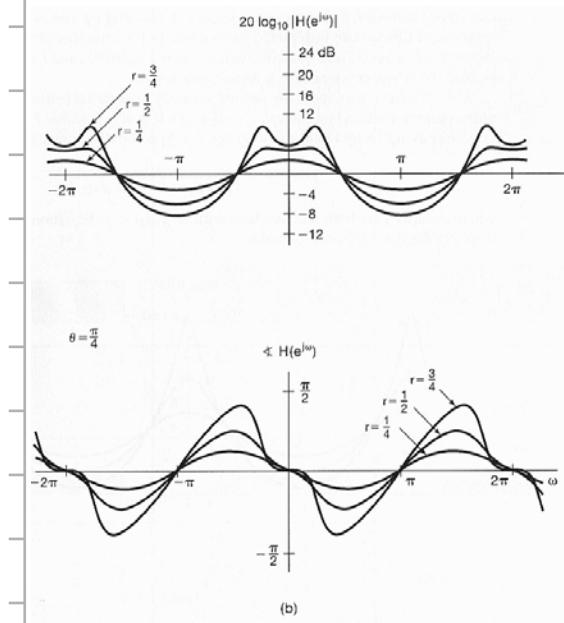


* Note: The plot for $r = \frac{3}{4}, \theta = 0$ has a different scale from the others.

■ Magnitude & Phase of Frequency Response:

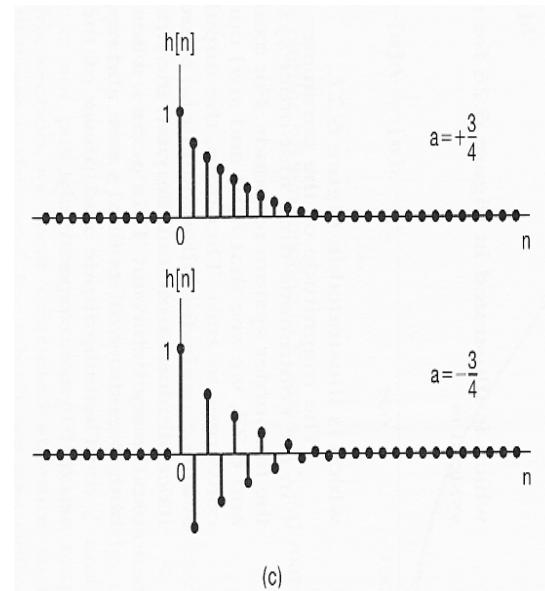
$$H(e^{j\omega}) =$$

$$\frac{1}{1 - 2r \cos(\theta) e^{-j\omega} + r^2 e^{-j2\omega}}$$



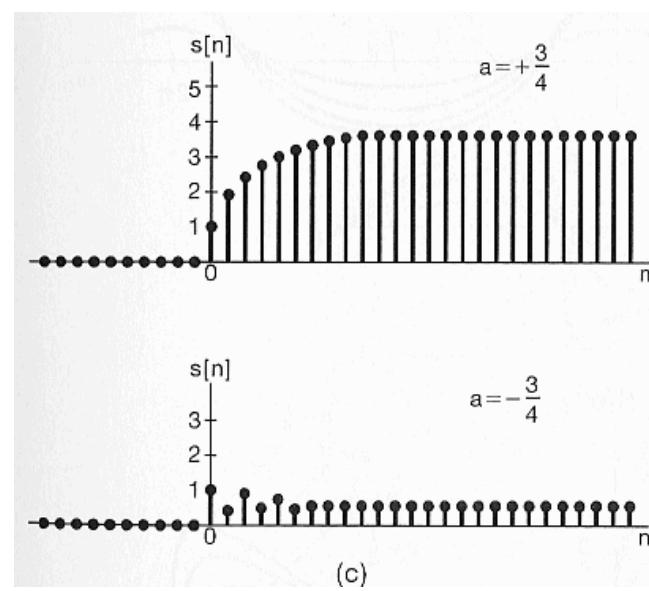
First-Order & Second-Order DT Systems

$h[n]$

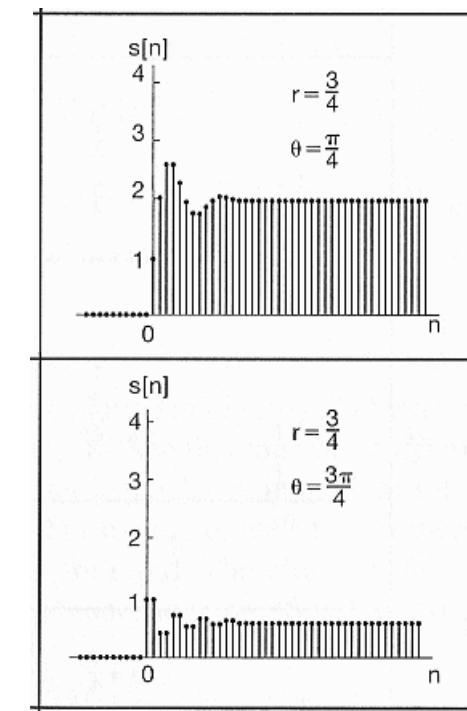
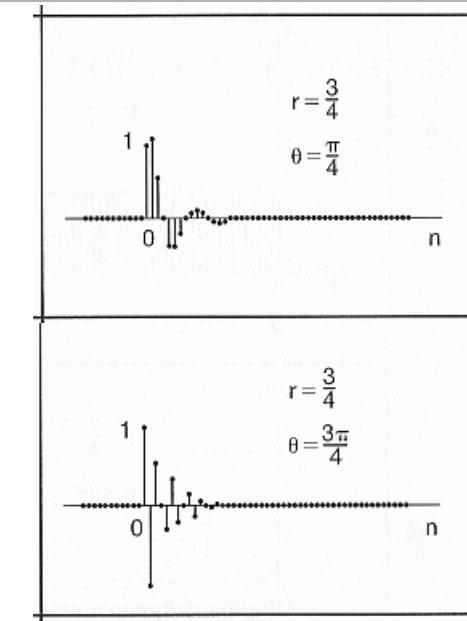


(c)

$s[n]$



(c)

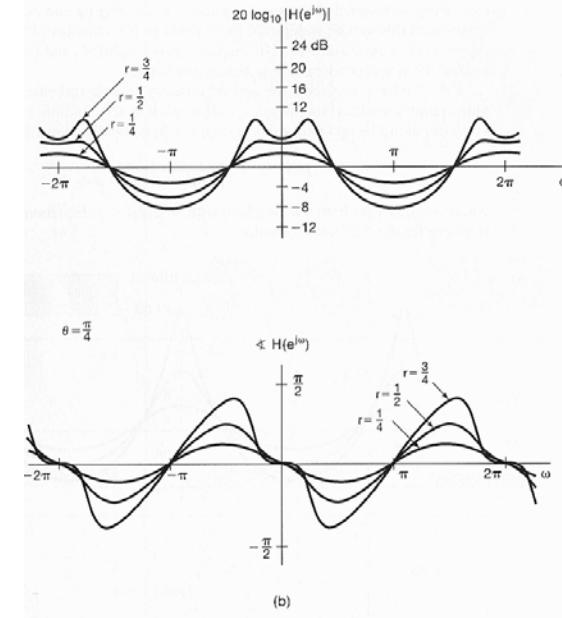
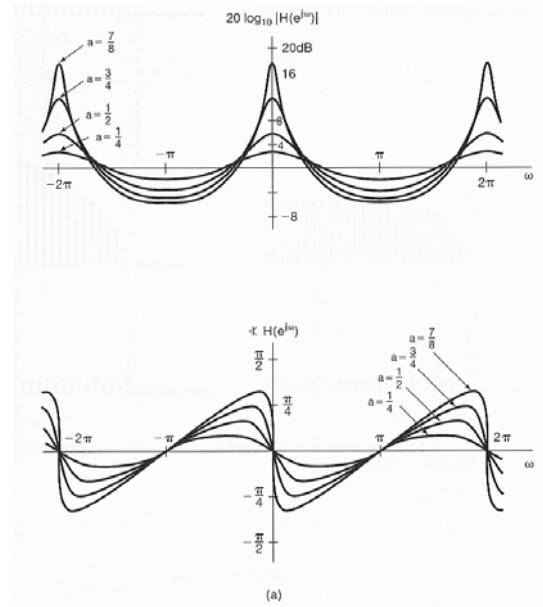


First-Order & Second-Order DT Systems

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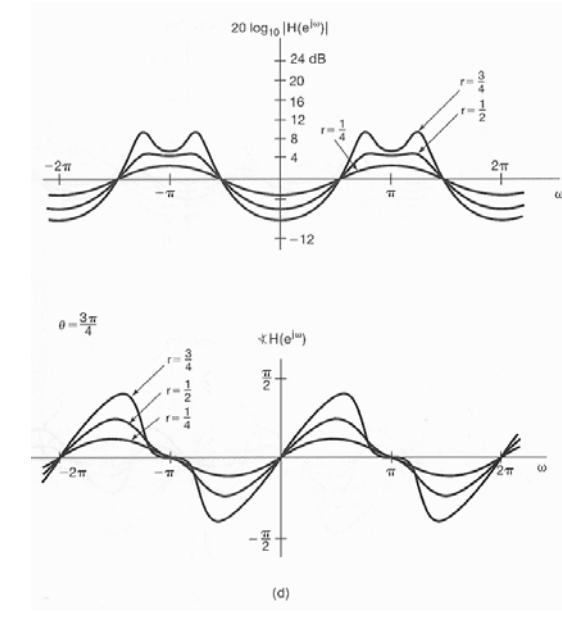
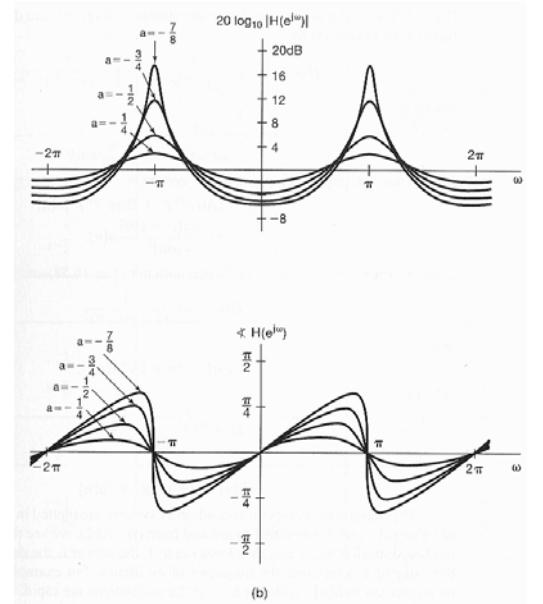
$$20 \log_{10} |H(e^{j\omega})|$$

$$\propto H(e^{j\omega})$$



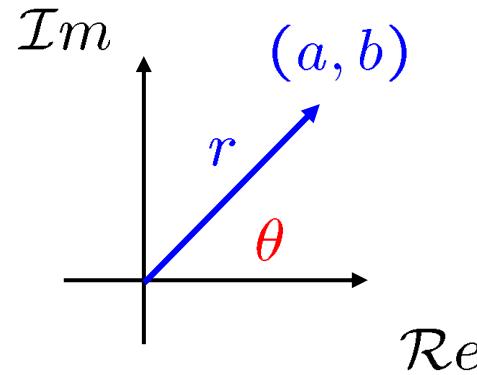
$$20 \log_{10} |H(e^{j\omega})|$$

$$\propto H(e^{j\omega})$$



- The Magnitude-Phase Representation of the Fourier Transform [\(p.423\)](#)
- The Magnitude-Phase Representation of Frequency Response of LTI Systems
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■ Magnitude & Phase Representation:



$$a + jb \Rightarrow \begin{cases} r = \sqrt{a^2 + b^2} \\ \tan(\theta) = \frac{b}{a} \end{cases} \Rightarrow a + jb = re^{j\theta}$$

$$X(jw) = \mathcal{R}e\{X(jw)\} + j \mathcal{I}m\{X(jw)\} = |X(jw)| e^{j\angle X(jw)}$$

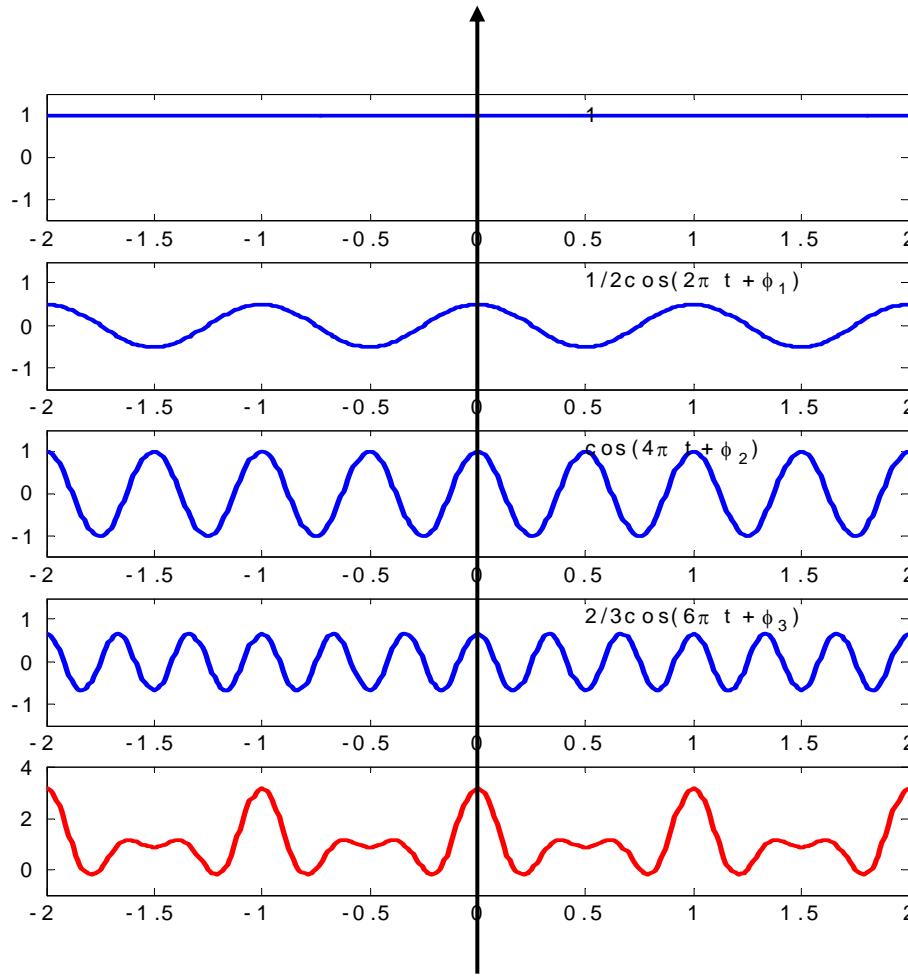
$$X(e^{jw}) = \mathcal{R}e\{X(e^{jw})\} + j \mathcal{I}m\{X(e^{jw})\} = |X(e^{jw})| e^{j\angle X(e^{jw})}$$

$|X(jw)|$ or $|X(e^{jw})|$: magnitude

$\angle X(jw)$ or $\angle X(e^{jw})$: phase angle

- Magnitude & Phase Angle:** $A \cos(w_0 t + \phi) = \frac{A}{2} e^{j\phi} e^{jw_0 t} + \frac{A}{2} e^{-j\phi} e^{-jw_0 t}$

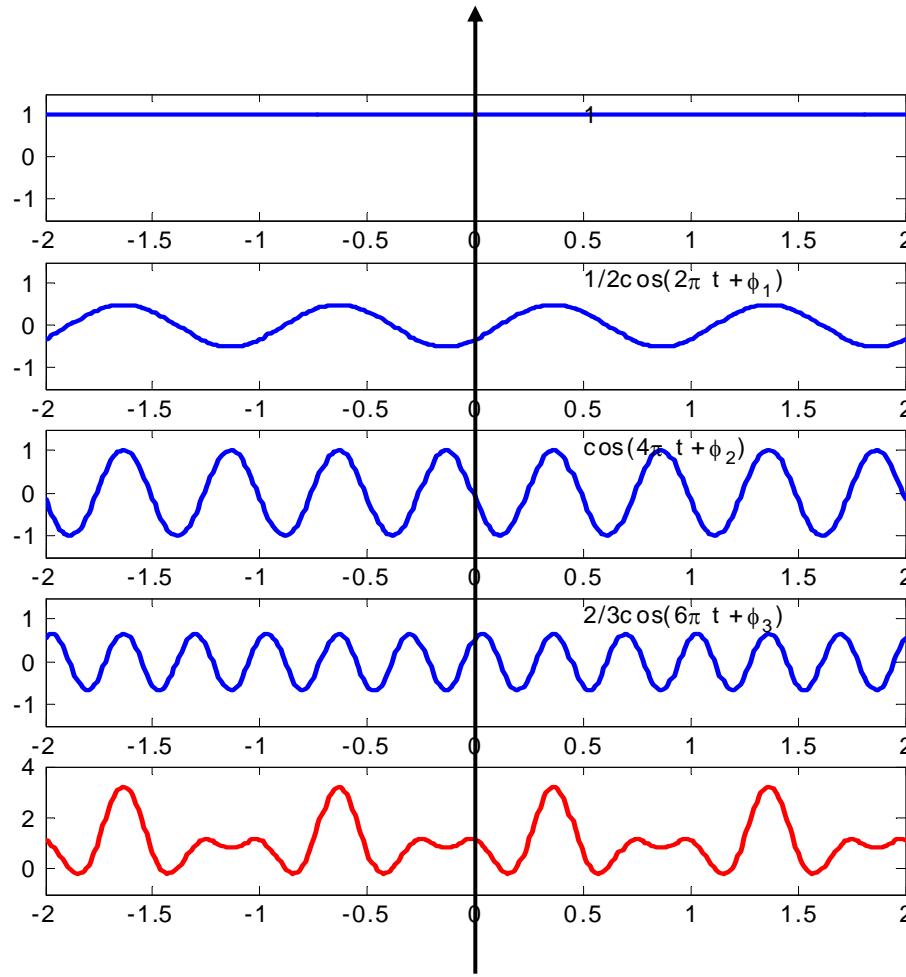
$$x(t) = 1 \cos(0\pi t + \phi_0) + \frac{1}{2} \cos(2\pi t + \phi_1) + 1 \cos(4\pi t + \phi_2) + \frac{2}{3} \cos(6\pi t + \phi_3)$$



$$\begin{cases} \phi_1 = 0 \text{ (rad)} \\ \phi_2 = 0 \text{ (rad)} \\ \phi_3 = 0 \text{ (rad)} \end{cases}$$

- Magnitude & Phase Angle:** $A \cos(w_0 t + \phi) = \frac{A}{2} e^{j\phi} e^{jw_0 t} + \frac{A}{2} e^{-j\phi} e^{-jw_0 t}$

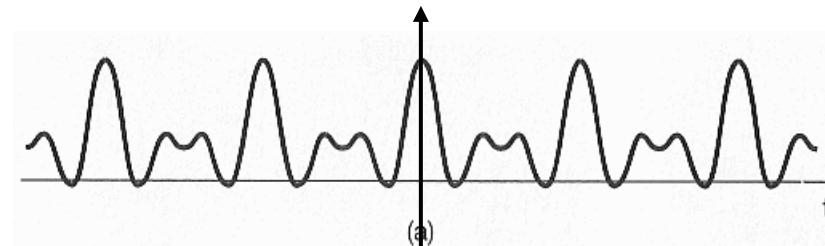
$$x(t) = 1 \cos(0\pi t + \phi_0) + \frac{1}{2} \cos(2\pi t + \phi_1) + 1 \cos(4\pi t + \phi_2) + \frac{2}{3} \cos(6\pi t + \phi_3)$$



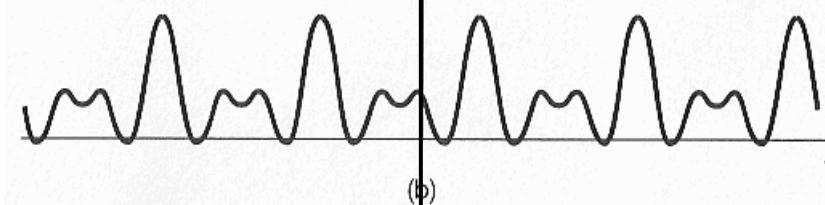
$$\begin{cases} \phi_1 = 4 \text{ (rad)} \\ \phi_2 = 8 \text{ (rad)} \\ \phi_3 = 12 \text{ (rad)} \end{cases}$$

■ Magnitude & Phase Angle: $A \cos(w_0 t + \phi) = \frac{A}{2} e^{j\phi} e^{jw_0 t} + \frac{A}{2} e^{-j\phi} e^{-jw_0 t}$

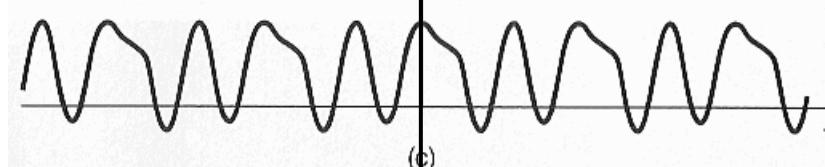
$$x(t) = 1 \cos(0\pi t + \phi_0) + \frac{1}{2} \cos(2\pi t + \phi_1) + 1 \cos(4\pi t + \phi_2) + \frac{2}{3} \cos(6\pi t + \phi_3)$$



$$\begin{cases} \phi_1 = 0 \text{ (rad)} \\ \phi_2 = 0 \text{ (rad)} \\ \phi_3 = 0 \text{ (rad)} \end{cases}$$



$$\begin{cases} \phi_1 = 4 \text{ (rad)} \\ \phi_2 = 8 \text{ (rad)} \\ \phi_3 = 12 \text{ (rad)} \end{cases}$$



$$\begin{cases} \phi_1 = 6 \text{ (rad)} \\ \phi_2 = -2.7 \text{ (rad)} \\ \phi_3 = 0.93 \text{ (rad)} \end{cases}$$



$$\begin{cases} \phi_1 = 1.2 \text{ (rad)} \\ \phi_2 = 4.1 \text{ (rad)} \\ \phi_3 = -7.02 \text{ (rad)} \end{cases}$$

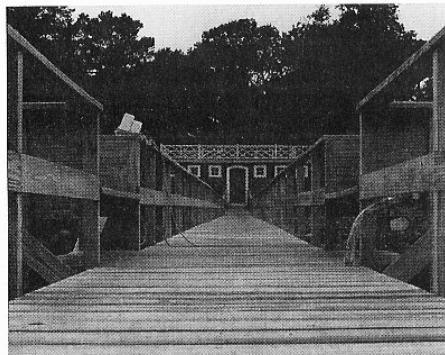
■ Magnitude & Phase Angle in Images:

$$x(t_1, t_2) \xleftrightarrow{\mathcal{F}} X(jw_1, jw_2)$$

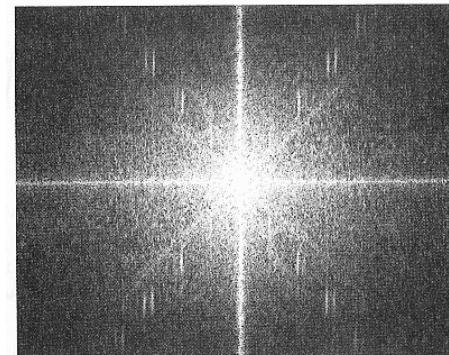
$$x[n_1, n_2] \xleftrightarrow{\mathcal{F}} X(e^{jw_1}, e^{jw_2})$$

$$|X(jw)| e^{j\angle X(jw)}$$

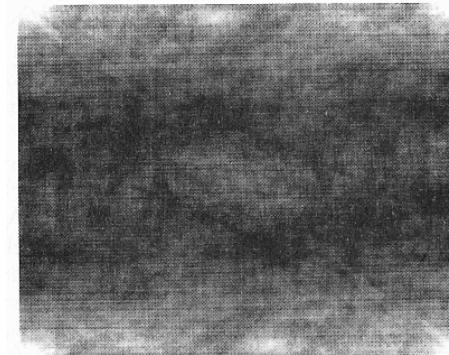
$$|X(e^{jw})| e^{j\angle X(e^{jw})}$$



image



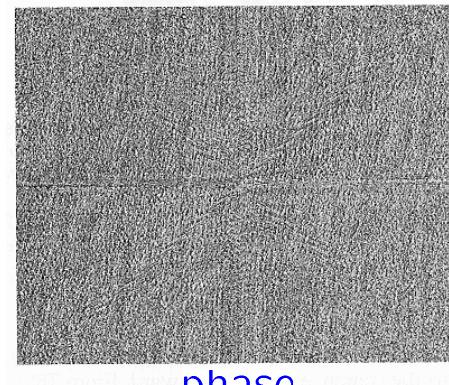
magnitude



mag + zero pha



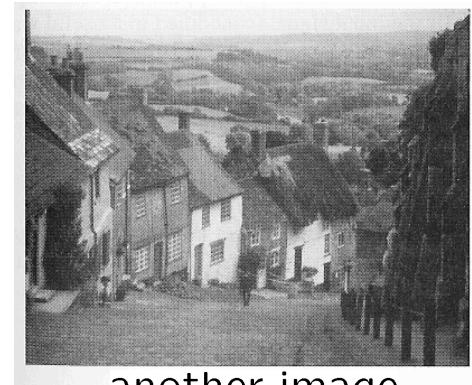
new mag + pha



phase



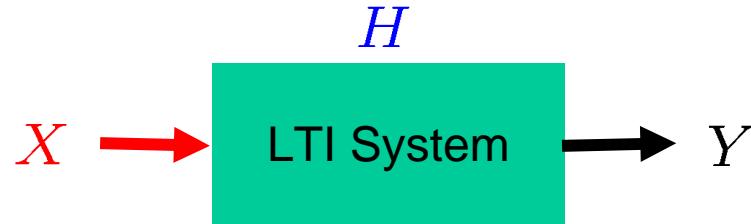
unit mag + pha



another image

- The Magnitude-Phase Representation of the Fourier Transform
- The Magnitude-Phase Representation of Frequency Response of LTI Systems (p.427)
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■ Magnitude & Phase Distortions:



$$Y(jw) = X(jw) H(jw)$$

$$Y(e^{jw}) = X(e^{jw}) H(e^{jw})$$

$$\Rightarrow |Y(jw)| = |X(jw)| |H(jw)|$$

magnitude distortion

$$|Y(e^{jw})| = |X(e^{jw})| |H(e^{jw})|$$

$$\Rightarrow \angle Y(jw) = \angle X(jw) + \angle H(jw)$$

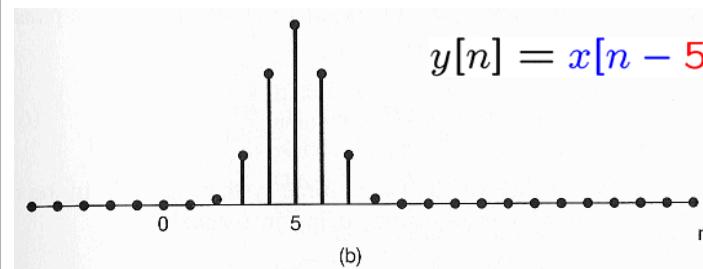
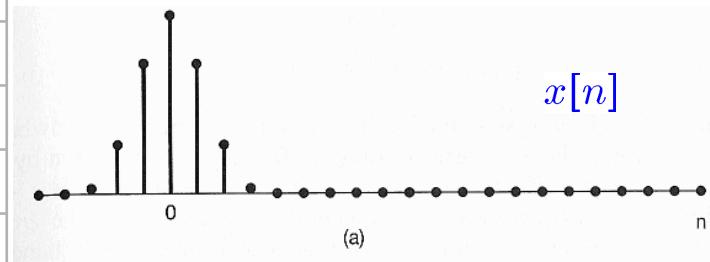
phase distortion

$$\angle Y(e^{jw}) = \angle X(e^{jw}) + \angle H(e^{jw})$$

$|H(jw)|$ or $|H(e^{jw})|$: gain of the system

$\angle H(jw)$ or $\angle H(e^{jw})$: phase shift of the system

■ Linear Phase:



$$y[n] = x[n - 5]$$

- $H_1(e^{jw}) = e^{-jwn_0}$

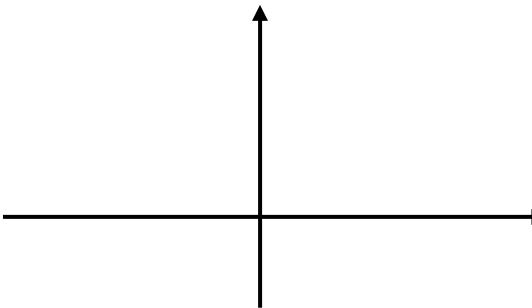
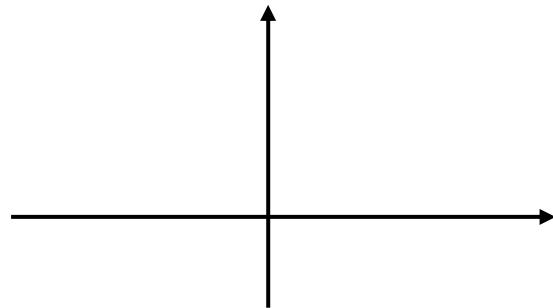
$$\Rightarrow \begin{cases} |H_1(e^{jw})| = 1 \\ \angle H_1(e^{jw}) = -wn_0 \end{cases}$$

$$\begin{aligned} Y_1(e^{jw}) &= H_1(e^{jw}) X(e^{jw}) \\ &= e^{-jwn_0} X(e^{jw}) \end{aligned}$$

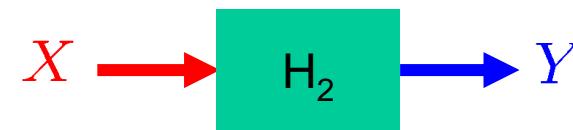
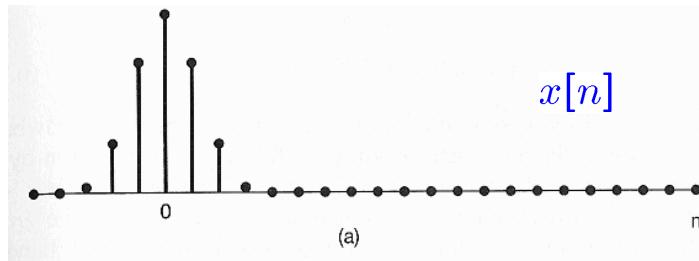
$$\Rightarrow y[n] = x[n - n_0]$$

$$\angle H_1(e^{jw}) =$$

$$-\frac{d}{dw} \{ \angle H_1(e^{jw}) \} =$$



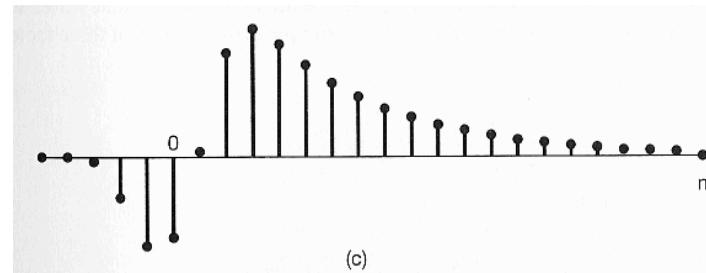
■ Linear Phase:



$$H_2(e^{jw}) = e^{jf(w)}$$

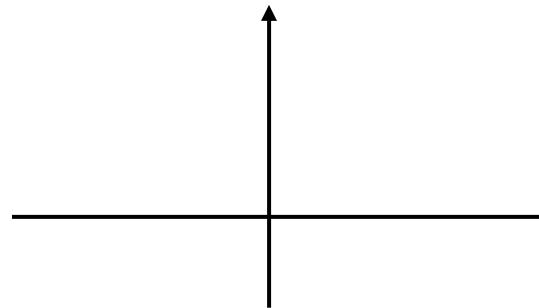
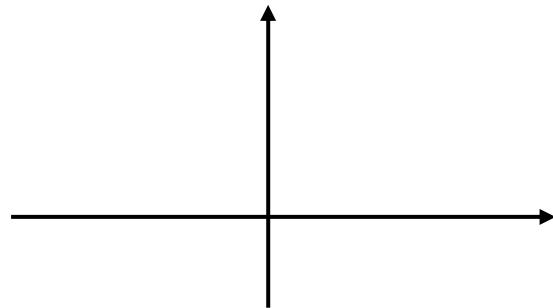
- $Y_2(e^{jw}) = H_2(e^{jw}) X(e^{jw})$

$$= e^{jf(w)} X(e^{jw})$$

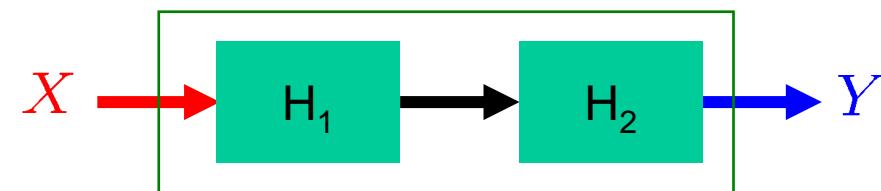
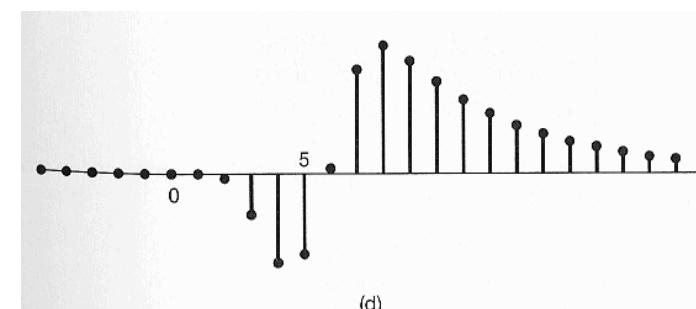
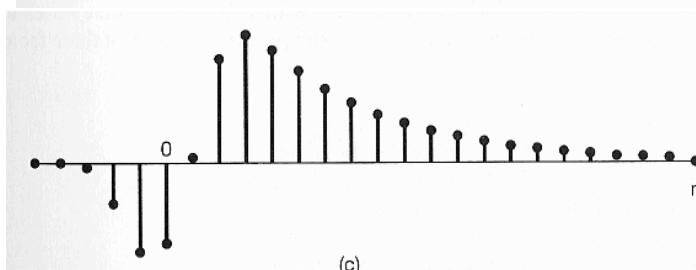
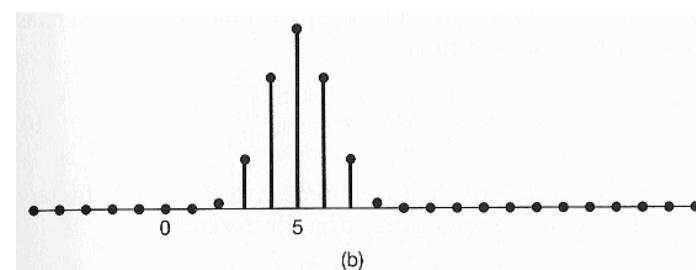
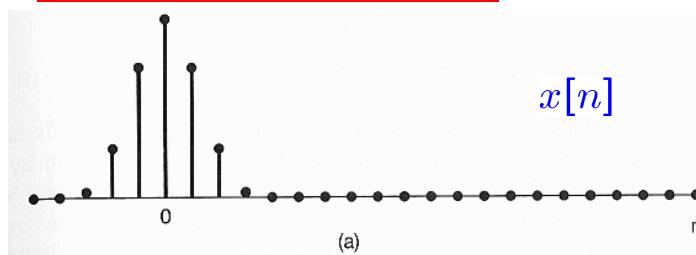


$$\nexists H_2(e^{jw}) =$$

$$- \frac{d}{dw} \left\{ \nexists H_2(e^{jw}) \right\} =$$



■ Linear Phase:



- $Y_3(e^{jw}) = H_2(e^{jw}) \ H_1(e^{jw}) \ X(e^{jw})$

$$H_3(e^{jw}) = H_2(e^{jw})H_1(e^{jw})$$

$$= H_2(e^{jw})e^{-jwn_0}$$

$$\equiv e^{j(f(w)-wn_0)}$$

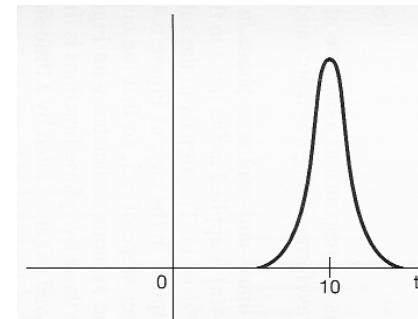
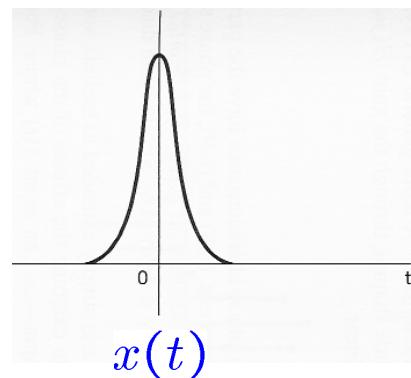
- Linear Phase:



$$H_1(jw) = e^{-jw\textcolor{red}{t}_0}$$

$$\Rightarrow \begin{cases} |H_1(jw)| = 1 \\ \arg H_1(jw) = -w\textcolor{red}{t}_0 \end{cases}$$

$$\Rightarrow y(t) = x(t - \textcolor{red}{t}_0)$$



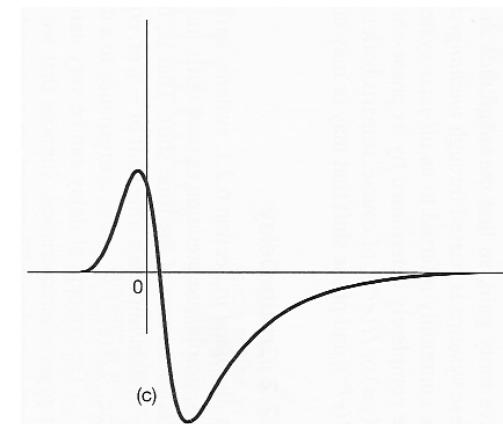
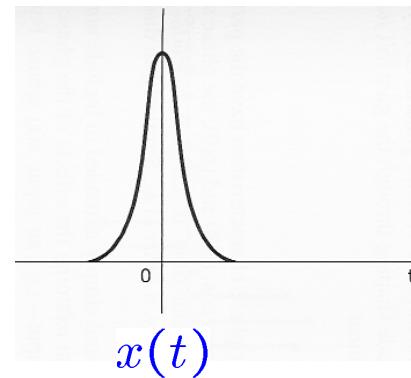
$$y(t) = x(t - 10)$$

$$\textcolor{red}{t}_0 = 10$$

- Linear Phase:



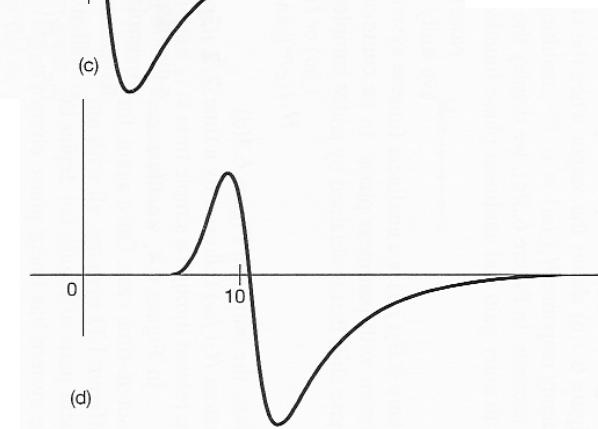
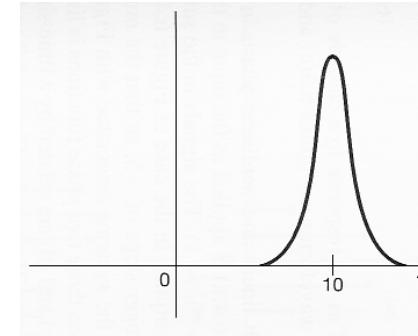
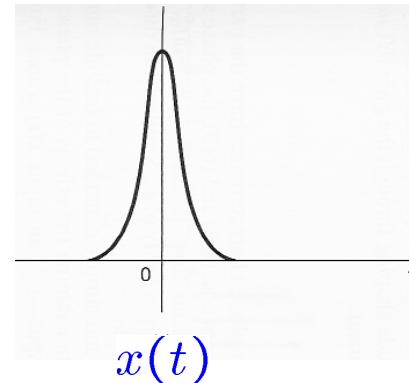
$$H_2(jw) = e^{j\phi(w)}$$



■ Linear Phase:



$$H_3(jw) = H_2(jw) \quad H_1(jw) = H_2(jw)e^{-jw t_0} = e^{j(f(w)-w t_0)}$$



- Group Delay & Phase:

- Linear Phase & Delay:

$$H_1(jw) = e^{-jw\color{red}t_0} \quad \Rightarrow \quad y(t) = x(t - \color{red}t_0) \quad \Rightarrow \text{delay} = \color{red}t_0$$

$$H_1(e^{jw}) = e^{-jw\color{red}n_0} \quad \Rightarrow \quad y[n] = x[n - \color{red}n_0] \quad \Rightarrow \text{delay} = \color{red}n_0$$

- Nonlinear Phase & Group Delay

$$H_2(jw) = e^{jf(w)} \quad \Rightarrow \quad \tau(w) = -\frac{d}{dw} \left\{ \arg H_2(jw) \right\}$$

■ Example 6.1:

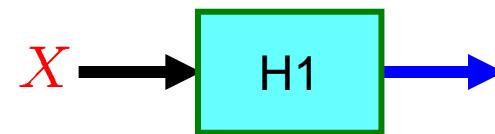
$$H(jw) = H_1(jw) \ H_2(jw) \ H_3(jw)$$

$$H_i(jw) = \frac{1 + (jw/w_i)^2 - 2j\zeta_i(w/w_i)}{1 + (jw/w_i)^2 + 2j\zeta_i(w/w_i)}$$

$$\Rightarrow \begin{cases} |H_i(jw)| = 1 \\ \angle H_i(jw) = -2 \arctan \left[\frac{2\zeta_i(w/w_i)}{1-(w/w_i)^2} \right] \end{cases}$$

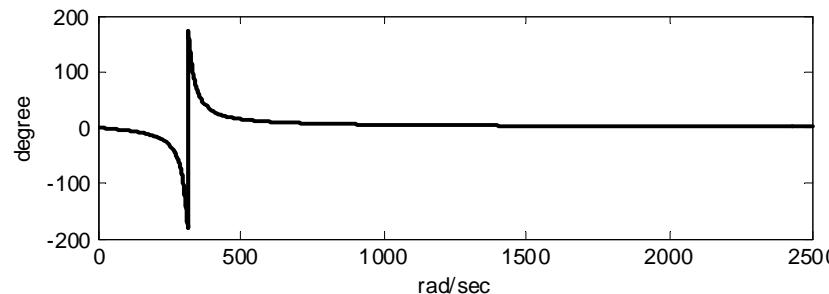
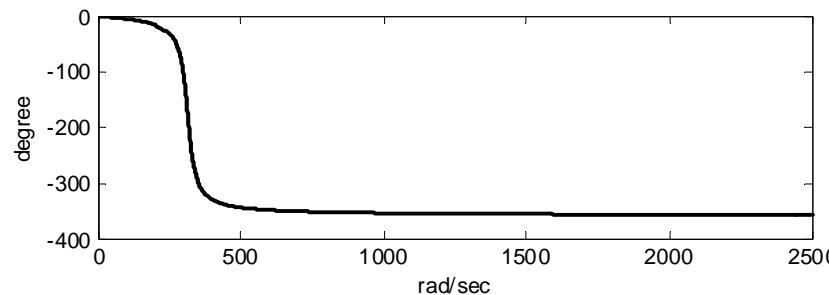
$$\Rightarrow \begin{cases} |H(jw)| = 1 \\ \angle H(jw) = \angle H_1(jw) + \angle H_2(jw) + \angle H_3(jw) \end{cases}$$

$$\Rightarrow \tau(w) = -\frac{d}{dw} \{\angle H(jw)\}$$



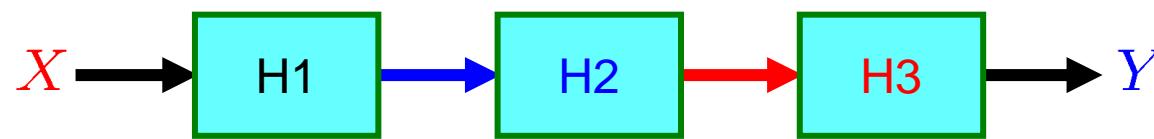
$$H_1(jw) = \frac{1 + (jw/w_1)^2 - 2j\zeta_1(w/w_1)}{1 + (jw/w_1)^2 + 2j\zeta_1(w/w_1)} \quad \left\{ \begin{array}{l} w_1 = 315 \text{ rad/sec} \\ \zeta_1 = 0.066 \\ f_1 \approx 50 \text{ Hz} \end{array} \right.$$

$$\Rightarrow \begin{cases} |H_1(jw)| = 1 \\ \angle H_1(jw) = -2 \arctan \left[\frac{2\zeta_1(w/w_1)}{1-(w/w_1)^2} \right] \end{cases}$$



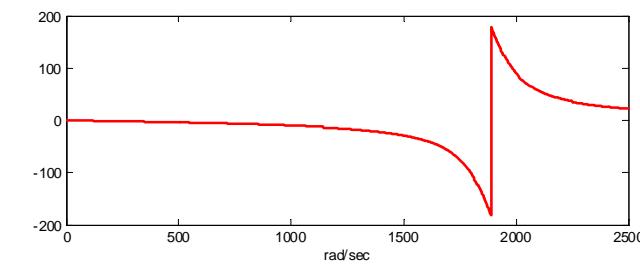
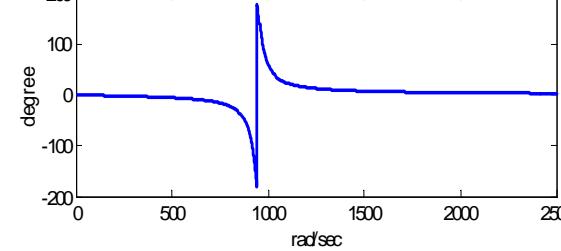
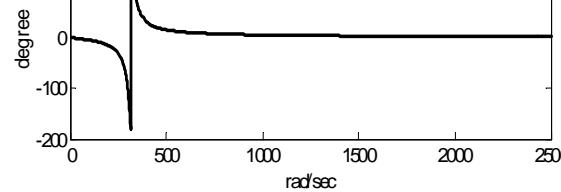
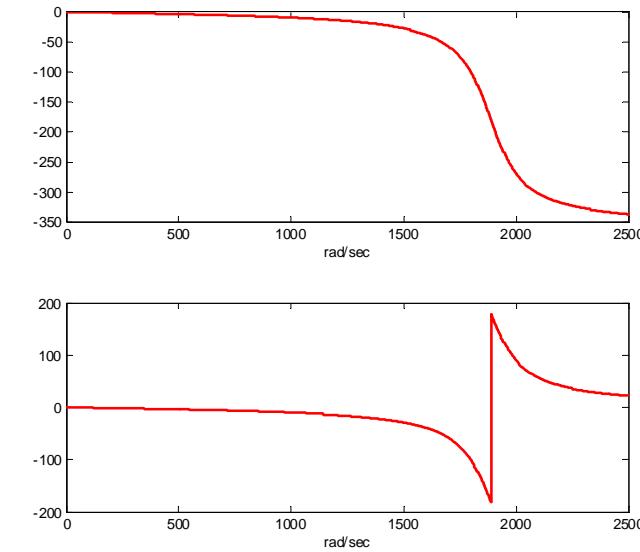
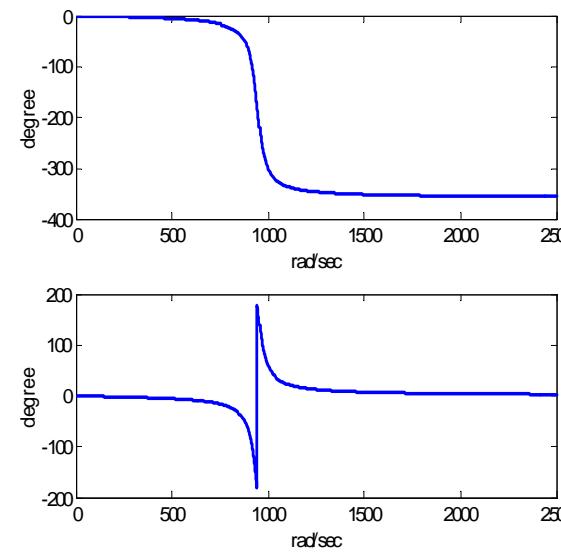
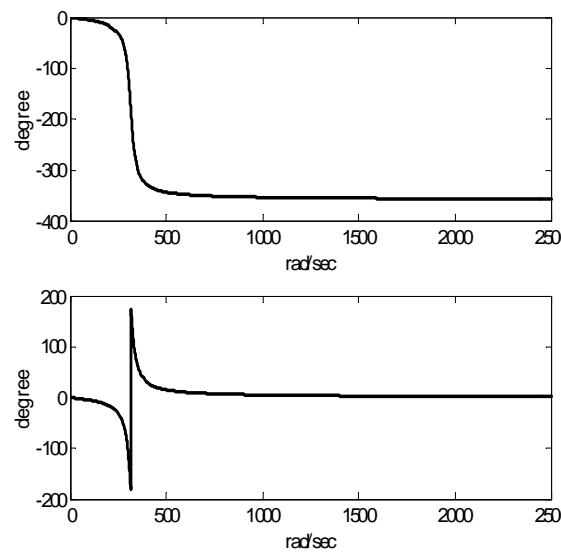
Magnitude-Phase Representation of Frequency Response of LTI Systems

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$$\left\{ \begin{array}{l} w_1 = 315 \text{ rad/sec} \\ w_2 = 943 \text{ rad/sec} \\ w_3 = 1888 \text{ rad/sec} \end{array} \right.$$

$$\left\{ \begin{array}{l} \zeta_1 = 0.066 \\ \zeta_2 = 0.033 \\ \zeta_3 = 0.058 \end{array} \right.$$



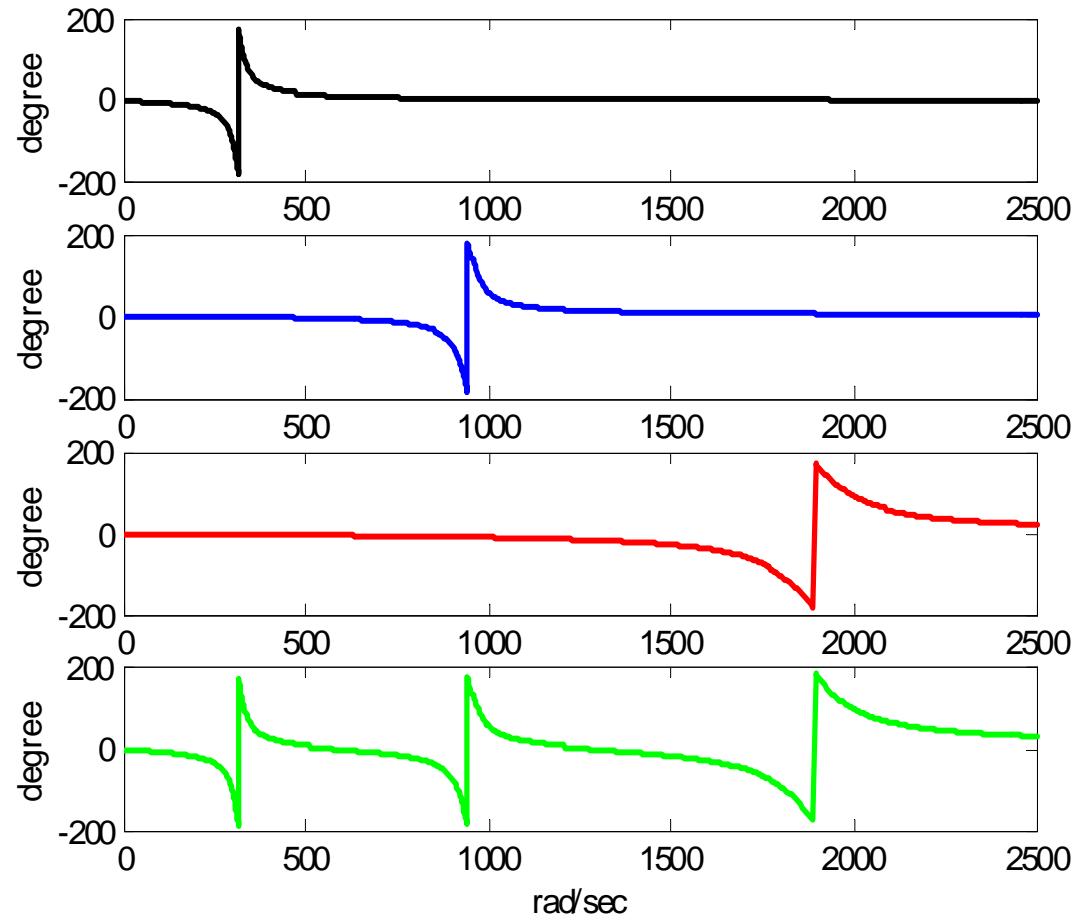
Magnitude-Phase Representation of Frequency Response of LTI Systems



$$\begin{cases} |H(jw)| = 1 \\ \arg H(jw) = \arg H_1(jw) + \arg H_2(jw) + \arg H_3(jw) \end{cases}$$

$$\begin{cases} w_1 = 315 \text{ rad/sec} \\ w_2 = 943 \text{ rad/sec} \\ w_3 = 1888 \text{ rad/sec} \end{cases}$$

$$\begin{cases} \zeta_1 = 0.066 \\ \zeta_2 = 0.033 \\ \zeta_3 = 0.058 \end{cases}$$



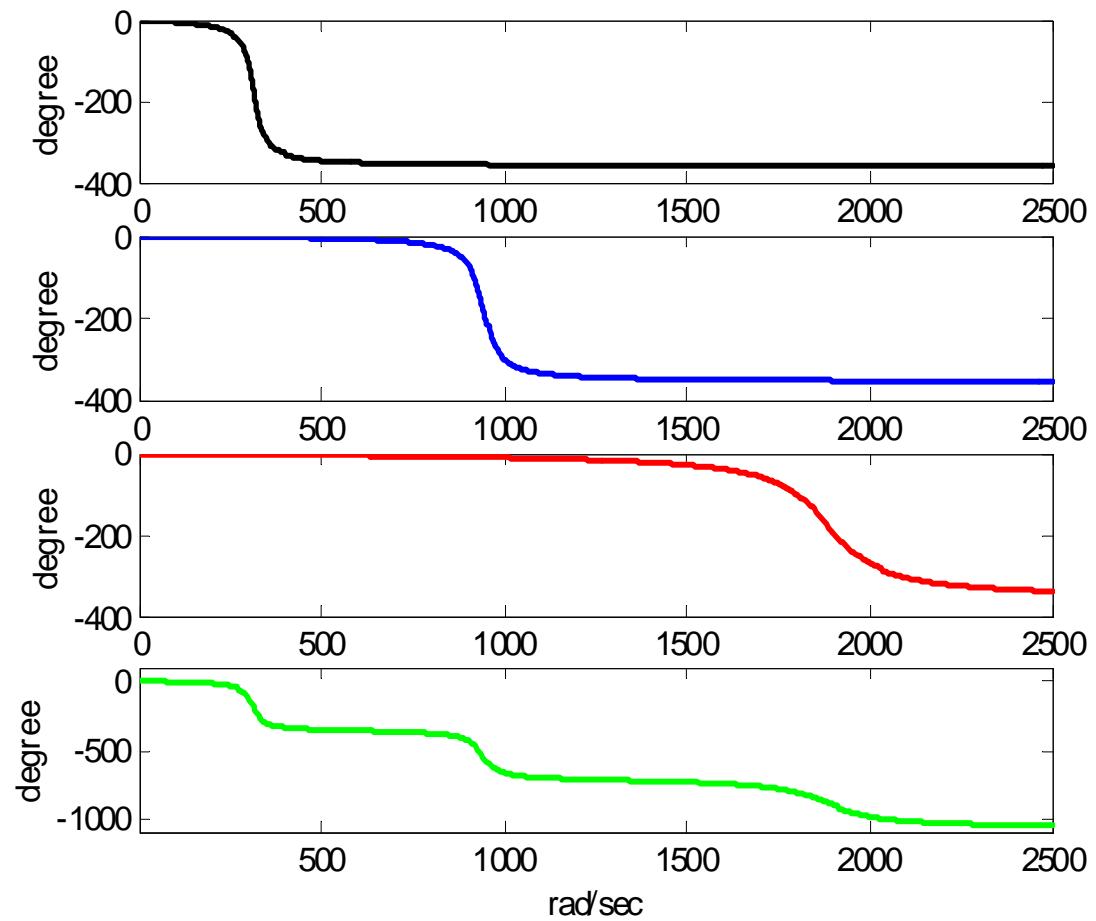
Magnitude-Phase Representation of Frequency Response of LTI Systems



$$\begin{cases} |H(jw)| = 1 \\ \arg H(jw) = \arg H_1(jw) + \arg H_2(jw) + \arg H_3(jw) \end{cases}$$

$$\begin{cases} w_1 = 315 \text{ rad/sec} \\ w_2 = 943 \text{ rad/sec} \\ w_3 = 1888 \text{ rad/sec} \end{cases}$$

$$\begin{cases} \zeta_1 = 0.066 \\ \zeta_2 = 0.033 \\ \zeta_3 = 0.058 \end{cases}$$



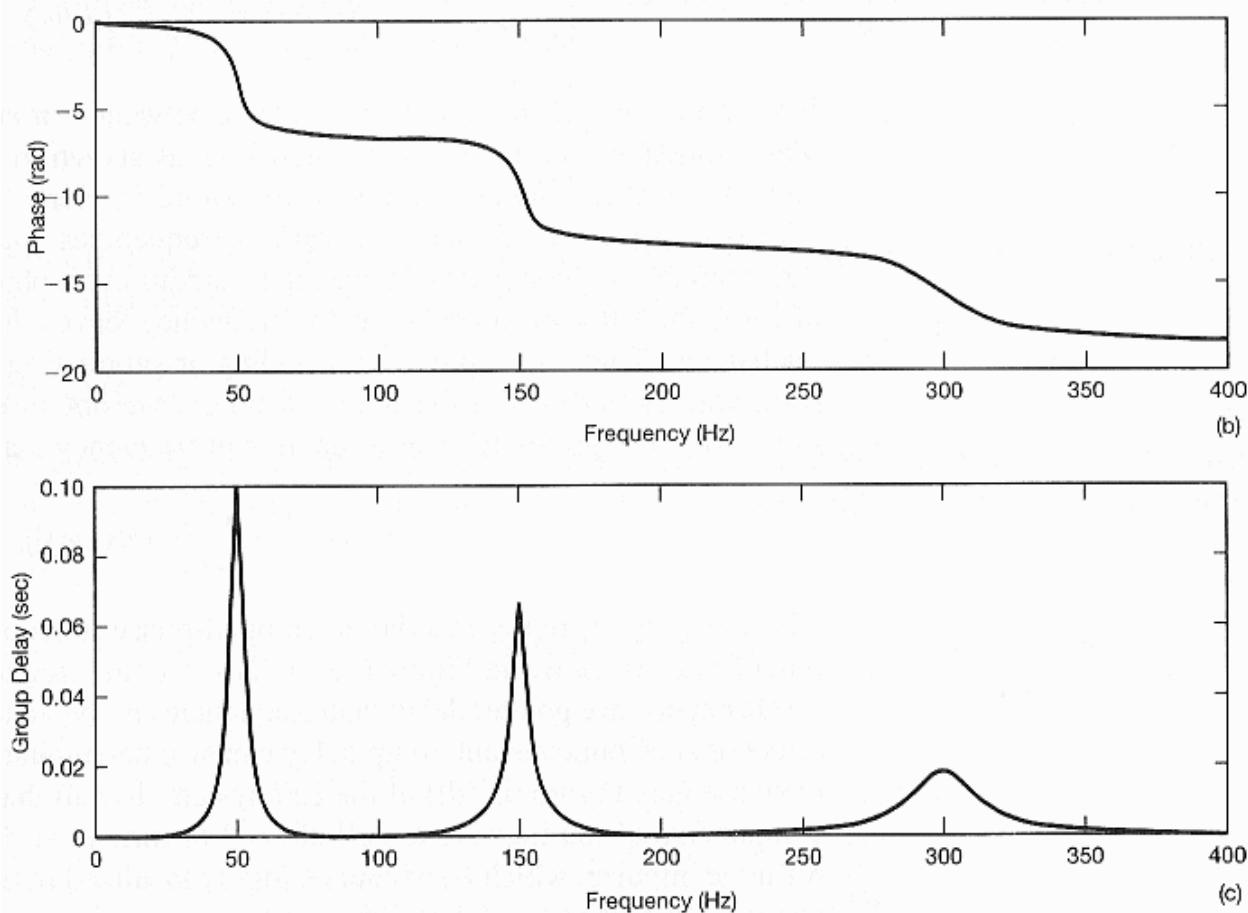
$$\tau(w) = - \frac{d}{dw} \left\{ \arg H(jw) \right\}$$

$$\begin{cases} w_1 = 315 \text{ rad/sec} \\ w_2 = 943 \text{ rad/sec} \\ w_3 = 1888 \text{ rad/sec} \end{cases}$$

$$\begin{cases} \zeta_1 = 0.066 \\ \zeta_2 = 0.033 \\ \zeta_3 = 0.058 \end{cases}$$

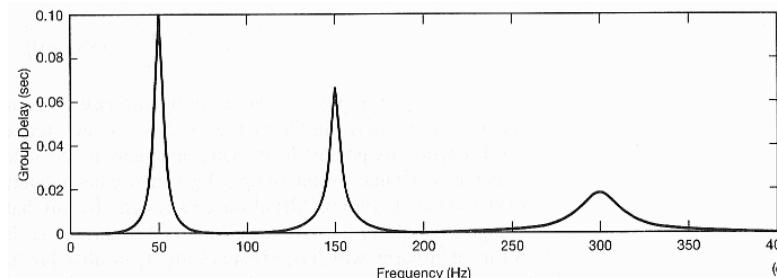
$$w_i = 2\pi f_i$$

$$\begin{cases} f_1 \approx 50 \text{ Hz} \\ f_2 \approx 150 \text{ Hz} \\ f_3 \approx 300 \text{ Hz} \end{cases}$$



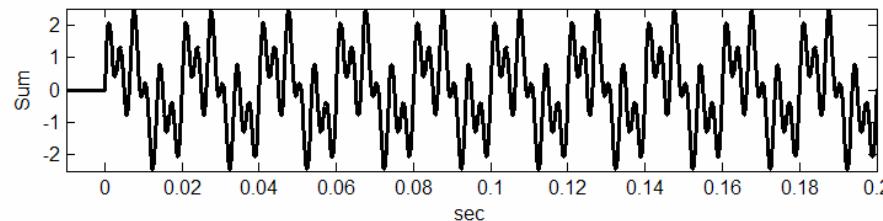
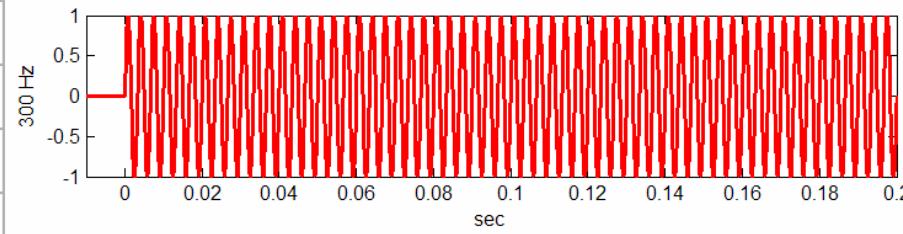
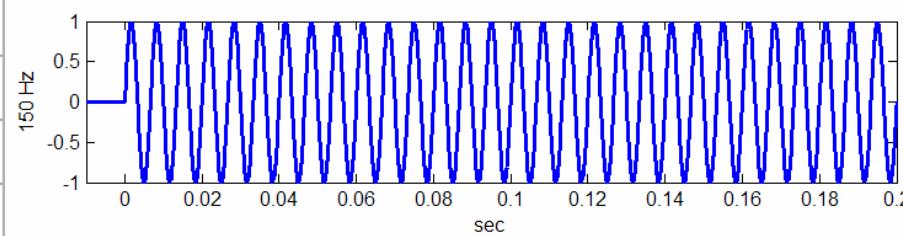
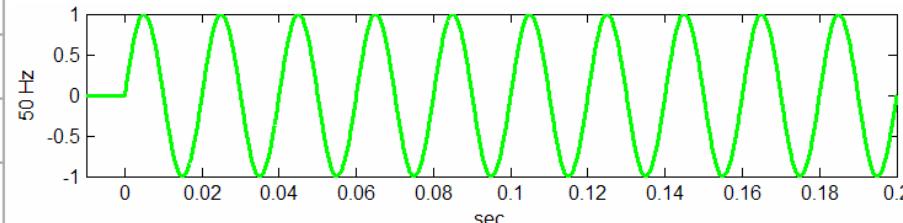
Magnitude-Phase Representation of Frequency Response of LTI Systems

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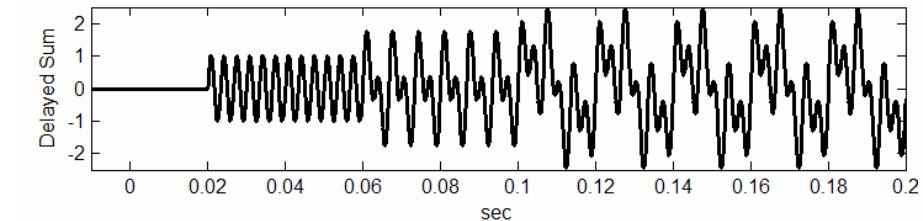
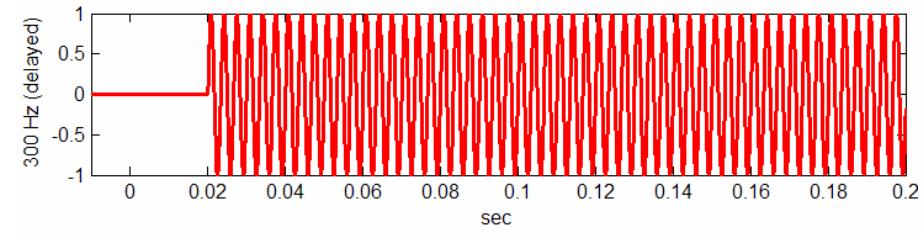
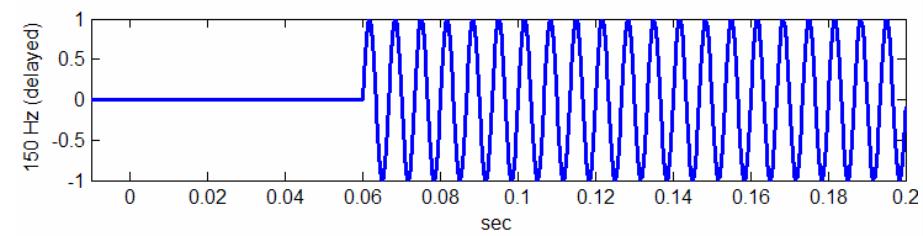
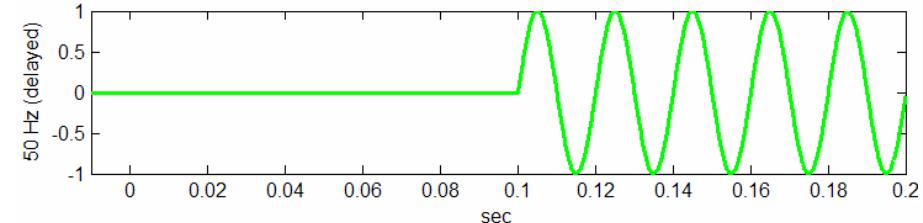


(c)

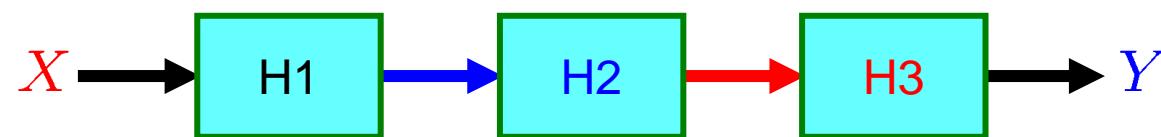
$$x(t) = x_1(t) + x_2(t) + x_3(t)$$



$$y(t) = y_1(t) + y_2(t) + y_3(t)$$



Magnitude-Phase Representation of Frequency Response of LTI Systems



$$x(t) = \delta(t)$$

$$X(jw) = 1, \forall w$$

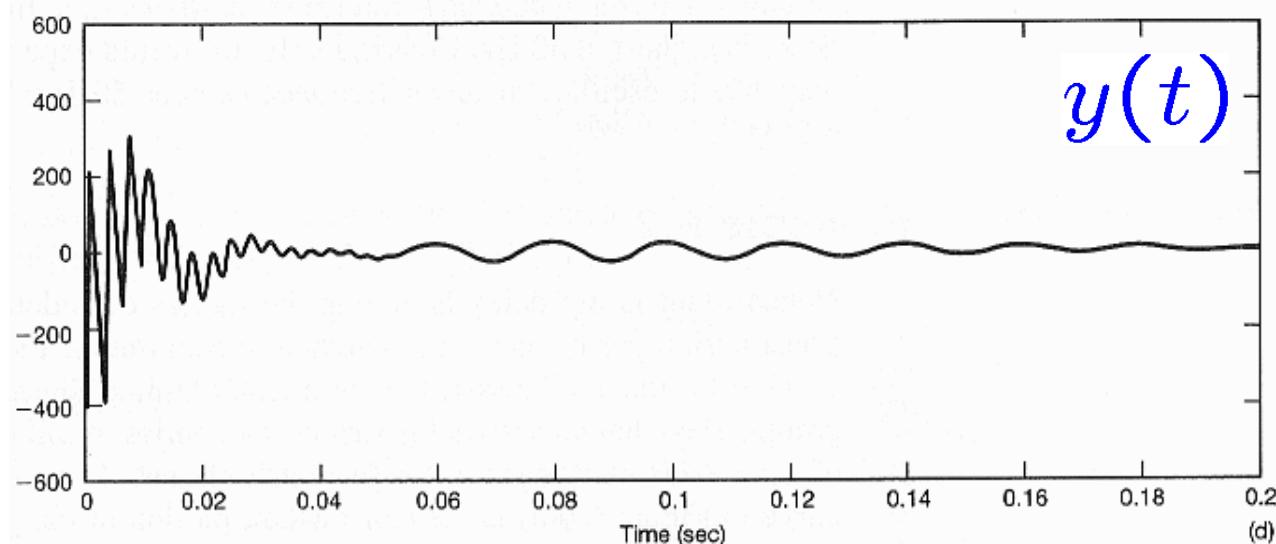
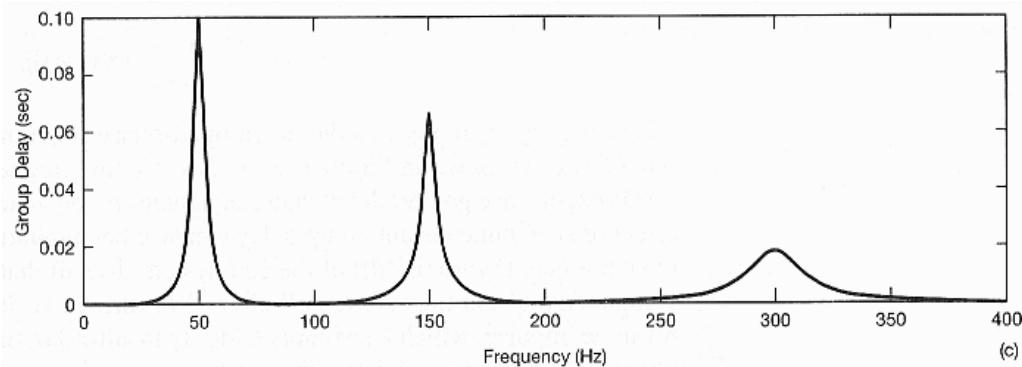
$$\begin{cases} w_1 = 315 \text{ rad/sec} \\ w_2 = 943 \text{ rad/sec} \\ w_3 = 1888 \text{ rad/sec} \end{cases}$$

$$\begin{cases} \zeta_1 = 0.066 \\ \zeta_2 = 0.033 \\ \zeta_3 = 0.058 \end{cases}$$

$$w_i = 2\pi f_i$$

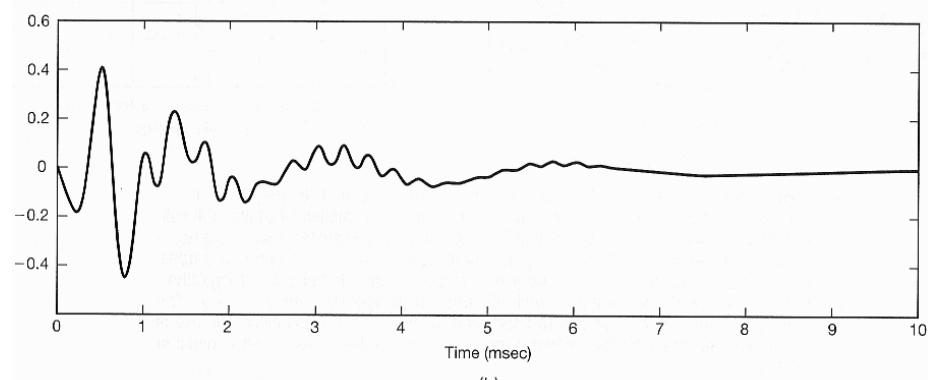
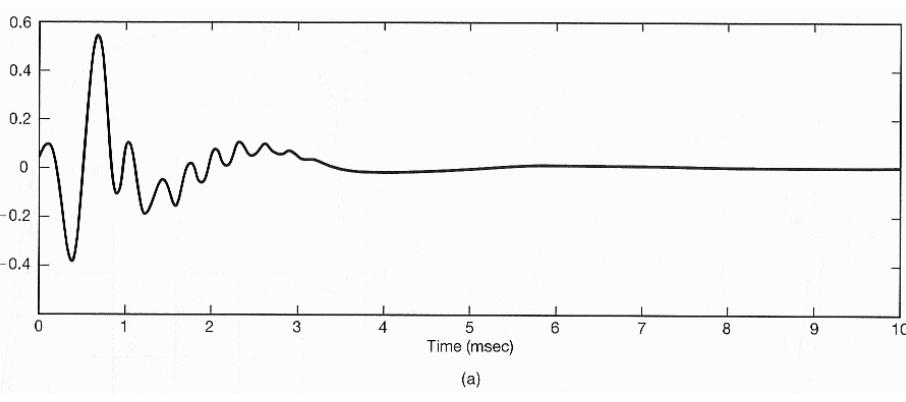
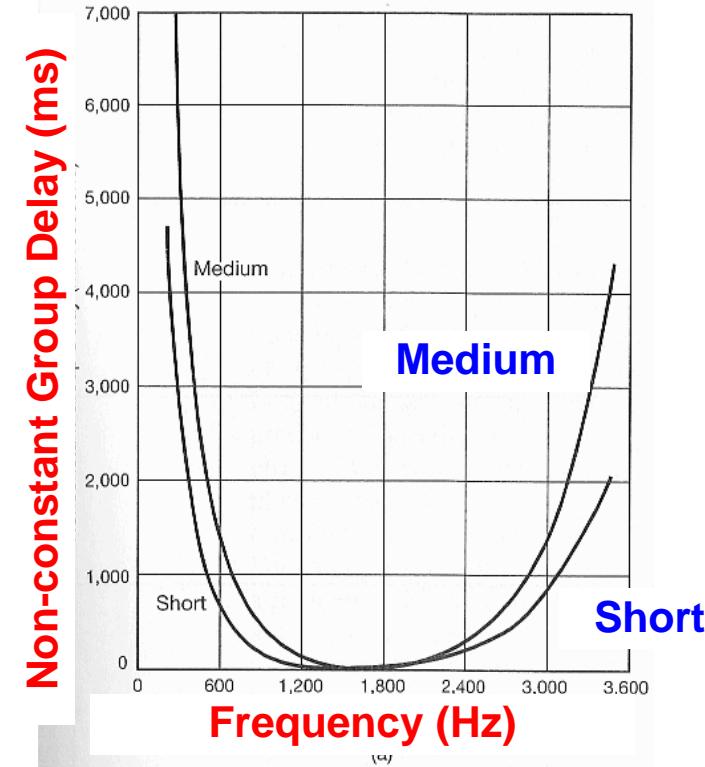
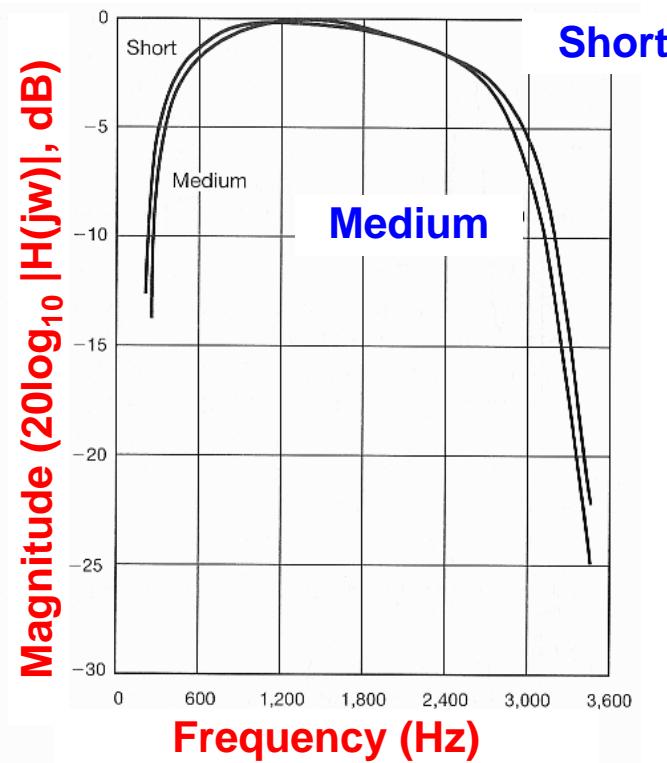
$$\begin{cases} f_1 \approx 50 \text{ Hz} \\ f_2 \approx 150 \text{ Hz} \\ f_3 \approx 300 \text{ Hz} \end{cases}$$

$$\begin{cases} |H(jw)| = 1 \\ \arg H(jw) = \arg H_1(jw) + \arg H_2(jw) + \arg H_3(jw) \end{cases}$$



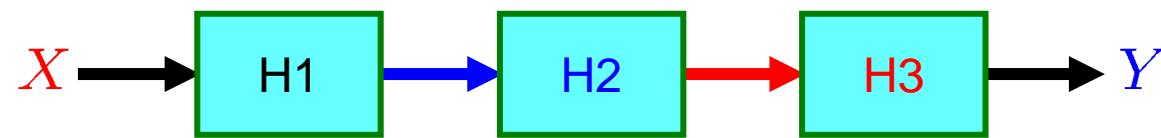
■ Example 6.2:

Analog Transmission Performance on the Switched Telecommunication Networks (AT&T/Bell)



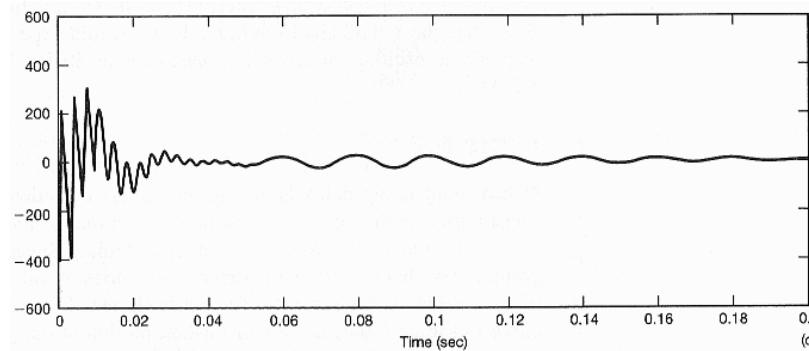
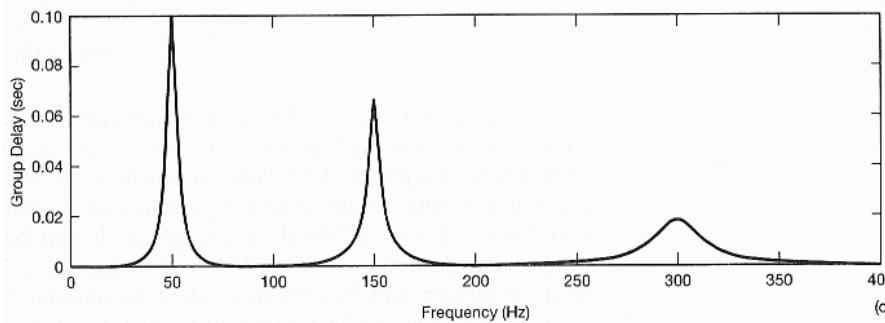
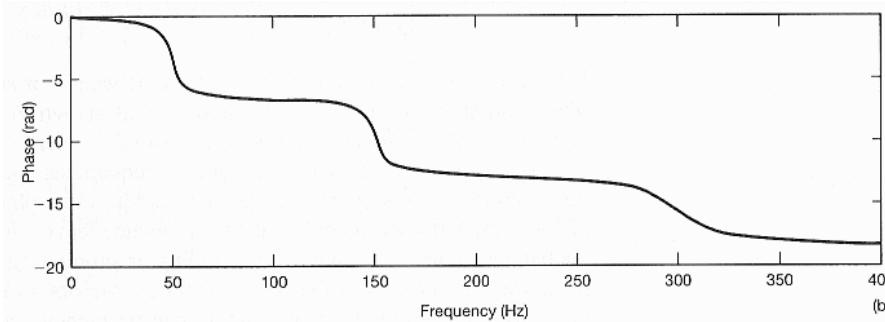
Phase Distortion and Group Delay

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$$\tau(w) = -\frac{d}{dw} \left\{ \Im H(jw) \right\}$$

$$x(t) = \delta(t)$$



- The Magnitude-Phase Representation of the Fourier Transform
- The Magnitude-Phase Representation of Frequency Response of LTI Systems
- Time-Domain Properties of Ideal Frequency-Selective Filters (p.439)
- Time-Domain and Frequency-Domain Aspects of Non-ideal Filters
- 1st-Order & 2nd-Order Continuous-Time Systems
- 1st-Order & 2nd-Order Discrete-Time Systems
- Time- & Frequency-Domain Analysis of Systems

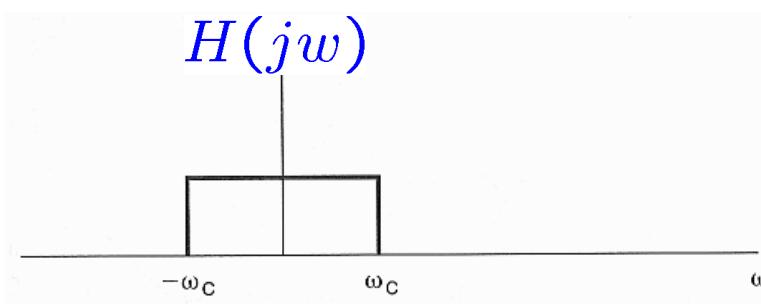
■ Ideal Lowpass Filters:

$$H(jw) = \begin{cases} 1, & |w| \leq w_c \\ 0, & |w| > w_c \end{cases}$$

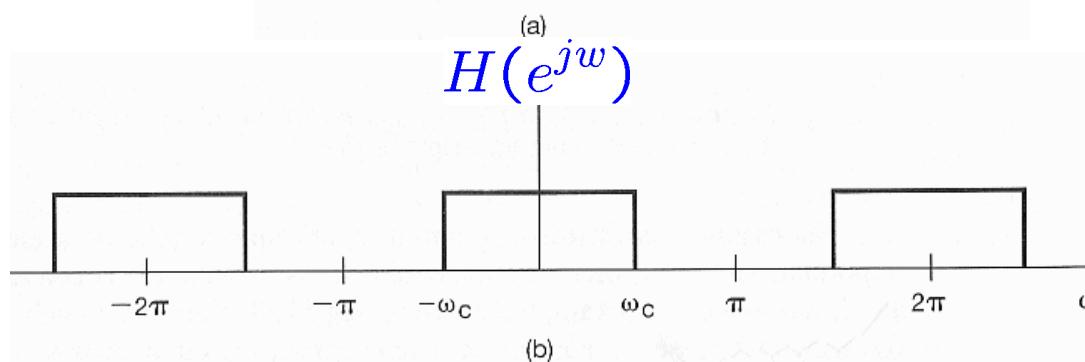
–unit gain

$$H(e^{jw}) = \begin{cases} 1, & |w| \leq w_c \\ 0, & w_c < |w| \leq \pi \end{cases}$$

–zero phase distortion

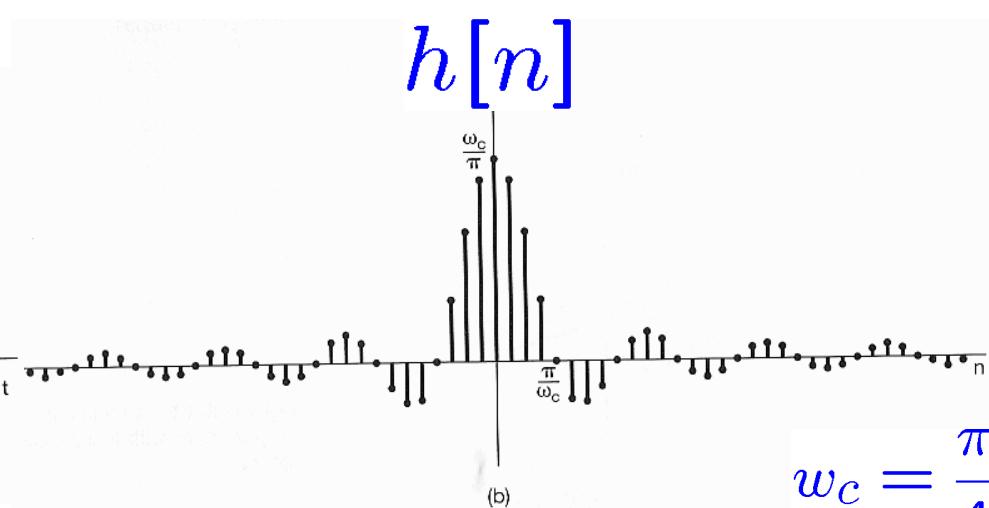
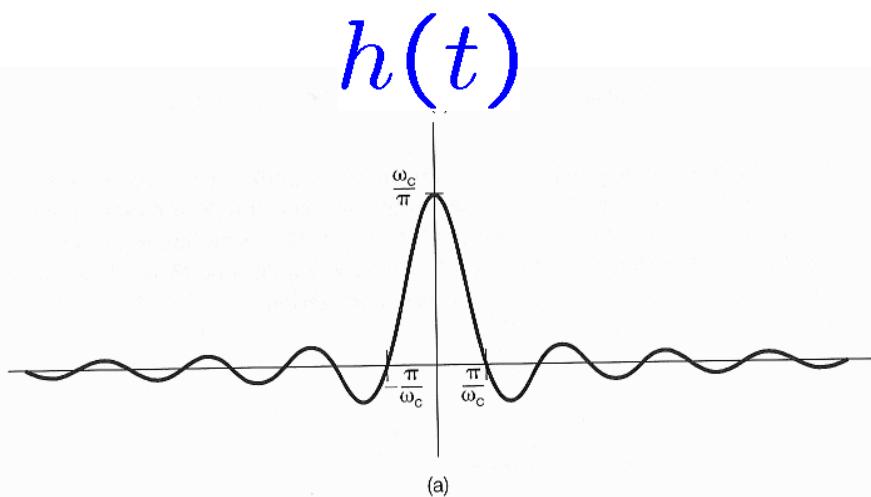


$\check{\chi} H(jw) \quad \check{\chi} H(e^{jw})$



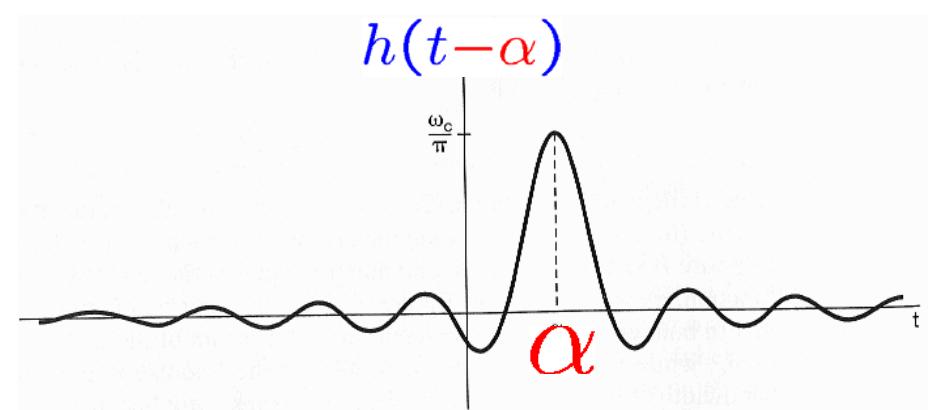
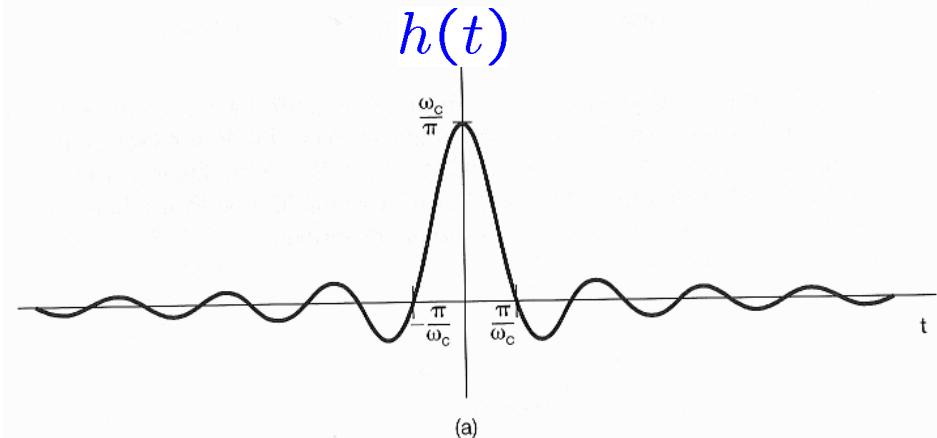
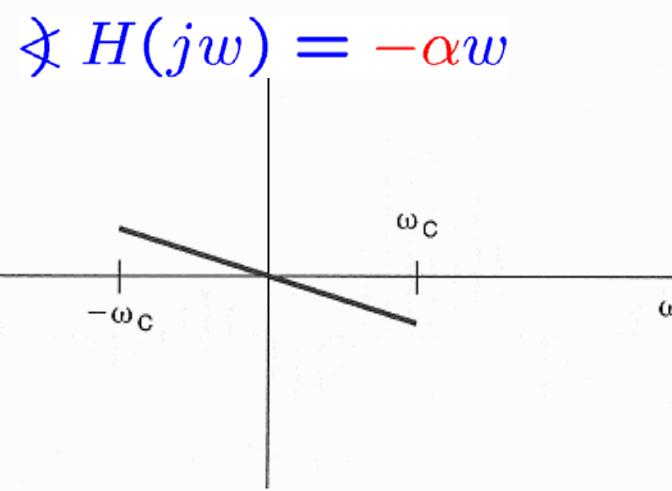
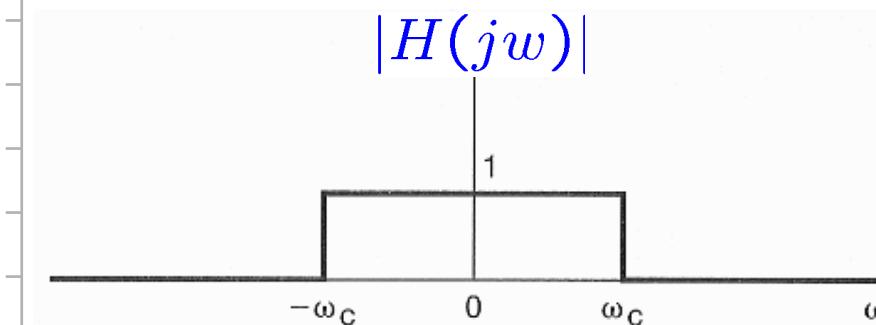
■ Ideal Lowpass Filters:

$$H(jw) = \begin{cases} 1, & |w| \leq w_c \\ 0, & |w| > w_c \end{cases} \Rightarrow \begin{cases} h(t) = \frac{\sin w_c t}{\pi t} \\ h[n] = \frac{\sin w_c n}{\pi n} \end{cases}$$
$$H(e^{jw}) = \begin{cases} 1, & |w| \leq w_c \\ 0, & w_c < |w| \leq \pi \end{cases}$$



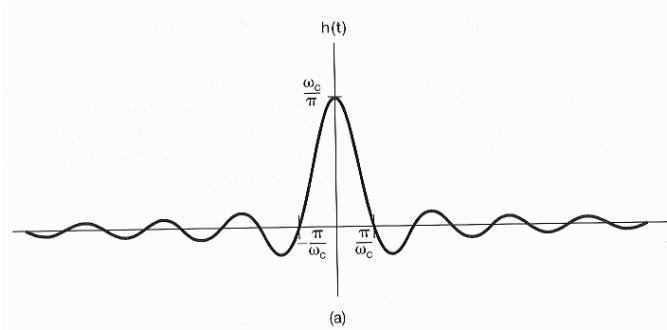
$$w_c = \frac{\pi}{4}$$

■ Ideal Lowpass Filters with Linear Phase:

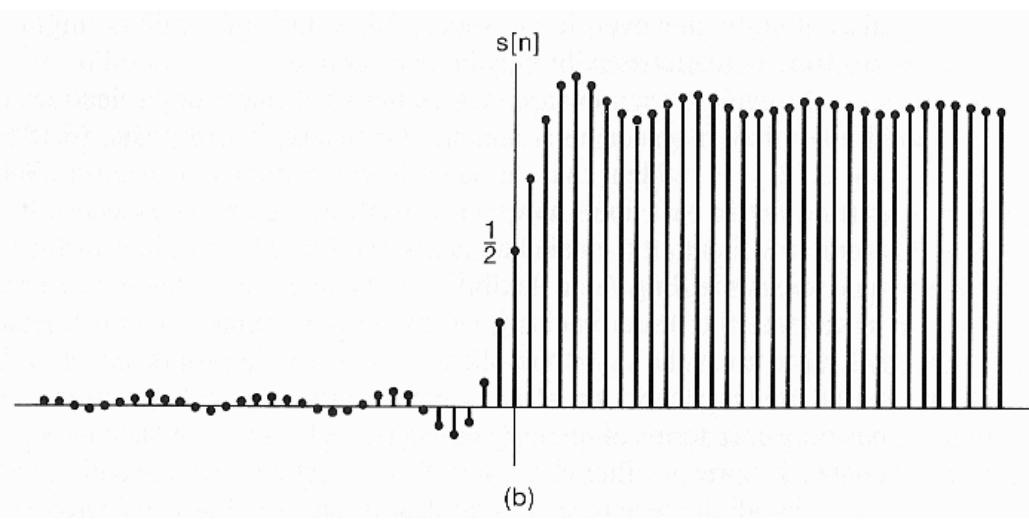
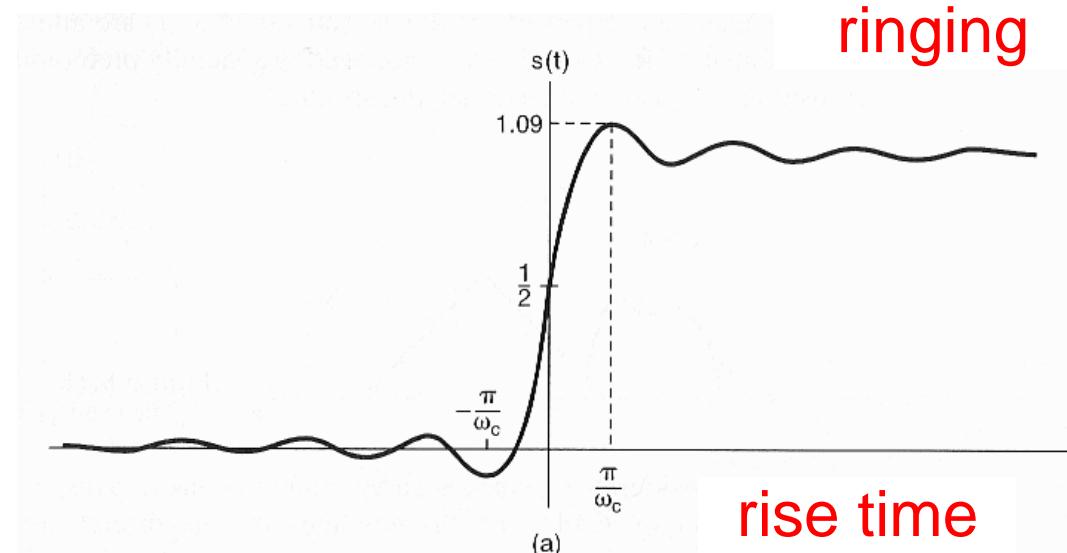
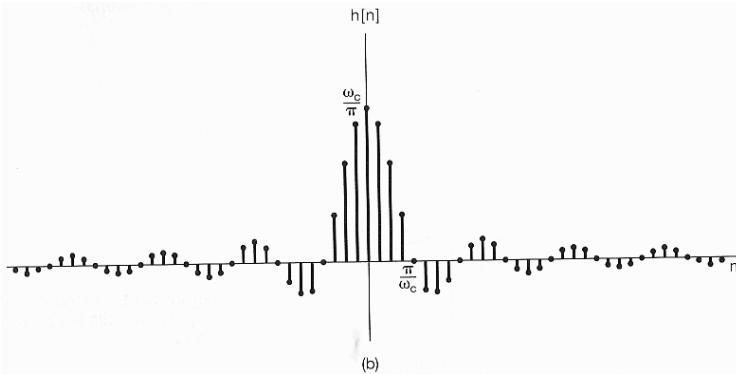


■ Step Response of Ideal Lowpass Filters:

$$s(t) = \int_{-\infty}^t h(\tau) d\tau$$

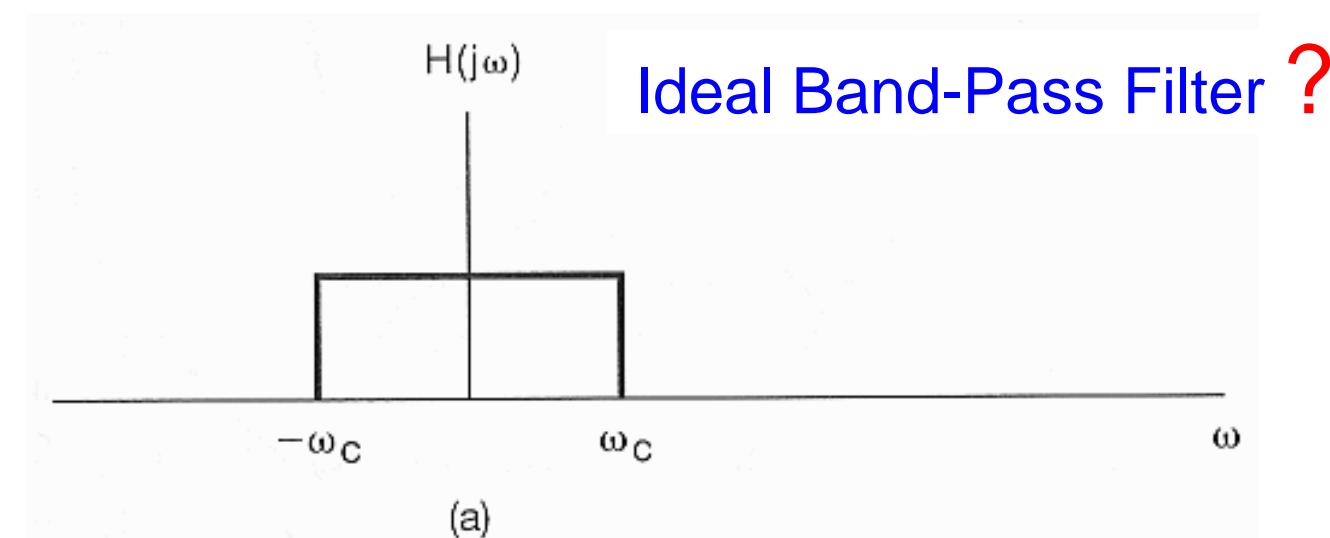
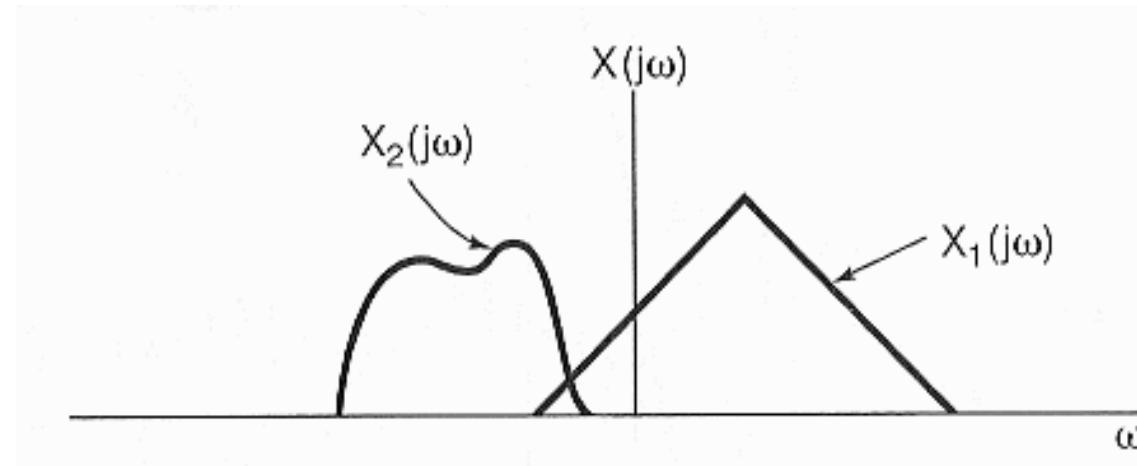


$$s[n] = \sum_{m=-\infty}^n h[m]$$

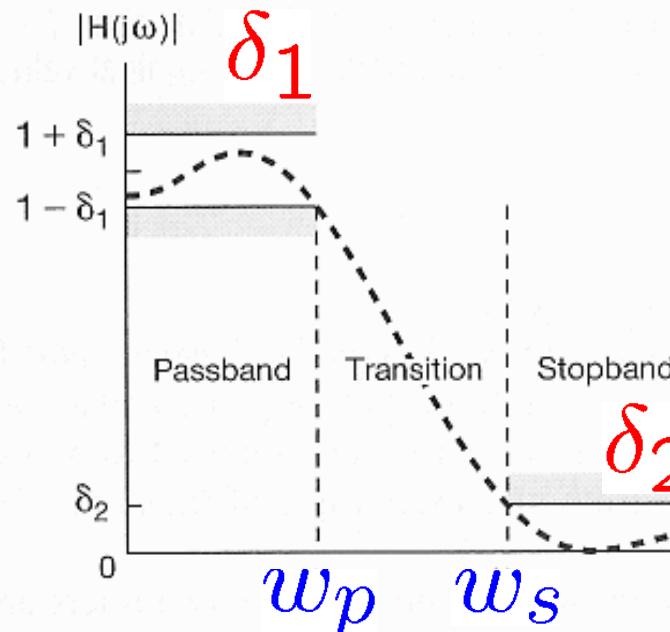


- The Magnitude-Phase Representation of the Fourier Transform
- The Magnitude-Phase Representation of Frequency Response of LTI Systems
- Time-Domain Properties of Ideal Frequency-Selective Filters (p.444)
- Time-Domain and Frequency-Domain Aspects of Non-ideal Filters
- 1st-Order & 2nd-Order Continuous-Time Systems
- 1st-Order & 2nd-Order Discrete-Time Systems
- Time- & Frequency-Domain Analysis of Systems

- Overlapping Spectra:



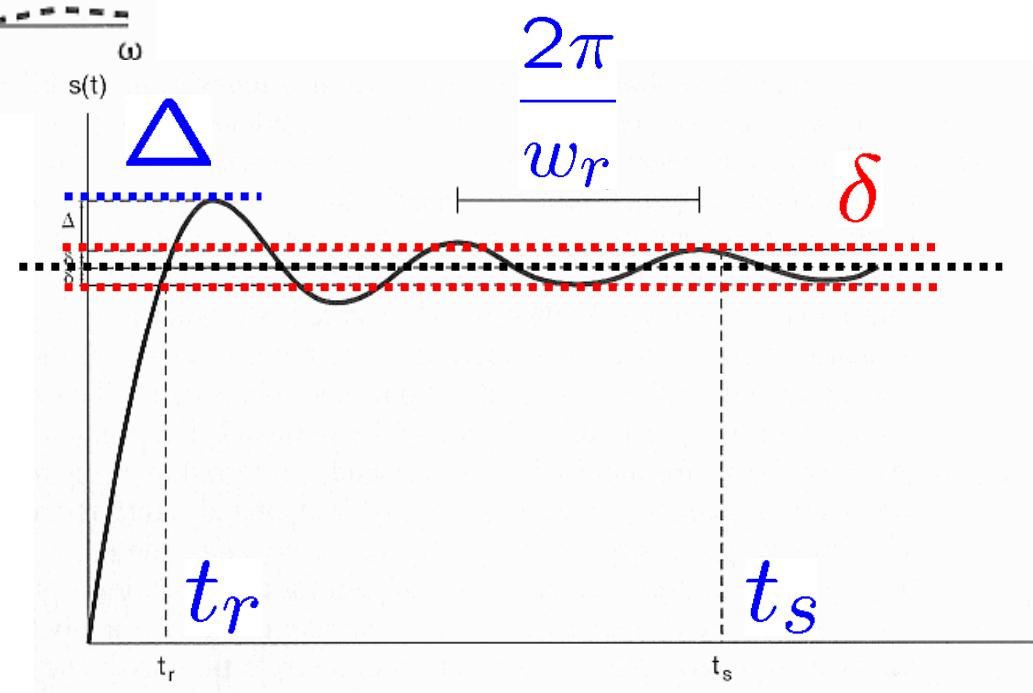
■ Desired Filter Characteristics:



δ_1 :	allowable passband ripple
δ_2 :	allowable stopband ripple
w_p :	passband edge
w_s :	stopband edge
$w_s - w_p$:	transition band



Δ :	overshoot
δ :	steady-state error
w_r :	ringing frequency
t_r :	rise time
t_s :	settling time



■ Example 6.3: Three Frequently Used Filters:

- Butterworth, Chebyshev, Elliptic filters

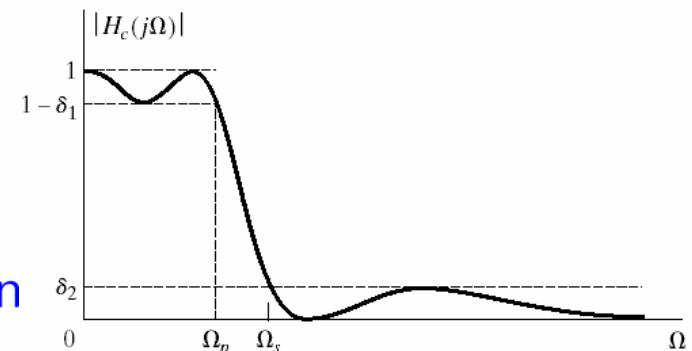
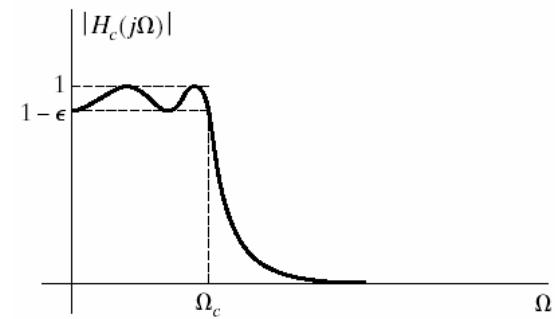
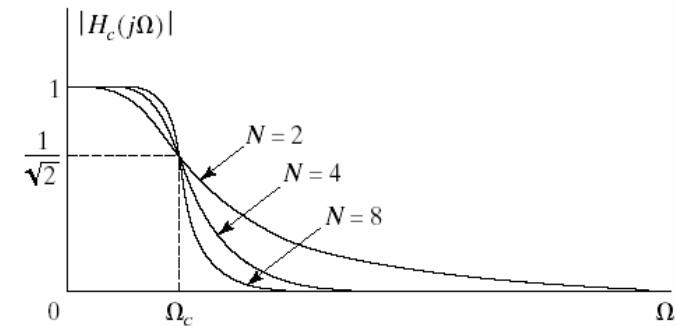
$$|H_c(j\Omega)|^2 = \frac{1}{1 + (\frac{j\Omega}{j\Omega_c})^{2N}}$$

$$|H_c(j\Omega)|^2 = \frac{1}{1 + \epsilon^2 V_N^2(\frac{\Omega}{\Omega_c})}$$

$$V_N(x) = \cos(N \cos^{-1} x)$$

$$|H_c(j\Omega)|^2 = \frac{1}{1 + \epsilon^2 U_N^2(\Omega)}$$

$U_N(x)$: Jacobian elliptic function

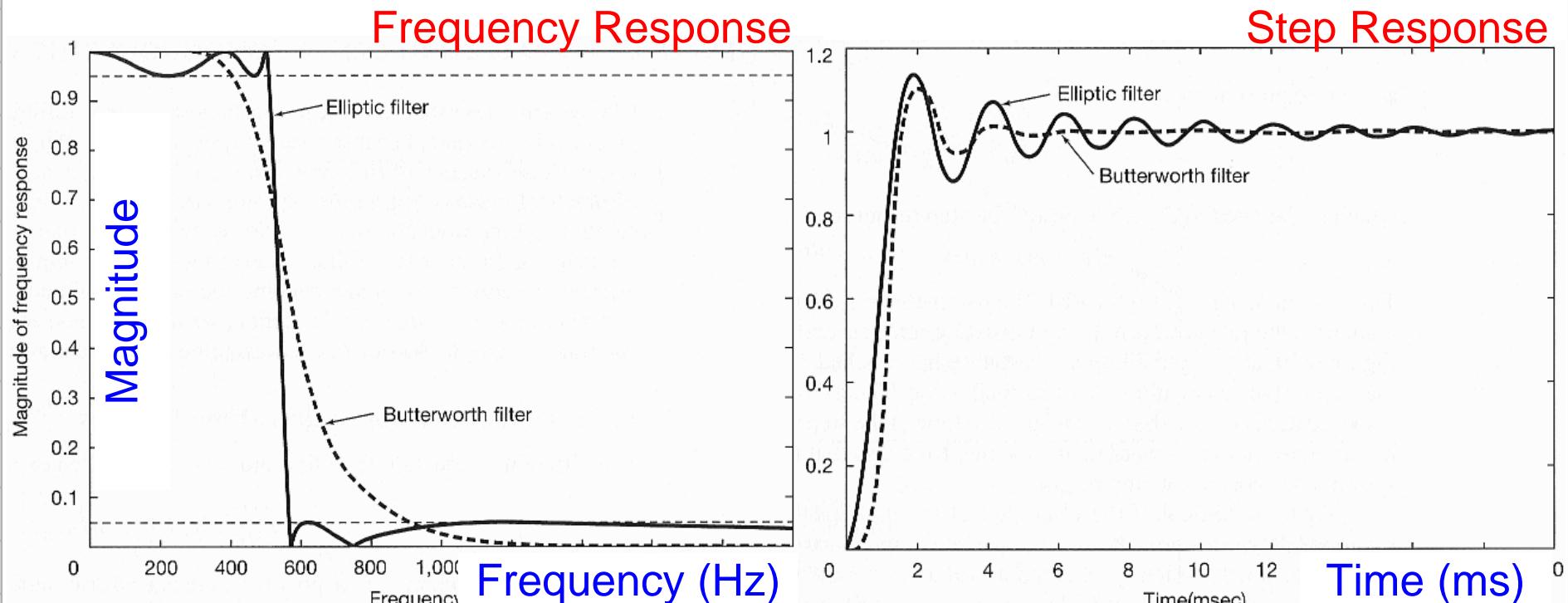


■ Example 6.3: Two Frequently Used Filters:

- Butterworth filter

- Fifth-order rational frequency response
- Cutoff frequency = 500 Hz

- Elliptic filter



- The Magnitude-Phase Representation of the Fourier Transform
- The Magnitude-Phase Representation of Frequency Response of LTI Systems
- Time-Domain Properties of Ideal Frequency-Selective Filters
- Time-Domain and Frequency-Domain Aspects of Non-ideal Filters
- 1st-Order & 2nd-Order Continuous-Time Systems
- 1st-Order & 2nd-Order Discrete-Time Systems
- Time- & Frequency-Domain Analysis of Systems

■ DT Non-recursive Filters:

- Recursive or infinite impulse response (IIR) filters

> Impossible to design a causal, recursive filter

with exactly linear phase (related to time delay)

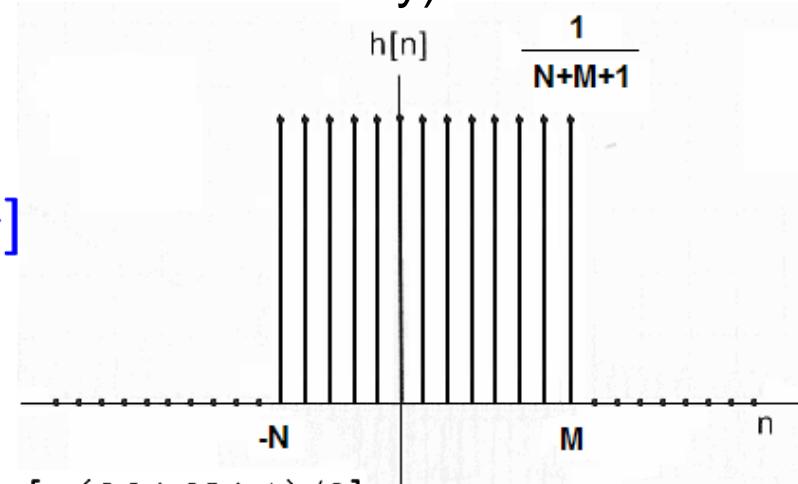
$$y[n] - a y[n-1] = x[n] \quad |a| < 1$$

$$\Rightarrow H(e^{jw}) = \frac{1}{1 - ae^{-jw}}$$

- Non-recursive or finite impulse response (FIR) filters

> Can have exactly linear phase (related to time delay)

$$y[n] = \frac{1}{N+M+1} \sum_{k=-N}^M x[n-k]$$



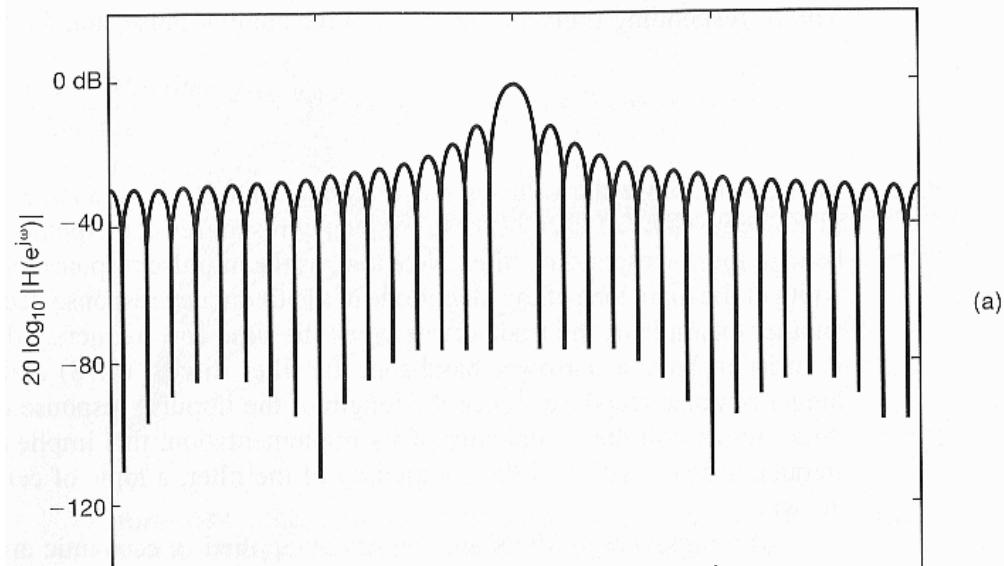
$$\Rightarrow H(e^{jw}) = \frac{1}{N+M+1} e^{jw[(N-M)/2]} \frac{\sin[w(M+N+1)/2]}{\sin(w/2)}$$

■ Log-Magnitude Plots:

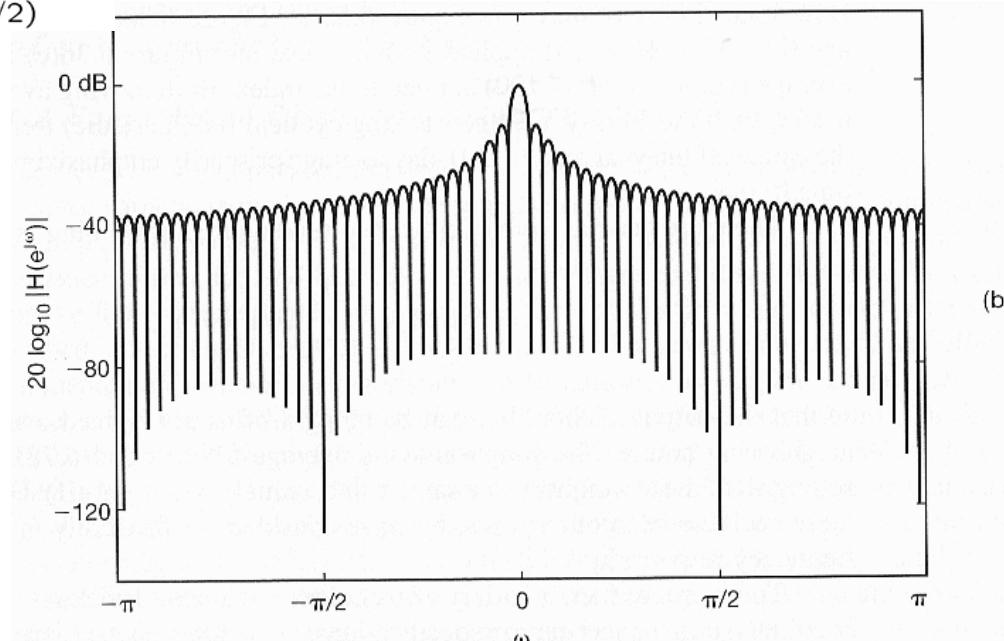
$$N + M + 1 = 33$$

$$H(e^{jw}) = \frac{1}{N + M + 1} e^{jw[(N-M)/2]} \frac{\sin[w(M+N+1)/2]}{\sin(w/2)}$$

$$N + M + 1 = 65$$

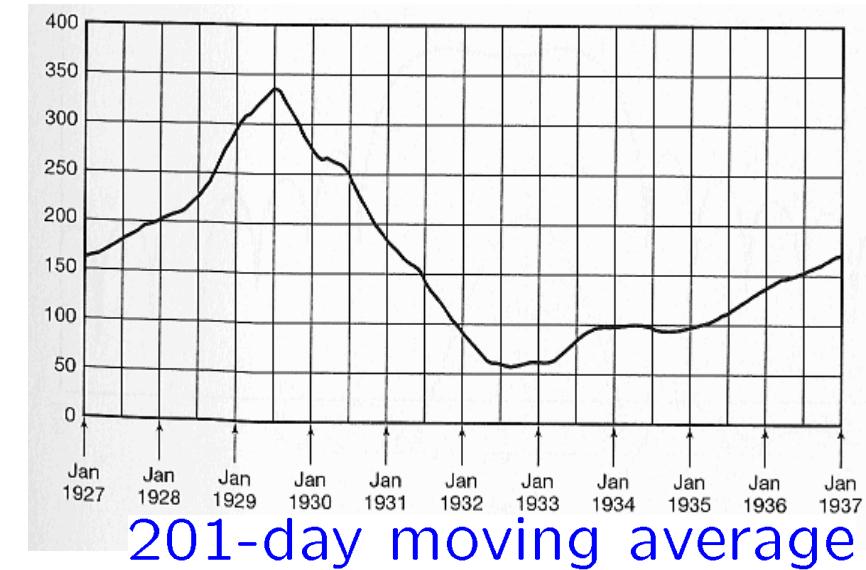
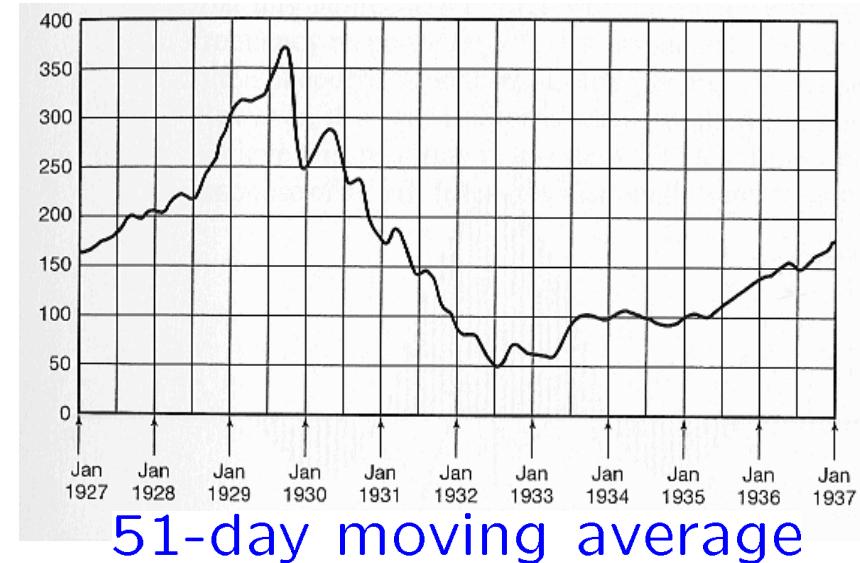
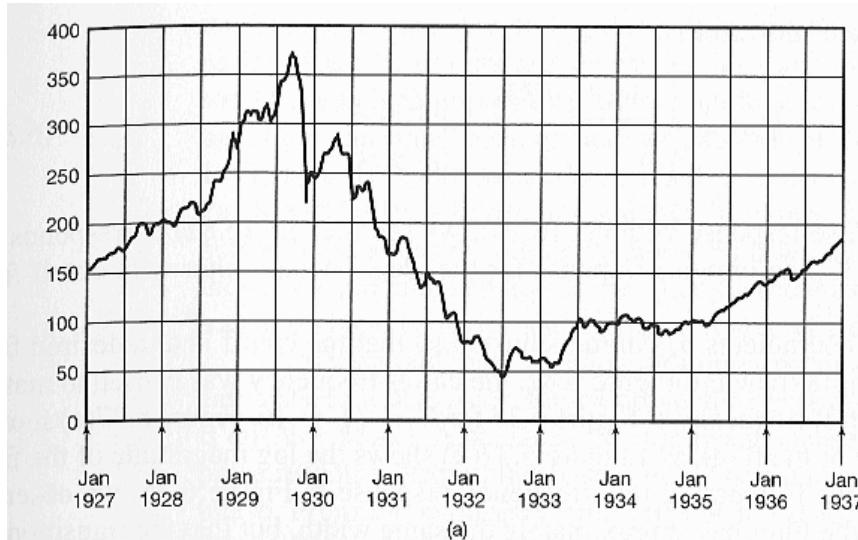


(a)



(b)

- Lowpass Filtering
on Dow Jones Weekly Stock Market Index:



■ General Form of DT Non-recursive Filters:

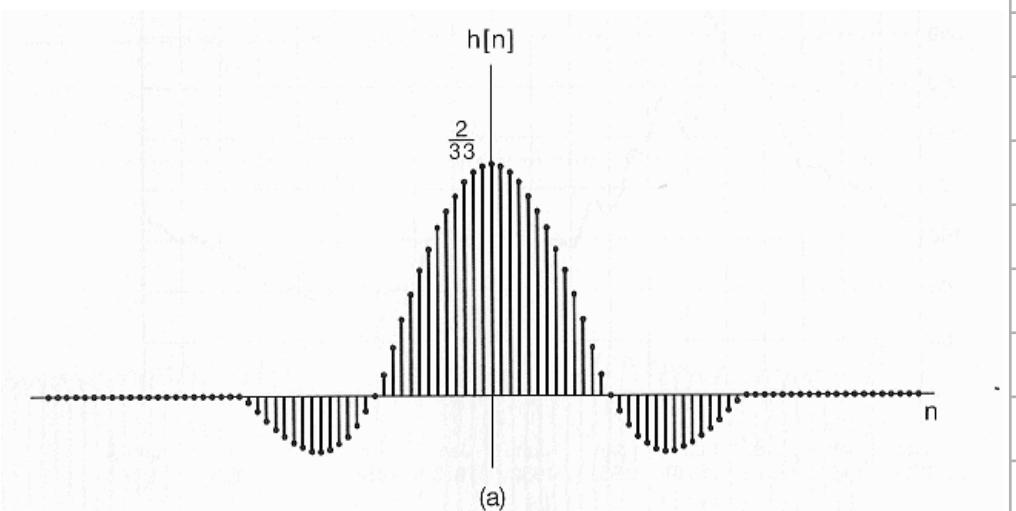
$$y[n] = \sum_{k=-N}^M b_k x[n - k]$$

$$y[n] = \sum_{k=-N}^M \frac{1}{N+M+1} x[n - k]$$

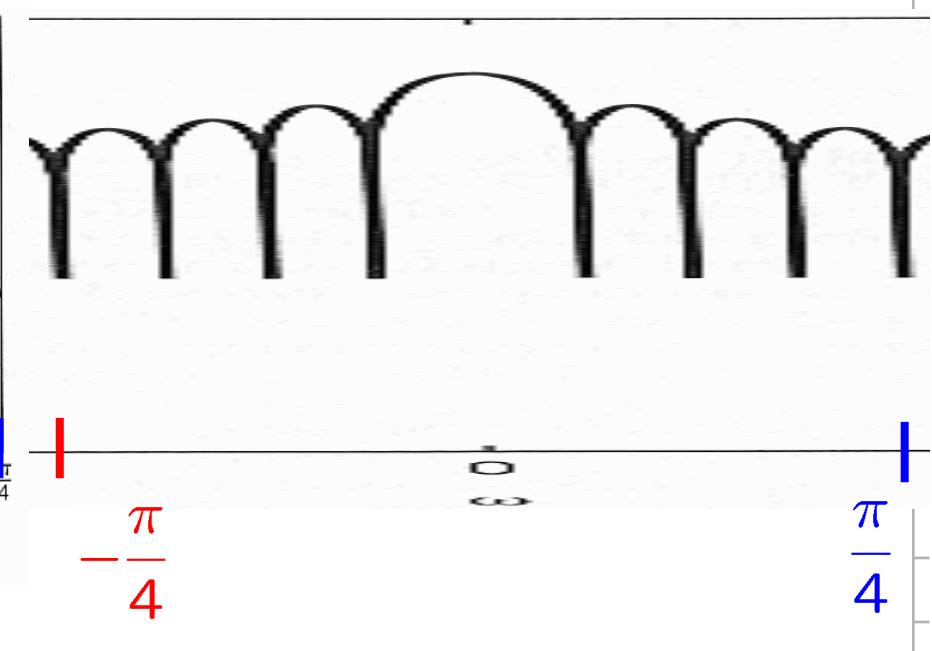
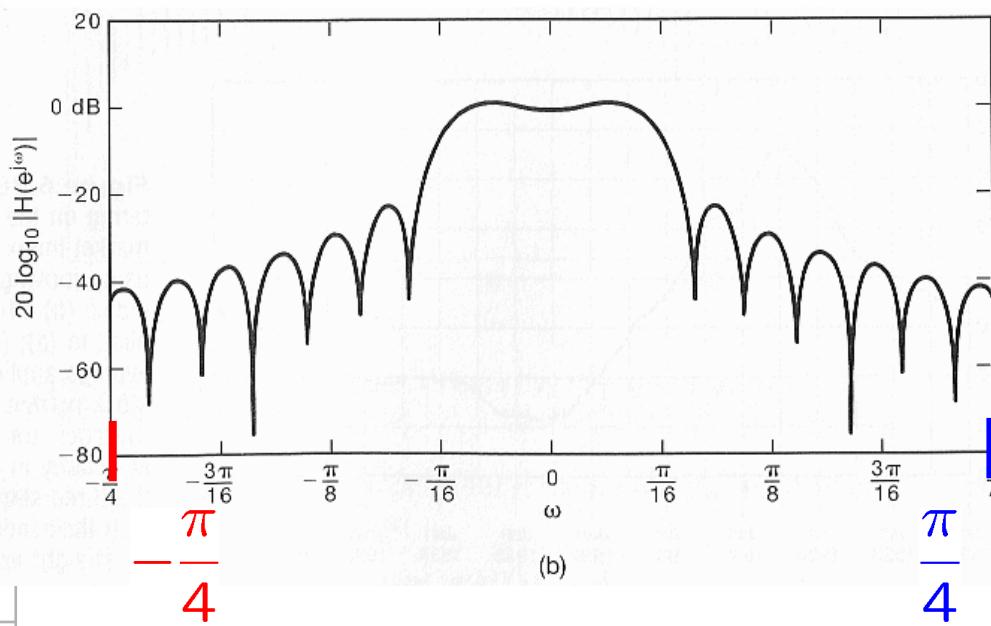
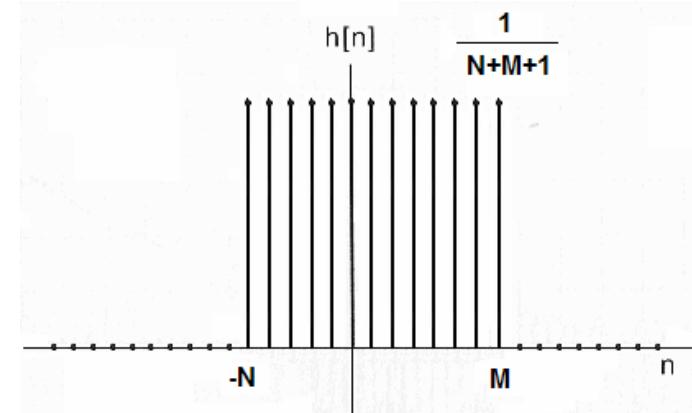
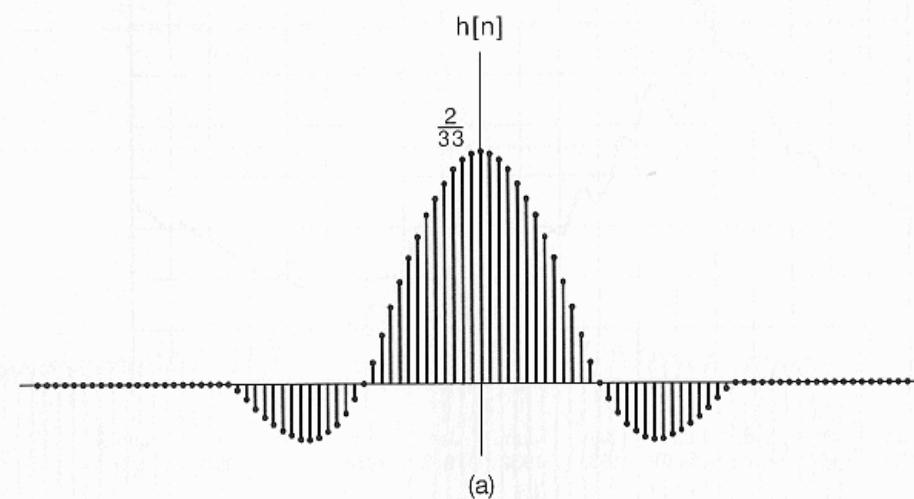
- Let $N = M = 16$:

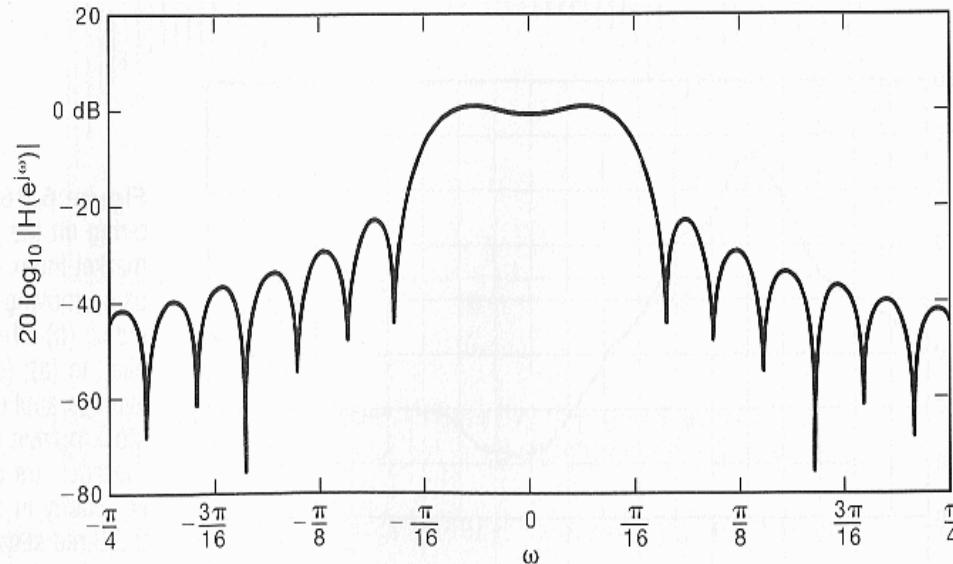
$$b_k = \begin{cases} \frac{\sin(2\pi k/33)}{\pi k}, & |k| \leq 32 \\ 0, & |k| > 32 \end{cases}$$

$$h[n] = \begin{cases} \frac{\sin(2\pi n/33)}{\pi n}, & |n| \leq 32 \\ 0, & |n| > 32 \end{cases}$$



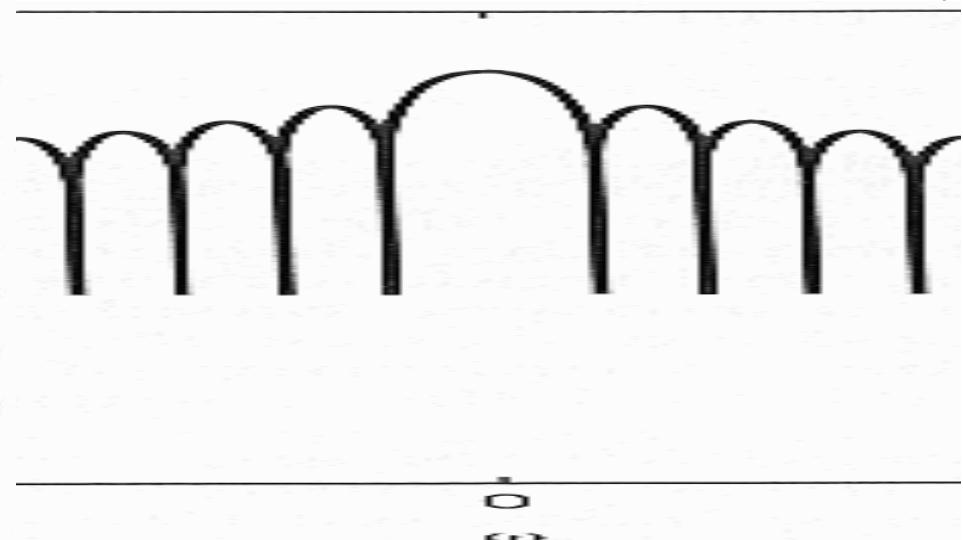
■ General Form of DT Non-recursive Filters:



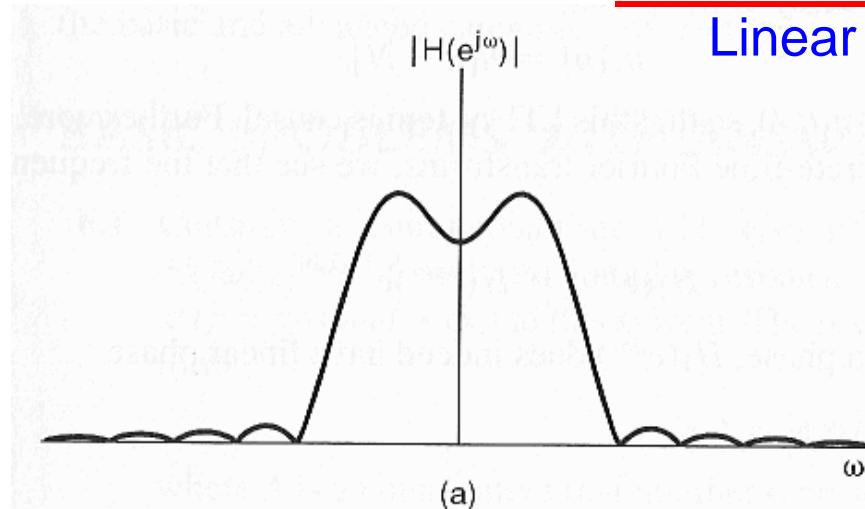
■ Comparison on a Linear Amplitude Scale:

(b)

Log Scale

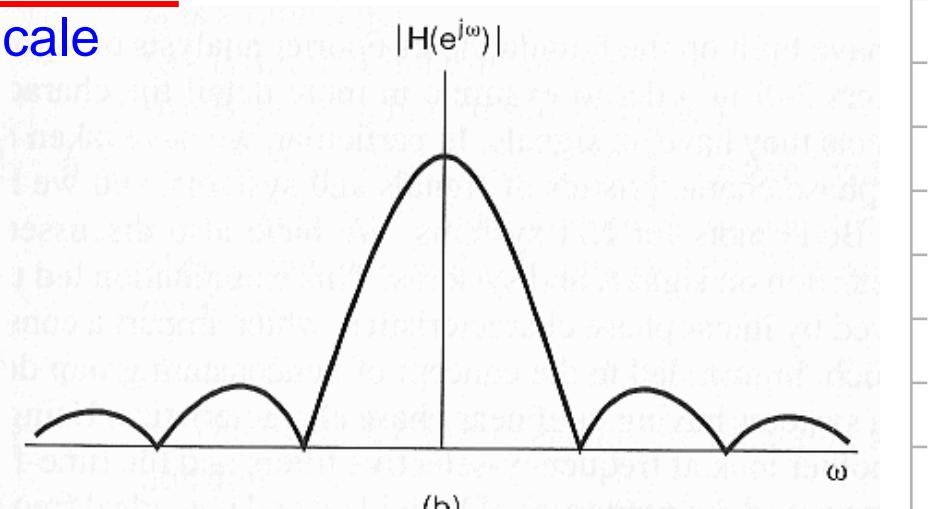


(b)



(a)

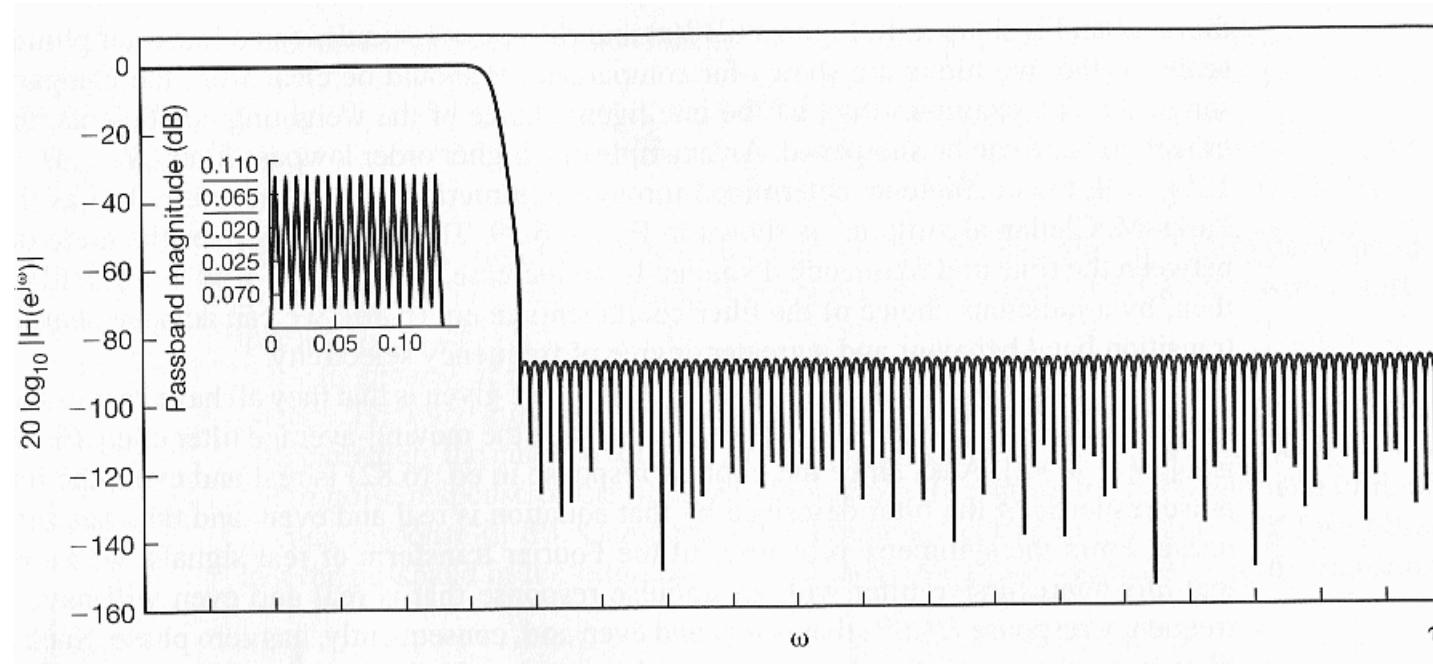
Linear Scale



(b)

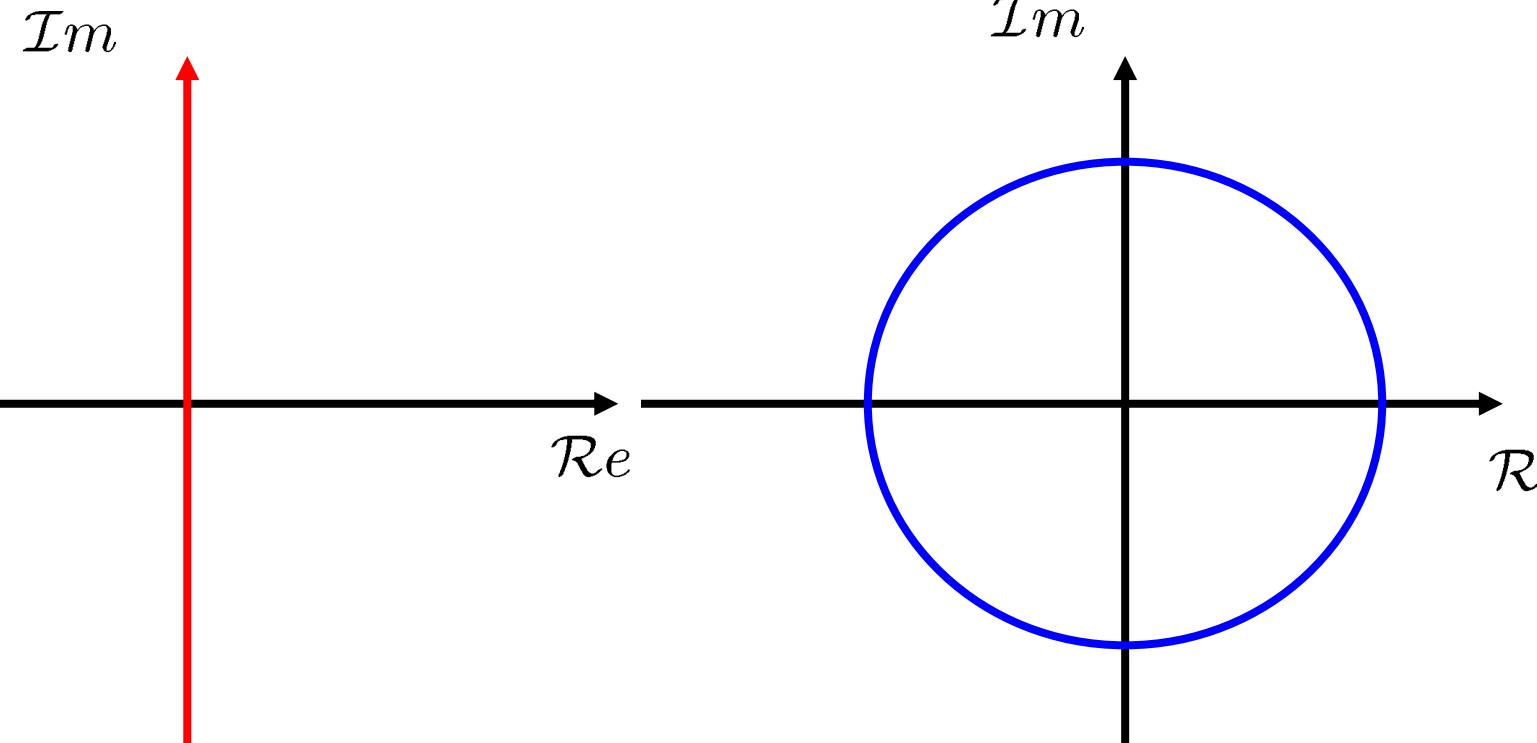
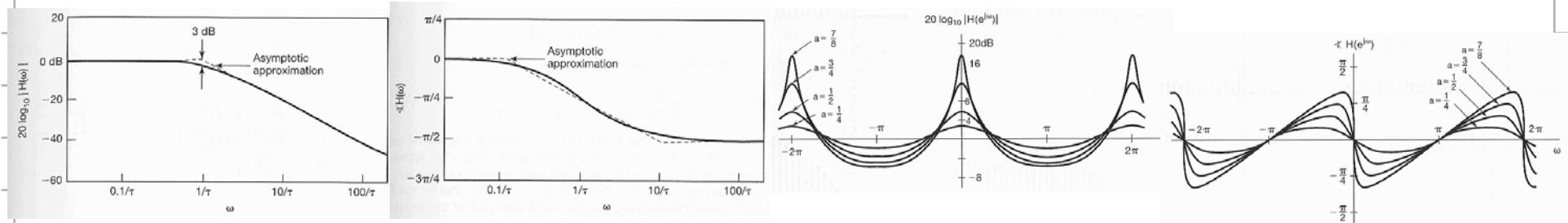
- Lowpass Non-recursive Filter with 251 Coefficients:

$$y[n] = \sum_{k=-N}^M b_k x[n - k]$$

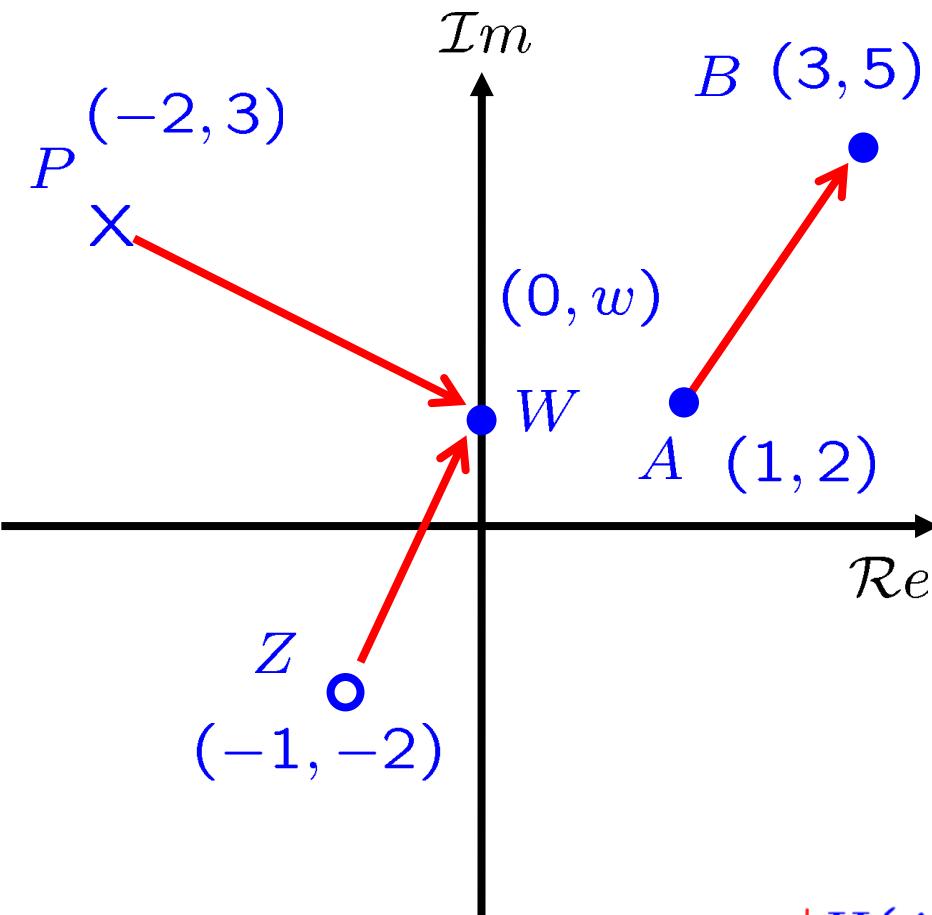


Coefficients determined by the Parks-McClellan algorithm

- Geometric Evaluation of the Fourier Transform of The Laplace Transform & Z-Transform
- Sec 9.4 (p. 674) and Sec 10.4 (p. 763)



■ In s-plane or z-plane:



$$H(s) = \frac{s - (-1 - 2j)}{s - (-2 + 3j)}$$

$$\begin{aligned}\overrightarrow{AB} &= (3 + 5j) - (1 + 2j) \\ &= 2 + 3j\end{aligned}$$

$$\overrightarrow{AB} = (3, 5) - (1, 2) = (2, 3)$$

$$|\overrightarrow{AB}| = \sqrt{2^2 + 3^2}$$

$$\cancel{\overrightarrow{AB}} = \tan^{-1} \frac{(5 - 2)}{(3 - 1)}$$

$$|H(jw)| = \frac{|jw - (-1 - 2j)|}{|jw - (-2 + 3j)|} = \frac{|\overrightarrow{ZW}|}{|\overrightarrow{PW}|}$$

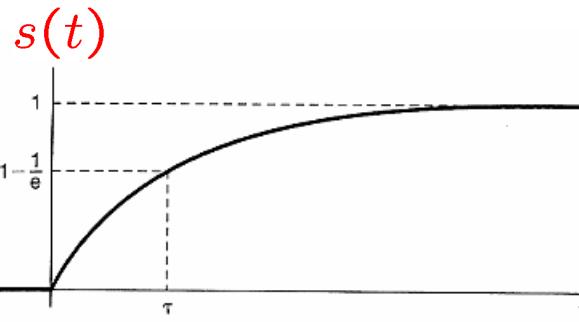
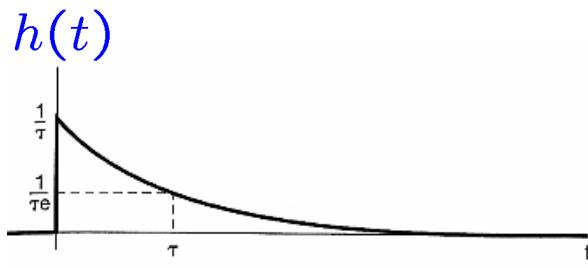
$$\cancel{H(jw)} = \cancel{\overrightarrow{ZW}} - \cancel{\overrightarrow{PW}}$$

Summary: Chap 6 - 1

$$\frac{d}{dt}y(t) + ay(t) = ax(t)$$

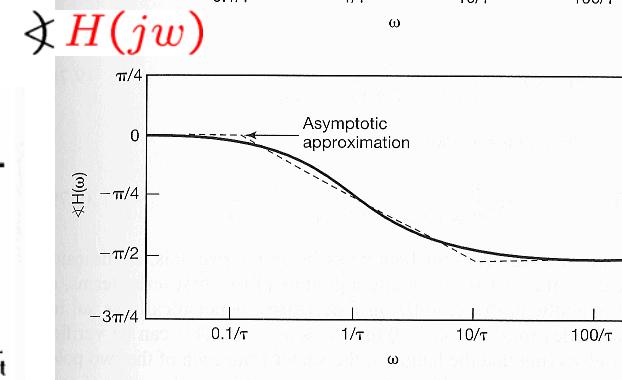
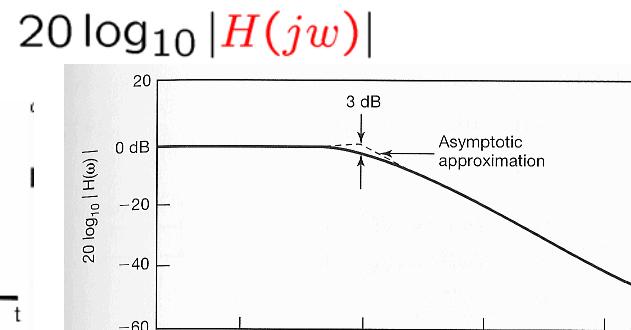
$$\Rightarrow H(jw) = \frac{a}{jw + a}$$

$$\Rightarrow H(s) = \frac{a}{s + a}$$

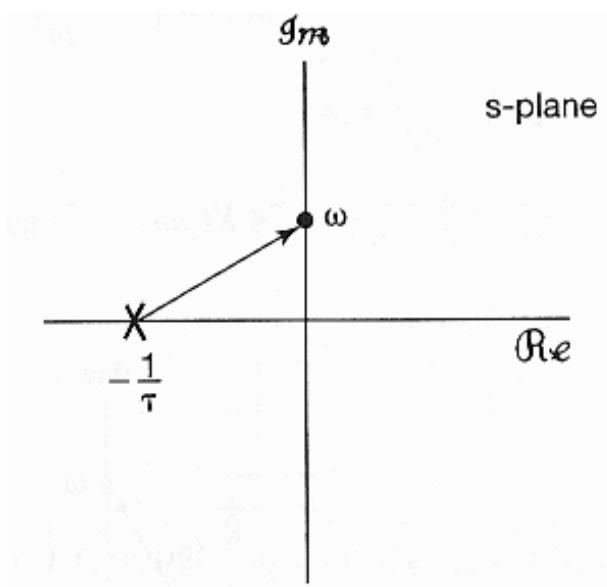


$$h(t) = a e^{-at} u(t)$$

$$s(t) = [1 - e^{-at}] u(t)$$



$$H(s)$$



Summary: Chap 6 - 2

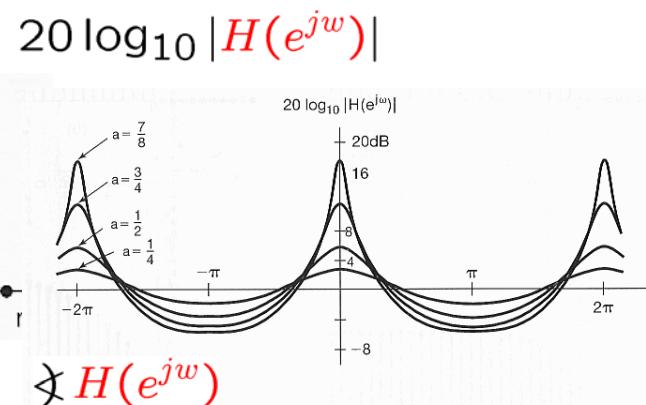
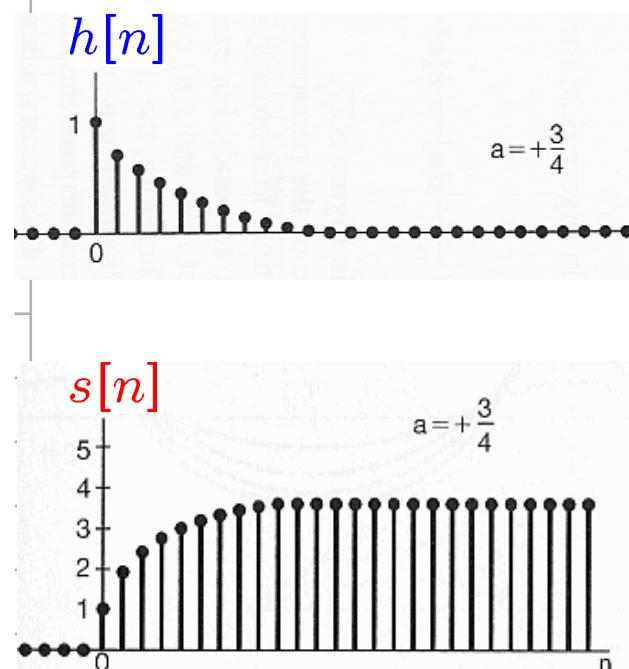
$$y[n] - a y[n-1] = x[n] \quad |a| < 1$$

$$\Rightarrow H(e^{j\omega}) = \frac{1}{1 - ae^{-j\omega}}$$

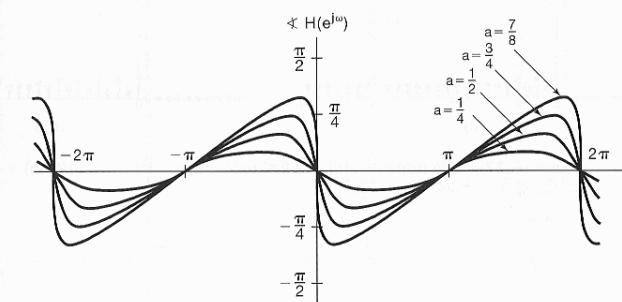
$$\Rightarrow H(z) = \frac{z}{z - a}, \quad |z| > |a|$$

$$\Rightarrow h[n] = a^n u[n]$$

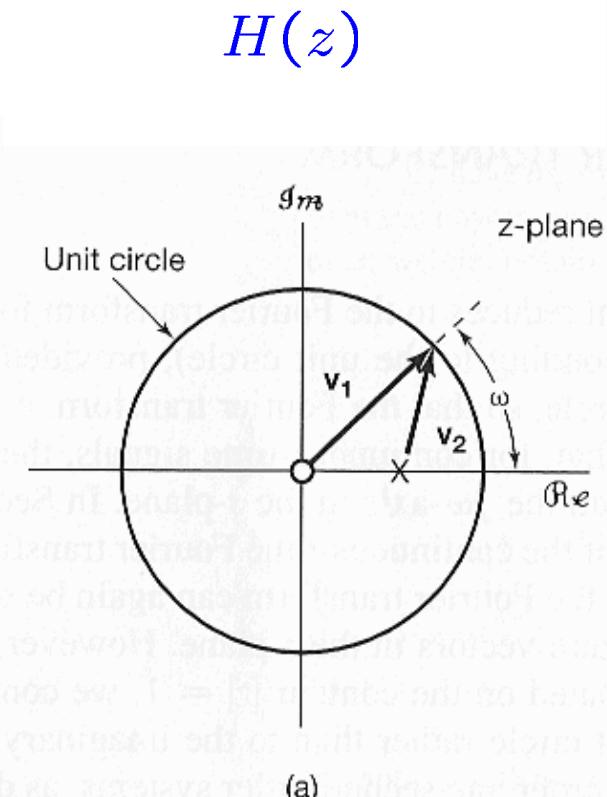
$$\Rightarrow s[n] = \frac{1 - a^{n+1}}{1 - a} u[n]$$



$\triangle H(e^{j\omega})$



(a)

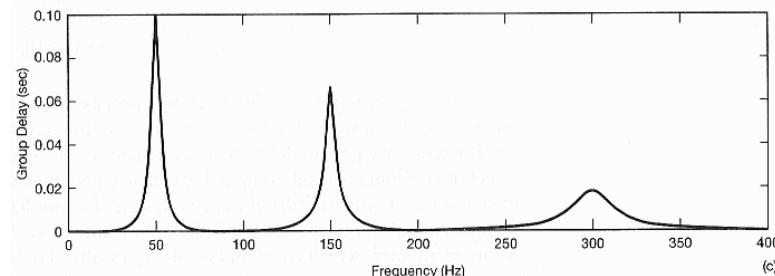
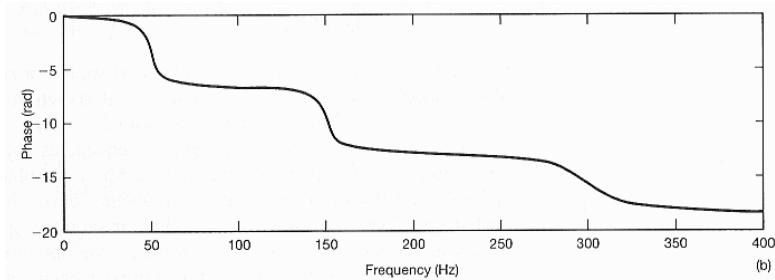
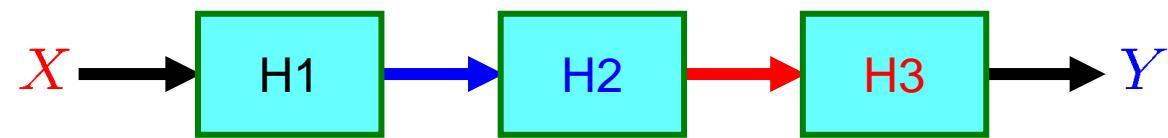


(a)

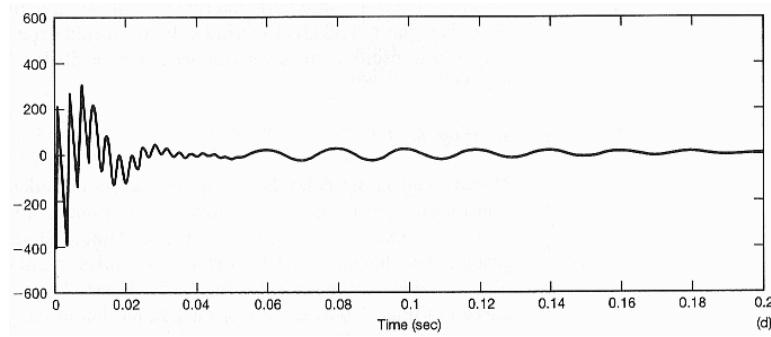
Summary: Chap 6 - 3

$$x(t) = \delta(t)$$

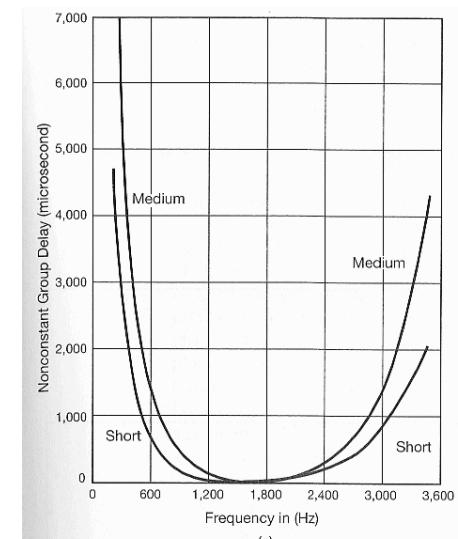
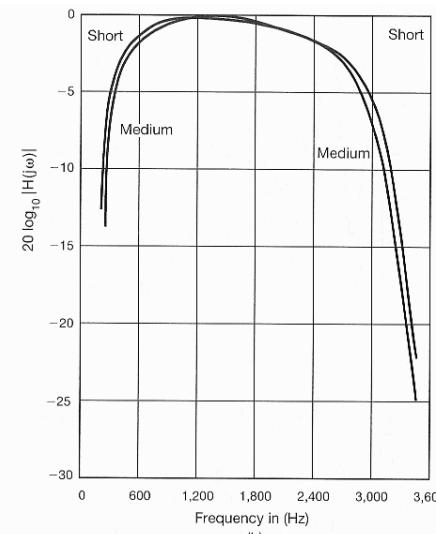
$$X(jw) = 1, \forall w$$



$y(t)$



$$\tau(w) = - \frac{d}{dw} \left\{ \arg H(jw) \right\}$$



Summary: Chap 6 - 4

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