

비선형 감쇠장치가 설치된 건축구조물의 내진 및
내풍 성능 평가를 위한 하이브리드 실험기법 및
가진시스템 설계

Hybrid Experimental Method and Excitation System De-
sign for Seismic and Wind-resistance Performance Evalu-
ation of Building Structures with Nonlinear Dampers

June 2, 2017

박은천

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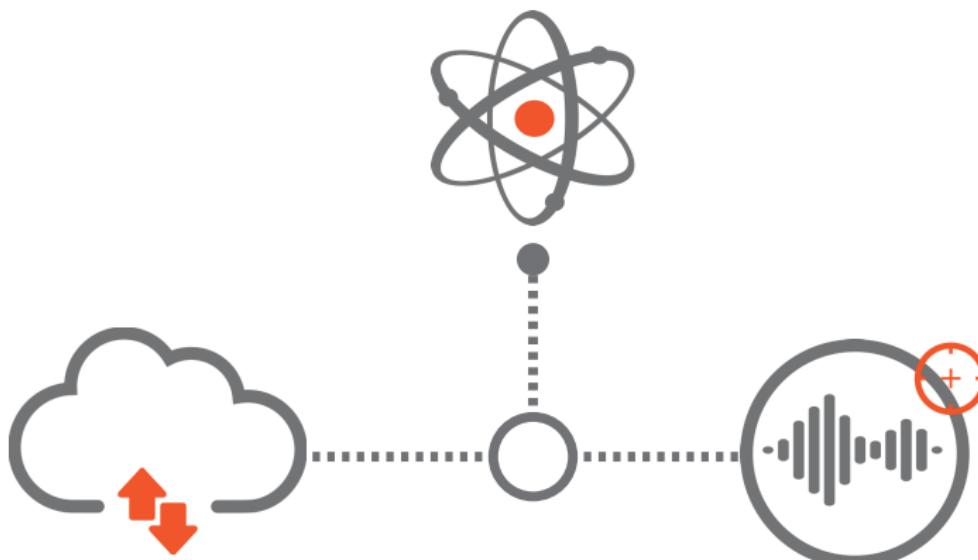
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5. RT-HYTEM with MR Damper
6. Conclusion

INTRODUCTION

INTRODUCTION

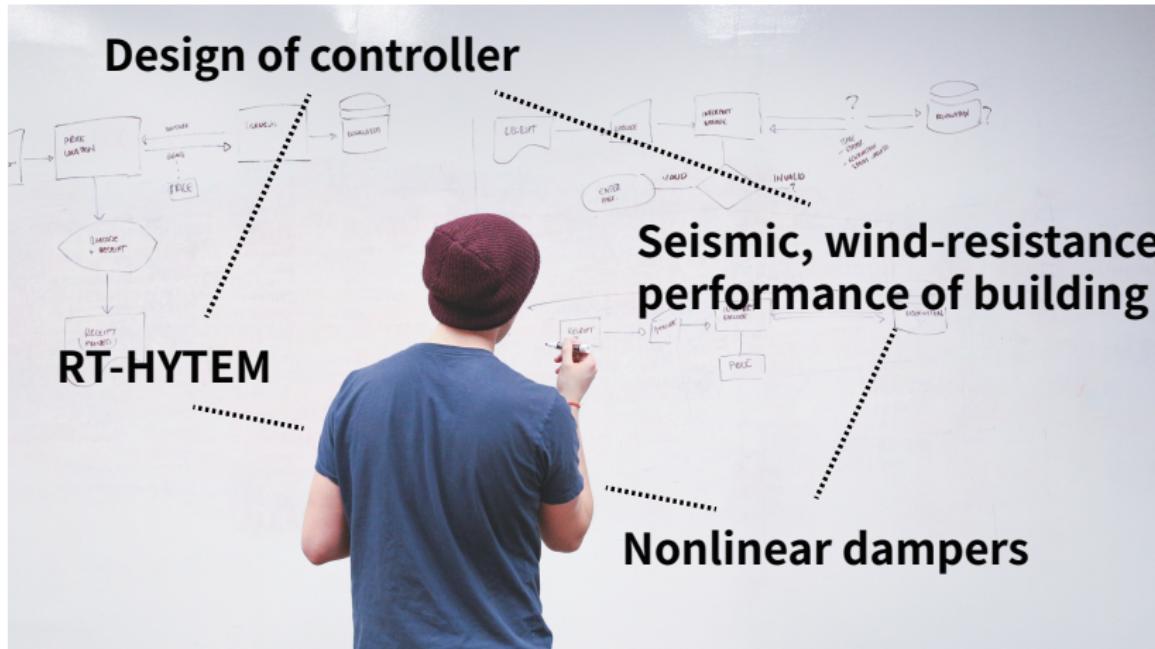
Goal of dissertation



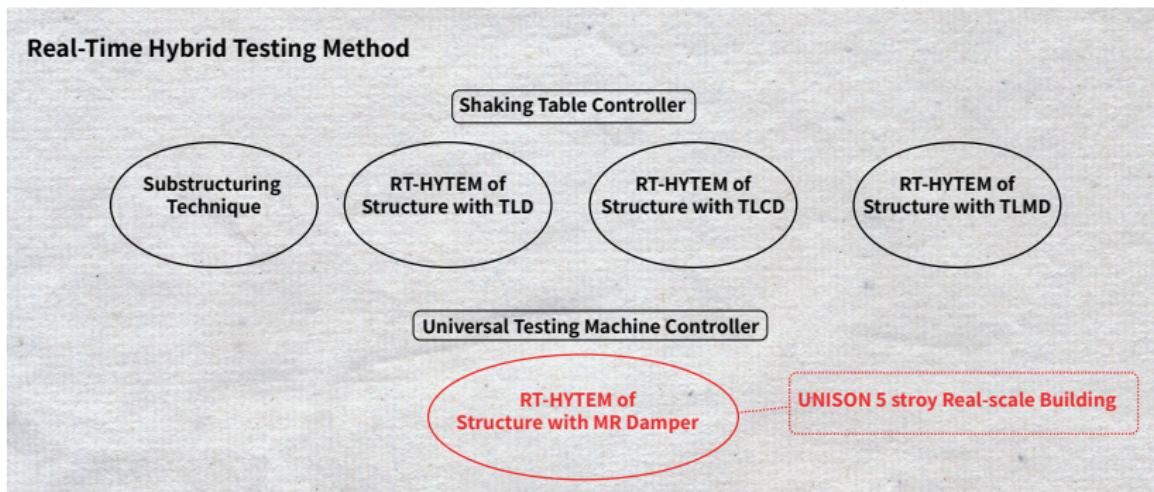
Real-Time Hybrid Testing Method

Design controller of actuators
for Simulating Dynamic Loads

INTRODUCTION



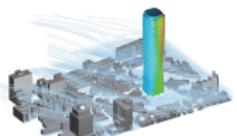
INTRODUCTION



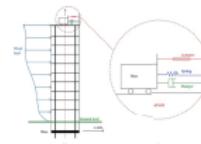
INTRODUCTION

Design Controller of Actuators

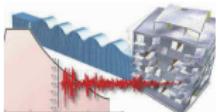
Pseudo wind-load excitation



76 story Benchmark Building



Pseudo earthquake excitation

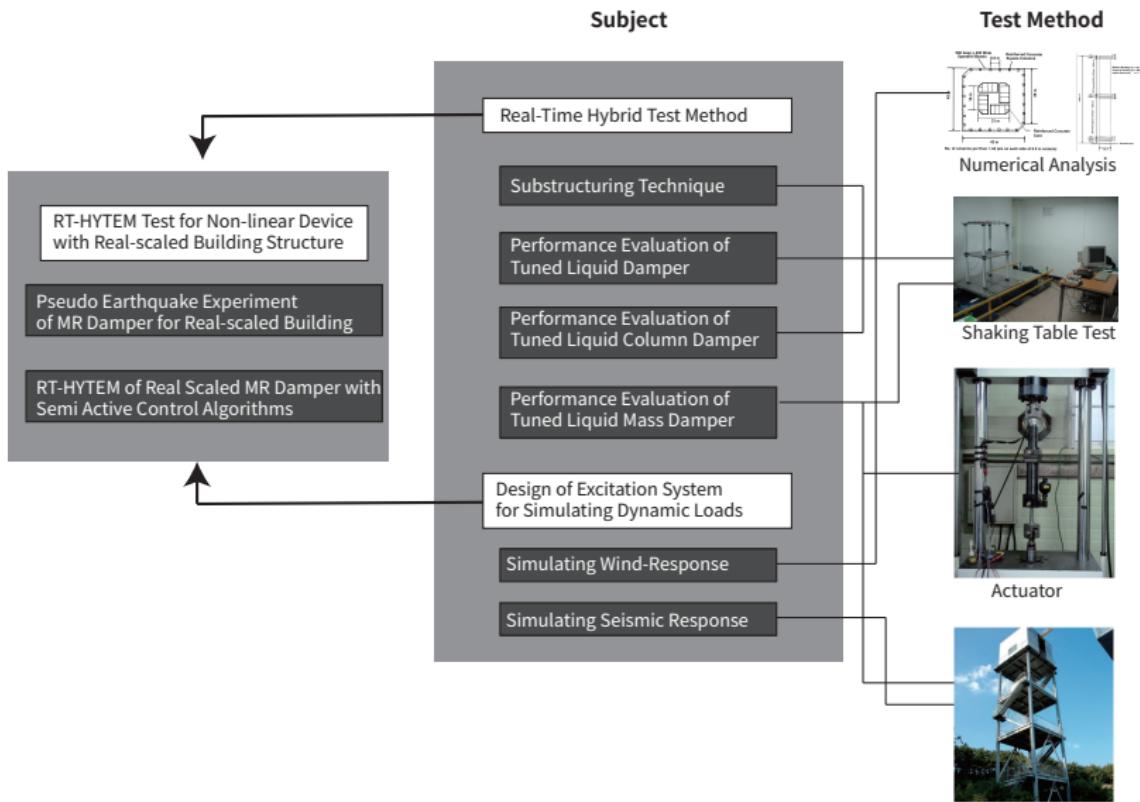


UNISON 5 story Real-Scale Building



Full-scale MR Damper

INTRODUCTION



PUBLICATIONS

INTERNATIONAL JOURNAL (국제저널 SCI급)

- **Eunchurn Park**, Kyung-Won Min, Sung-Kyung Lee, Sang-Hyun Lee, Heon-Jae Lee, Seok-Jun Moon, Hyung-Jo Jung, “**Real-time Hybrid Test on a Semi-actively Controlled Building Structure Equipped with Full-scale MR Dampers**”, Journal of Intelligent Material Systems and Structures; 21(18):1831-1850. DOI:10.1177/1045389X10390253 · 2.17 Impact Factor
- Heon-Jae Lee, Hyung-Jo Jung, Seok-Jun Moon, Sung-Kyung Lee, **Eun-Churn Park**, Kyung-Won Min, “**Experimental Investigation of MR Damper-based Semiactive Control Algorithms for Full-scale Five-story Steel Frame Building**”, Journal of Intelligent Material Systems and Structures; 21(10):1025-1037. DOI:10.1177/1045389X10374162 · 2.17 Impact Factor
- Jae-Sung Heo, Sung-Kyung Lee, **Eunchurn Park**, Sang-Hyun Lee, Kyung-Won Min, Hongjin Kim, Jiseong Jo, Bong-Ho Cho, “**Performance test of a tuned liquid mass damper for reducing bidirectional responses of building structures**”, The Structural Design of Tall and Special Buildings; 18(7):789 - 805. DOI:10.1002/tal.486 · 0.83 Impact Factor
- **Eun-Churn Park**, Sang-Hyun Lee, Kyung-Won Min, Lan Chung, Sung-Kyung Lee, Seung-Ho Cho, Eunjong Yu, Kyung-Soo Kang, “**Design of an actuator for simulating wind-induced response of a building structure**”, SMART STRUCTURES AND SYSTEMS; 4(1). DOI:10.12989/ss.2008.4.1.085 · 1.16 Impact Factor
- Sung-Kyung Lee, **Eun Churn Park**, Kyung-Won Min, Ji-Hun Park, “**Real-time substructuring technique for the shaking table test of upper substructures**”, Engineering Structures; 29(9):2219-2232. DOI:10.1016/j.engstruct.2006.11.013 · 1.77 Impact Factor
- Sung-Kyung Lee, **Eun Churn Park**, Kyung-Won Min, Sang-Hyun Lee, Ji-Hun Park, “**Experimental implementation of a building structure with a tuned liquid column damper based on the real-time hybrid testing method**”, Journal of Mechanical Science and Technology; 21(6):885-890. DOI:10.1007/BF03027063 · 0.70 Impact Factor
- Sung-Kyung Lee, **Eun Churn Park**, Kyung-Won Min, Sang-Hyun Lee, Lan Chung, Ji-Hun Park, “**Real-time hybrid shaking table testing method for the performance evaluation of a tuned liquid damper controlling seismic response of building structures**”, Journal of Sound and Vibration; DOI:10.1016/j.jsv.2006.12.006 · 1.86 Impact Factor

DOMESTIC JOURNAL (국내저널 KCI등재)

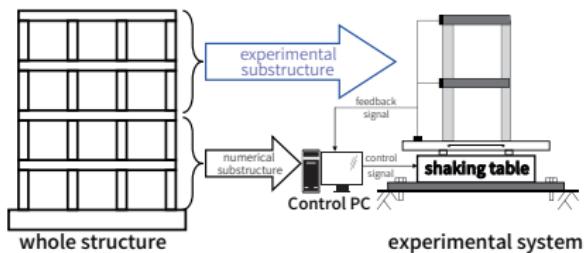
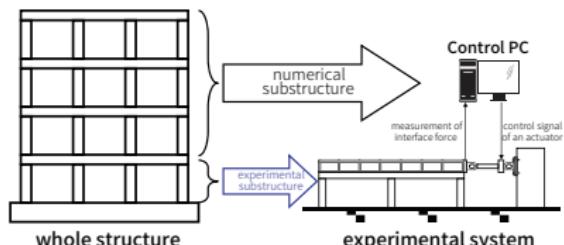
- 민경원, 이성경, 박은천, “진동대실험에 의한 동조액체기둥감쇠기의 동적특성”, 한국소음진동공학회논문집 (Transactions of the Korean society for noise and vibration engineering) v.19 no.6 = no.147, pp.620 - 627, 2009, 1598-2785
- 박은천, 이성경, 이현재, 문석준, 정형조, 민경원, “대형 MR감쇠기가 설치된 건축구조물의 실시간 하이브리드 실험 및 준능동 알고리즘 적용”, 한국전산구조공학회논문집 (Journal of the computational structural engineering institute of Korea) v.21 no.5, pp.465 - 474, 2008, 1229-3059
- 이성경, 민경원, 박은천, “TMD와 TLCD를 이용한 2방향 감쇠기의 동적특성”, 한국전산구조공학회논문집 (Journal of the computational structural engineering institute of Korea) v.21 no.6, pp.589 - 596, 2008, 1229-3059
- 허재성, 이성경, 박은천, 이상현, 김홍진, 조지성, 조봉호, “실시간 하이브리드 진동대 실험법에 의한 양방향 TLMD의 진동제어 성능평가”, 한국소음진동공학회논문집 (Transactions of the Korean society for noise and vibration engineering) v.18 no.5 = no.134, pp.485 - 495, 2008, 1598-2785
- 허재성, 박은천, 이상현, 이성경, 김홍진, 조봉호, 조지성, 김동영, 민경원, “건축구조물의 2방향 진동제어를 위한 동조액체질량감쇠기”, 한국소음진동공학회논문집 (Transactions of the Korean society for noise and vibration engineering) v.18 no.3 = no.132, pp.345 - 355, 2008, 1598-2785
- 허재성, 박은천, 이성경, 이상현, 김홍진, 조지성, 조봉호, 주석준, 민경원, “실물크기 구조물에 설치된 동조액체질량감쇠기의 성능실험”, 한국전산구조공학회논문집 (Journal of the computational structural engineering institute of Korea) v.21 no.2, pp.161 - 168, 2008, 1229-3059
- 윤경조, 박은천, 이현재, 문석준, 민경원, 정형조, 이상현, “준능동 MR감쇠기가 설치된 실물크기 구조물의 분산제어 알고리즘 성능평가”, 한국소음진동공학회논문집 (Transactions of the Korean society for noise and vibration engineering) v.18 no.2 = no.131, pp.255 - 262, 2008, 1598-2785

DOMESTIC JOURNAL (국내저널 KCI등재)

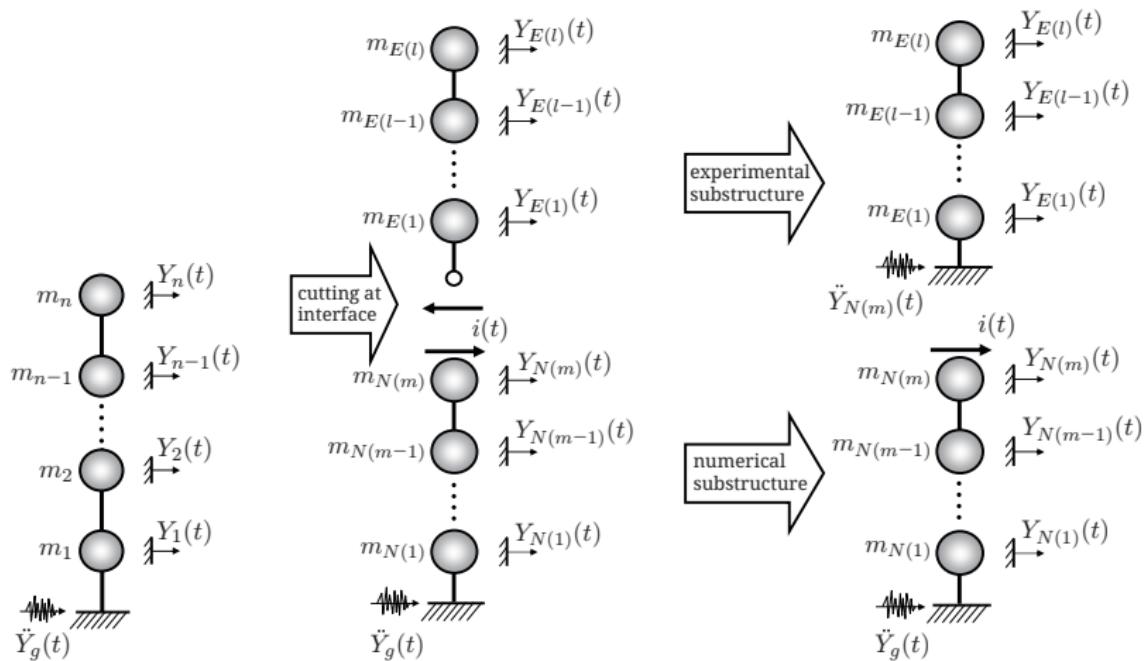
- 박은천, 이성경, 윤경조, 정희산, 이현재, 최강민, 문석준, 정형조, 민경원, “실시간 하이브리드 실험법을 이용한 대형 MR감쇠기의 제진 성능평가”, 한국소음진동공학회논문집 (Transactions of the Korean society for noise and vibration engineering) v.18 no.1 = no.130, pp.131 - 138, 2008, 1598-2785
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- 이상현, 박은천, 윤경조, 이성경, 유은종, 민경원, 정란, 민정기, 김영찬, “실물 크기 구조물의 강제진동실험 및 지진응답 모사를 위한 HMD제어기 설계”, 한국지진공학회논문집 (Journal of the earthquake engineering society of Korea) v.10 no.6 = no.52, pp.103 - 114, 2006, 1226-525x
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RT-HYTEM

REAL-TIME HYBRID TESTING METHOD



DYNAMIC EQUILIBRIUM IN EXPERIMENTAL STRUCTURE



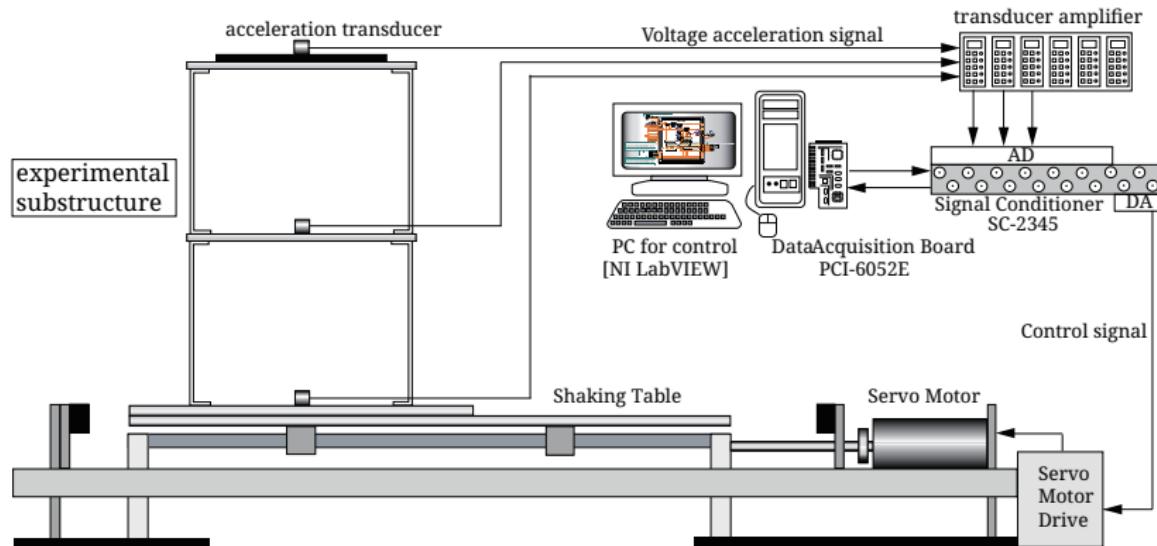
(a) Whole structure

(b) Separation
whole structure(c) Experimental and numeri-
cal substructure

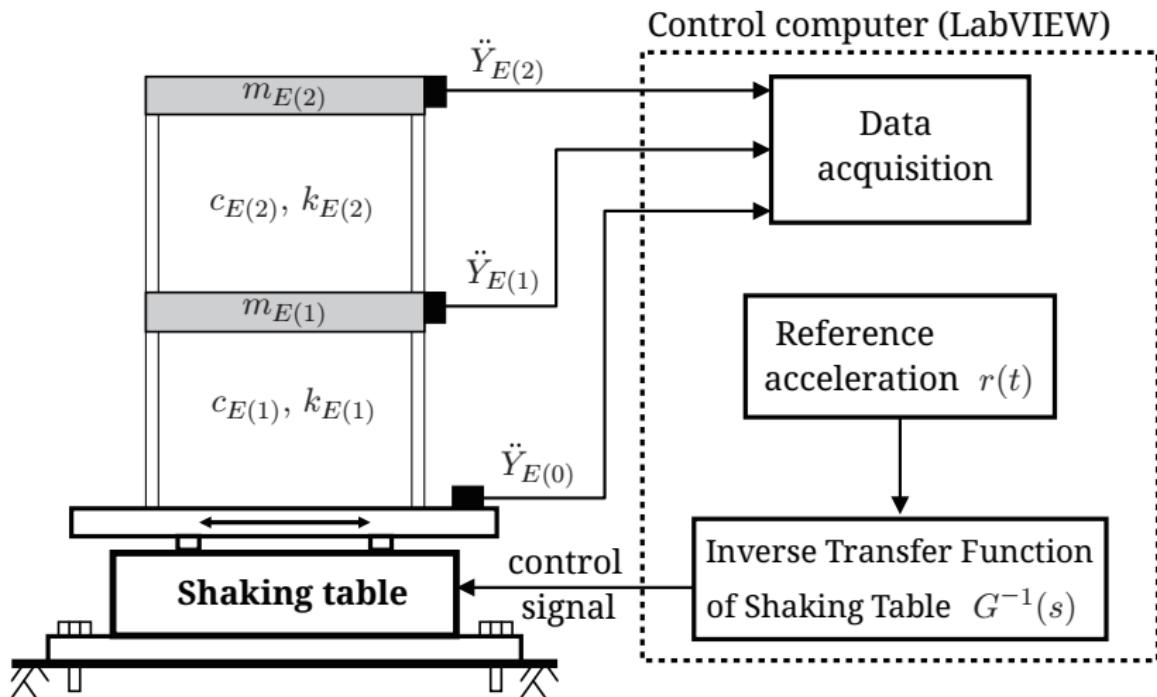
OVERALL VIEW OF EXPERIMENTAL SYSTEM



SCHEMATIC DIAGRAM OF EXPERIMENTAL SYSTEM



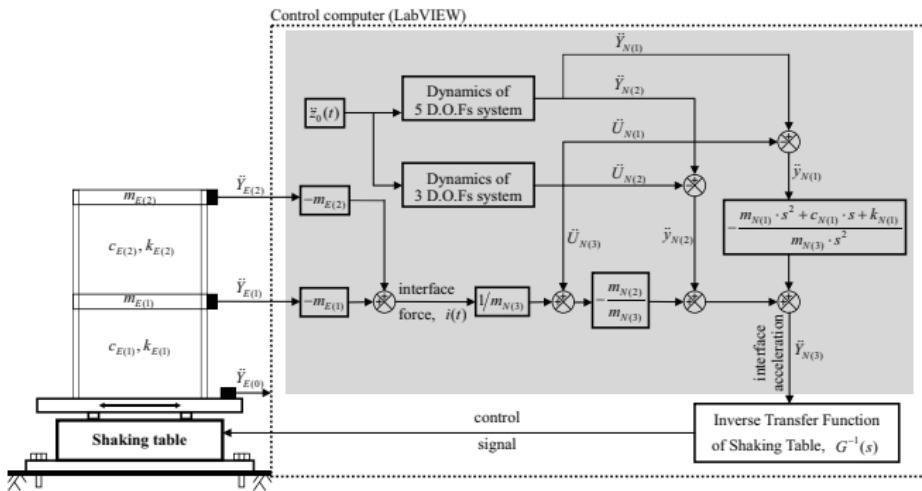
FLOW CHART OF THE EXPERIMENTAL SYSTEM CONTROLLER



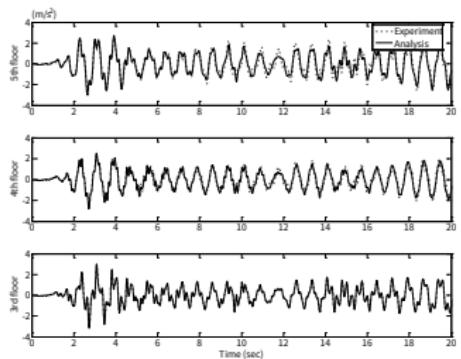
INTERFACING FORCE

$$i(t) = -m_{E(1)} \ddot{Y}_{E(1)}(t) - m_{E(2)} \ddot{Y}_{E(2)}(t) \quad (1)$$

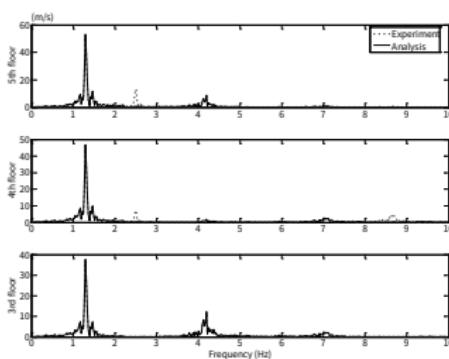
$$\ddot{Y}_{N(3)}(t) = -c_{N(3)} (\dot{Y}_{N(3)} - \dot{Y}_{N(2)}) - k_{N(3)} (Y_{N(3)} - Y_{N(2)}) + i(t) \quad (2)$$



COMPARISONS OF RESULTS

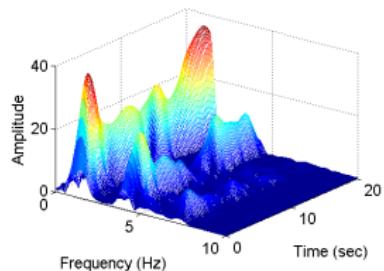


(a) Time domain

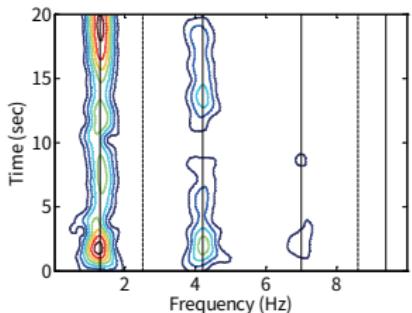


(b) Frequency domain

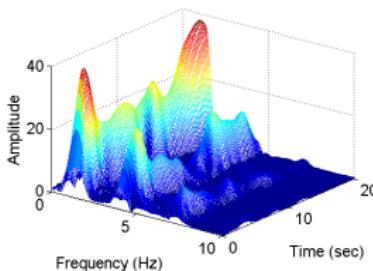
SPECTROGRAM COMPARISON OF RESULTS



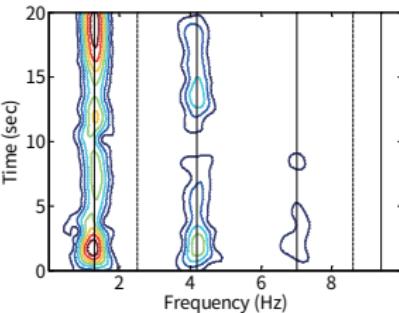
(a) experiment without feedback



(c) experiment without feedback

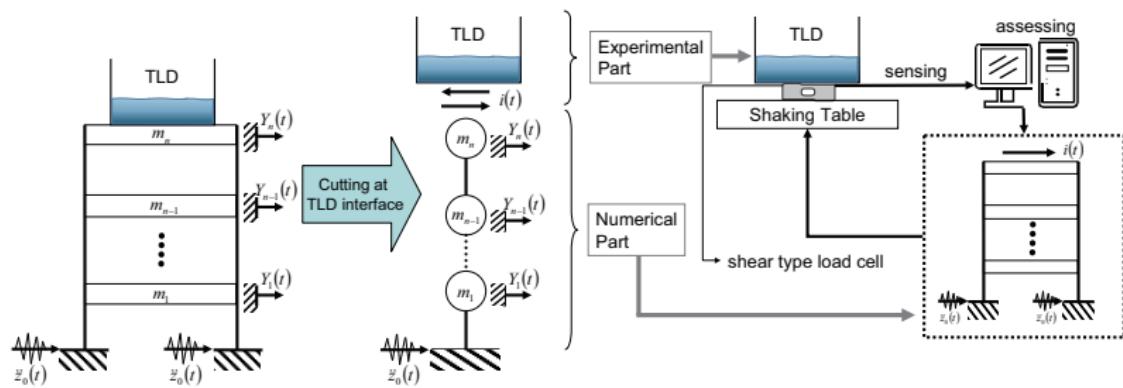


(b) numerical analysis measured

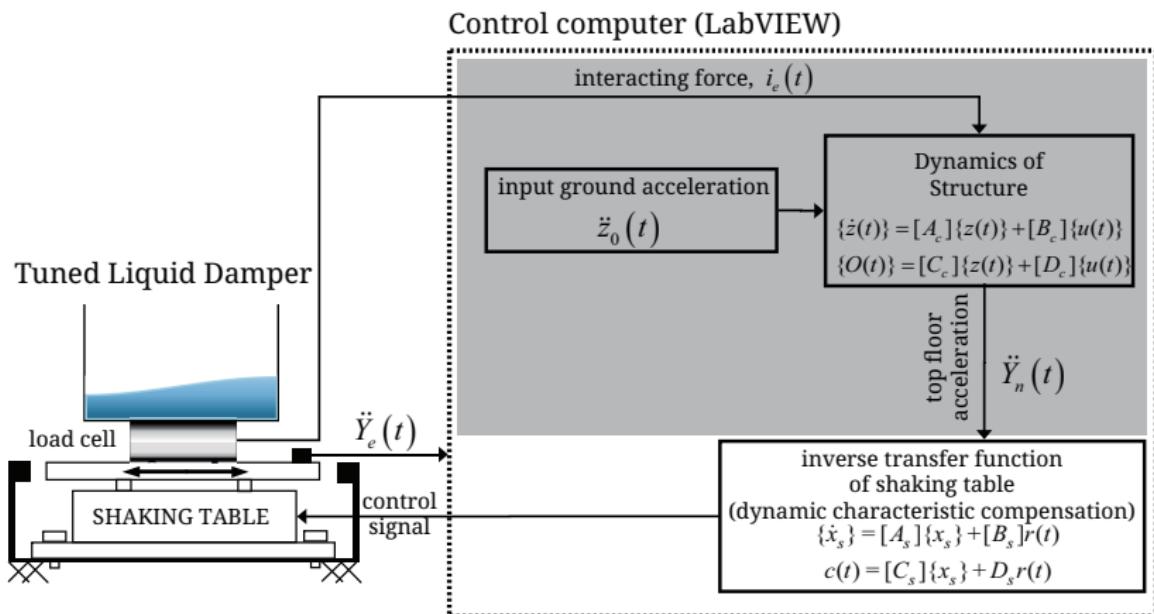


(d) numerical analysis

RT-HYTEM FOR A TLD WITH BUILDING STRUCTURE



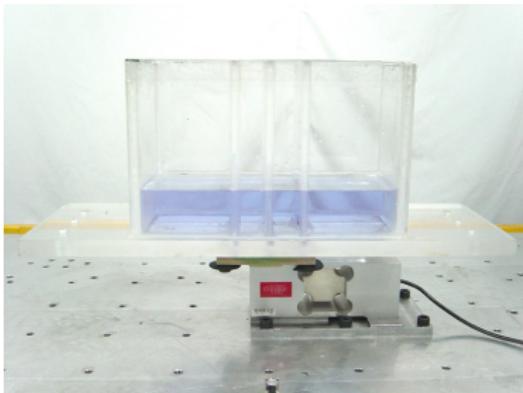
RT-HYTEM FOR THE PERFORMANCE EVALUATION OF A TLD



RT-HYTEM FOR THE PERFORMANCE EVALUATION OF A TLD

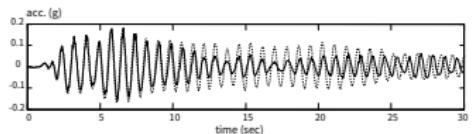


(a) Conventional shaking table test

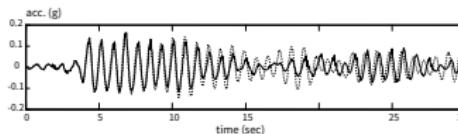


(b) Real-time hybrid shaking table test

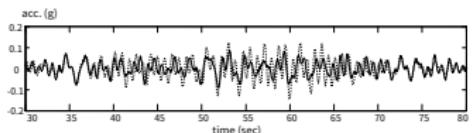
RT-HYTEM FOR THE PERFORMANCE EVALUATION OF A TLD



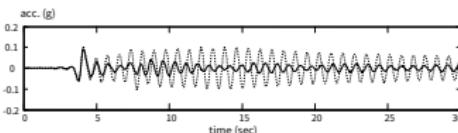
(a) El Centro



(b) Hachinohe



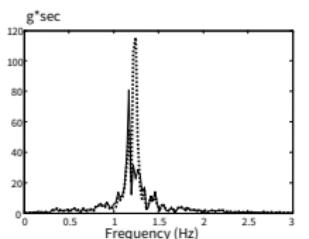
(c) Mexico city



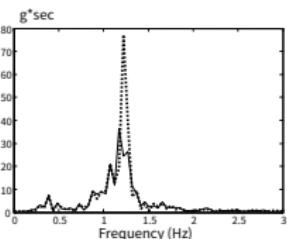
(d) Northridge

dotted line : without control, solid line : with control

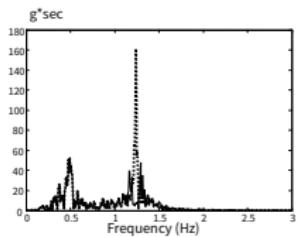
RT-HYTEM FOR THE PERFORMANCE EVALUATION OF A TLD



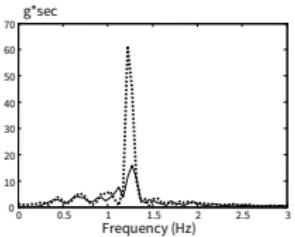
(a) El Centro



(b) Hachinohe



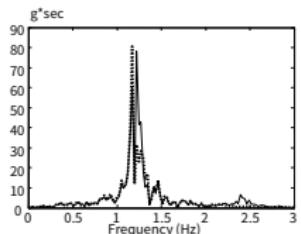
(c) Mexico city



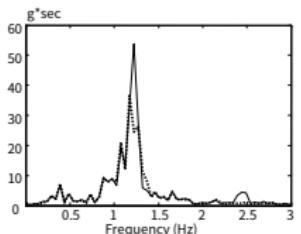
(d) Northridge

dotted line : without control, solid line : with control

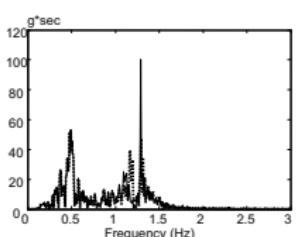
RT-HYTEM FOR THE PERFORMANCE EVALUATION OF A TLD



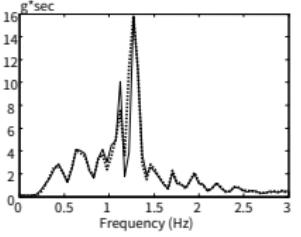
(e) El Centro



(f) Hachinohe



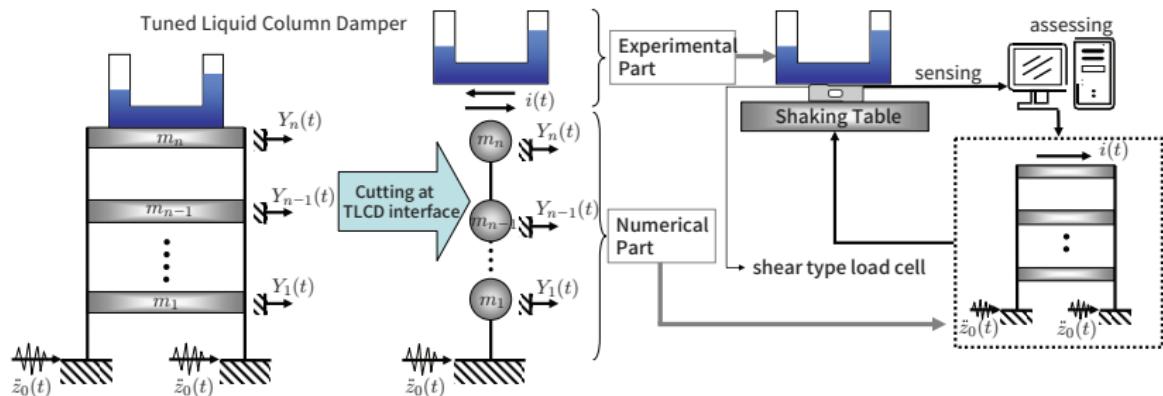
(g) Mexico city



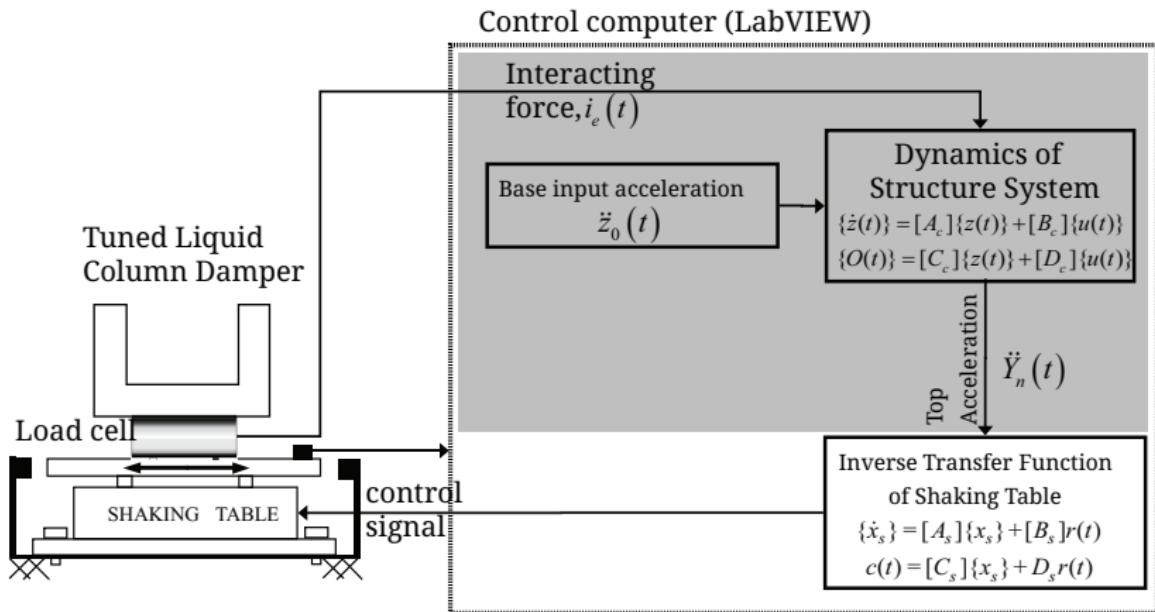
(h) Northridge

dotted line : conventional shaking table test, solid line :
real-time hybrid test

RT-HYTEM FOR THE PERFORMANCE EVALUATION OF A TLCD



RT-HYTEM FOR THE PERFORMANCE EVALUATION OF A TLCD



RT-HSTTM FOR THE PERFORMANCE EVALUATION OF A TLCD

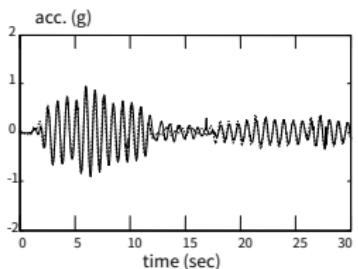


(a) conventional
method

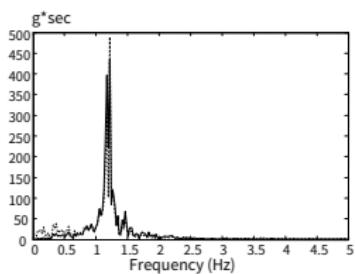


(b) real-time hybrid testing
method

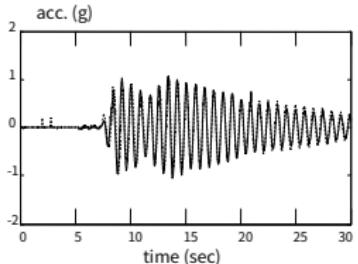
RT-HSTTM FOR THE PERFORMANCE EVALUATION OF A TLCD



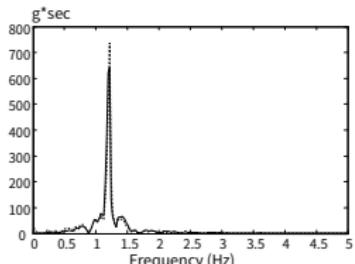
(a) El Centro Earth-
quake(time domain)



(b) El Centro Earth-
quake(frequency
domain)

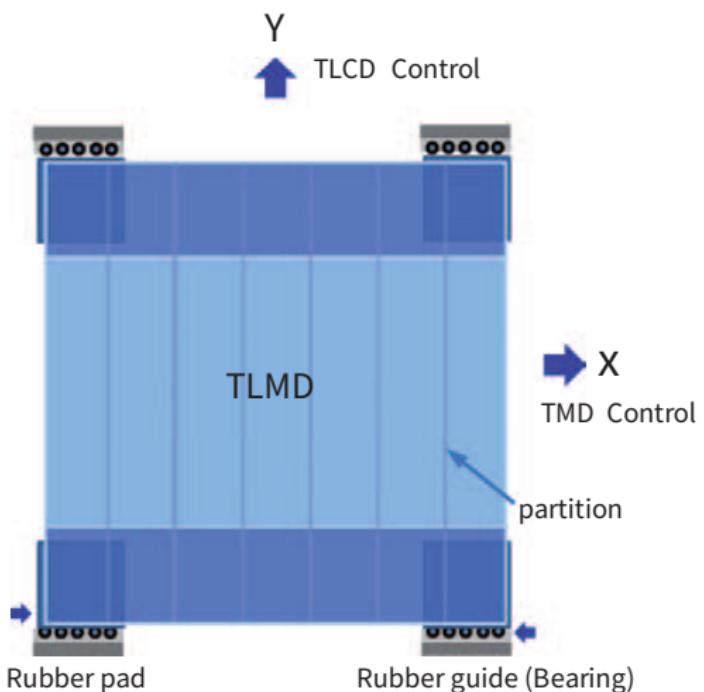


(c) Kobe Earth-
quake(time domain)

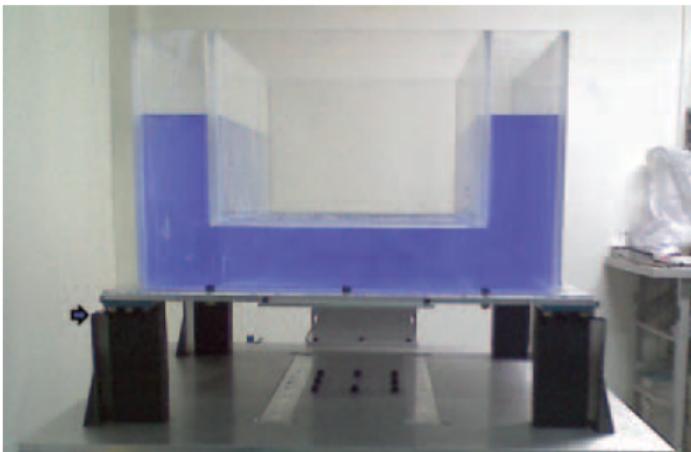


(d) Kobe Earth-
quake(frequency
domain)

RT-HYTEM FOR THE PERFORMANCE EVALUATION OF A TLMD



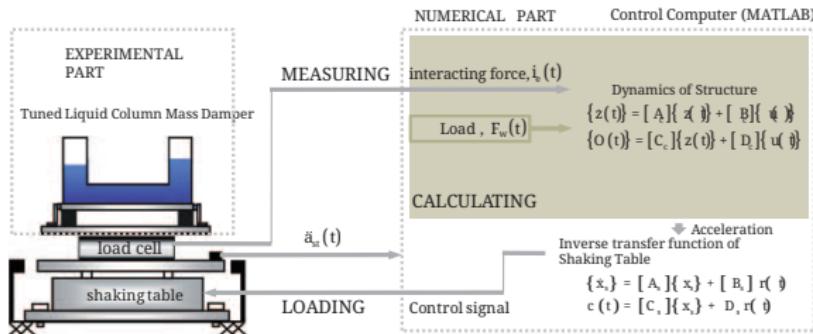
RT-HYTEM FOR THE PERFORMANCE EVALUATION OF A TLMD



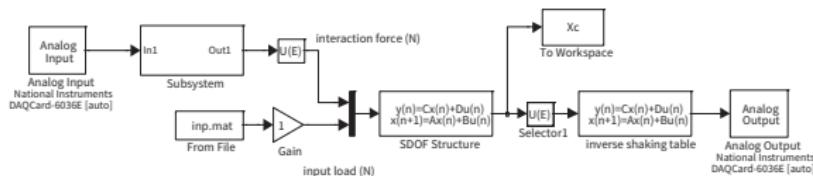
Design parameter	TLCD control direction	TMD control direction
Sifness or liquid length	0.98m (liquid length)	1990 N/m (stiffness)
Frequency (Hz)	0.73	0.82
Mass (kg)	35	75

Table: Design parameters of a TLMD model

RT-HYTEM FOR A TLMD WITH A BUILDING STRUCTURE

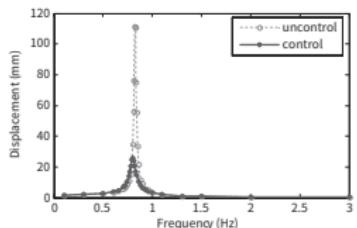


(a) Design of the controller

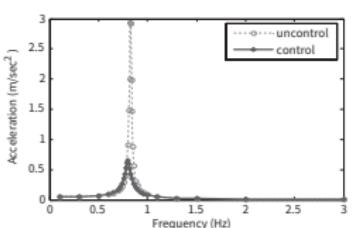


(b) MATLAB Simulink window Target

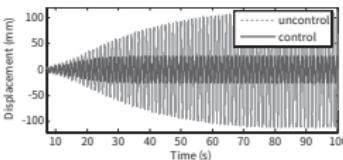
RT-HYTEM FOR A TLMD WITH A BUILDING STRUCTURE



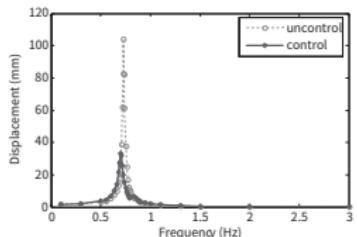
(a) Disp. TMD dir.



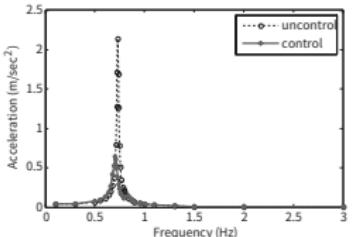
(b) Acc. TMD dir.



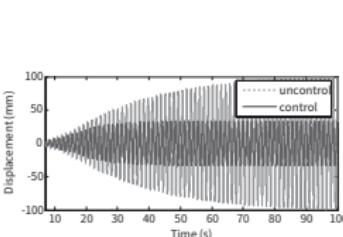
(c) Disp. TMD dir.



(d) Disp. TLCD dir.



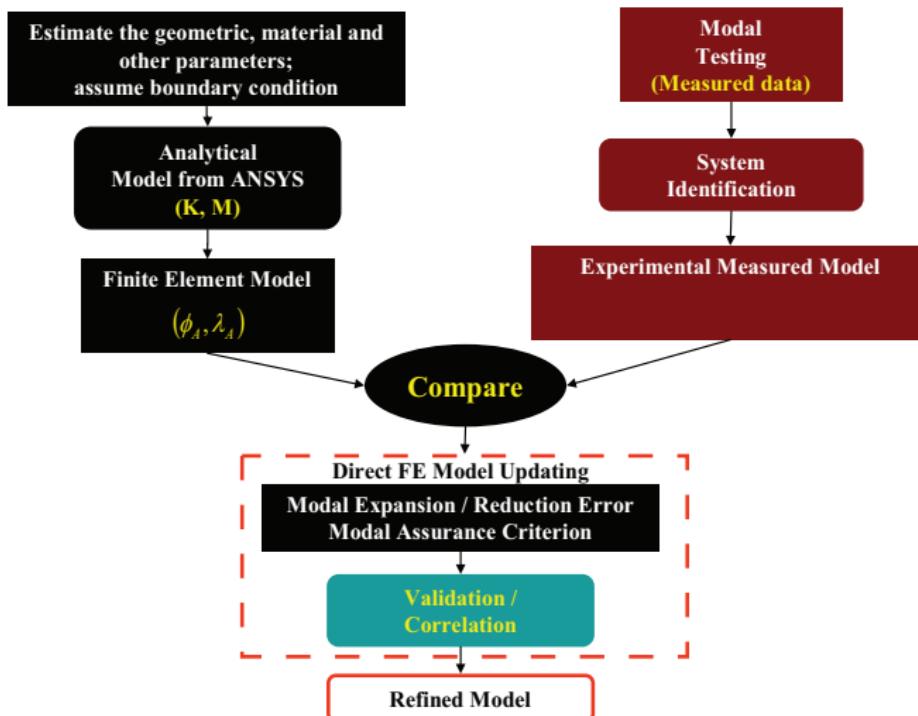
(e) Acc. TLCD dir.



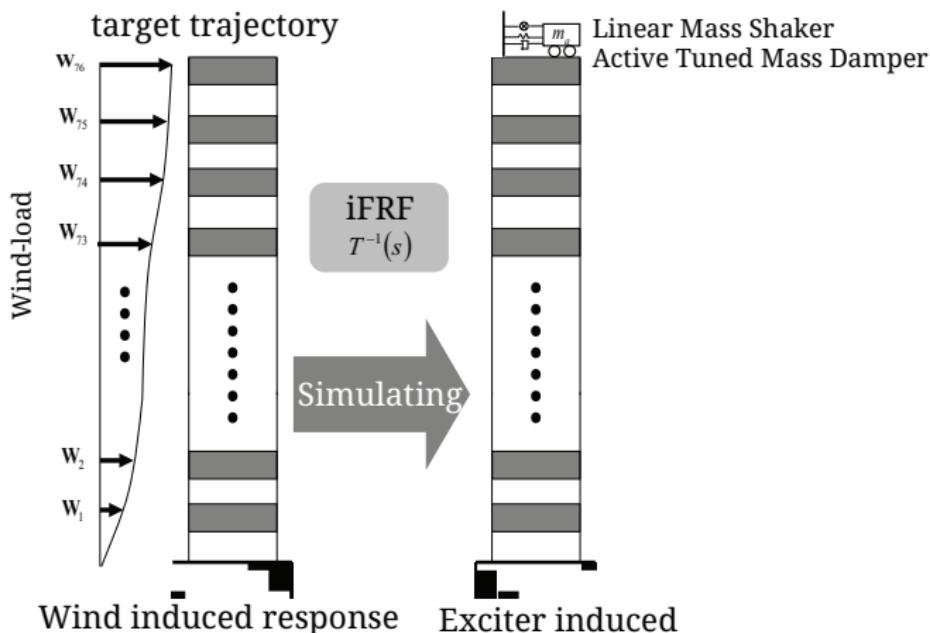
(f) Disp. TLCD dir.t

DESIGN OF CONTROLLER

DESIGN OF AN ACTUATOR FOR SIMULATING WIND RESPONSE



DESIGN OF AN ACTUATOR FOR SIMULATING WIND RESPONSE



Scheme of simulation of wind induced responses using LMS and ATMD

DESIGN OF AN ACTUATOR FOR SIMULATING WIND RESPONSE

Force of actuator

$$\begin{aligned}\dot{\mathbf{z}} &= \mathbf{A}\mathbf{z} + \mathbf{B}_f f + \mathbf{B}_u u \\ y &= \mathbf{C}\mathbf{z} + \mathbf{D}_f f + \mathbf{D}_u u\end{aligned}\tag{3}$$

$$\begin{aligned}\mathbf{T}_{yf} &= \mathbf{Y}_f(s)\mathbf{F}(s)^{-1} = \mathbf{C}(s\mathbf{I} - \mathbf{A})^{-1}\mathbf{B}_f \\ \mathbf{T}_{yu} &= \mathbf{Y}_u(s)\mathbf{U}(s)^{-1} = \mathbf{C}(s\mathbf{I} - \mathbf{A})^{-1}\mathbf{B}_u\end{aligned}\tag{4}$$

$$\begin{aligned}\hat{\mathbf{U}}(s) &= \hat{\mathbf{T}}_{yu}^{-1}\hat{\mathbf{Y}}_u(s) \\ &= \hat{\mathbf{T}}_{yu}^{-1}\hat{\mathbf{Y}}_f(s) \\ &= \hat{\mathbf{T}}_{yu}^{-1}\hat{\mathbf{T}}_{yf}\mathbf{F}(s)\end{aligned}\tag{5}$$

DESIGN OF AN ACTUATOR FOR SIMULATING WIND RESPONSE

Filter and envelop function

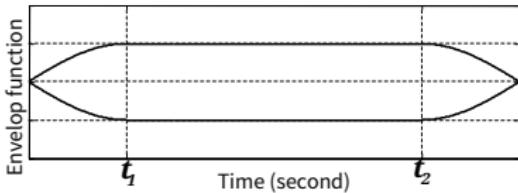
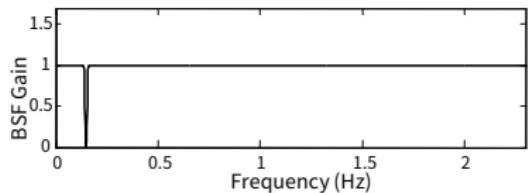
$$\hat{\mathbf{U}}_p(\omega) = G(\omega)\hat{\mathbf{U}}(s) \quad (6)$$

where,

$$G(\omega) = \frac{1 - a_{co}}{2} \cos\left(\frac{2\pi}{\omega_2 - \omega_1}\omega\right) + \frac{1 + a_{co}}{2} \quad (7)$$

$$a_{co} = \begin{cases} \omega < \omega_1 & : 1 \\ \omega_1 \leq \omega \leq \omega_2 & : 0 \\ \omega > \omega_2 & : 1 \end{cases} \quad (8)$$

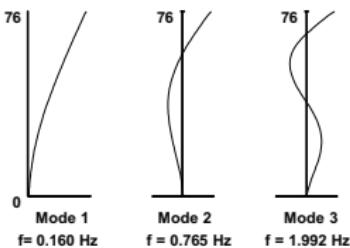
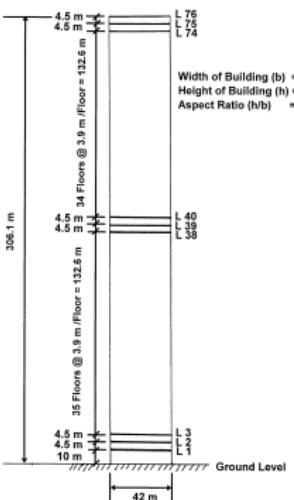
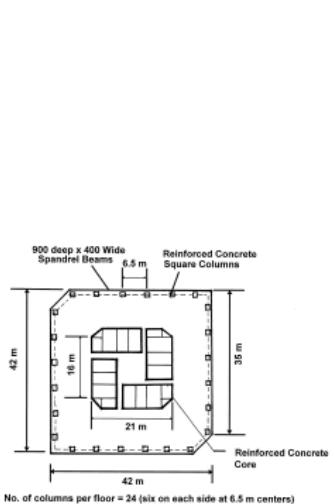
DESIGN OF AN ACTUATOR FOR SIMULATING WIND RESPONSE



- (a) The shape of the band-stop fil- (b) The shape of the envelop func-
ter tion

Exciter gain shape of the band-stop filter and the envelop
function.

DESIGN OF AN ACTUATOR FOR SIMULATING WIND RESPONSE



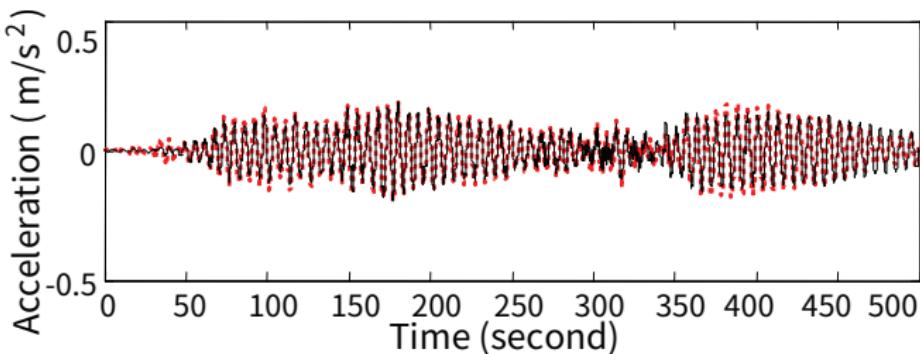
(c) Plan View of the 76-story Building

(d) Elevation View of the Building.

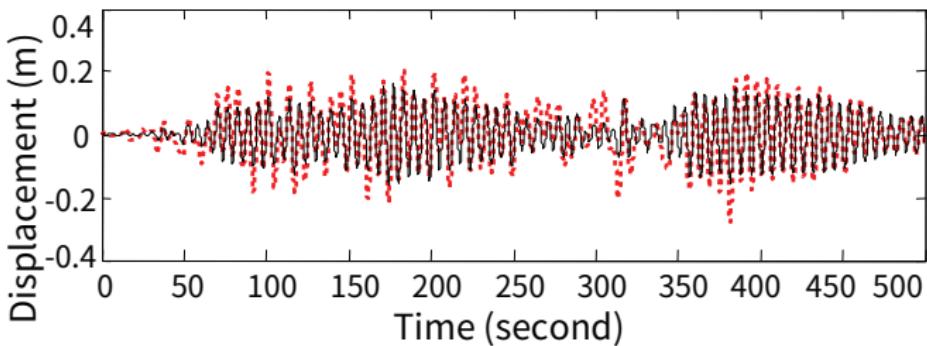
(e) Mode shapes of the Building.

76th story benchmark model.

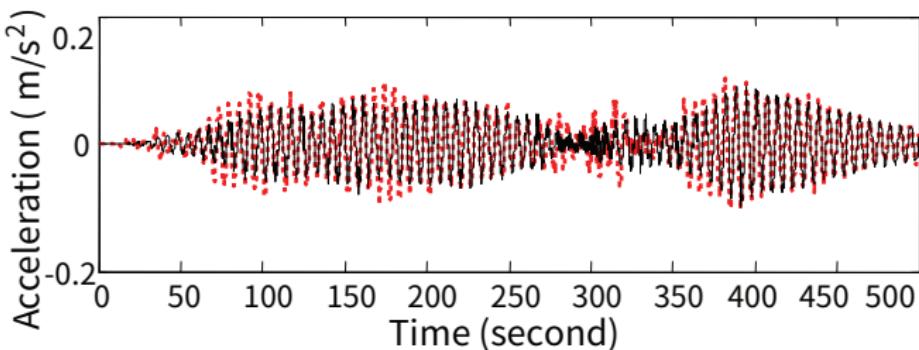
DESIGN OF AN ACTUATOR FOR SIMULATING WIND RESPONSE



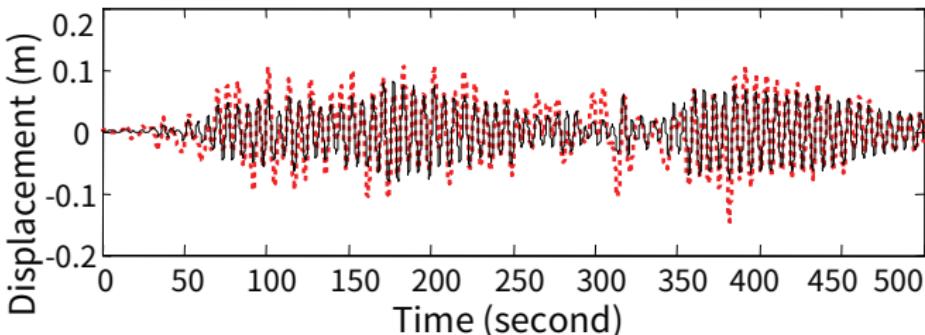
(a) 76th story acceleration response



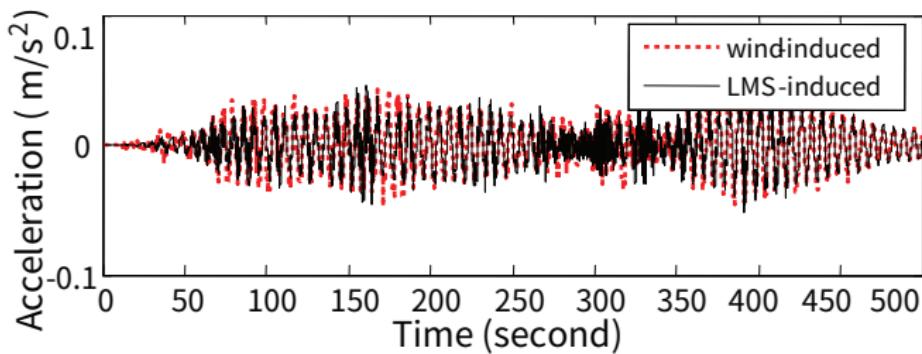
DESIGN OF AN ACTUATOR FOR SIMULATING WIND RESPONSE



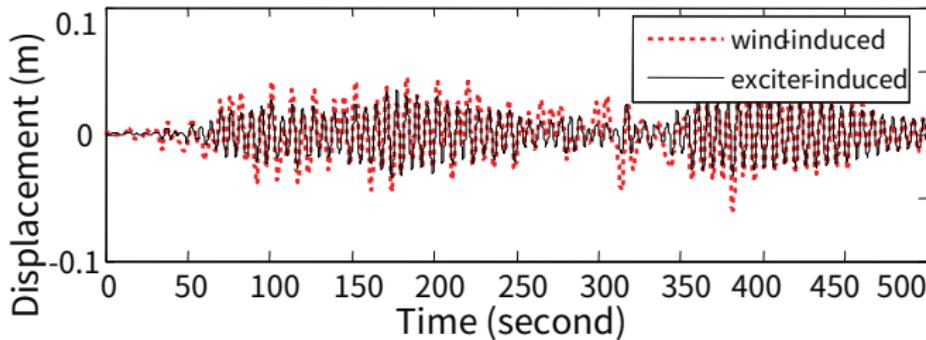
(a) 50th story acceleration response



DESIGN OF AN ACTUATOR FOR SIMULATING WIND RESPONSE



(a) 30th story acceleration response



DESIGN OF AN ACTUATOR FOR SIMULATING WIND RESPONSE

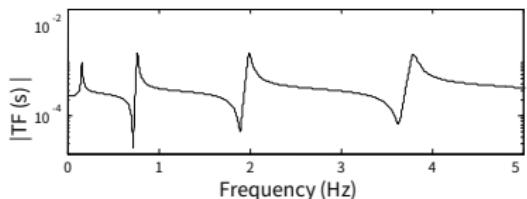
ATMD Excitation

$$\mathbf{M}\mathbf{x} + \mathbf{C}\mathbf{x} + \mathbf{K}\mathbf{x} + \mathbf{H}u = \eta\mathbf{W} \quad (9)$$

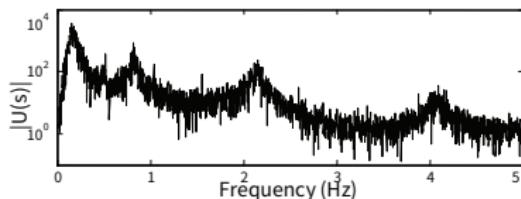
Equation of motion of the building

$$\begin{bmatrix} \mathbf{M}_s & 0 \\ \mathbf{0} & m_t \end{bmatrix} \begin{Bmatrix} \mathbf{x}_s \\ \ddot{x}_t \end{Bmatrix} + \begin{bmatrix} \mathbf{C}_s + c_t \mathbf{B}_t \mathbf{B}_t^\top & -c_t \mathbf{B}_t \\ -c_t \mathbf{B}_t^\top & c_t \end{bmatrix} \begin{Bmatrix} \mathbf{x}_s \\ \dot{x}_t \end{Bmatrix} + \begin{bmatrix} \mathbf{K}_s + k_t \mathbf{B}_t \mathbf{B}_t^\top & -k_t \mathbf{B}_t \\ -k_t \mathbf{B}_t^\top & k_t \end{bmatrix} \begin{Bmatrix} \mathbf{x}_s \\ x_t \end{Bmatrix} = \begin{bmatrix} -\mathbf{B}_t \\ 1 \end{bmatrix} u \quad (10)$$

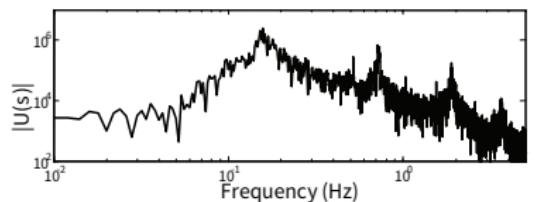
DESIGN OF AN ACTUATOR FOR SIMULATING WIND RESPONSE



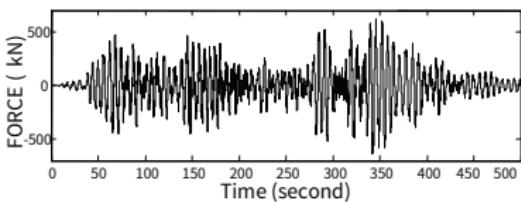
(a) Transfer function of ATMD induced structure



(b) Frequency response of ATMD acceleration



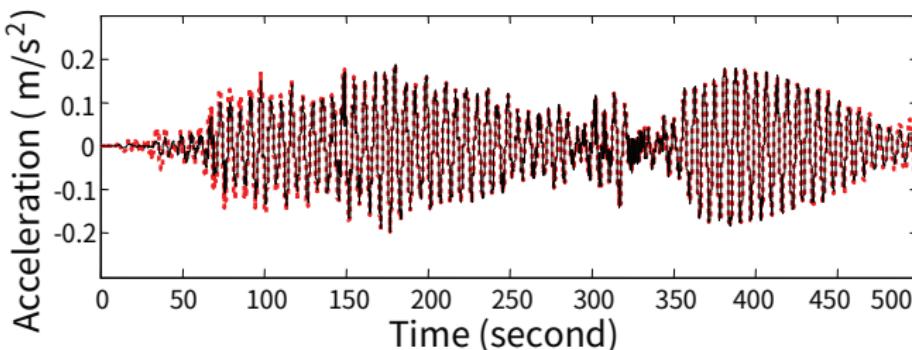
(c) Frequency response of ATMD actuator force



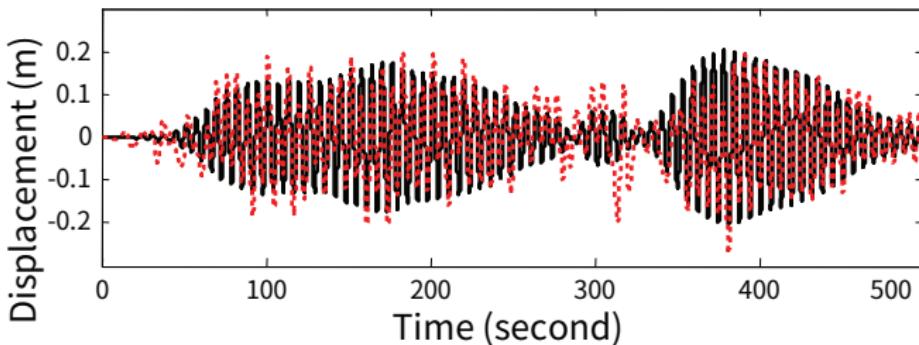
(d) Time history of ATMD actuator force

ATMD Excitation.

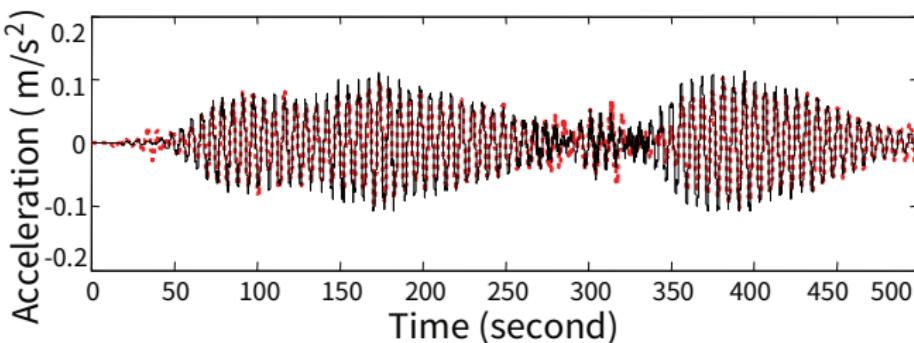
DESIGN OF AN ACTUATOR FOR SIMULATING WIND RESPONSE



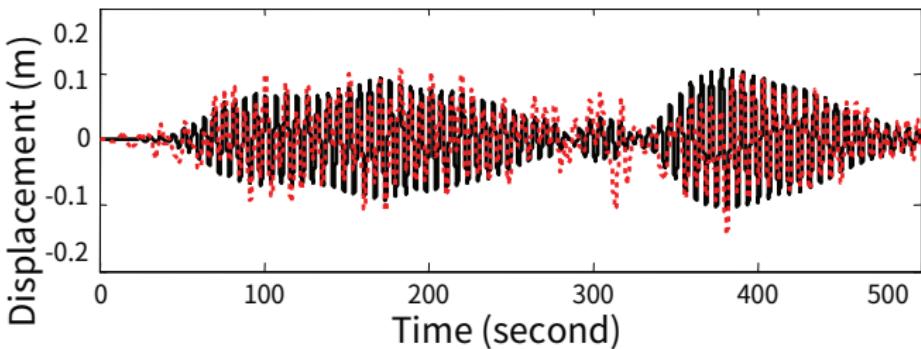
(a) 76th story acceleration response



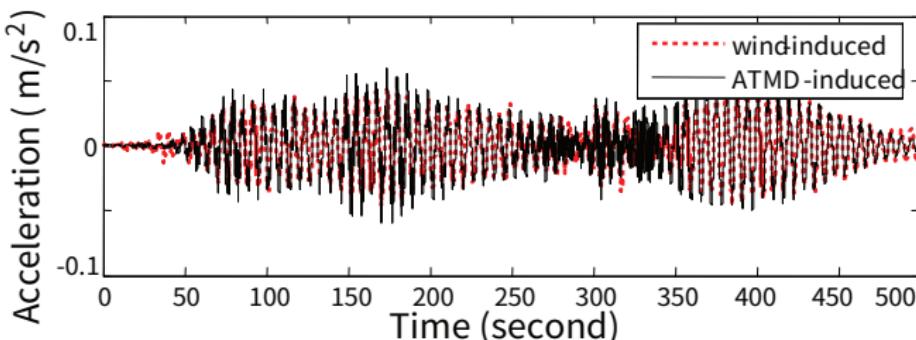
DESIGN OF AN ACTUATOR FOR SIMULATING WIND RESPONSE



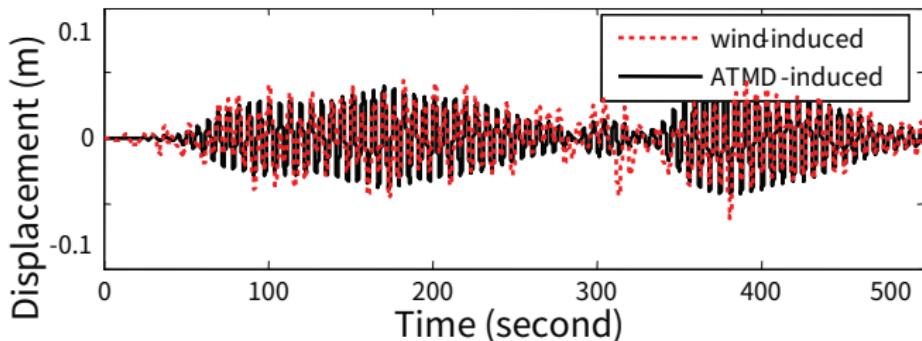
(a) 50th story acceleration response



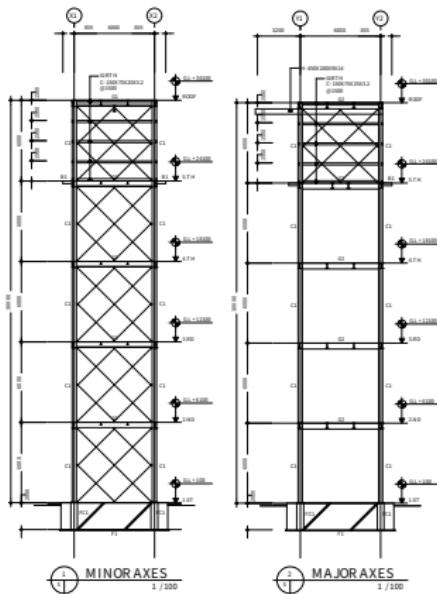
DESIGN OF AN ACTUATOR FOR SIMULATING WIND RESPONSE



(a) 30th story acceleration response



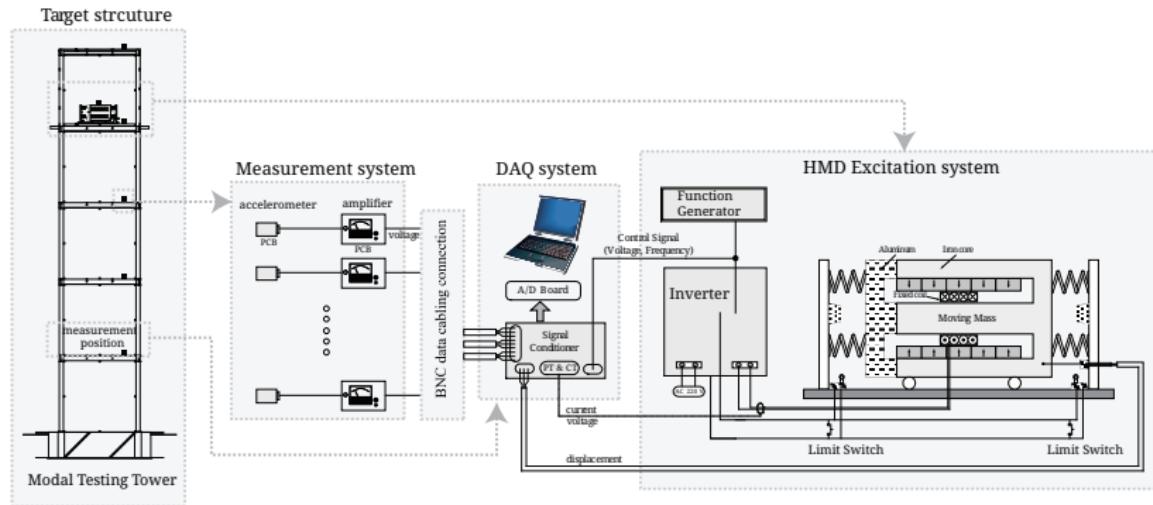
FORCED VIBRATION TEST OF REAL-SCALED BUILDING



(a) minor axis (b) major axis

Elevation view of the target structure.

FORCED VIBRATION TEST OF REAL-SCALED BUILDING



Schematic diagram of the field measurement, data acquisition and exciting system.

FORCED VIBRATION TEST OF REAL-SCALED BUILDING



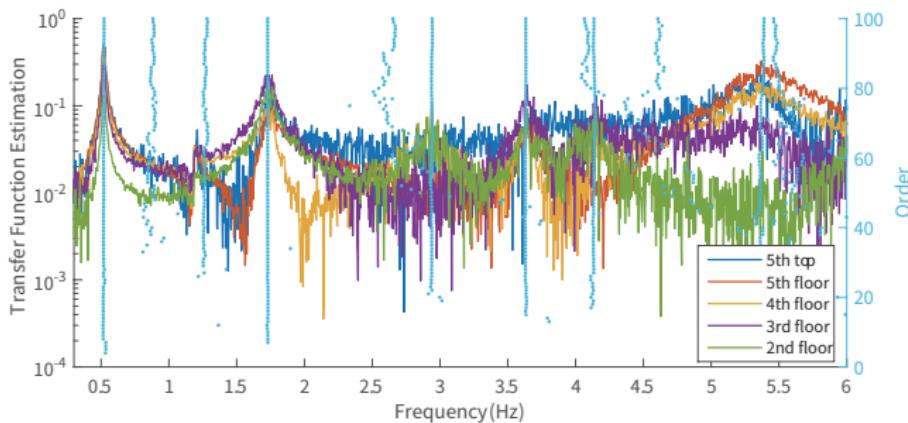
(a) The measurement and data acquisition system



(b) The accelerometer installation

Installation pictures of the measurement, data acquisition and exciting system.

FORCED VIBRATION TEST OF REAL-SCALED BUILDING



The transfer function from the absolute acceleration of the HMD to those of the structure.

Modes	Frequency (Hz) & COV (%)	Damping ratio (%) & COV (%)
1	0.52(1.82)	1.46(14.42)
2	1.73(0.13)	2.71(9.40)
3	2.94(0.10)	3.54(1.93)
4	4.14(0.08)	1.72(1.70)
5	5.36(0.23)	3.84(3.56)

FORCED VIBRATION TEST OF REAL-SCALED BUILDING

$$\mathbf{K}\Phi = \mathbf{M}_a\Phi\Lambda, \Phi^\top \mathbf{M}_a\Phi = \mathbf{I} \quad (11)$$

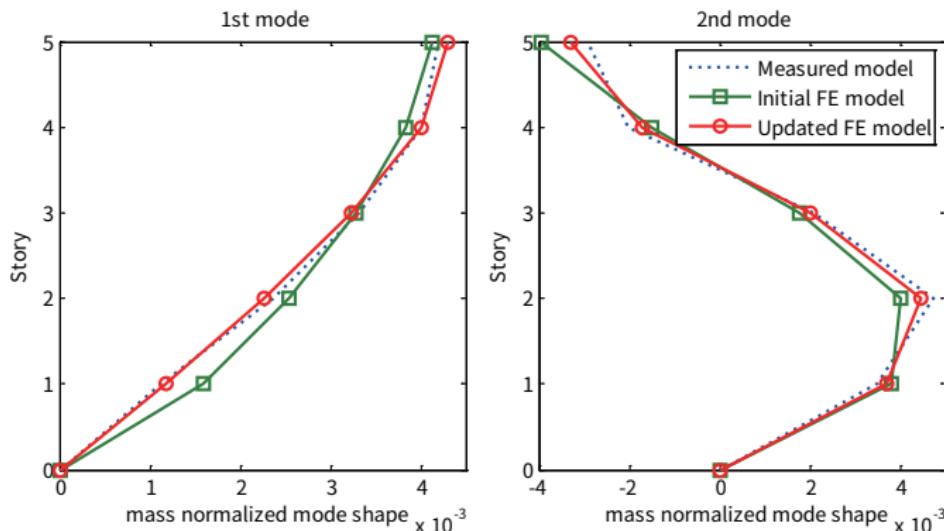
$$\mathbf{K}^\top = \mathbf{K} \quad (12)$$

$$J = \frac{1}{2} \left\| \mathbf{N}^{-1} (\mathbf{K} - \mathbf{K}_a)^{-1} \right\| \quad (13)$$

$$\Phi = \Phi_m \left[\Phi_m^\top \mathbf{M}_a \Phi_m \right]^{-1/2} \quad (14)$$

$$\begin{aligned} \mathbf{K} = & \mathbf{K}_a - \mathbf{K}_a \Phi \Phi^\top \mathbf{M}_a - \mathbf{M}_a \Phi \Phi^\top \mathbf{K}_a \\ & + \mathbf{M}_a \Phi \Phi^\top \mathbf{K}_a \Phi \Phi^\top \mathbf{M}_a + \mathbf{M}_a \Phi \Lambda \Phi^\top \mathbf{M}_a \end{aligned} \quad (15)$$

FORCED VIBRATION TEST OF REAL-SCALED BUILDING



The mode shape comparison of initial, the measured and the updated FE models.

FORCED VIBRATION TEST OF REAL-SCALED BUILDING

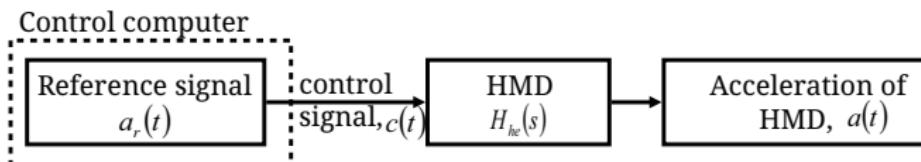
$$\begin{aligned}\underline{\mathbf{z}} &= \mathbf{A}\mathbf{z} + \mathbf{B}_b \ddot{u}_b + \mathbf{B}_h \ddot{u}_h \\ \mathbf{y} &= \mathbf{C}\mathbf{z} + \mathbf{D}_b \ddot{u}_b + \mathbf{D}_h \ddot{u}_h\end{aligned}\quad (16)$$

$$\begin{aligned}\mathbf{T}_h &= \mathbf{Y}_h(s) \mathbf{U}_h(s)^{-1} = \mathbf{C}(s\mathbf{I} - \mathbf{A})^{-1} \mathbf{B}_h + \mathbf{D}_h \\ \mathbf{T}_b &= \mathbf{Y}_b(s) \mathbf{U}_b(s)^{-1} = \mathbf{C}(s\mathbf{I} - \mathbf{A})^{-1} \mathbf{B}_b\end{aligned}\quad (17)$$

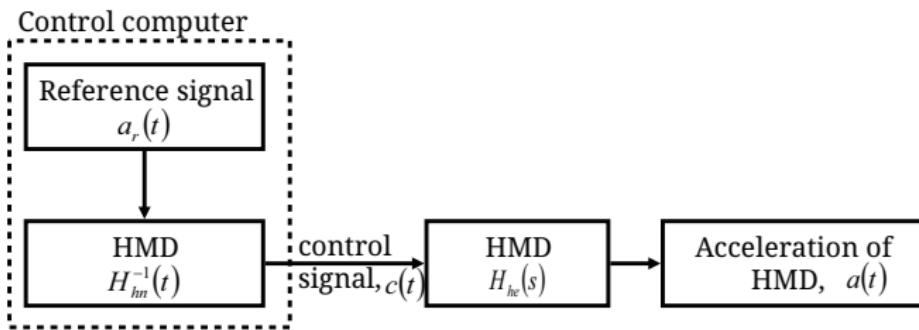
$$\mathbf{U}_h(s) = \mathbf{T}_h^{-1} \mathbf{Y}_h(s) = \mathbf{T}_h^{-1} \mathbf{Y}_b(s) = \mathbf{T}_h^{-1} \mathbf{T}_b \mathbf{U}_b(s) \quad (18)$$

$$\hat{U}_h(s) = \hat{T}_h^{-1} \hat{Y}_h(s) = \hat{T}_h^{-1} \hat{Y}_b(s) = \hat{T}_h^{-1} \hat{T}_b \hat{U}_b(s) \quad (19)$$

FORCED VIBRATION TEST OF REAL-SCALED BUILDING



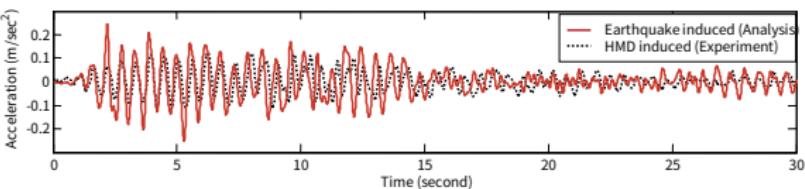
(a) Definition of the transfer function of the HMD



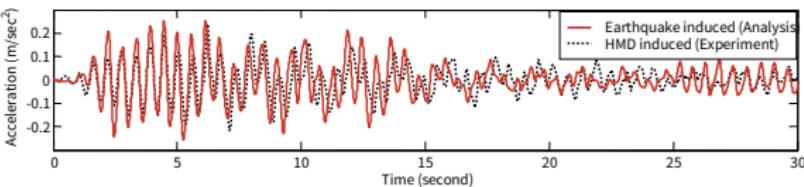
(b) Compensation the dynamics of HMD using the inverse transfer function

Schematic diagram of the HMD controller.

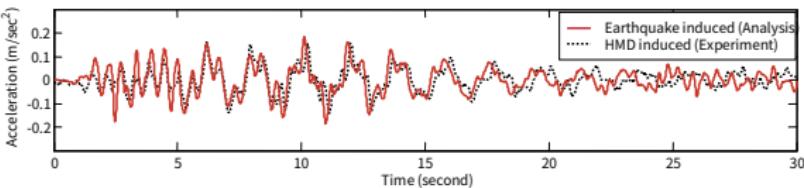
FORCED VIBRATION TEST OF REAL-SCALED BUILDING



(a) 1st floor acceleration

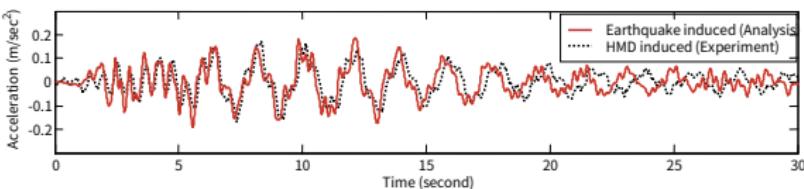


(b) 2nd floor acceleration

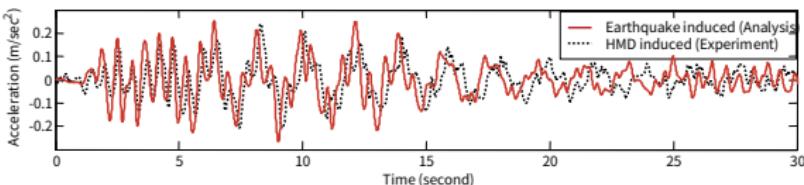


(c) 3rd floor acceleration

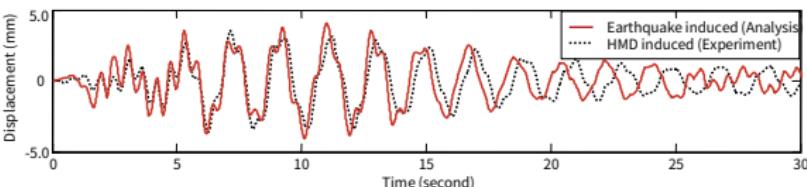
FORCED VIBRATION TEST OF REAL-SCALED BUILDING



(d) 4th floor acceleration



(e) 5th floor acceleration



(f) 1st floor displacement

FULL SCALED MR-DAMPER

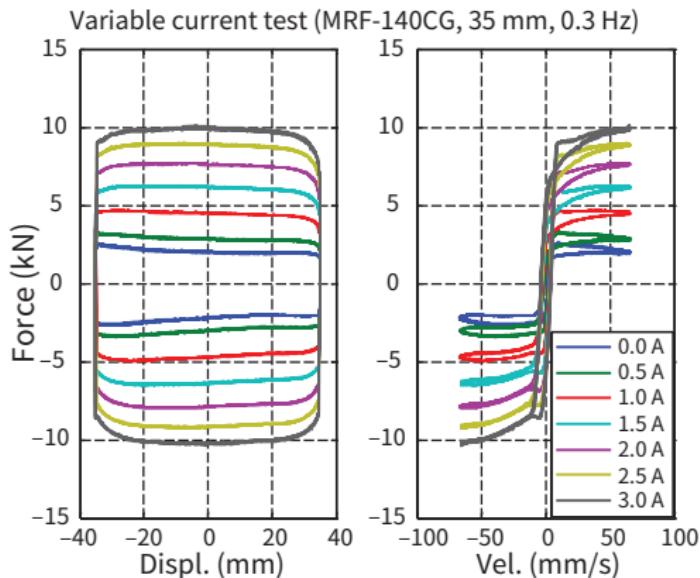


(g) Components of full scaled MR Damper



(h) Manufactured full scaled MR Damper

FULL SCALED MR-DAMPER



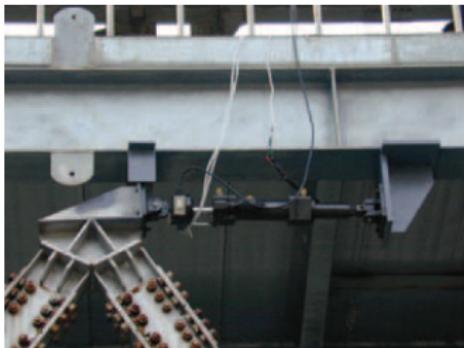
Manufactured MR damper with capacity of 1.0 ton

FULL STATE VARIABLE FEEDBACK FOR SEMI-ACTIVE ALGORITHMS

$$P = \lim_{t \rightarrow \infty} E\left(\left[\mathbf{x} - \hat{\mathbf{x}}\right] \left[\mathbf{x} - \hat{\mathbf{x}}\right]^\top\right) \quad (20)$$

$$\begin{aligned} \hat{\mathbf{x}} &= (\mathbf{A} - \mathbf{LC}) \hat{\mathbf{x}} + [\mathbf{L} \quad \mathbf{B} - \mathbf{LD}] \begin{Bmatrix} \mathbf{y} \\ \mathbf{u} \end{Bmatrix} \\ \begin{Bmatrix} \hat{\mathbf{y}} \\ \hat{\mathbf{x}} \end{Bmatrix} &= \begin{bmatrix} \mathbf{C} \\ \mathbf{I} \end{bmatrix} \hat{\mathbf{x}} + \begin{bmatrix} \mathbf{0} & \mathbf{D} \\ \mathbf{0} & \mathbf{0} \end{bmatrix} \begin{Bmatrix} \mathbf{y} \\ \mathbf{u} \end{Bmatrix} \end{aligned} \quad (21)$$

MR DAMPER TEST



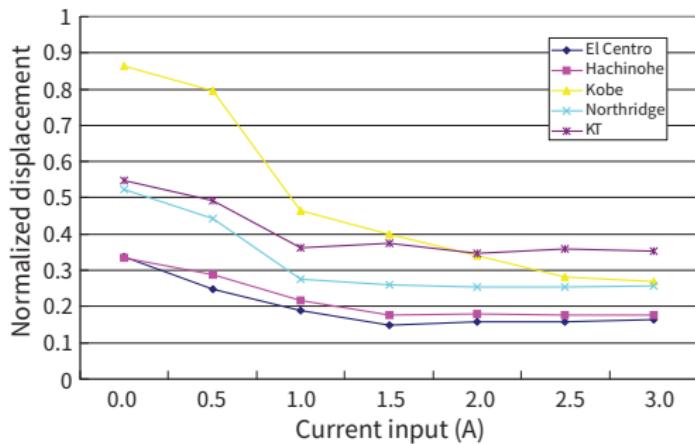
(i) Installation of MR damper and load cell



(j) LVDT type displacement sensor (Midori America LP-19FB)

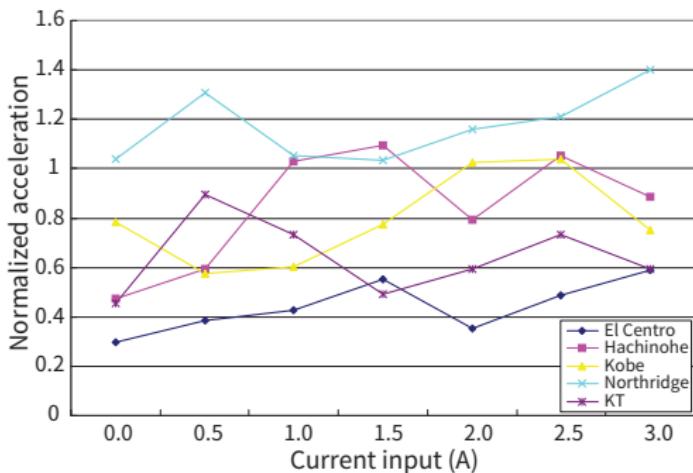
MR damper installation

MR DAMPER OPTIMAL PASSIVE CONTROLLED RESULT



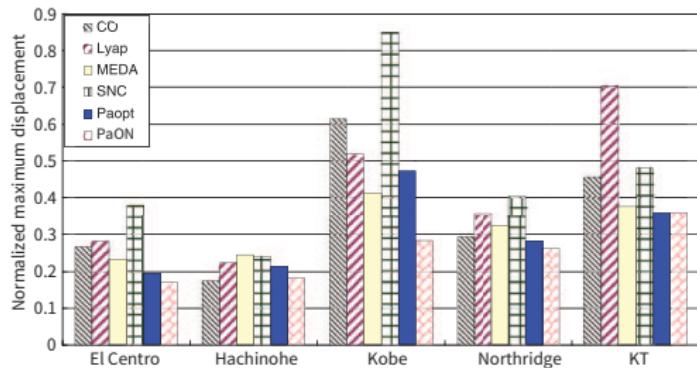
Normalized maximum displacement of passive control cases (first floor).

MR DAMPER OPTIMAL PASSIVE CONTROLLED RESULT



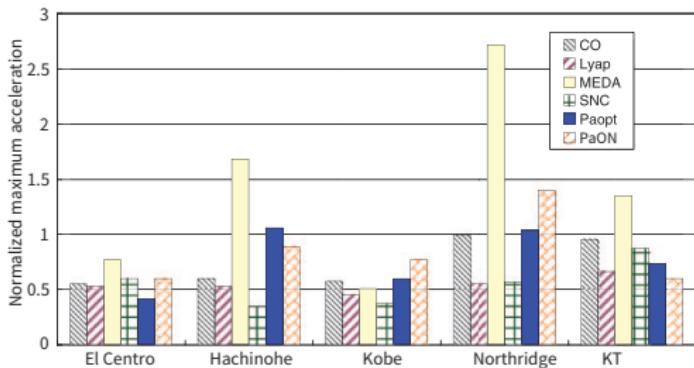
Normalized maximum acceleration of passive control cases.

MR DAMPER SEMI-ACTIVE CONTROLLED RESULT



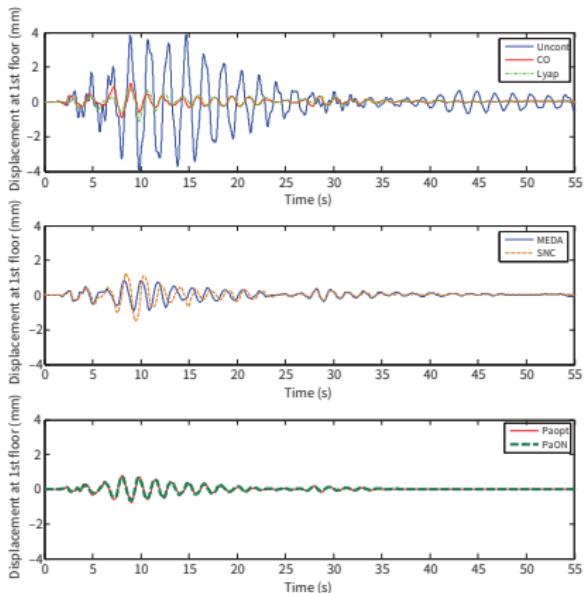
Normalized maximum displacement comparison of MR damper-based control systems.

MR DAMPER SEMI-ACTIVE CONTROLLED RESULT



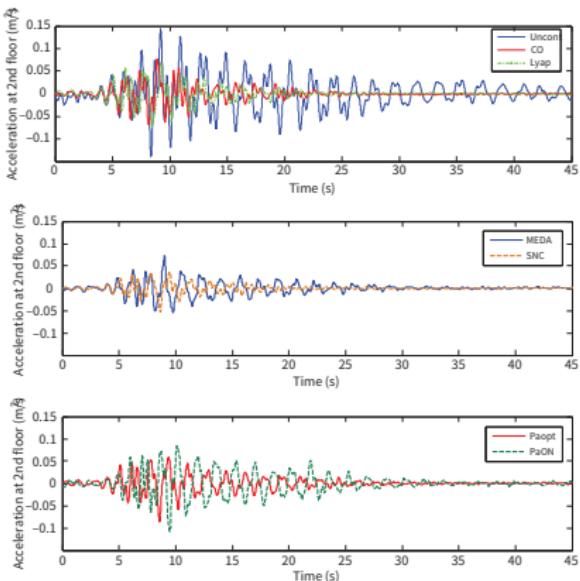
Normalized maximum acceleration comparison of MR damper-based control systems.

MR DAMPER TEST TIME-HISTORY RESULT



Time history responses of displacement at the first floor under the El Centro earthquake.

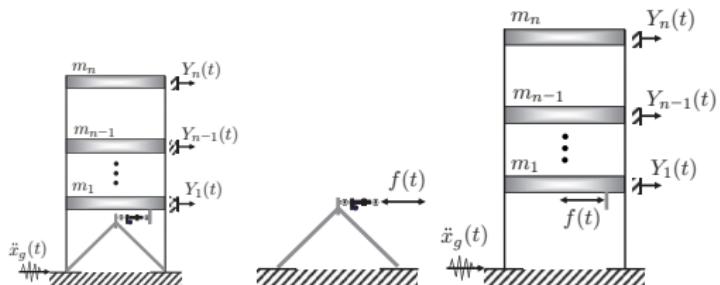
MR DAMPER TEST TIME-HISTORY RESULT



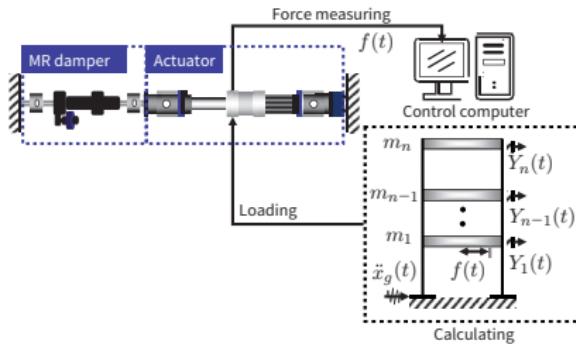
Time history responses of acceleration at the second floor under the Kobe earthquake.

RT-HYTEM WITH MR DAMPER

RT-HYTEM BUILDING STRUCTURE WITH MR DAMPER



(a) structural (b) experimental and numeri-
control system cal substructures



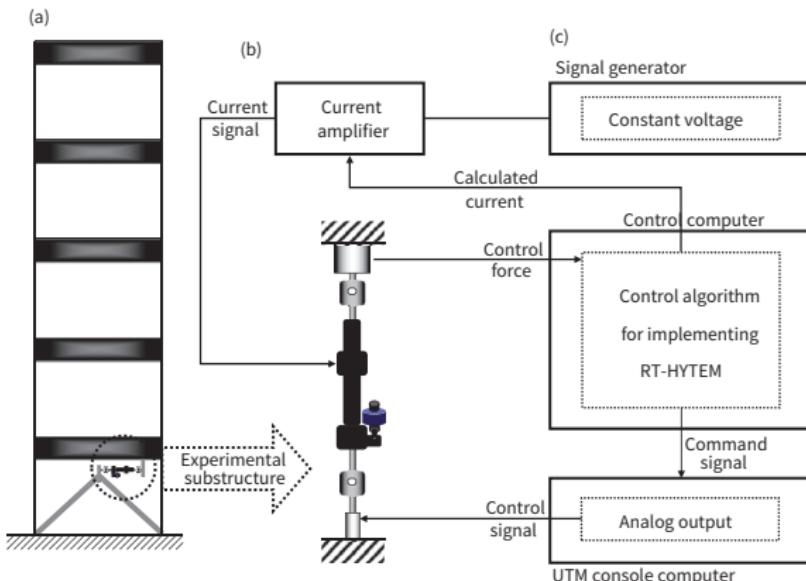
(c) implementation of RT-HYTEM

RT-HYTEM BUILDING STRUCTURE WITH MR DAMPER



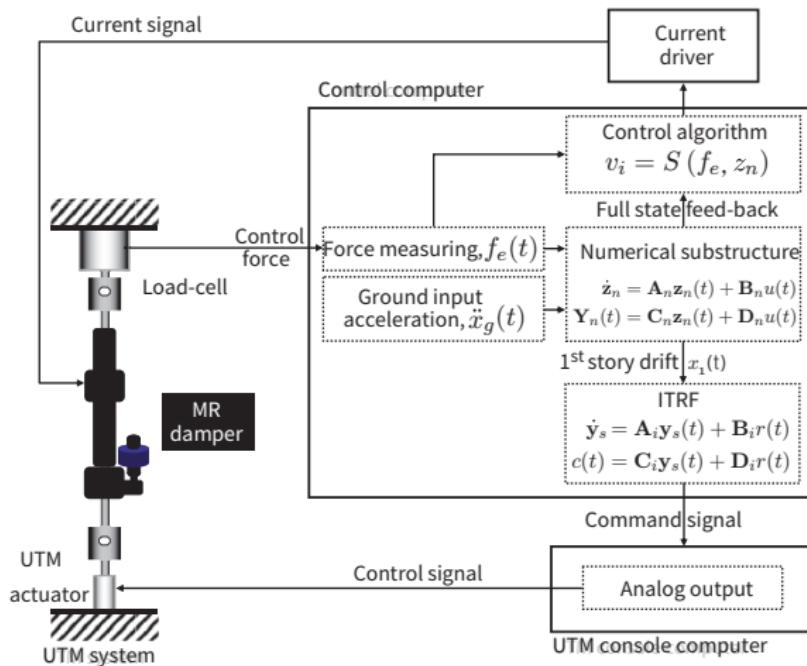
Configuration of experimental system.

RT-HYTEM BUILDING STRUCTURE WITH MR DAMPER



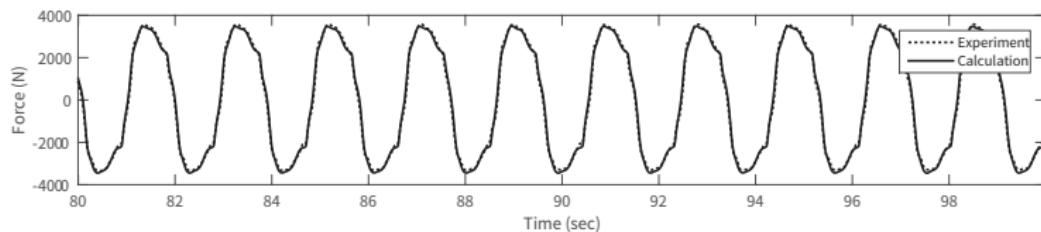
Schematic view of experimental set-up: (a) building model installed with an MR damper, (b) UTM installed MR damper, and (c) experimental instrumentation

RT-HYTEM BUILDING STRUCTURE WITH MR DAMPER

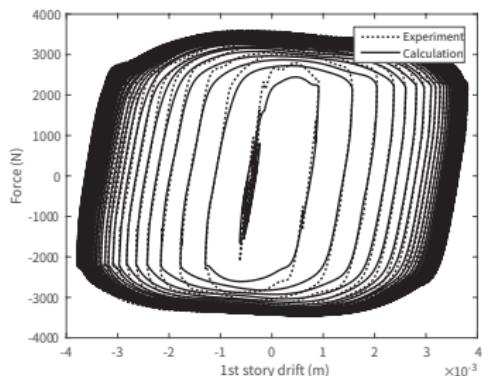


Integrated controller for implementing RTHTM.

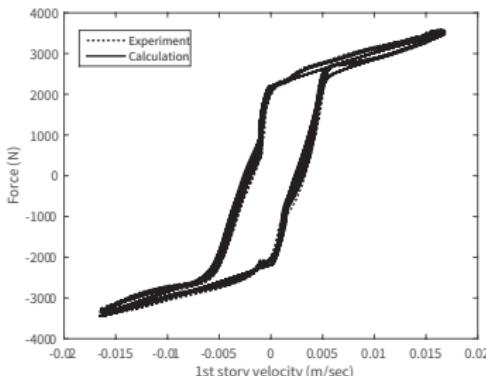
RT-HYTEM BUILDING STRUCTURE WITH MR DAMPER



(a) time history of force

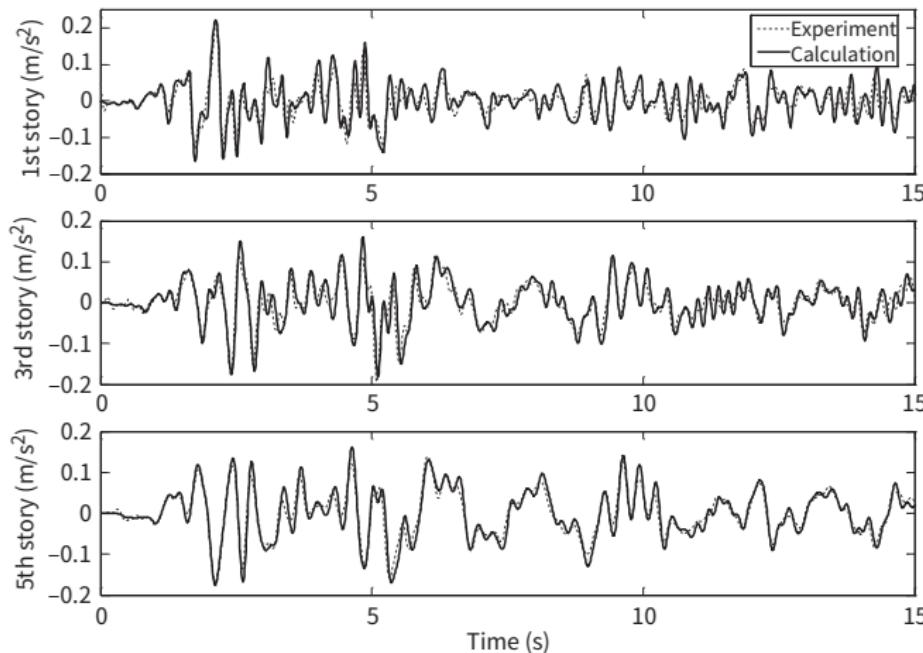


(b) force-displacement relation



(c) force-velocity relation

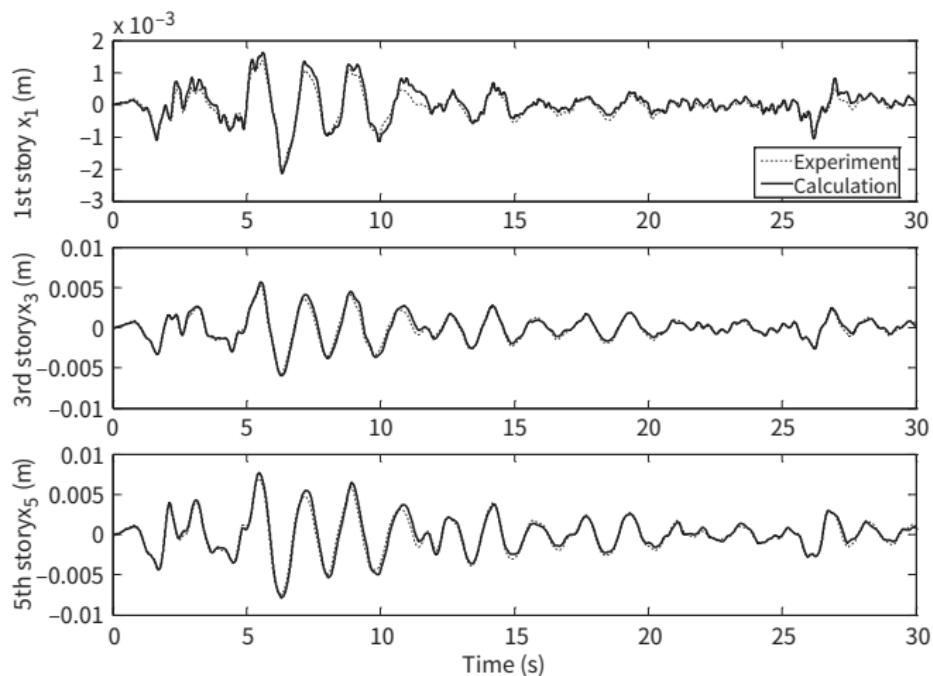
RT-HYTEM BUILDING STRUCTURE WITH MR DAMPER



(a) absolute acceleration responses

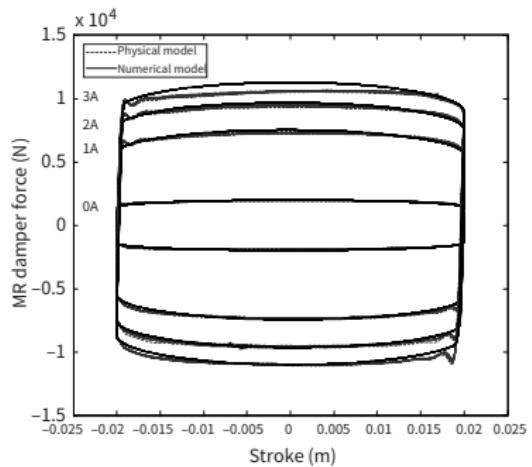
Comparison between calculated and experimentally

RT-HYTEM BUILDING STRUCTURE WITH MR DAMPER

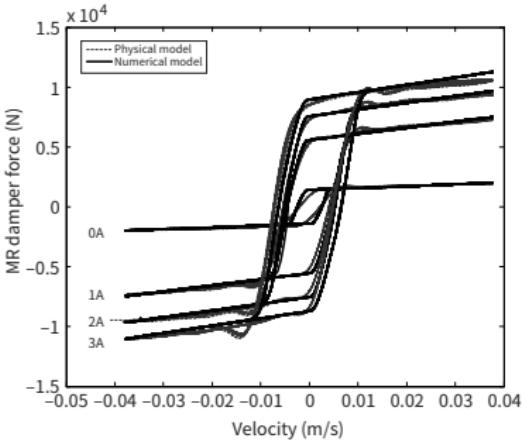


(b) displacement responses

RT-HYTEM BUILDING STRUCTURE WITH MR DAMPER



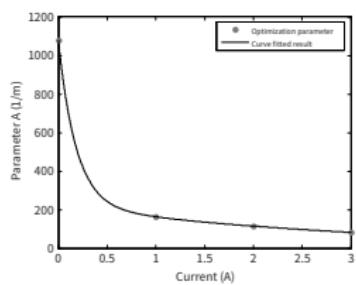
(a) force-displacement relation



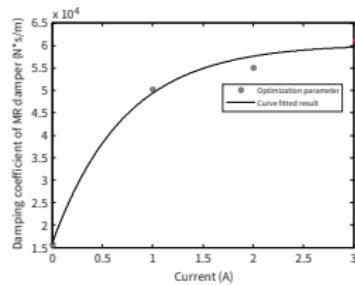
(b) force-velocity relation

Identified Bouc-Wen parameters and the numerical model of an MR damper.

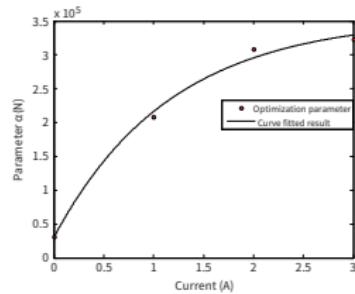
RT-HYTEM BUILDING STRUCTURE WITH MR DAMPER



(a) shape parameter

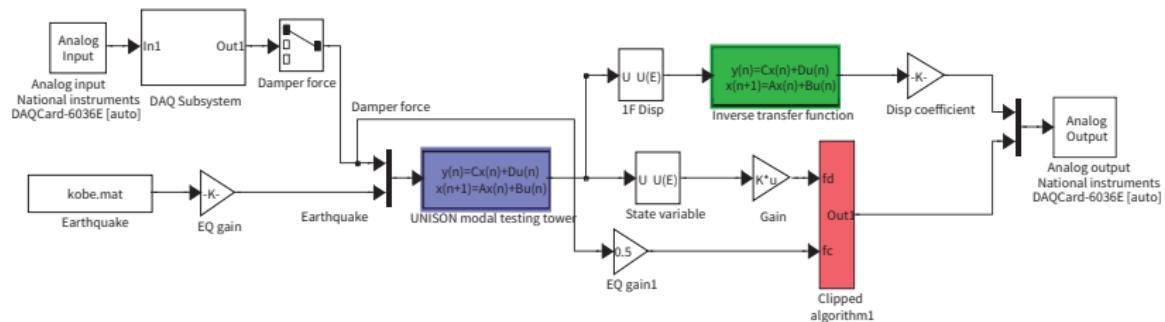


(b) damping coefficient of an MR damper

(c) shape parameter α

Identified Bouc-Wen parameters and the numerical model of an MR damper.

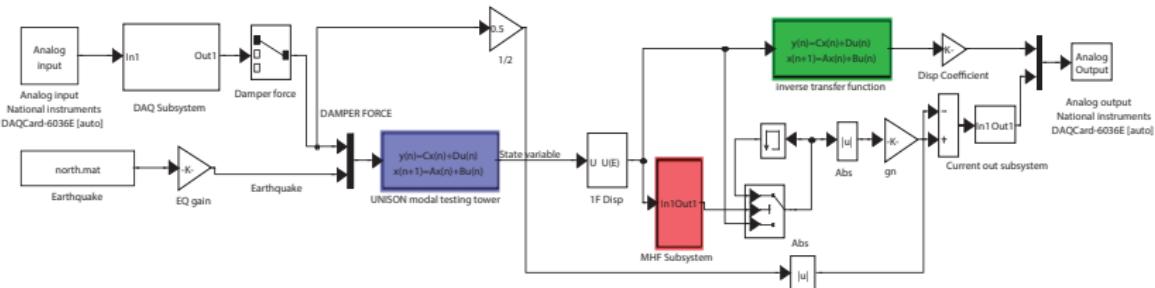
RT-HYTEM BUILDING STRUCTURE WITH MR DAMPER



Clipped-optimal and RT-HYTEM integrated controller.

$$v_i = V_{\max} H(\{f_{c_i} - f_i\} f_i) \quad (22)$$

RT-HYTEM BUILDING STRUCTURE WITH MR DAMPER



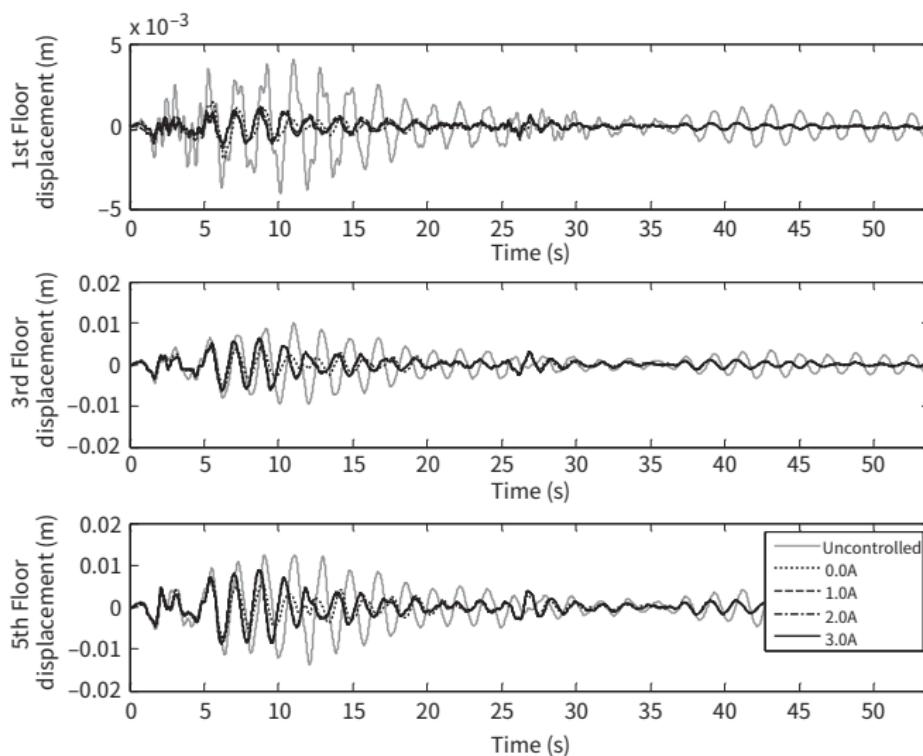
MHF and RT-HYTEM integrated controller.

$$N_i(t) = g_i |P[\Delta_i(t)]| \quad (23)$$

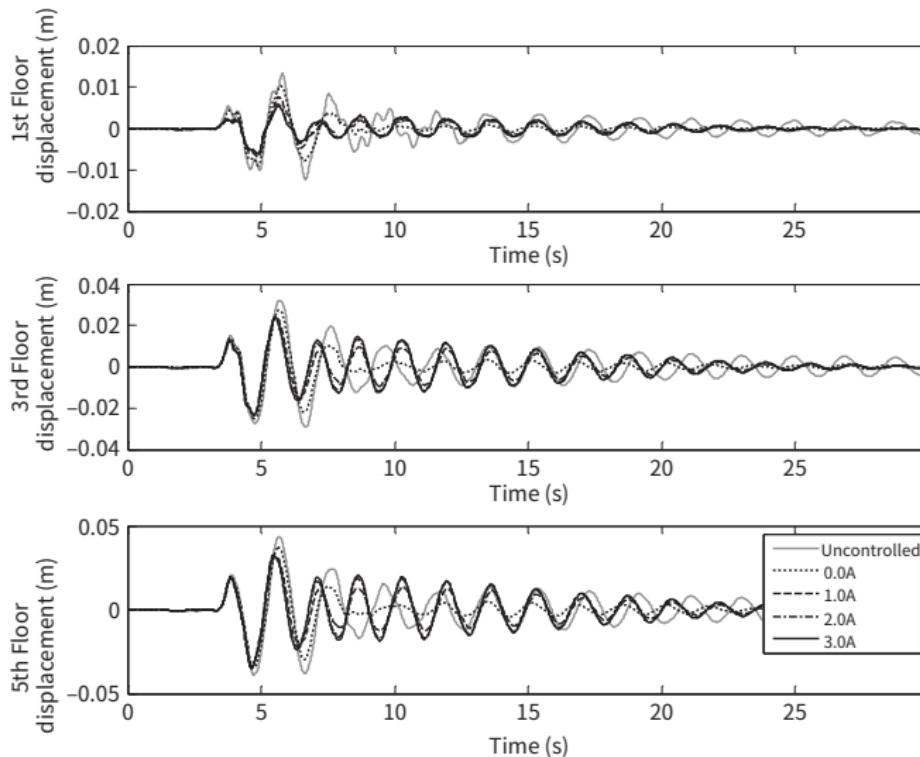
$$f_{n_i} = \mu g_i |P[\Delta_i(t)]| = g_{n_i} |P[\Delta_i(t)]| \quad (24)$$

$$v_i = V_{\max} H(f_{n_i} - |f_i|) \quad (25)$$

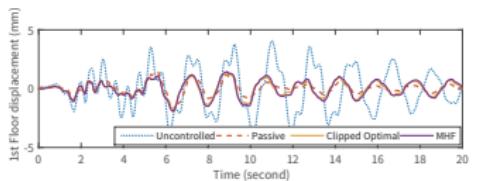
RT-HYTEM BUILDING STRUCTURE WITH MR DAMPER



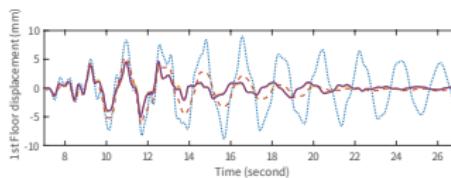
RT-HYTEM BUILDING STRUCTURE WITH MR DAMPER



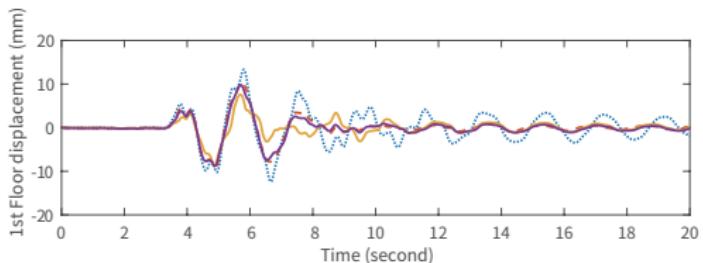
RT-HYTEM BUILDING STRUCTURE WITH MR DAMPER



(a) El Centro earthquake



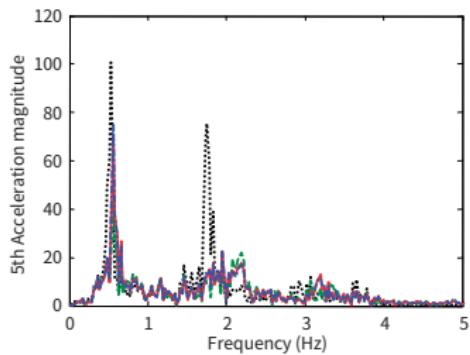
(b) Kobe earthquake



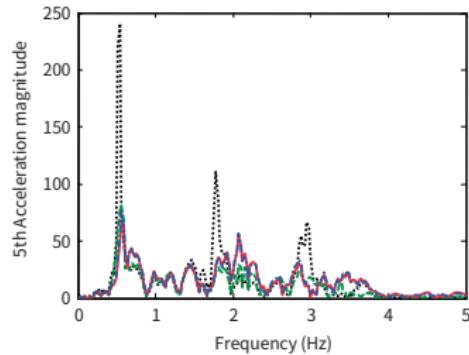
(c) Northridge earthquake

Passive and semi-active RT-HYTEM experimental results(time domain).

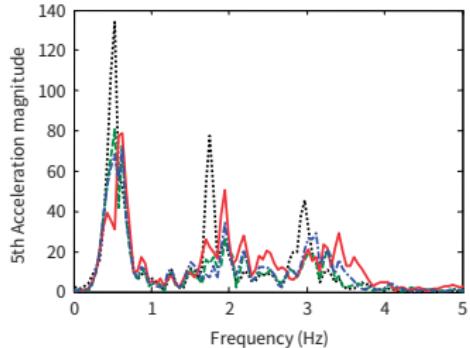
RT-HYTEM BUILDING STRUCTURE WITH MR DAMPER



(a) El Centro earthquake



(b) Kobe earthquake



Uncontrolled
Passive control
Clipped optimal
Modulated homogenous friction

CONCLUSION

CONCLUSION

- 실시간 하이브리드 실험법과 동적 응답을 구현하는 가진시스템 설계법을 제안
- 부분구조 실험법을 수행하였으며, TLD와 TLCD 그리고 새로운 형태의 2방향 제어장치 TLMD 하이브리드 실험과 일반적인 진동대 실험을 비교
- 풍하중 구현을 위해 76층 벤치마크 건물을 목표로 수치해석적으로 검증
- 실물규모 5층 건물에서 유사 지진응답을 구현하는 실험을 수행
- 실물규모 5층 건물에 1톤급 MR감쇠기를 설치하고 Passive 및 준능동 알고리즘을 적용하여 유사지진 응답 실험을 수행
- 1톤급 실물크기의 MR감쇠기를 UTM에 장착하여 실시간 하이브리드 실험법으로 제어성능을 검증

수정 사항

- Abstract와 Introduction 수정 중, 3장 4장을 다시 구성 중.
- 민경원 교수님 : Real-time Hybrid Testing Method, Real-time Substructure Test, Real-time Hybrid Shaking Table Test Method -> 용어 통일 (수정 중)
- 정란 교수님 : Real-time Hybrid Testing Method라는 용어를 쓰는지, Hybrid 라는 용어를 쓰는것이 맞는지 고려바람 -> 많은 문헌에서 실험 모델과 수치 해석 모델을 동시에 하는 Hybrid 실험을 언급함, Abstract 4장에 대한 설명이 이해하기 어려움 수정 바람 (수정 완료)
- 이상현 교수님 : 논문 제목 수정 (수정 완료), 용어 약자를 풀어쓰는 구문이 반복됨 (수정 중)
- 김준희 교수님 : Introduction에 전체 논문 구성을 설명하는 것이 중요, 3장 MR damper 실험을 했기 때문에 4장에서 RT-HYTEM이 다시 나오면 3장과 4장을 합치는 방법을 제안함.