

SimFem

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1 Geometry and finite elements

1.1 Simplices

We consider an arbitrary non-degenerate simplex $K = (x_0, x_1, \dots, x_d)$. The (signed) volume of K is given by

$$|K| = \frac{1}{d!} \det(x_1 - x_0, \dots, x_d - x_0) = \frac{1}{d!} \det(1, x_0, x_1, \dots, x_d) \quad 1 = (1, \dots, 1)^T. \quad (1)$$

The $d+1$ sides S_k (co-dimension one, $d-1$ -simplices or facets) are defined by $S_k = (x_0, \dots, \cancel{x_k}, \dots, x_d)$. The height is $d_k = |P_{S_k} x_k - x_k|$, where P_S is the orthogonal projection on the hyperplane associated to S . We have

$$d_k = d \frac{|K|}{|S_k|} \quad (\text{and for } d = 3 \ |S_k| = \frac{1}{2} |u \times v|)$$

1.2 Finite elements

The $d + 1$ basis functions of the Courant element are the barycentric coordinates λ_i defined as being affine with respect to the coordinates and $\lambda_i(x_j) = \delta_{ij}$. The constant gradient is given by

$$\nabla \lambda_i = -\frac{1}{d_i} \vec{n}_i.$$

The relation with the $d + 1$ Crouzeix-Raviart basis functions ψ_i is given by

$$\psi_i = 1 - d\lambda_i$$

Finally the $d + 1$ Raviart-Thomas basis functions ξ_i , associated to side S_i , i.e. the opposite node x_i , are given by

$$\xi_i = \frac{x - x_i}{d_i} = \frac{1}{d_i} \sum_{\substack{j=0 \\ i \neq j}}^d x_j \lambda_j$$

1.3 Numerical integration

Any polynomial in the barycentric coordinates can be integrates exactly.

$$\int_K \prod_{i=1}^{d+1} \lambda_i^{n_i} dv = d!|K| \frac{\prod_{i=1}^{d+1} n_i!}{\left(\sum_{i=1}^{d+1} n_i + d\right)!} \quad (2)$$

see [EisenbergMalvern73], [VermolenSegal18].

Let $V = \text{Vect}(\phi)$. For a smooth function f and $u = \sum_j u_j \phi_j$ we use an approximation based on $\text{Vect}(\psi)$ such that $\psi_l(x_k) = \delta_{kl}$ and

$$f(u) \approx \sum_k f(u(x_k)) \psi_k = \sum_k f\left(\sum_j u_j \phi_j(x_k)\right) \psi_k$$

Then

$$\begin{aligned} \int_K f(u) \phi_i &\approx \sum_k f_k \int_K \psi_k \phi_i, \quad f_k = f\left(\sum_l u_l \phi_l(x_k)\right) \\ \int_K f'(u)(\phi_j) \phi_i &\approx \sum_k f'_{k,j} \int_K \psi_k \phi_i, \quad f'_{k,j} = f'\left(\sum_l u_l \phi_l(x_k)\right) \phi_j(x_k) \end{aligned}$$

For $\psi = \phi$ this becomes considerably cheaper:

$$\begin{aligned} \int_K f(u) \phi_i &\approx \sum_k f_k \int_K \phi_k \phi_i, \quad f_k = f(u_k) \\ \int_K f'(u)(\phi_j) \phi_i &\approx f'_j \int_K \phi_j \phi_i, \quad f'_k = f'(u_k) \end{aligned}$$

1.4 Element matrices for C^1

1.4.1 Mass matrix

$$M_{ij} = \begin{cases} \frac{2d||K||}{(2+d)!} & i=j \\ \frac{d||K||}{(2+d)!} & i \neq j \end{cases} \quad M^{1D} = |K| \begin{bmatrix} \frac{1}{3} & \frac{1}{6} \\ \frac{1}{6} & \frac{1}{3} \end{bmatrix}, \quad M^{2D} = |K| \begin{bmatrix} \frac{1}{6} & \frac{1}{12} & \frac{1}{12} \\ \frac{1}{12} & \frac{1}{6} & \frac{1}{12} \\ \frac{1}{12} & \frac{1}{12} & \frac{1}{6} \end{bmatrix}, \quad M^{3D} = |K| \begin{bmatrix} \frac{1}{10} & \frac{1}{20} & \frac{1}{20} & \frac{1}{20} \\ \frac{1}{20} & \frac{1}{10} & \frac{1}{20} & \frac{1}{20} \\ \frac{1}{20} & \frac{1}{20} & \frac{1}{10} & \frac{1}{20} \\ \frac{1}{20} & \frac{1}{20} & \frac{1}{20} & \frac{1}{10} \end{bmatrix}$$

Lumped mass

$$\tilde{M}_{ij} = \begin{cases} \frac{|K|}{(1+d)} & i=j \\ 0 & i \neq j \end{cases}$$

2 Test problems

2.1 Advection-Diffusion-Reaction

$$\operatorname{div}(\beta u) - \operatorname{div}(k \nabla u) + \psi(u) = f \quad \text{in } \Omega, \quad u = u^D \text{ on } \Gamma_D, \quad k \frac{\partial u}{\partial n} = q^D \text{ on } \Gamma_N \quad (3)$$

2.1.1 Courant element

$$\int_{\Omega} \psi(u) v + \int_{\Omega} k \nabla u \cdot \nabla v - \int_{\Omega} u \beta \cdot \nabla v + \int_{\partial \Omega} \beta_n^+ u v = \int_{\Omega} f v + \int_{\partial \Omega} |\beta_n^-| u^D v$$

Piecewise constant approximation for k

$$\begin{aligned} \int_K \nabla \lambda_i \cdot \nabla \lambda_j &= |K| \frac{n_i}{d_i} \cdot \frac{n_j}{d_j} = |K| \frac{|S_i|}{d|K|} \frac{|S_j|}{d|K|} n_i \cdot n_j = \frac{1}{d^2|K|} \tilde{n}_i \cdot \tilde{n}_j \\ - \int_K u \beta \cdot \nabla \lambda_i &= u(x_K) |K| \beta \cdot \frac{n_i}{d_i} = u(x_K) \frac{1}{d} \beta \cdot \tilde{n}_i \\ - \int_S f \frac{\partial v_i}{\partial n} &= -f(x_S) |S| \nabla v_i \cdot n = f(x_S) |S| \frac{1}{d_i} n_i \cdot n = f(x_S) |S| \frac{|S_i|}{d|K|} n_i \cdot n = f(x_S) \frac{\tilde{n}_i \cdot \tilde{n}}{d|K|} \end{aligned}$$

2.2 Turing

We consider a reaction-diffusion system on $\Omega =]-1, +1[^d$

$$\begin{cases} \frac{\partial u}{\partial t} - k_u \Delta u = f(u, v) & \text{in } \Omega, & \frac{\partial u}{\partial n} = 0 & \text{on } \partial \Omega, \\ \frac{\partial v}{\partial t} - k_v \Delta v = g(u, v) & \text{in } \Omega, & \frac{\partial v}{\partial n} = 0 & \text{on } \partial \Omega, \end{cases} \quad (4)$$

Alan Turing discovered that the astonishing effect of destabilization by diffusion [Turing52], which leads to pattern formation ¹

$$f(u, v) = (a - u) - \psi(u, v), \quad g(u, v) = \psi(u, v). \quad (5)$$

An equilibrium point satisfies

$$u^* = a, \quad \psi(a, v^*) = 0$$

The linear stability analysis is based on the Jacobian

$$\begin{bmatrix} -1 - \psi'_u & -\psi'_v \\ \psi'_u & \psi'_v \end{bmatrix} \Rightarrow \text{tr} = \psi'_v - \psi'_u - 1, \quad \det = -\psi'_v$$

The brusselator is given by

$$\psi(u, v) = bu - u^2v \quad (\psi'_u = b - 2uv, \quad \psi'_v = -u^2). \quad (6)$$

An equilibrium point of (6) necessarily satisfies $u^* = a$ and $v^* = b/a$. We now have

$$\text{tr} = -b + 2uv - u^2 - 1, \quad \det = u^2$$

and for the equilibrium point

$$\text{tr}^* = -1 - b + 2b - a^2 = b - 1 - a^2, \quad \det^* = a^2$$

We conclude that a Hopf bifurcation appears if $b > a^2 + 1$.

2.2.1 The influence of diffusion

We consider an expansion into eigenfunctions of the Laplace operator with eigenvalues $l \geq 0$. For the frequency l we have the Jacobian

$$\begin{bmatrix} -1 - \psi'_u - k_u l & -\psi'_v \\ \psi'_u & \psi'_v - k_v l \end{bmatrix} \Rightarrow \text{tr} = \psi'_v - \psi'_u - 1 - (k_u + k_v)l,$$

$$\det = (1 + k_u l)(k_v l - \psi'_v) + k_v l \psi'_u = k_u k_v l^2 + (k_v(\psi'_u + 1) - k_u \psi'_v)l - \psi'_v$$

For the brusselator we have at the equilibrium

$$\det = k_u k_v l^2 + (k_u a^2 - k_v(b - 1))l + a^2.$$

The discriminant is

$$\Delta = (k_u a^2 - k_v(b - 1))^2 - 4a^2 k_u k_v$$

¹For an introduction and references see https://en.wikipedia.org/wiki/Reaction-diffusion_system.

which is positive ($a = 1$) for

$$b \leq b^* = 1 + \frac{k_u}{k_v} + 2\frac{\sqrt{k_u}}{\sqrt{k_v}} \quad (7)$$

The critical frequency is

$$l^* = \frac{k_v(b^* - 1) - k_u}{2k_u k_v} = 2k_u^{-1/2} k_v^{-3/2}$$

The data for our test problems are

$$(\text{cas 1}) \quad a = 1.0, \quad b = 2.1, \quad k_u = 0.0, \quad k_v = 0.0, \quad T = 20.0$$

$$(\text{cas 2}) \quad a = 1.0, \quad b = 1.9, \quad k_u = 0.0001, \quad k_v = 0.01, \quad T = 20.0$$

$$u_0(x) = \begin{cases} 1 & \text{if for all } i \ x_i \in [-0.4, 0.0] \\ 0 & \text{else} \end{cases} \quad v_0(x) = \begin{cases} 1 & \text{if for all } i \ x_i \in [-0.2, 0.2] \\ 0 & \text{else} \end{cases}$$