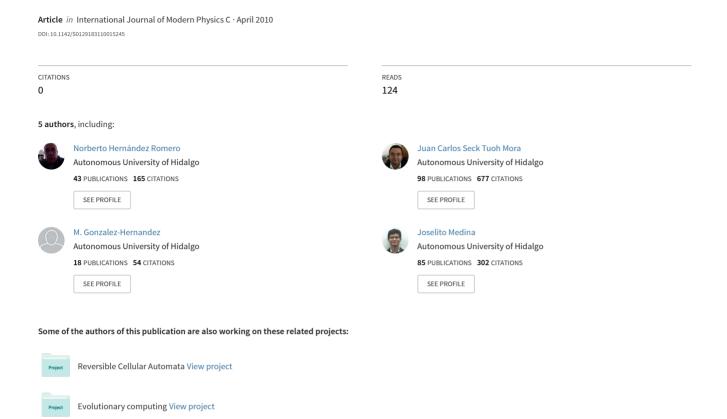
Modeling a Nonlinear Liquid Level System by Cellular Neural Networks



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MODELING A NONLINEAR LIQUID LEVEL SYSTEM BY CELLULAR NEURAL NETWORKS

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This paper presents the analogue simulation of a nonlinear liquid level system composed by two tanks; the system is controlled using the methodology of exact linearization via state feedback by cellular neural networks (CNNs). The relevance of this manuscript is to show how a block diagram representing the analogue modeling and control of a nonlinear dynamical system, can be implemented and regulated by CNNs, whose cells may contain numerical values or arithmetic and control operations. In this way the dynamical system is modeled by a set of local-interacting elements without need of a central supervisor.

Keywords: Cellular neural networks; nonlinear systems; block diagrams.

PACS Nos.: 05.10.-a, 07.05.Tp, 87.16.-A, 87.18.Sn.

1. Introduction

In general, it is difficult and sometimes impossible to find an analytical (or even a numerical) solution for nonlinear systems modeled by differential equations in order to predict their dynamical behavior; moreover, this one often has a more complicated form when it is desired to include a nonlinear control. This situation yields the study of unconventional paradigms such as analogue computation for solving this kind of problems. This paper presents the application of cellular neural networks

(CNNs) for simulating a block diagram representing the analogue computation of a nonlinear liquid level system, including a closed-loop feedback to achieve a complete control of the system.

CNNs are hybrid models between artificial neural networks and cellular automata with continuous values, specified by a parallel interaction of cells where each has a simple behavior conditioned by the state of the neighboring cells. They were firstly conceived by Chua for image processing and pattern recognition.^{1,2} CNNs have been widely investigated because they can produce complex behaviors in a natural way and have been used in an extensive number of applications such as signal processing,³ simulation and control of chaotic systems,^{4,5} circuit design,⁶ robotic navigation control,⁷ and modeling brain activity,⁸ among others.

CNNs are appropriate for achieving analogue computation because they can easily simulate the behavior of block diagrams, which are tools classically employed in every engineering field for representing real dynamical systems by means of an analogue language. The original part of this paper is the implementation of a CNN for simulating block diagrams performing the analogue computation of a nonlinear liquid level system composed by two non-coupled tanks. This system is described by two nonlinear differential equations whose dynamics is regulated by a feedback control applying the exact linearization technique. ^{9,10} This paper represents an advance from previous results in Ref. 11 about modeling linear systems.

The rest of the paper is organized as follows: Section 2 presents the analogue modeling and control of the liquid level system by block diagrams. Section 3 explains the implementation, simulation and control of the liquid level system by CNNs. The final section gives the concluding remarks of the paper.

2. Modeling and Control of a Liquid Level System

The system examined is composed by two non-coupled tanks (see Fig. 1) where:

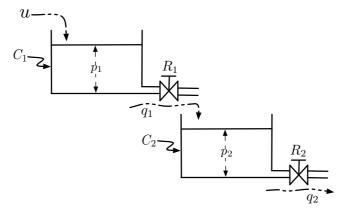


Fig. 1. Liquid level system formed by two non-coupled tanks.

- u is the input flow in tank 1.
- p_i is the hydrostatic pressure in tank i.
- R_i is the resistance in valve i.
- C_i is the capacitance in tank i.
- q_i is the output liquid flow from tank i.

The nonlinearity of the system is given by the turbulent flow in the tanks which is generally modeled by:

$$q_i = R_i \sqrt{p_i} \,. \tag{1}$$

The volume of liquid in both tanks in a given time interval is determined by:

$$C_1 dp_1 = (u - q_1)dt$$
, $C_2 dp_2 = (q_1 - q_2)dt$. (2)

It is desired to control p_2 applying an action control in the input flow u; hence it is suitable to let Eq. (2) be characterized in function of the hydrostatic pressure. Taking unitary values for C_i and R_i we have that $q_i = \sqrt{p_i}$, in this way:

$$\frac{dp_1}{dt} = u - \sqrt{p_1}, \quad \frac{dp_2}{dt} = \sqrt{p_1} - \sqrt{p_2}.$$
(3)

Taking the standard notation in state variables $(x_1 = p_1 \text{ and } x_2 = p_2)$ the output y of the system is generated by x_2 . This dynamical system can be simulated by analogue computation using block diagrams (see Ref. 11); the diagram associated to this particular case is presented in Fig. 2.

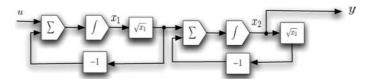


Fig. 2. Block diagram modeling the liquid level system.

It is described in Ref. 9 the exact linearization technique for this type of systems; briefly, this technique consists of expressing the nonlinear system as a linear one by means of a coordinate transformation, applying then a classical linear control and finally converting the result into a nonlinear control law. The coordinate transformation is defined as follows:

$$q_1 = x_2 q_2 = \sqrt{x_1} - \sqrt{x_2}$$
 (4)

and the nonlinear control law is determined by:

$$u = \frac{x_1}{\sqrt{x_2}} + 2\sqrt{x_1}v. (5)$$

The coordinate transformation in Eq. (4) yields that the system can be treated as a linear one which is controlled by state feedback and pole placement methods.

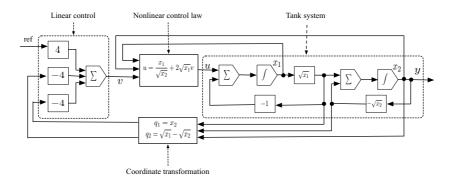


Fig. 3. Liquid level system controlled by the exact linearization technique.

The previous technique is implemented in analogue computation utilizing the block diagram in Fig. 3; in this one, the different parts of the system (liquid level system, coordinate transformation, nonlinear control law, linear control and state feedback) are performed in analogue way by blocks based on simple arithmetic operations; these blocks are connected by signals carrying out the information for solving the system.

It is evident that the analogue computation outlined by the block diagram in Fig. 3 is conformed by a set of locally-interacting simple parts, this agrees with the nature of a CNN, so it is possible for an implementation of the system in this environment.

3. Control of the Liquid Level System by CNNs

This paper applies the definition of one-dimensional CNNs based on a previous model presented in Ref. 11, where the set of states contains both real values and arithmetic operators; besides taking neighborhoods of different sizes in order to simulate the corresponding analogue computation.

A CNN consists of a set of states \mathcal{S} , where the set of finite sequences of states is described by \mathcal{S}^* . For every $w \in \mathcal{S}^*$, let m_w be the number of states in w. These states are indexed from left to right, starting from position 0, thus w_i is the state at position i mod m_w and $w_{[i,\ldots,j]}$ is the block of states from i to j. The CNN has an initial condition (or configuration) $c^0 \in \mathcal{S}^*$; the superscript indicates the current time and will be omitted when it is understood. Let $\Phi \subset \mathcal{S}^*$ be a set of neighborhoods, where for every $w \in \Phi$ there is a mapping or evolution rule $\phi(w) = a \in \mathcal{S}$ executing a set of logical and arithmetic operations when the neighborhood appears in the current configuration. If $c_{[i,\ldots,j]}^t = w \in \Phi$ then $c_j^{t+1} = \phi(w)$; otherwise $c_j^{t+1} = c_j^t$.

Thus ϕ yields a new configuration c^{t+1} ; periodic boundary conditions are applied to have complete neighborhoods for all the states in the configuration. We are using neighborhoods with right-sided evolutions for producing a shift of the information from left to right during the dynamics of the CNN.

For the nonlinear liquid level system, the associated block diagram has four arithmetic operators: sums, integrators, square roots, and products by constant values. They are executed using real values, so some cells of the CNN will keep real states described by $v \in \mathbb{R}$ and the previous operations shall be implemented by action states with some particular properties λ defining the way in which the operations are executed to implement the block diagram.

With states in Table 1, Eq. (6) performs an integration using Euler's method.^a

$$v_1 I v_2 C S v_3$$
. (6)

In Eq. (6) state v_2 keeps the product of v_1 by an integration step 1; this result is accumulated in v_3 by CS after a predefined number of iterations. In order to model the system described by the block diagram in Fig. 3, this one is divided in four parts: liquid level system, coordinate transformation, nonlinear control law and linear control.

Let us take first the liquid level system in Fig. 2, all its arithmetic operators can be implemented using the action states in Table 1; with them, an initial configuration c^0 is defined in Fig. 4 showing how the block diagram is implemented.

The neighborhoods required for determining this configuration are in Table 2.

Operation	Symbol	λ_1	λ_2	Neighborhood	Evolution			
Square Root	SR	NA	NA	$c_{i-1}\mathrm{SR}_i c_{i+1}$	$c_{i+1} = \sqrt{c_{i-1}}$			
Multiplier	I	$r \in \mathbb{R}$	$m \in \mathbb{Z}$	$c_{i-m}\cdots I_i c_{i+1}$	$c_{i+1} = c_{i-m} * r$			
Copy	$^{\mathrm{C}}$	$m\in \mathbb{Z}$	NA	$c_{i-m}\cdots C_i c_{i+1}$	$c_{i+1} = c_{i-m}$			
Product	PR	$m_1 \in \mathbb{Z}$	$m_2 \in \mathbb{Z}$	$c_{i-m_2}\cdots c_{i-m_1}\cdots P_i c_{i+1}$	$c_{i+1} = c_{i-m_1} * c_{i-m_2}$			
Inverse Product	P^*	$m_1 \in \mathbb{Z}$	$m_2 \in \mathbb{Z}$	$c_{i-m_2}\cdots c_{i-m_1}\cdots P^*_{i}c_{i+1}$	$c_{i+1} = \frac{1}{c_{i-m_1}} * c_{i-m_2}$			
Sum	SU	$m_1 \in \mathbb{Z}$	$m_2\in\mathbb{Z}$	$c_{i-m_2}\cdots c_{i-m_1}\cdots S_i c_{i+1}$	$c_{i+1} = c_{i-m_1} + c_{i-m_2}$			
Conditional Sum	CS	$\min \in \mathbb{Z}$	$\max \in \mathbb{Z}$	$c_{i-1}CS_ic_{i+1}$	if $(\min < \max)$ $\min = \min + 1$ else $\min = 0$ $c_{i+1} = c_{i+1} + c_{i-1}$			

Table 1. Action states for implementing a block diagram.

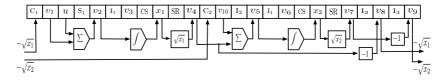


Fig. 4. Initial configuration of the CNN modeling the liquid level system.

^aThis method is chosen for simplicity and gives the sufficient accuracy for this case, of course, more efficient integration methods can be used.

Neighborhood	Evolution	Comment
$v_1 u S_1 v_2$	$v_2 = u + v_1$	$v_1 = -\sqrt{x_1}$, where initially $x_1 = 0$
$v_2 \mathbf{I}_1 v_3 \mathbf{CS} x_1$	$x_1 = x_1 + v_3$ where $v_3 = v_2 * r$	r = 0.1.
$x_1 SR v_4$	$v_4 = \sqrt{x_1}$	
$v_4 \cdots v_{10} S_2 v_5$	$v_5 = v_4 + v_{10}$	$v_{10} = -\sqrt{x_2}$, where initially $x_2 = 0$
$v_5 \mathbf{I}_1 v_6 \mathbf{CS} x_2$	$x_2 = x_2 + v_6$ where $v_6 = v_5 * r$	r = 0.1
$x_2 SRv_7$	$v_7 = \sqrt{x_2}$	
$v_4 \cdots I_2 v_8$	$v_8 = v_4 * r$	r = -1
$v_7 \cdots I_3 v_9$	$v_9 = v_4 * r$	r = -1
$v_8 \cdots C_1 v_1$	$v_1 = v_8$	
$v_9\cdots C_2v_{10}$	$v_{10}=v_9$	

Table 2. Neighborhoods modeling the liquid level system.

								c_9										c_{19}						
C1	0.000	1.000	S1	0.000	H.	0.000	0	0.000	SR	0.000	C2	0.000	52	0.000	H	0.000	0	0.000	SR	0.000	12	0.000	13	0.000
C1	0.000	1.000	S1	1.000	11	0.000	0	0.000	SR	0.000	C2	0.000	S2	0.000	n	0.000	0	0.000	SR	0.000	12	-0.000	13	-0.000
C1	-0.000	1.000	S1	1.000	11	0.100	1	0.000	SR	0.000	C2	-0.000	S2	0.000	it	0.000	0	0.000	SR	0.000	12	-0.000	13	-0.000
C1	-0.000	1.000	S1	1.000	- 11	0.100	. 0	0.100	SR	0.000	C2	-0.000	52	0.000	it	0.000	0	0.000	SR	0.000	12	-0.000	13	-0.000
C1	-0.000	1.000	\$1	1.000	It:	0.100	0	0.100	SR	0.316	C2	-0.000	\$2	0.000	It	0.000	0	0.000	SR	0.000	12	-0.000	13	-0.000
C1	-0.000	1.000	S1	1.000	- 11	0.100	0	0.100	SR	0.316	C2	-0.000	\$2	0.316	. It	0.000	0	0.000	SR	0.000	12	-0.316	13	-0.000
C1	-0.316	1.000	S1	1.000		0.100	.0	0.100	SR	0.316	C2	-0.000	52	0.316	Ħ	0.032	1	0.000	SR	0.000	12	-0.316	13	-0.000
C1	-0.316	1.000	\$1	0.684	10	0.100	0	0.100	SR	0.316	C2	-0.000	52	0.316	it	0.032	0	0.032	SR	0.000	12	-0.316	13	-0.000
C1	-0.316	1.000	\$1	0.684	11	0.068	0	0.100	SR	0.316	C2	-0.000	\$2	0.316	11	0.032	0	0.032	SR	0.178	12	-0.316	13	-0.000
C1	-0.316	1.000	\$1	0.684	It	0.068	0	0.100	SR	0.316	C2	-0.000	\$2	0.316	it	0.032	0	0.032	SR	0.178	12	-0.316	13	-0.178
C1	-0.316	1.000	51	0.584	11	0.068	0	0.100	SR	0,316	C2	-0.178	52	0.316	11	0.032	0	0.032	SR	0.178	12	-0.316	13	-0.178
C1	-0.316	1.000	\$1	0.684	- 15	0.068	0	0.100	SR	0.316	C2	-0.178	52	0.138	11	0.032	0	0.032	SR	0.178	12	-0.316	13	-0.178
C1	-0.316	1.000	\$1	0.684	11	0.068	0	0.100	SR	0.316	C2	-0.178	\$2	0.138	H	0.014	0	0.032	SR	0.178	12	-0.316	13	-0.178
C1	-0.316	1.000	\$1	0.684	11	0.068	1	0.100	SR	0.316	C2	-0.178	52	0.138	Ħ	0.014	0	0.032	SR	0.178	12	-0.316	13	-0.178
C1	-0.316	1.000	S1	0.684	lt.	0.068	.0	0.168	SR	0.316	C2	-0.178	52	0.138	It	0.014	0	0.032	SR	0.178	12	-0.316	13	-0.178
C1	-0.316	1.000	81	0.684	11	0.068	0	0.168	SR	0.410	C2	-0.178	52	0.138	Ħ.	0.014	0	0.032	SR	0.178	12	-0.316	13	-0.178
C1	-0.316	1.000	81	0.684	11	0.068	0	0.168	SR	0.410	C2	-0.178	\$2	0.233	11	0.014	0	0.032	SR	0.178	12	-0.410	13	-0.178
C1	-0.410	1.000	S1	0.684	- 11	0.068	0	0.168	SR	0.410	C2	-0.178	52	0.233	in .	0.023	1	0.032	SR	0.178	12	-0.410	13	-0.178
C1	-0,410	1.000	\$1	0.590	- 11	0.068	0	0.168	SR	0.410	C2	-0.178	52	0.233	n	0.023	0	0.055	SR	0.178	12	-0.410	13	-0.178

Fig. 5. Evolution of the CNN modeling the liquid level system.

Figure 5 displays 19 evolutions of the CNN evolving from the initial configuration in Fig. 4 taking a unitary input u in cell 3, in particular cells 9 and 19 contain the numerical solutions of the differential equation system. The evolution shows how the information goes from left to right and the feedback of the system is given after 12 timesteps. In the initial configuration, cell 8 is a conditional sum CS (a local control unit) used for obtaining a right computation, the initial parameters in c_8^0 are: min = 10 and max = 11; thus c_8^1 holds that min = max, letting pass the information in the following timestep. Analogously, the initial parameters in c_{18}^0 are: min = 6 and max = 11; the same behavior is repeated every 11 steps.

The integration step defined in the CNN (as parameter of cell 6) is 0.1 secs., so we need 1100 evolutions for calculating 10 seconds of dynamical response. The values in cells 9 and 19 are taken every 11 steps and graphed in Fig. 6; we can see the expected exponential responses of x_1 and x_2 for the unitary input u.

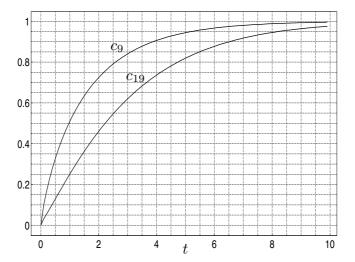


Fig. 6. Hydrostatic-pressure response simulated by the CNN.

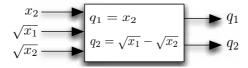


Fig. 7. Block diagram modeling the coordinate transformation.

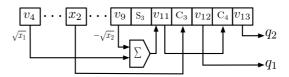


Fig. 8. CNN modeling the coordinate transformation.

Now, the remaining parts of the control for the liquid level system in Fig. 3 will be described by other CNNs; taking the values previously exposed in the cells of the CNN in Fig. 4. The analogue computation for the coordinate transformation is given in Fig. 7.

This diagram is performed by the initial condition of the CNN depicted in Fig. 8, where $\sqrt{x_1}$ and $-\sqrt{x_2}$ are taken from cells v_4 and v_9 in Fig. 4.

The arithmetic operations in Fig. 8 are implemented using the action states in Table 1; thus the needed neighborhoods are shown in Table 3.

The action states C_3 and C_4 in these neighborhoods are used to copy the values of x_2 and $\sqrt{x_1} - \sqrt{x_2}$ in order to have the representation of the block diagram in one piece for clarity; nevertheless it is not necessary for the correct analogue computation of the solution.

Neighborhood	Evolution	Comment
$v_4,\ldots,v_9S_3v_{11}$	$v_{11} = v_4 + v_9$	$v_4 = \sqrt{x_1} \text{ and } v_9 = -\sqrt{x_2}$
$x_2,\ldots,\mathrm{C}_3v_{12}$	$v_{12} = q_1 = x_2$	
v_{11},\ldots,C_4v_{13}	$v_{13} = q_2 = v_{11}$	

Table 3. Neighborhoods for the coordinate transformation.

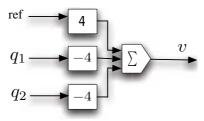


Fig. 9. Block diagram for the linear control based on state feedback.

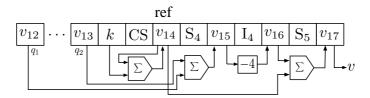


Fig. 10. CNN modeling the linear control by state feedback.

Figure 9 shows the analogue computation for the linear control where ref is the desired value in the output of the system, q_1 and q_2 are the signals in the feedback updated by their corresponding gains to calculate the control action v.

In order to observe the action of the nonlinear control in the overall system, the desired reference ref is periodically incremented to control the error between the output and the wished reference to 0. Figure 10 shows the CNN implementation of the block diagram in Fig. 9.

The neighborhoods composing the CNN in Fig. 10 are exposed in Table 4, values v_{12} and v_{13} are the output of the coordinate-transformation in Fig. 8 containing the estimations of q_1 and q_2 respectively. To calculate the reference change in the input of the system, the first neighborhood of Table 4 is utilized; in this neighborhood the value v_{14} corresponds to the ref variable in Fig. 9. Cell k is a fixed value which is added periodically to v_{14} in a determined number of evolutions controlled by the parameters min and max of cell CS, these ones are explicitly specified when all the cells in the CNN are delineated to simulate the whole liquid level system.

Finally, the nonlinear control is fulfilled by the analogue computation in Fig. 11. Figure 12 shows the initial configuration of the CNN representing the nonlinear control in Fig. 11 using the neighborhoods in Table 5. Cells x_1 , v_4 , v_7 , v and u are

Neighborhood	Evolution	Comment
$kCSv_{14}$	$v_{14} = v_{14} + k$	Initially $v_{14} = 4$, $k = 4$
$v_{12}\cdots v_{13}\cdots S_4v_{15}$	$v_{15} = v_{12} + v_{13}$	$v_{12} = q_1, v_{13} = q_2$
$v_{15}I_4v_{16}$	$v_{16} = v_{15} * r$	r = -4
$v_{14}\cdots v_{16}\mathrm{S}_5v_{17}$	$v_{17} = v_{14} + v_{16}$	v_{17} is the control action v

Table 4. Neighborhoods modeling the linear control by state feedback.

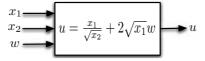


Fig. 11. Block diagram for the nonlinear control law.

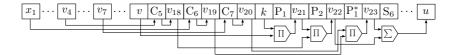


Fig. 12. CNN modeling the nonlinear control law.

elements of the preceding CNNs communicating the other parts of the liquid level system. Thus the nonlinear control law is implemented from cell C_5 up to S_6 .

Since almost all values in the corresponding block diagram have been calculated in the previous CNNs; essentially the neighborhoods modeling the nonlinear control law are based on copies of earlier values established in the above initial configurations. These neighborhoods are presented in Table 5.

Figure 13 depicts in a compact form the way in which all the previous initial configurations (liquid level system, coordinate transformation, linear control, and nonlinear control law) are connected to specify the complete CNN modeling and control the liquid level system subjected to perturbations in the reference, every cell is indexed according to our computational implementation (which is not necessarily unique). The final CNN has 54 cells where cells c_{36} and c_{46} hold the values x_1 and x_2 respectively.

The first valid value of x_1 is calculated in 13 evolutions, this one is used to compute x_2 after 17 evolutions of the automaton. Therefore, once valid values for x_1 and x_2 are obtained, it takes other 17 timesteps to generate again valid values of these variables; in this way 17 evolutions are equivalent to one integration step of 0.1 s in the liquid level system. The computation of x_1 and x_2 is locally controlled by conditional-sum states in cells c_{35} and c_{45} , where the initial parameter min in c_{35} is 6 and for c_{45} is 2 and, max = 17 in both cases.

It is desired to increase the reference of p_2 in one unit every five seconds for observing the action of the control system, so cell CS in the linear control part of

Neighborhood	Evolution	Comment
$v_4 \cdots C_5 v_{18}$	$v_{18} = v_4$	where $v_4 = \sqrt{x_1}$
$x_1 \cdots C_6 v_{19}$	$v_{19} = x_1$	
$v_7 \cdots C_7 v_{20}$	$v_{20} = v_7$	where $v_7 = \sqrt{x_2}$
$v_{17}\cdots k\mathrm{P}_1v_{21}$	$v_{21} = v_{17} * k$	where $v_{17} = w$ and $k = 2$
$v_{18}\cdots v_{21}\mathrm{P}_2v_{22}$	$v_{22} = v_{18} * v_{21}$	$v_{22} = 2\sqrt{x_1}w$
$v_{19}\cdots v_20\cdots P_1^*v_{23}$	$v_{23} = v_{19}/v_{20}$	$v_{23} = x_1/\sqrt{x_2}$
$v_{22}\cdots v_{23}S_6u$	$u = v_{22} + v_{23}$	$u = x_1/\sqrt{x_2} + 2\sqrt{x_1}w$

Table 5. Neighborhoods modeling the nonlinear control.

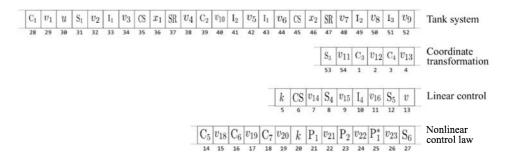


Fig. 13. Complete configuration of the CNN controlling the liquid level system.

the CNN has parameter min = 0 and max = 850 to yield the increment of ref. In this way, 3400 evolutions of the CNN are needed to produce 20 seconds of analogue simulation and control; where values in cells c_{36} and c_{46} can be taken every 17 evolutions to get the dynamics of the liquid level system; these ones are graphed in Fig. 14, proving that the system reaches the desired reference for x_2 every five seconds and Fig. 16 shows the evolution of the CNN, the first configuration has the initial conditions of the system, with $c_{36} = c_{46} = 0.01$.

In order to determine the initial conditions of the system $(x_1 = c_{36} \text{ and } x_2 = c_{46})$, it is necessary to analyze the equation in Fig. 11; if $x_1 = 0$ the system is not controllable and does not matter if the value is x_2 . If $x_1 > 0$ and $x_2 = 0$, the output of the controller is infinite and we do not have a correct operation. Therefore the valid initial conditions are provided by $x_1 > 0$ and $x_2 > 0$; as a consequence, in this paper we have fixed initial conditions near to 0 for observing a complete evolution of the nonlinear control law.

4. Comments about the Complexity and Parallelism of the CNN

Since the CNN is just implementing and simulating the block diagram associated with the liquid level system, the complexity of the CNN is in straightforward

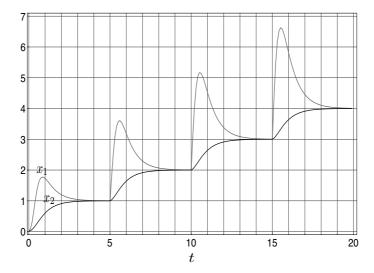


Fig. 14. Dynamical response of x_1 and x_2 for 3400 evolutions of the CNN.

relation with the one related to the block diagram. For a given block diagram, let Γ be the number of basic operations^b required for executing it.

For the block diagram in Fig. 3 and its four subdiagrams, let us associate γ_1 with the number of basic operations for accomplishing the linear control, in the same way let us tie in γ_2 with the nonlinear control law, γ_3 with the tank system and γ_4 with the coordinate transformation. Thus for $1 \le i \le 4$, one iteration of the liquid level system is achieved in $\Gamma = \sum_i \gamma_i$ operations. Let m be the number of iterations required for controlling the system, hence its complexity is given by $m\Gamma$.

Every subdiagram is implemented by a part of the CNN which works in a serial way, so the correct calculation of the nonlinear control law depends on having the right value of the linear control and the same happens for the other parts. But the internal operations of each subdiagram can be parallelized in the CNN, of course, respecting the dependencies in the variable computation which is the common issue in parallel processing.

Let γ_i' be the number of necessary operations for the adequate calculation of every subdiagram in the corresponding fragment of the CNN, therefore, since γ_1 consists of a single operation, hence $\gamma_1' = \gamma_1$. In the case of the nonlinear control law, the root calculation and products are parallelized in the CNN, so $\gamma_2' = \gamma_2 - 2$.

For the tank system and the coordinate transformation, in the associated block subdiagrams in Fig. 3 the output of the integrator block (x_2) is parallelized in the CNN for obtaining q_2 , thus $\gamma_3' + \gamma_4' = \gamma_3 + \gamma_4 - 1$.

^bIn our case we have sum and product of n variables, square root, scalar product, copy from one variable to an other and Euler integration.

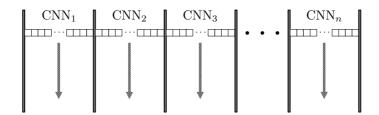


Fig. 15. Parallel evolutions of different CNNs each with distinct parameters.

			c35 c36	C45 C46
d 0000 2 0000 4	000 0 4000 S1 0000 H 0	00 S2 0.000 d3 0.000 d4 0.000 d5 0.000 2.000 P1 0.000 P1 0.000 P3 0.000 d5 0.000 d5 0.000	53 0000 2 0000 0 0010 R 0000 d 0000 53 0	0000 2 0000 0 0010 R 0000 B 0000 H 0000 SH 0000
c 000 2 000 4	000 0 4000 St 0000 F -0	00 S2 4000 d3 0000 d4 0010 d5 0000 2000 P1 0000 P1 0000 P1 0000 S3 0000 d5 0000	53 0000 & 0000 0 0010 R 0100 J 0000 S3 0	0000 2 0000 0 0010 R 0100 B 4000 M 4000 SA 0000
d 000 2 000 4	000 0 4000 St 0010 H 4	00 S2 4000 d3 0:100 d4 0:010 d5 0:100 2000 P1 8:000 P1 0:000 P1 0:000 S3 0:000 d5 4:000	53 E000 & E000 0 E000 R E100 & 4000 53 E	0100 0 0000 0 0010 R 0100 0 4100 W 4100 SH 0100
d 0010 d 0100 4	000 0 4000 St 0010 H 4	40 S2 4000 d3 0:100 d4 0:100 d5 0:100 2000 P1 8:000 P1 0:800 P1 0:100 S3 0:000 d5 0:100	53 0000 E 0000 0 0000 R 0100 J -0100 53 0	0100 2 0010 0 0010 R 0100 B 4100 W 4100 SH 0000
d 000 2 000 4	000 0 4000 St 0.110 ft -0	40 S2 3860 d3 0.100 d4 0.010 d5 0.100 2000 P1 8000 P1 0.800 P1 0.100 S3 0.900 d5 4.100	53 4100 E 0000 0 0010 R 0100 0 4100 53 0	0000 2 0010 0 0010 R 0100 B 4100 W 4100 SA 0000
d 6000 d 6000 4	000 0 4000 St 0010 H 4	40 S2 3860 d3 0.100 d4 0.010 d5 0.100 2.000 P1 7820 P1 0.800 P1 0.100 S3 0.900 d5 4.100	53 0800 E 4000 0 0000 R 0100 J 4100 S3 0	0000 2 0000 0 0010 R 0100 0 4100 M 4100 SA 0000
d 0010 d 0000 4	000 0 4,000 St 0,010 H -0	4 S2 3560 d 0:00 d 0:00 d 0:10 d 0:10 2000 P 7520 P 0:752 P 0:00 S3 0:500 d 0:100	\$3 0,800 E 0,000 0 0,000 R 0,100 27 4,100 \$3 0	0000 2 0000 0 0010 R 0100 D 4100 W 4100 SW 0000
d 80% 2 800 4	000 0 4000 St 0010 ft 4	40 S2 3860 d 0:00 # 0:00 d 0:00 P 7:126 P 0:762 P1 0:00 S3 0:882 d 0:00	53 0800 Q 0000 0 0000 R 0100 J 4100 S3 0	0000 0 0000 0 0010 R 0100 0 4100 W 4100 SA 0000
d 0010 d 0000 4	000 0 4000 St 0.010 H -0	40 S2 3960 d3 0.100 d4 0.010 d5 0.100 2000 P1 7825 P1 0.712 P1 0.100 S3 0.882 d5 0.100	\$3 0.792 E 0.000 0 0.000 R 0.100 d 4.100 \$3 0	0000 2 0000 0 0010 R 0100 U 4100 M 4100 SA 0000
d 0010 2 0000 4	000 0 4000 St 0010 H 4	40 S2 3860 d3 0.700 d4 0.070 d5 0.700 2000 P7 7320 P7 0.732 P7 0.700 S3 0.872 d5 0.700	53 0.792 0 0.079 0 0.000 R 0.100 d 4.100 S3 0	0000 0 0000 0 0010 R 0100 B 4100 W 4100 S4 0000
d 0010 2 0000 4	000 0 4000 St 0010 ft -0	40 SZ 3560 d 0.100 d 0.100 d 0.100 d 0.100 2000 P1 7.525 P1 0.752 P1 0.100 S3 0.882 d 0.100	53 0772 0 0079 0 0070 R 0100 d 4:00 S3 0	0000 2 0000 0 0010 R 0100 B 4100 W 4100 S4 0000
d 0010 d 0000 4	000 0 4000 St 0010 H 4	4 S 390 d 0:00 4 0:10 d 0:10 d 0:10 200 P 750 P 0:70 P 0:00 S 080 d 4:00	\$3 0.792 0 0.071 0 0.000 R 0.100 d 4.100 \$3 0	0000 2 0000 0 0010 R 0100 B 4100 W 4100 SH 0000
d 0010 2 0000 4	000 0 4000 St 0010 H -0	A S2 3860 d 0:00 x 0:00 d 0:00 d 0:00 2000 P 7520 P 0:752 P 0:00 S3 1882 d 0:00	\$3 0.792 0 0.079 1 0.010 R 0.100 d 4.100 S3 0	0000 0 0000 0 0010 R 0100 B 4100 M 4100 SM 0000
d 0010 d 0000 4	000 0 4000 St 0010 H 4	4) SZ 3960 d 0.100 d 0.110 d 0.110 d 7.100 2000 P 7.525 P 0.752 P 0.100 SS 0.862 d 0.100	SS 0.792 0 0.079 0 0.095 R 0.100 cf 4.100 SS 0	0000 E 0000 0 0010 R 0100 B 4100 M 4100 SM 0000
d 000 d 000 4	000 0 4000 St 0010 H 4	K S2 3860 d 0.000 # 0.089 d 0.100 2000 P 7520 P 0.752 P 0.000 S3 0.862 d 0.100	S3 0792 0 0079 0 0099 R 0299 0 -0.100 S3 0	0000 2 0000 0 0010 R 0100 B 4100 W 4100 S4 0000
d 0010 2 0000 4	000 0 4000 S1 0010 H -0	40 S2 3560 d 0269 d 0169 d 0170 2000 P 7520 P 0752 R 0562 S3 1662 d 0170	S3 0.792 0 0.079 0 0.089 R 0.299 0 4.100 S3 0	0.199 £ 0.000 0 0.010 R 0.100 B 4.100 M 4.299 S4 0.199
d 000 2 039 4	000 0 4,000 St 0010 H -0	40 S2 3960 d3 0299 d4 0089 d5 0100 2000 P1 7500 P1 2365 P1 0860 S3 1584 d5 40299	53 0.792 Q 0.079 D 0.089 R 0.299 d -0.100 S3 D	0.196 C 0.025 1 0.010 R 0.100 D 4.100 W 4.299 SW 0.198
d 0000 d 0.994	000 0 4000 S1 0,209 T1 -0	40 S2 3860 d3 0289 d4 0388 d5 0100 2000 P1 7920 P1 2365 P1 0860 S3 3227 d5 4298	53 1385 Ø 1079 O 1089 R 1239 Ø 4300 S3 O	0195 & 0020 0 0030 R 0100 & 4100 W 4299 S4 0199

Fig. 16. Complete CNN modeling and controlling the liquid level system.

Finally, if Γ' is the number of operations achieved for the CNN, we have that $\Gamma' = \Gamma - 3$. In this way for m iterations of the system, the complexity of the CNN is given by $m(\Gamma - 3)$ which is almost the same obtained by the serial procedure.

Nevertheless, the relevance of the proposed method lies in the simplicity of the CNN and that the feedback of the system is produced by periodic boundary conditions, thus we may have n copies of the CNN, each with distinct conditions (for instance: initial values, integration steps or perturbation times) and execute them in parallel (Fig. 15), in order to analyze different behaviors at the same time. Usually this parallelization is a heavy computational task with a classic implementation of block diagrams, but due to the local interactions and the lack of a central control in the case of CNNs, this task can be constructed in an easier way with the application of a quiescent state which serves as a barrier separating every CNN.

5. Concluding Remarks

The previous sections have established the analogue modeling and control by CNNs for the dynamics associated to a nonlinear system, using as link the corresponding block diagram. In this way, the cells of the CNN keep both data or arithmetic and

logic operators to perform the same analogue task that the block diagram, and the evolution of the CNN provides the desired approximation to the solution of the problem; in this particular case, the control of a liquid level system. The advantage of using CNNs is that they can be easily implemented avoiding the necessity of a complex global control by their parallel nature.

Meanwhile the execution time of a single CNN and the serial realization of the block diagram is almost the same for a small number of iterations, the convenience of this procedure lies on managing in an easier way n copies of the CNN, each with distinct parameters, for observing different behaviors of the system in parallel. Further research implies performing this kind of CNNs in parallel hardware as FPGAs and extending the analysis for nonlinear systems with multiple input and multiple output values.

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